# BRISBANE CITY COUNCIL 

## Sewage Pump Station SP218

Westlake Drv

Contract: BW 70103-026
Job Number: WT400052

ELECTRICAL INSTALLATION

## OPERATIONS and MAINTENANCE MANUAL

## VOLUME 2

INSTALLATION BY:
SJ Electric (Qld) Pty Ltd
19 Elliot Street
Albion Qld 4010
Telephone: 0732561522 Fax: 0732561533

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## Sewage Pump Station SP218 Westlake Drv

## Electrical Drawing List 1

## Site Installation

| Sheet No. | Drawing No. | Title |
| :---: | :--- | :--- |
| 00 | $486 / 5 / 7-0096-000$ | Site Cover Sheet |
| 01 | $486 / 5 / 7-0096-001$ | Power Distribution Schematic Diagram |
| 02 | $486 / 5 / 7-0096-002$ | Pump 01 Schematic Diagram |
| 03 | $486 / 5 / 7-0096-003$ | Pump 02 Schematic Diagram |
| 04 | $486 / 5 / 7-0096-004$ | $\quad$ [RESERVED] Sump Pump |
| 05 | $486 / 5 / 7-0096-005$ | Generator Control Schematic Diagram |
| 06 | $486 / 5 / 7-0096-006$ | Common Controls Schematic Diagram |
| 07 | $486 / 5 / 7-0096-007$ | Common RTU I/O Schematic Diagram |
| 08 | $486 / 5 / 7-0096-008$ | RTU Power Distribution Schematic Diagram |
| 09 | $486 / 5 / 7-0096-009$ | RTU Digital Inputs Termination Diagram |
| 10 | $486 / 5 / 7-0096-010$ | RTU Digital Inputs Termination Diagram |
| 11 | $486 / 5 / 7-0096-011$ | RTU Digital Outputs Termination Diagram |
| 12 | $486 / 5 / 7-0096-012$ | RTU Analogs \& Miscellaneous Termination Diagram |
| 13 | $486 / 5 / 7-0096-013$ | Common Controls Termination Diagram |
| 14 | $486 / 5 / 7-0096-014$ | Equipment List |
| 15 | $486 / 5 / 7-0096-015$ | Cable Schedule |
| 16 | $486 / 5 / 7-0096-016$ | Switchboard Label Schedule |
| 17 | $486 / 5 / 7-0096-017$ | Switchboard Construction Details |
| 18 | $486 / 5 / 7-0096-018$ | Switchboard Construction Details |
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| 21 | $486 / 5 / 7-0096-021$ | Dry Well Pump Disconnection Box |
| 22 | $486 / 5 / 7-0096-022$ | Switchboard General Arrangement Elevations - Double Sided |
| 23 | $486 / 5 / 7-0096-023$ | Switchboard General Arrangement Sections - Double Sided |
| 24 | $486 / 5 / 7-0096-024$ | [RESERVED] Generator External Connection Box |
| 25 | $486 / 5 / 7-0096-025$ | Switchboard Slab \& Conduit Details |
| 26 | $486 / 5 / 7-0096-026$ | Switchboard Slab \& Conduit Details |
| 27 | $486 / 5 / 7-0096-027$ | Switchboard Slab \& Conduit Details |





Q-Pulse Id TMS 1025


Q-Pulse Id TMS 1025
Active $10 / 12 / 2014$







Q-Pulse Id TMS 1025
Active 10/12/2014


Q-Pulse Id TMS 1025
















## Sewage Pump Station SP218 Westlake Drv

## Electrical Drawing List 2

Factory Test

| Sheet No. | Drawing No. | Title |
| :---: | :--- | :--- |
| 00 | $486 / 5 / 7-0096-000$ | Site Cover Sheet |
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| 02 | $486 / 5 / 7-0096-002$ | Pump 01 Schematic Diagram |
| 03 | $486 / 5 / 7-0096-003$ | Pump 02 Schematic Diagram |
| 04 | $486 / 5 / 7-0096-004$ | [RESERVED] Sump Pump |
| 05 | $486 / 5 / 7-0096-005$ | Generator Control Schematic Diagram |
| 06 | $486 / 5 / 7-0096-006$ | Common Controls Schematic Diagram |
| 07 | $486 / 5 / 7-0096-007$ | Common RTU I/0 Schematic Diagram |
| 08 | $486 / 5 / 7-0096-008$ | RTU Power Distribution Schematic Diagram |
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| 12 | $486 / 5 / 7-0096-012$ | RTU Analogs \& Miscellaneous Termination Diagram |
| 13 | $486 / 5 / 7-0096-013$ | Common Controls Termination Diagram |
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| 17 | $486 / 5 / 7-0096-017$ | Switchboard Construction Details |
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| 24 | $486 / 5 / 7-0096-024$ | [RESERVED] Generator External Connection Box |
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| 27 | $486 / 5 / 7-0096-027$ | Switchboard Slab \& Conduit Details |
|  |  |  |



## SP218 WESTLAKE DRIVE SEWAGE PUMPING STATION

## SITE COVER SHEET



| STANDARD VARIABLES |  |
| :---: | :---: |
| DESCRIPTION | VALUES |
| CT MEtERING ISOLATOR | 1160 A SLB 1603 P |
| NORMAL SUPPLY MAIN SWITCH | 250A SLOONE／250 |
| GENERATOR SUPPLY MAIN SWITCH | 250 A SLOONE／250 |
| PUMP1 CIRCUIT BREAKER | 100A S1256／100 |
| PUMP2 CIRCUIT BREAKER | 100 A S1256／100 |
| DRY WELI SUMP PUMP CRRCUIT BREAKER | 16 A DICB6336 |
| PUMP VSD SIZE | F［202P3］K |
| PUMP RATING | 31．5kW66A |
| PUMP EM．STOP CONTACTOR | CA7－12 |
| SUMP PUMP RATING | 22kW 6.8 A |
| SUMP PUMP CONTACTOR \＆TOL | CA7－16［17－24－6 |
| WET WELL LEVEL TRANSMITTER |  |
|  | NOT APPICAB：E |
| DELIVERY PRESSURE TRANSMIT TER | BRRL4X6G6THA2X 50 n |
| Wet weli ul trasouc ievel semsor | WOT APPLICAB：E |
| FLOWMGE EPR RAWGE | WOT APPILCAB！E |
| RADIO | DR900－66A02－00 |
| EMERGENCY PUMPING TIME | 26.5 sec |
| No of SINGLE POINT PROBES | 6 |
| INCOMING MAINS SUPPLY CABLE | $50 \mathrm{ma}^{2}$ |
| MAIN EARTHING CABLE | $16 \mathrm{~mm}^{2}$ |
| INCOMING GENERATOR SUPPLY CABLE | 16 ma |
| PUMP MOTOR SUPPLY CABLE | $16 \mathrm{~mm}^{2}$ |
|  |  |
|  |  |
|  |  |


| ARD DESIGN |  |  |
| :---: | :---: | :---: |
| OPTION | DESCRIPTION | Fitted |
| A |  | N0 |
| B |  | N0 |
| c | WDIVIDUAL PUMP REFLUX VALVE PROXIMITY SWITCH | YES （10） |
| D |  | N0 |
| E | Station dry well sump．PuMp and level inication sensors and relays |  |
| F | STATION PERMANENT GENERATOR－ATS AND CONTROL CONNECTIONS | YES |
| 6 |  | W0 |
| H | STATON DELVERY FIOWFETER | W NO |
| 1 | BACKUP COMMUNICATION－GSM | YES 0 |
| J | PUMP CONNECTION（Via Dry Well J－box） | Yes |
| K | Cathout protection | ${ }^{*}$ 囦 NO |
| L | MOTOR THERMISTORS（Via Dry Well －－Box） | YES ${ }^{\text {柬 }}$ |
| M | ouvar chitas | 圃 N0 |
| N | CURRENT TRANSFORMER（CTI METERRG | Yes |
| 0 | PUMPS ELECTRICAL INTERLOCK MMains 8 Generator） | YES $\mathrm{R} \times \mathrm{O}$ |
| P | WET WELI WASHEA | 罒 № |
| Q |  | W ${ }^{\text {NO}}$ |
| R | Telemetry radio | YES 相 |
| S | WET Well ulipasomi leve semsar | NO |
| T | DOUBLE SIDED SWITCHBOARD | YES |
| U | DELIVERY PRESSURE TRANSMITTER | Yes and |
| ， | CHEMCAL DOSNG | No |












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# SP218 WESTLAKE DRIVE SEWAGE PUMPING STATION <br> SITE COVER SHEET 

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| DWG No． | SIIE COVER SHEET TITLE | SHEET | REVISIONS |  |  |  |
| 486／57／－0096－000 |  | 00 | 0 |  |  |  |
| 486／5／7－0096－001 | POWER DIS RRBUTION SCHEMAITC DIAGRAM | 01 | 0 | A |  |  |
| 486／577－0096－002 | PUMP OIS SHEMATIC DIAGGAM | 02 | 0 | A |  |  |
| 486／577－0096－003 | PUMP 02 SCHEMATC DIAGRAM | 03 | － | A |  |  |
| 486／577－0096：006 | DRY WELL SUMP PUMP SCHEMATC DIAGGAM | 04 | 0 | A |  |  |
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| 4886／577－0096－013 | COMMOO CONTROLS TERAINATION DIAGRAM | 13 |  | A |  |  |
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| 486／577－0096－015 | Cable Schidule | 15 | 0. | A |  |  |
| 4866／577－0096－016 | SWITCHBOARO LABLL SCHEOLE | 16 |  | A |  |  |
| 486／577－0096－017 | SWITCHBOARD Construction detalls | 17 | 0 | A |  |  |
| $486 / 5 / 7-0096-018$ | SWITCHBOARD Cons truction detalls | ${ }^{18}$ | 0 | ${ }^{\text {A }}$ |  |  |
| 486／577－0096－099 | Level Probes ano Pressure Trans ilit ir installation detall | 19 | 0 | ${ }^{\text {A }}$ |  |  |
| 486／5／7－0096－020 |  | 20 |  |  |  |  |
| 486／5／7－0096－021 | ORY WELL PUMP DISCONNECTION BOX | In | 0 | A |  |  |
| 486／5／7－0096－022 | SwITCHBOARO GENERAL ARRANGGMENT ELEVATIONS－Double siled | 22 |  | ${ }^{\text {A }}$ |  |  |
| 486／577－0096－023 | SWITCHBoaro general arrangeener sections－Dovile side | 23 | 0 | A |  |  |
| 486／571－006－024 |  | 24 |  |  |  |  |
| 486／577－0105－025 | SLAB \＆Conour detalls－Sheer 1 of 3 | 25 | 0 | A |  |  |
| 486／577－0105－026 | SLAB \＆Conout detall－Sheet 2 of 3 | 26 | 0 | A |  |  |
| 486／577－0105－027 | SLAB \＆Conolit detall－Sheet 3 of 3 | 27 | $\bigcirc$ | A |  |  |
|  |  |  |  |  |  |  |



| STANDARD DESIGN OPTIONS |  |  |
| :---: | :---: | :---: |
| OPTION | DESCRIPTION | FiTIED |
| A |  | 四 No |
| B |  | 雨 № |
| c | MOIVIDUAL PUMP Reflux valve proxmit swich | Yes san |
| 0 |  | 匈 N0 |
| E | STATION DRY＇WELL SUMP PUMP AND LEVEL NOICATION SENSORS ANO RELAYS |  |
| F | STATION PERMANENT GENERATOR－ATS ANO CONTROL CONNECTIONS | Yes $\times$ |
| 6 |  | 0 |
| H |  | 函 N0 |
| 1 | BACKUP COMMUNCATION－ $65 M$ | Yes |
| ， | PUMP Connection（Via ory well - －80x | Yes |
| k | Catmot pootetion | N N0 |
| L | MOTOR THEPMIS ToRS［Via Dry well $1-B \mathrm{Bx}$ ） | Yes |
| M | Dovup Cowize： | ＊${ }^{\text {No }}$ |
| N | CURRENT TRANSFORMER ITTI METERMG | YES里 |
| 0 | PUMPS ELEETRRICAL LTIERLOCK MMins 2 Generator） | Yes mom |
| P | wET Wet waster | N |
| 0 |  | N |
| R | Telemetry railo | Yes |
| 5 | We welli utarsowlevet sembai | ＊No |
| T | DOUBELE SIDED SWITCHBOARD | Yes |
|  | DELIVERY PRESSURE TRANSMITER | YES |
| $v$ | Temmat oosmi | （ N0 |

Sheet 00

| － |  |  |  |  | ORAFEO | P．hague | Pind Simestap pracue | 10.650 |  |  |  | TME COVER SHEET | Sheeino． 0 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | For Construction | P． H | A．w． | 仡 | ORAFTWGC CHEC | A． Wi ITHOFT | ． | E．Q No．DATE | Practral desticmmanager oate |  | WESTLAKE DRIVE |  | Stisgne mamerdaummg ano | A |
| ${ }^{\circ} 10509$ | ISSUED FOR TENDER | H． | Aw． | ${ }^{2}$ | CAO PLI | 57－0096806 | ora | 808\％：10．009 |  | － | SEWAGE PUMP STATION |  | 486／5／7－0096－000 | A |
| Nopant |  | ORN． | APD | Relcerene Omams |  |  | Ofscing yitex | R．P．E． Ne：Date | Cluentolegate oate |  |  |  |  |  |



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SSM089

## STANDARD SEWAGE PUMP STATION

## SWITCHBOARD CHANGEOVER COMMISSIONING PLAN

| Site ID and Name | STD 18 | WeStINKE DRJVE |
| :--- | :---: | :---: | :---: |
| Commissioning Date | $10 / 11$ | 2009 |

In Attendance


Note: Printed copies of this document should be verified for currency against the published electronic copy.

## 1 INTRODUCTION

This document is the standard testing procedure for a switchboard change over at a sewage pumping station. The procedure ensures that for a two pump sewage pump station, at least one pump will be operational at all times. The basic cutover procedure is as follows:

1. Install temporary pumping system (pump controller and generator).
2. Disconnect sewage Pump \#2 from existing switchboard and connect to temporary pumping system.

PUMP \#1 IS NOW RUNNING THE STATION FROM EXISTING SWITCHBOARD
3. Fully commission Pump \#2 on the temporary pumping system.

PUMP \#2 IS NOW RUNNING THE STATION FROM TEMPORARY PUMPING SYSTEM
4. Disconnect Pump \#1, consumer mains, on site generator and all field instrumentation from the existing switchboard.
5. Install new switchboard and connect to consumer mains.
6. Connect Pump \#1 to the new switchboard and test in "emergency pumping" mode (via the "Emergency Start" switch).

## PUMP \#2 IS STILL RUNNING THE STATION FROM THE TEMPORARY PUMPING SYSTEM AND PUMP \#1 CAN BE RUN UNDER "EMERGENCY PUMPING" MODE FROM NEW SWITCHBOARD.

7. Connect all field instrumentation.
8. Test Pump \#l on the new switchboard to operate in "Local" and "Remote" modes. Full commissioning done separately

## PUMP \#1 IS NOW RUNNING THE STATION FROM NEW SWITCHBOARD

9. Connect Pump \#2 to the new switchboard and Test on the new switchboard. Full commissioning done separately.
10. Complete the Site Acceptance Test (SAT) including pumps, RTU and SCADA testing.

NOTE: This testing procedure will only be acceptable on sites that do NOT need two pumps to run during the cut over procedure.
(Confirm the current running conditions of the existing switchboard before commencing).
For sites that require two pumps to run simultaneously under dry weather conditions during the proposed cut over period, a site-specific cut over procedure must be developed to incorporate adequate flow control measures (ie tankers or temporary pumps).

| Doc Id: | 006142 | Active Date: $1-11-10$ Dec 2008 |
| :--- | :--- | :---: |
| Printed: | $10 / 12 / 2008$ | Owner: Alex Withoft |
| Note: | Printed copies of this document should be verified for currency against the published electronic copy. |  |

## 2 Pre - Change Over Works Checklist

The following checklist is to be completed and signed by the electrical contractor

### 2.1 SWITCHBOARD FACTORY ACCEPTANCE TEST

| Contractor Task | Cqmpleted |
| :--- | :--- |
| FAT has been completed as per BW FAT Document and all defects that were <br> identified have been rectified. |  |

### 2.2 CONCRETE SLAB EXTENSION

| Contractor Task | Result |
| :--- | :---: |
| Confirm the concrete slab extension is complete including all necessary conduits. | OK Q |

### 2.3 SUPPLY AUTHORITY

| Contractor Task | Outcome |
| :---: | :---: |
| The relevant supply authority has been organised to install the metering into the New Switchboard. <br> If direct metering supply authority not required. NA | Company Eavergo $\qquad$ Booked for $10,11,09$ <br> @ $\qquad$ (time) <br> Ref \# $\qquad$ |

### 2.4 NEW RADIO ANTENNA MAST LOCATION

| Contractor Task | Result |  |
| :--- | :--- | :--- |
| Check the location of the antenna mast and ensure that the new position will not <br> be directly below electrical transmission lines. | Location OK |  |

### 2.5 DISCHARGE MAINS PRESSURE TRANSDUCER

| Contractor Task | Completed |
| :---: | :---: |
| Install delivery pressure transducer on the discharge rising main. Transducer is calibrated to the specified range (as per spec). $\text { OKPA to } 500 \mathrm{kPA}$ | $\begin{aligned} & \text { Installed OK } \\ & \text { Range } \underline{(m) t 05(m)} \end{aligned}$ |

### 2.6 TEMPORARY GENERA TOR SIZE

| Contractor Task | Completed |
| :---: | :---: |
| Note the kW of each pump. | $\begin{aligned} & \text { Pump } \# 1 \frac{37}{37} \cdot 5 \mathrm{~kW} \\ & \text { Pump \#2 } 37 \cdot 5 \mathrm{~kW} \\ & \hline \end{aligned}$ |
| If a Hire Generator is required <br> ONSITE Genexatio | Genset Size $\qquad$ kVA <br> Date Booked 11 $\qquad$ <br> Delivery Date $\qquad$ <br> Delivery Time $\qquad$ |



### 2.7 PUMP STATION PRELIMINARY OPERATIONAL CHECKS

| BW Task | Checked |
| :--- | :---: |
| These are checks are helpful to ensure the pump station is fully operational and <br> that no delay will be incurred due to any pump station problem out side of the <br> contract. These task are desirable to have completed before the SAT but are not <br> essential. The job can proceed if they are not done. <br> Commissioning Manager to request networks maintenance to inspect and rectify if <br> necessary |  |
| The reflux valves and associated limit switches are working correctly. |  |
| The discharge pressure connection point is available and that the isolation valve is <br> functioning correctly. |  |
| The dry well exhaust fan is working correctly and quietly. | OK |
| The wet well does not need pumping out. | OK D |
| The flow meter is functioning correctly. | OK D |
| The stand bye generator can start and has sufficient fuel. | OK D |

[^0]
## 3. Change Over Works

The following sequence of change over works is the order in which they must be followed. One pump must be operational at all times. After each phase has been completed, the -commissioning manager will record the results and instruct the commissioning team to commence work on the next phase.

### 3.1 INSTALL TEMPORARY PUMPING SYSTEM

### 3.1.1 Register with Control Room

| Contractor Task | Outcome |
| :--- | :--- |
| Call the Brisbane Water Control Room Operator (CRO) and inform him that you are <br> on site. Record the CRO's Name and Officer Code and record the time of the call. <br> Advise CRO that you are performing a switchboard changeover and that you will <br> initially be taking one pump off line. Give the operator your contact name and <br> number and advise the operator that communications will be lost to the pump <br> station until the job is finished. | Name: |

### 3.1.2 Existing Switchboard Parameters



### 3.1.3 Prepare and Install Temporary Pump Controller and Generator



Electrical Contactor's Supervisor


BW Commissioning Manager



Signature:

Printed: 10/12/2008

[^1]
### 3.2 CONNECT PUMP \#2 TO TEMPORARY PUMPING SYSTEM

| Contractor Task | Outcome |
| :--- | :--- |
| On the existing switchboard, Isolate sewage pump (Pump \#2) as per BW Isolation <br> Tag and Lock Out procedure. (Unplug from Decontactor). |  |
| Disconnect Pump \#2 from the existing switchboard and remove the power cables |  |
| from the switchboard. |  | OK | Connect Pump \#2 power cables to the temporary pump controller. |
| :--- |
| Electrically test Pump \#2 to temporary pump controller connections. |
| Switch the existing switchboard to "Local" and confirm Pump \#1 is stopped. |
| Manual Test of Temporary PumpIng System: (Confirm Pump Direction) <br> Manually start the submersible pump and closely monitor wet well level to confirm <br> that the level is dropping. When confirmed, stop pump. |
| Auto Test of Temporary Pumping System: (Confirm Pump Cycle) <br> Allow the temporary pumping system to complete one full start and stop cycle <br> automatically to confirm complete system is functioning correctly. <br> This is a HOLD point. Do not proceed until the temporary pump is confirmed to <br> be controlling the wet well level. |

### 3.3 DISCONNECT AND REMOVE EXISTING SWITCHBOARD

### 3.3.1 Disconnect Pump \#1 and Remove Existing Switchboard


A) Per PrEvious Note:

USE EXis)anc Board as Temp (oatpoller with onsite Generation
moved the other Pump oo new switilboard

-L NEW SWITCHBOARD
ew switchboard (For Sites with Option F Only)

| : | Outcome |
| :---: | :---: |
| ct the required (new or existing) earth cable | New |
|  | Existing $\square$ |
| ct the required (new or existing) mains cable | Now Existing |
| ses mains cable insulation resistance to earth. | A $\qquad$ Megohm <br> B $\qquad$ Megohm: <br> C $\qquad$ Megohm |
| stance | 0.05 ohms |
| ise continuity | R to L1 OKL <br> W to L2 OKD <br> B to L3 OKR <br> N to Nuetral OKD  |

upply Authority Metering

|  | Outcome |
| :---: | :---: |
| onnected kWhr Meter <br> CT Mexiren a | OKQ |

## : New Switchboard

|  | Outcome |
| :---: | :---: |
| phase pole fuses from lock out box as per BW Isolation and Lock | OK $\square^{-2}$ |
| hboard main incomer is turned "Off". | OK $\square^{-}$ |
| \# pole fuses. |  |
| itch | OKन |
| Itages | $\frac{A B-4 / 5 V}{C A}$ |
| \%on and ensure it is the same as determined earlier. | OKC |
| ection. | OK |



## 3．5 CONNECT PUMP \＃1 TO THE NEW SWITCHBOARD

| Contractor Task | Outcome |
| :---: | :---: |
| At the beginning of this procedure，Pump \＃2 is operating under the control of the temporary switchboard running from the Generator． | OK |
| Isolate submersible Pump \＃1 and Pump \＃2 at the new switchboard，as per BW Isolation and Lock Out procedure．（Decontactors） | OK， |
| Via the MERACHAL plug in sockets provided on the switchboard reconnect the power and control cables for Pump \＃1（this is the pump that is not connected to the generator set） |  |
| Install and connect the hydrostatic level probe to the transmitter． | Range 0 to ，m |
| Confirm that level is indicating on the display． | OK $0^{\text {a }}$ |
| Before beginning the next step ensure that the well level is between＇Start＇and ＇Stop＇level and Pump \＃2 is not running． <br> Isolate Pump \＃2 to prevent it from running during the next test | OKg |
| De－isolate this now connected Pump \＃1．Check the rotation by starting the pump via the local＂Emergency Start＂switch and confirming the wel well level drops by at least 1\％． | OK |
| Start Pump \＃ 1 again and Check the 3 phase motor current and compare with original readings． <br> PUMP \＃1 Can now be run in emergency and local，under the control of the new switchboard． |  |
| De－isolate Pump \＃2 so that the station is again under the control of the temporary switchboard． | OK $\square$ |

## 3．6 CONNECT FIELD INSTRUMENTATION TO THE NEW SWITCHBOARD

## 3．6．1 Field Devices

| Contractor Task | Outcome |
| :---: | :---: |
| Connect the delivery pressure probe to the transmitter | OKQ Oto＿Mtrs |
| Install and connect the Multitrode LR3 wet weil high level relay Probe | OK at Mtrs |
| Install and connect the Multitrode SIR surcharge imminent level relay Probe | OK at mirs |
| Connect the thermistors for each pump（sites with option｜only） | OKEA N／A |
| Connect the moisture in oil sensor for each pump（sites with option A only） | OK 邱 N／A［ |
| Connect the moisture in stator for each pump（sites with option B1 only） | OK 回 N／A D |
| Connect the motor bearing temperature for each pump（sites with option B2 only） | OK ¢P N／A Q |
| Connect the reflux valve micro switch for each pump（sites with option C only） | OK凹 N／A $\square$ |
| Connect the upstream manhole surcharge imminent probe（sites with option D only） | OK W／N／A O |
| Connect the Multitrode LR2 sump pump start／stop probes（sites with option E only） | OKd／N／A $\square$ |
| Connect the Multitrode LR4 sump pump high／trip probes（sites with option E only） | OKD／N／A $\square$ |
| Connect the sump pump（sites with option E only） | OKロ N／A $\square$ |



### 3.7 CONNECT PUMP \#2 TO THE NEW SWITCHBOARD

### 3.7.1 Connect Pump \#2 to New Switchboard

| Contractor Task | Outcome |
| :---: | :---: |
| At the beginning of this procedure, Pump \#1 is operating under the control of the new switchboard running from the supply authority. | OKø |
| Shut down the generator and disconnect Pump \#2 from the temporary switchboard | OK才 |
| Ensure Pump \#2 circuit breaker at the new switchboard is still isolated and locked out as per BW Isolation and Lock Out procedure. | OKt |
| Via the MERACHAL plug in sockets provided on the switchboard, connect the power and control cables for Pump \#2. | OK |
| De-isolate this now connected submersible pump. Check the rotation by starting the pump via the local "Emergency Start" switch and confirming the wet well level drops by at least $1 \%$. | OK |
| Start Pump \# 2 again and Check the 3 phase motor current and compare with original readings. <br> PUMP \#2 Can now be run in emergency and local, under the control of the new switchboard. | $\begin{aligned} & \text { A } \frac{57}{7} \text { Amps } \\ & \text { B. } 57 \text { Amps } \\ & \text { C } 57 \text { Amps } \end{aligned}$ |

### 3.8 COMMISSIONING OF THE PUMP STATION COMMUNICATIONS

### 3.8.1 Radio Antenna Installation

| BW Programmer Task | Outcome |
| :--- | :---: |
| Install new mast with Antenna, orientate antenna to the position determined in <br> section 3.1.2 connect coaxial cable plugs. | OK D |

### 3.8.2 Telemetry and SCADA Communications Checks

| BW Programmer Task | Outcome |
| :--- | :---: |
| Brisbane Water programmer must complete the following procedures |  |
| From the SSM086 Standard Fixed Speed Sewage Pumping Station (S.A.T.) | OK 口 |
| Section 1: Setup and Pre-Comm/ssioning Checks 1.1 to 1.8 |  |



### 3.9 COMMISSIONING OF THE PUMP STATION PUMPING SYSTEM

### 3.9.1 Commissioning of Pump \#1 and Pump\#2

| BW Programmer \& Contractor Task | Outcome |
| :--- | :---: |
| Before beginning the next step ensure that the well level is between "Start and <br> Stop" level (Station under the control of the new board) | OK |
| Brisbane Water Programmer must complete the following procedures <br> From the SSMO86 Standard Fixed Speded Sewage Pumping Station (S.A.T.) <br> Section2: On Site Commissioning Procedure 2.1 to 2.9 | OK |

### 3.9.2 Commissioning of the SCADA Monitor and Control System

| BW Programmer \& Contractor Task | Outcome |
| :--- | :--- |
| Brisbane Water Programmer must complete the following procedures |  |
| From the SSMO86 Standard Fireo SpeedSewage Pumping Station (S.A.T.) | OK of |
| Section3: On Site Commissioning Procedure |  |

### 3.10 INSTALL GENERATOR MAINS (FOR SITES WITH PERMANENT GENERATORS - OPTION F)

| Contractor Task | Outcome |
| :---: | :---: |
| Record insulation resistance of the 3-phases | At 2 Sow Megohm <br> Btree Megohm. <br> $C$ thor Megohm |
| Record earth resistance | C.OS ohms |
| Connect the generator 10 cables | OK |
| Point to point phase continuity | R to L1 OKE <br> W to L2 OKU <br> B to L3 OKIT |



## 3．11 SITE ACCEPTANCE TESTING

## 3．11．1 Site Acceptance Testing（S．A．T）－Remaining Tests

| BW Programmer \＆Contractor Task | Outcome |
| :---: | :---: |
| Once pump 2 has been commissioned <br> Complete any remaining procedures in Section 2 <br> from the SSM086 Standard Fixed Speed Sewage Pumping Station（S．A．T．） | OK叩／ |
| Check operation of SIR for 20 sec ．with probe to prove probe operation and operation of 2 pumps | OK |
| Check operation LR3 with probe to prove RTU and probe | OK |
| Seal conduits with denso and grout under switchboard． | OK ${ }^{\text {O }}$ |
| Check Energex Phase Fail Input． | OKロ |
| Confirm automatic control of pumps． | OK口 |
| Check Parmoter 203 of Softstanter is a positive value UST | OK ${ }^{\text {O }}$ |
| Confirm correct operation of all door locks | OK |
| Confirm Operation \＆Maintenance Manual left on site． | OK ロ |

## 3．11．2 SCADA Testing

| BW Programmer \＆Contractor Task | Outcome |
| :--- | :--- |
| The Brisbane Water Programmer must complete the following procedures with the |  |
| assistance from the Commissioning Engineer and SCADA Commissioning Engineer |  |
| in the Control Room． |  |
| From the SSMO86 Standard Fixed Speed Sewage Pumping Station（S．A．T．） <br> Section3：SCADA Commissioning Procedure |  |

## 3．11．3 Preliminary Work Completion by Electrical Contractors

| Contractor Task | Outcome |
| :--- | :---: |
| Leave the site clean and tidy and hazard free． | OKV |
| Confirm with BW that the job is complete and their staff can leave． | OKロ |
| Confirm with BW that BW staff will lock up the site on completion of the switchboard <br> change over work． | OK |
| Note：If there is a problem with finishing the work due to unforeseen circumstance <br> refer to the Risk Analysis attached． | OKQ |

## 3．11．4 Register Control Room

| BW Programmer \＆Contractor Task | Outcome |
| :--- | :--- |
| Commissioning Engineer to call the Control Room Operator（CRO）and inform him |  |
| that the site works is complete and that the site is now fully in＂Remote＂control and | Name． |
| that all alarms are to be acted on as per the alarm instructions． |  |
| C．R．O．to confirm that the site is healthy and that there are no alarms active． | CRO |
| Record the C．R．O．＇s name and Officer Code and record the time of the call． | TIME： |



Signature：

| Doc Id： | 006142 | Active Date： $1-11-10$ Dee 2008 | Brisbane Water Confidential |
| :--- | :--- | :---: | :---: |
| Printed： | $10 / 122008$ | Ownes：Alex Wiuhon |  |
| Note： | Printed copies of this document should be verificd for currency against the published electronic copy． |  |  |

## 4 Post Change Over Checklist

### 4.1 DELIVERABLES FROM RTU PROGRAMMER

| BW Programmer | Date Completed |
| :--- | :---: |
| Within 7 days of the change over the following must be completed and signed off by <br> the BW Programmer0 |  |
| Complete Section 4: Post Commissioning |  |
| from the SSM086 Standard Fixed Speed Sewage Pumping Station (S.A.T.) | , |
| The BW Programmer will ensure that the Control Room Acceptance (CRA) form is <br> signed by the Manager of the Control Room Officers. The form is to be handed to <br> the Contracts Manager (CM). | , 1, |

### 4.2 DELIVERABLES FROM ELECTRICAL CONTRACTOR

| Contractor Task | Date Completed |
| :--- | :---: |
| All documentation required under the contract is to be provided with the time <br> specified (AS BUILT's, Eleclrical Certificates etc). | $/$, |

### 4.3 DELIVERABLES FROM COMMISSIONING MANAGER

| Commissioning Manager | Date Completed |
| :--- | :---: |
| All documentation is handed to the Project Manager to that the new switchboard <br> asset can be capitalised and handed over to the customer. |  |
| Factory Acceptance Test Sheet - Completed \& signed off. |  |
| Electrical Inspection Sheet - Completed \& signed off. |  |
| Site Acceptance Test Sheet - Completed \& signed off. | OK Q |
| Commissioning Plan - Completed \& signed off. | OK D |
| Control Room Acceptance Form - Completed \& signed off | OK Q |
| As built Drawings have been updated, drafted and taken to site along with the Site <br> Specific Functional Specification, | OK |

### 4.4 SUGGESTIONS FOR IMPROVEMENT

| Suggestion | Recommended By |
| :--- | :---: |
|  |  |
|  |  |
|  |  |



Signature:

| Doc ld: | 006142 | Active Date: $1-11-10$ Dec 2008 |
| :--- | :--- | :--- |
| Printed: | $10 / 12 / 2008$ | Owner: Alex Withof |
| Note: | Printed copies of this document should be verified for currency against the published clectronic copy. |  |

TEST SHEET

SWITCHBOARD ID:

SP /18
DATE:... 17 lifo? JOB No.: 4 ب 700052 CUSTOMERS ADDRESS: ......... WK ST LA BR


TEST EQUIPMENT:
mrbco
moLt.
serial no: $\qquad$ 518.8005 $\qquad$ 595090174

TEST DUE DATE: $\qquad$ 29/1/10 $\qquad$ 29/1/10 $\qquad$

NAME:
liter caus Li c no: $\quad 5379$ / SIGNATURE: ..
: Electric (Qld) Pty. Ltd.
FACTORY ACCEPTANCE TEST SHEET 1:

: ミlectric (Qld) Pty. Ltd.


FACTORY ACCEPTANCE TEST SHEET 1B:

|  |  <br> Process Operation |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Reference/ Acceptance Criteria | Passed |  |
| 1. | Ensure Insulation test as per QA3CH-15 have been completed | SJ QA3CH-15 <br> AS 3000 <br> Insulation resistance greater than 1 megohm ph to earth Hi pot test 2.5 kv ph-eth for 1 minute | 人 | 2aj $0 / 6 a$ |
| 2. | Ensure Checks 1 to 11 as per QA3CH-020 have been completed | SJ QA3CH-020 <br> Point to Point check of schematics. <br> Visual Check of wiring. | $\checkmark$ | z\%/iojon |
| 3. | - Check Automatic Transfer Switch is functioning by confirming the signals from relays CTSG and CTSN. | Drawing 456/5/7ncu** -001 \& 005 | $\gamma$ | $20 / 10 / 003$ |
| 4. | Check operation of Energex Power On phase failure relay PFRE and correct signal is being received by RTU | Drawing isci/s/7-ciort -001 $\qquad$ Remove one phase from relay sensing circuit to simulate loss of power. | $\checkmark$ | 201/ci/ay |
| 5. | Check operation of Station Power On phase failure relay PFRS and correct signal is being received by RTU | Drawing $\qquad$ $-001$ Remove one phase from relay sensing circuit to simulate loss of power. | 1 | zopliolocy |

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## FACTORY ACCEPTANCE TEST SHEET 2:

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Reference/ Acceptance Criteria | Passed | Date |
| 1. | Ensure Insulation test as per QA3CH-15 have been completed | SJ QA3CH-15 <br> AS 3000 <br> Insulation resistance greater than 1 megohm ph to earth <br> Hi pot test 2.5 kv ph-eth for 1 minute | 2 | 20)/10/4.c7 |
| 2. | Ensure Checks 1 to 11 as per QA3CH-020 have been completed | SJ QA3CH-020 <br> Point to Point check of schematics. Visual Check of wiring. | $\Omega$ | 2a/w/on |
| 3. | Check voltage is available on line side of circuit breaker Q9 | Drawing $256 / 5 / 7-8096-001$ <br> 415 vac ph to ph. <br> 240 vac ph to n <br> 240 vac ph to eth | $\cdots$ | zaj/10/00 |
| 4. | Ensure all distribution circuit breakers are "OFF" and operate circuit breaker Q9 and confirm voltage is available to distribution chassis. | $\begin{aligned} & \text { Drawing } \frac{3 x i j s / 7}{415} \text { vac ph to ph. } \\ & 240 \text { vac ph to } n \\ & 240 \text { vac ph to eth } \end{aligned}$ | $\sim$ | -20/10/69 |
| 5. | Ensure Station Mains Power Failure Relay Circuit Breaker Q10 is "OFF" and close circuit breaker for PFRS Relay supply. |  | $\bigcirc$ | zop/rajor |
| 6. | Confirm voltage is available to line side of Station Mains Power Failure Relay Circuit Breaker. Close circuit breaker and confirm voltage is available to Line side of PFRS Relay. | Drawing $\qquad$ $456 / 557 \pi 6096-001$ 415 vac ph to ph . <br> 240 vac ph to n 240 vac ph to eth | $\sim$ | ralic/ua |

s. lectric (Qld) Pty. Ltd.

| 7. | Repeat Step 6 above for circuit breaker Q11, Q12, Q13, Q14, Q16, Q17, Q19, Q20 and Q21 | Drawing $256 / 5 / 7-60066=001$ <br> 415 vac ph to ph (Where applicable). <br> 240 vac ph to n <br> 240 vac ph to eth | - | 74/16/an |
| :---: | :---: | :---: | :---: | :---: |
| 8. | Check operation of the following RCD's and note tripping times: <br> - Q11 <br> - Q12 <br> - Q13 <br> - Q19 <br> - Q21 | Drawing Lscis/ $7 \cdots \operatorname{civ9}$-001 Tripping Time: | $\gamma$ |  |


| Tests Completed By | Witnessed By | Accepted By |
| :---: | :---: | :---: |
| Hatrin Marliham |  |  |
| Date zu/ielar | Date | Date |
| Comments: |  |  |
|  |  |  |
|  |  |  |
| Instruments Used: |  |  |

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FACTORY ACCEPTANCE TEST SHEET 3:

| PROJECT: | Pump Station SP Zif |
| :---: | :---: |
| Client: | Brisbane Water |
| Job No. | WT4000035 |
| Equipment: | SPzif_Switchboard |
| Section: | RTU Connection |
| Drawing: | -istj5/7-cent -001 \& 006 |


|  | Process Operation | Reference/ Acceptance Criteria | Passed | Date |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Ensure Insulation test as per QA3CH-15 have been completed | SJ QA3CH-15 <br> AS 3000 <br> insulation resistance greater than 1 megohm ph to earth <br> Hi pot test 2.5 kv ph-eth for 1 minute | , | 209/10/069 |
| 2. | Ensure Checks 1 to 11 as per QA3CH-020 have been completed | SJ QA3CH-020 <br> Point to Point check of schematics. Visual Check of wiring. | 2 | ra/kelca |
| 3. | Ensure Laptop GPO, circuit breaker Q13 is "OFF" and operate RTU circuit breaker Q30 on DB Chassis and ensure: <br> RTU Power Supplies are operating correctly. | Drawing $\qquad$ -001 240 vac ph to n on power supply input. 24 vdc on power supply output | $\checkmark$ | 2010jous |
| 4. | Close Laptop GPO Circuit Breaker and: <br> Check GPO polarity. <br> Check GPO switch is functioning. <br> Check operation of RCD device. | Drawing $484 / 5 / 2$ exac 001 | $\Gamma$ | solula.s |
| 7. | Confirm operation of door switches. | Drawing intojspacex 001 \& 006 | $\sim$ | 70110/09 |

! Electric (Qld) Pty. Ltd.

| Tests Completed By | Witnessed By | Accepted By |
| :---: | :---: | :---: |
| Aarren Meskhem |  |  |
| Date zelicior | Date | Date |
| Comments: |  |  |
|  |  |  |
|  |  |  |
| Instruments Used: multimeler, megneor |  |  |
|  |  |  |

## Electric (QId) Pty. Ltd.

## FACTORY ACCEPTANCE TEST SHEET 4

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Process Operation | Reference/ Acceptance Criteria | Passed | Date |
| 1. | Ensure Insulation test as per QA3CH-15 have been completed | ```SJ QA3CH-15 AS 3000 Insulation resistance greater than 1 megohm ph to earth Hi pot test 2.5 kv ph-eth for 1 minute``` | $\cdots$ | Te/ic/er |
| 2. | Ensure Checks 1 to 11 as per QA3CH-020 have been completed | SJ QA3CH-020 <br> Point to Point check of schematics. Visual Check of wiring. | - | "c/ue/a - |
| 3. | Check voltage is available on line side of motor circuit breaker Q4. | $\text { Drawing }+451 / 5 / 7<06-002$ $415 \text { vac ph to ph }$ | $\cdots$ | $2 \mathrm{c} / 16 / \mathrm{cos}$ |
| 4. | Ensure control circuit breaker Q4-1 is "OFF" and emergency stop is operated, close circuit breaker Q4 and confirm voltage is available on line side of circuit breaker Q4. | $\begin{aligned} & \text { Drawing } \frac{-5+5 / 5 / 7-0,0 w t}{}-002 \\ & 415 \text { vac } \mathrm{ph} \text { to } \mathrm{ph} \end{aligned}$ | $\underline{2}$ | 20/10/09 |
| 5. | Check voltage is available on line side of control circuit breaker Q4-1, close circuit breaker and ensure: <br> - 1K4 Control Supply Relay is operating correctly. | $\begin{aligned} & \text { Drawing } 456 / 5 / 7-00.96-002 \\ & 240 \text { vac ph to } \mathrm{n} \end{aligned}$ | $\Omega$ | 20/icloci |
| 6. | Release emergency stop and confirm operation of isolating contactor 1 K 1 and confirm voltage is available to VSD. | $\begin{aligned} & \text { Drawing } \frac{\operatorname{cst} /}{} / 5 / 7 \text {-enart }-002 \\ & 415 \mathrm{vac} \mathrm{ph} \text { to } \mathrm{ph} \end{aligned}$ | $\sim$ | zariofon |
|  |  |  |  |  |

## Electric (Qld) Pty. Ltd.

| 7. | Confirm operation of Pump 1 Digital Inputs. | Drawing $\operatorname{cst/s/7-cas)t-002~}$ | - | 20/6\%/c. 9 |
| :---: | :---: | :---: | :---: | :---: |
| 8. | Confirm Operation of Pump 1 Digital Outputs |  | - | 4. $/ 1 \times 1 / 0 \cdot 7$ |
| 9. | Confirm Operation of Pump 1 Analog 1/O | Drawing 48tis/7 | - | roprajor |
| 10. | Confirm Operation of cubicle fan by manually operating the thermostat 1FC | Drawing csids/7-caxib -002 | $\gamma$ | 20\%/0/0.4 |


| Tests Completed By | Witnessed By | Accepted By |
| :---: | :---: | :---: |
| Awn Mriklem |  |  |
| Date zolicier | Date | Date |
| Comments: |  |  |
|  |  |  |
|  |  |  |
| Instruments Used: multimeter, megyer |  |  |

## 三lectric (Qld) Pty. Ltd.

## FACTORY ACCEPTANCE TEST SHEET 5:

|  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Reference/ Acceptance Criteria | Passed | Date |
| 1. | Ensure Insulation test as per QA3CH-15 have been completed | ```SJ QA3CH-15 AS 3000 Insulation resistance greater than 1 megohm ph to earth Hi pot test 2.5 kv ph-eth for }1\mathrm{ minute``` | - | 201/6/4.7 |
| 2. | Ensure Checks 1 to 11 as per QA3CH-020 have been completed | SJ QA3CH-020 <br> Point to Point check of schematics. Visual Check of wiring. | $\checkmark$ | 70/10/09 |
| 3. | Check voltage is available on line side of motor circuit breaker Q5. | $\text { Drawing } \frac{256 / 5 / 7-a ; i 6}{}-003$ <br> 415 vac ph to ph | $\square$ | -2, $/ 10 / \mathrm{col}$ |
| 4. | Ensure control circuit breaker Q5-1 is "OFF" and emergency stop is operated, close circuit breaker Q5 and confirm voltage is available on line side of circuit breaker Q5 . |  415 vac ph to ph | 2 | 20/ic/er |
| 5. | Check voltage is available on line side of control circuit breaker Q5-1, close circuit breaker and ensure: <br> - 2K4 Control Supply Relay is operating correctly. |  | $\sim$ | repluglon |
| 6. | Release emergency stop and confirm operation of isolating contactor 2 K 1 and confirm voltage is available to VSD. | $\begin{aligned} & \text { Drawing } \frac{456 / 5 / 7 \text { remak }}{415 \text { vac }} \mathrm{ph} \text { to } \mathrm{ph} \end{aligned}$ | - | $\because C$ /la/as |
|  |  |  |  |  |

Electric (Qld) Pty. Ltd.

| 7. | Confirm operation of Pump 1 Digital Inputs. |  | $\sim$ | 20/iclua |
| :---: | :---: | :---: | :---: | :---: |
| 8. | Confirm Operation of Pump 1 Digital Outputs |  | $\sim$ | 20\%10/a |
| 9. | Confirm Operation of Pump 1 Analog I/O | Drawing 4si/s/7-cont-003 | < | 20/ialon |
| 10. | Confirm Operation of cubicle fan by manually operating the thermostat 2FC | Drawing 466/y/r -tatil -003 | - | 20\%idecis |


| Tests Completed By | Witnessed By | Accepted By |
| :---: | :---: | :---: |
| Aars- Markhan |  |  |
| Date zoliofoa | Date | Date |
| Comments: |  |  |
|  |  |  |
| Instruments Used: multimeter, megegar |  |  |
|  |  |  |

amome

Ref: Test Certificate P218.doc

## TEST CERTIFICATE

SJ Electric (Qld) Pty. Ltd.
19 Elliot Street.
Albion Qld. 4010
R.E.C. 7623

Attention: Wendy Wong
Level 2 TC Beime Centre, 315 Brunswick Street Mall, Fortitude Valley Q 4006

Work performed for Brisbane Water at SP218 at Westlake Dr under contract BW: 70103-06/07-026 (SJO Electric Job Number WT400052)

Installation Tested.
New Pump Station Switchboard located at Westlake Drive Riverhills.

Test Date
17/11/09
Testing.
The certificate certifiy's that the electrical installation to the extent it is affected by the electrical work has been tested to ensure it is electrically safe and is in accordance with the requirements of the wiring rules and the electrical safety regulation 2002. C.J. Holmes (endorsee to electrical contracting license 7623)

Signed.


BRISBANE CITY COUNCIL

## Sewage Pump Station SP218

## Westlake Drv

Contract: BW 70103-026
Job Number: WT400052

## ELECTRICAL INSTALLATION

## OPERATIONS and MAINTENANCE MANUAL

## VOLUME 1

INSTALLATION BY:
SJ Electric (Qld) Pty Ltd
19 Elliot Street
Albion Qld 4010

## INDEX

| SECTION | Sewage Pump Station - SP218 Westlake Drv |
| :---: | :---: |
| Volume 1 $1 .$ | GENERAL <br> 1.. 1 General Workplace Health \& Safety <br> 1.. 2 Project Overview <br> 1.. 3 Plant Maintenance <br> 1.. 4 Electrical Control System <br> 1..5 Control \& Monitoring System |
| Volume 1 <br> 2. | MANUFACTURER'S TECHNICAL DATA <br> 2.1 Terasaki XS 400 Circuit Breakers. <br> 2.2 Sprecher and Schuh CA-7Contactors. <br> 2.3 Critec TDS -180-4S-277 Surge Diverter <br> 2.4 Critec TDF-10A-240V Surge Filter. <br> 2.5 Critec DAR-275V Alarm Relay <br> 2.6 Crompton Phase Failure Relay. <br> 2.7 Multitrode MTR Level Relay <br> 2.8 Trio DR900-06A02-D0 Radio. <br> 2.9 Polyphaser IS-50NX Impulse Suppressor. <br> 2.10 Powerbox Radio/DC converter. <br> 2.11 Powerbox Modem/DC converter. <br> 2.12 Multitrode Level Probe <br> 2.13 Emotron Soft Starter MSF2.0 <br> 2.14 AICHI Automatic Transfer Switch <br> 2.15 Vega Delivery Pressure Transmitter <br> 2.16 Endress \& Hauser Wet Well Level Transmitter |
| Volume 2 <br> 3. | DRAWINGS |
| Volume 2 4. | INSPECTION \& TEST RESULTS |
| Volume 2 <br> 5. | COMPLIANCE CERTIFICATES |

## Page 1

### 1.1 General Workplace Health and Safety

- The Workplace Health and Safety Act (1995) sets out the laws about Workplace Health and Safety for all workplaces, workplace activities and specified high risk plant. The Electrical Safety Act (2002) sets out the laws covering electrical safety. Nothing in this document is designed, in any way, to undermine the authority of the Acts.
- All reasonable care must always be taken to ensure the plant is without risk to the health and safety of personnel operating and maintaining plant and equipment.
- Employers have an obligation to ensure the workplace health and safety of all personnel at work.
- It is employer responsibility to ensure that all persons entering or working on the premises use appropriate personal protective equipment.
- Personal protective equipment includes gloves, safety glasses, hard hats, ear protection, safe foot ware and, where necessary, specialist protective clothing for hazardous areas.
- Any item of equipment should always be isolated before maintenance or repairs commence to ensure that inadvertent operation of the item does not result in risk to the health and safety of any person.
- Where the item is isolated, any total or partial shutdown should not allow a hazardous situation to be created.
- Where the item cannot be isolated, another person should be stationed at the controls of the item and an effective means of direct communication should exist between the persons carrying out the maintenance and the person at the controls.


## Page 2

## General Operating Principles

- All persons working the premises must be qualified Electrical Engineers or electrical trades persons capable of performing the required tasks competently. All personnel must also be familiar with plant and equipment.
- Adequate information, instruction, training and supervision must be provided to enable personnel to perform work without risk to health and safety.
- Work in an orderly way.
- Plan work in advance to avoid hazardous situations.
- Warn others of any hazards.
- Make inquiries before starting work, particularly on any unfamiliar installation or equipment.
- Before any work begins ensure that any instructions received or given are fully understood.
- Concentrate on the task on hand.
- Do not distract others or allow yourself to be distracted by foolish actions.
- Work from a safe and convenient position that provides a maximum working space that you do not have to over reach, you cannot slip, trip or stumble and so endanger yourself and others.
- Keep the working area tidy and free of unwanted materials and equipment.
- Use insulated tools where possible.
- Inspect tools and equipment regularly and ensure that any necessary maintenance is carried out.
- Keep yourself in good health.
- Do not work if ill or over tired, to the extent that your concentration, movement or alertness is affected. Illness or fatigue can endanger yourself and others.


## Page 3

### 1.2 Project Overview

Contract BW70103-026as for the manufacture and testing of ten (1) new pump station switchboards for various locations throughout Brisbane.

Equipment provided by SJ Electric ensures safe and efficient operation of the pump stations. Equipment supplied and installed by SJ Electric includes: -

- Switchboards
- Instrumentation
- Civil Works

The switchboard incorporates the latest technology in motor control, power monitoring, and instrumentation. It is important engineers, technicians and operators are familiar with the equipment installed before attempting any adjustments, modifications or maintenance.

The following Sections of this manual contain a comprehensive description of all equipment supplied, by SJ Electric. It is recommended that this manual be referred to before carrying out any work on any equipment.

## Page 4

### 1.3 Plant Maintenance

To ensure proper operation of the plant the following should be observed: -

- The plant should be kept clean and tidy at all times. Not only is this of aesthetic value, it extends equipment life.
- Check that all plant and equipment is operating correctly. Correctly operating equipment promotes overall plant efficiency.
- All items and areas of equipment should be hosed down and cleaned regularly.


## WARNING

- Avoid directly hosing any drive motor or electrical item.
- All maintenance, service, modifications and significant deviations from Normal operating conditions should be recorded in the Plant Service Log
- After a month of operation, check the tension of all bolts associated with the plant and thereafter periodically. Bolted connections on painted surfaces can loosen due to thinning of the paint underneath the bolt head-bearing surface. Motor mounting bolts and other bolted connections subjected to vibration should be periodically checked for loosening.


## WARNING <br> - Before starting work on any item ensure that the power supply is isolated, tagged off, and the item cannot be started.

- The importance of preventative maintenance cannot be over-emphasized. Regular maintenance and suitable care of the equipment will ensure a long and reliable service life of the equipment.
- Many stoppages can be avoided by following the recommended maintenance procedures. Do not wait until you hear the grinding of equipment that has broken down. If you see any item wearing down, replace it, before it causes damage to other associated items.


## Page 5

## Preventive Maintenance

Maintenance procedures recommended to extend switchboard life are outlined as follows:-

- Switchboard exterior should be regularly wiped down with a solvent base cleaner such as "Spray \& Wipe". This will ensure longevity of the powder-coated surface.
- Accessible areas like distribution boards and motor starter panels should be cleaned with a vacuum cleaner to remove dust and foreign matter.
- PLC panels should be maintained as dust free as possible. Dusting with a dry rag is recommended - taking care not allows dust inside the I/0 modules or processor.
- When removing or installing PLC modules care should be taken to ensure that power is turned off to the rack before modules are removed or installed.
- Connections and efficient operation of circuit breakers, contactors and isolators should be checked every 12 months - especially where connected to busbars.
- Busbar connections should be checked every 12 months.
- Globes for indicator lights should be checked on a weekly basis with any faulty lamps replaced.
- Cubicle Fans Filter should be inspected and cleaned frequently.


### 1.4 Electrical Control System

## General Description

The switchboards are manufactured from 3 mm aluminium and are suitable for location outdoors; the switchboards have been designed by Brisbane Water and contain several separate sections including:

- Incoming Section.
- Metering.
- Motor Starter Section.
- Distribution Section.
- RTU Section.


### 1.5 Control and Monitoring System.

The control and monitoring of the system is performed by the Brisbane Water telemetry system and was not included in this contract.

# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218

## Westlake Drv

Equipment Type: Circuit Breaker
Location:
Main IncomerPump Circuit Breakers
Model Numbers: ..... XS 400
Manufacturer:
Terasaki
Supplier:
NHP Pty Ltd25 Turbo Drive
Coorparoo QLD ..... 4151
Ph: 0738916008
Fx: 0738916139

## TemBreak MCCBs

## XS400 series thermal magnetic type

Adjustment range 63-100 \% of nominal current rating.

- Standards AS 2184/AS/N2S 3947-2.
- Adjustable thermal and magnetic trip.


## XS400CJ ( 35 kA ) 3 pole

| Ampere <br> rating | Min | Max | Cat. No. |
| :--- | :--- | :--- | :--- |
| 250 | 160 | 250 | XS400CJ 250 3 |
| 400 | 250 | 400 | XS400CJ 400 3 |
| 400 | Non-Auto (5 kA for 0.3 sec$)$ | ${ }^{7}$ ) | Refer page 5-48 |



| 250 | 160 | 250 | X5400CJ 2504 |
| :---: | :---: | :---: | :---: |
| 400 | 250 | 400 | XS400CJ 4004 |
| XS400NJ ( 50 kA ) 3 pole |  |  |  |
| 250 | 160 | 250 | XS400NJ 2503 |
| 400 | 250 | 450 | XS400NJ 4003 |
| XS400NJ ( 50 kA ) 4 pole |  |  |  |
| 250 | 160 | 250 | XS400NJ 2504 |
| 400 | 250 | 400 | XS400NJ 4004 |


| Dimensions (mm) <br> Description | Height | Width | Depth | kg |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| XS400CJ/NJ | 3 pole | 260 | 140 | 103 | 4.7 |
| 4 pole | 260 | 185 | 103 | 6.1 |  |
|  |  |  |  |  |  |

Notes: ${ }^{1}$ ) Load-break isolating switch only - no protection.
${ }^{2}$ ) MCCBs only.
$\left.{ }^{7}\right)$ Poles in series. Refer applications Section 13.

| Short circuit capacity <br> Model |  |  |
| :--- | :--- | :--- |
| I/C | Voltage |  |
| XS400CJ | $35 \mathrm{kA}($ AS 2184) | 415 V 50 Hz |
| XS400NJ | 50 kA | 415 V 50 Hz |
|  |  |  |
| DC use $\left.{ }^{~}\right)$ | I/C | Voltage |
| XS400CJ | 40 kA | 250 V DC |
| XS400NJ | 40 kA | 250 VDC |

Refer to ratings chart at the front of this section. For ratings to AS/NZS 3947-2 and AS 2184, and les/Icu.

| Cross reference table | Section |
| :--- | :--- |
| Accessories | 6 |
| Selectivity \& cascade | 13 |
| Application data | 13 |
| Characteristic curves | 7 |
| Motor starting | 13 |
| Connection \& mounting details | 7 and 8 |
| Detailed dimen. - MCCB only | 7 |
| - motor operators 7 |  |


| Product extensions | Section |
| :--- | :--- |
| Chassis (TemWay, MHC, UHC) | 6 |
| TemCurve | 13 |
| Residual current relays | 11 |

Base standards
IEC 60947-2
BS EN 60947 Part 2
VDE 0660 Part 1
AS/NZS 3947-2/Aust./NZ
AS 2184-1990/Australia ${ }^{7}$ )
JIS C 8372/JAPAN
JEC 160/JAPAN

Approvals ASTA/UK, Aust. standards
Marine
NK/JAPAN
Lloyds R/UK
ABS/USA
GL/GERMANY
BV/FRANCE
DNV NORWAY

# Standard TemBreak circuit breaker Selection guide 

 DIMENSIONS (mm)

| DIMENSIONS ( mm ) |  | 78 | $30$ | 90 | 120 | 30 | 90 | 120 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{H}{3}^{+}$ | $\stackrel{+}{\square}$ |  |  |  |  |  |  |  |
|  | b | 148 | 155 |  |  | 155 |  |  |
| 寻 | c | 98 | 86 |  |  | 86 |  |  |
|  | $4 \frac{d}{d}$ | 116 | 104 |  |  | 104 |  |  |
| Weight (kg) * marked standard type |  | 1.3 | 0.51 | 1.3 | 1.58 | 0.51 | 1.3 | 1.58 |
| CONNECTION AND MOUNTINGS |  |  |  |  |  |  |  |  |
| front connect (FC) | terminal screw | * | - |  |  | * |  |  |
|  | attached flat bar | - | - | 0 |  | - | 0 |  |
|  | solderless terminal (PWC) | 0 | 0 |  |  | 0 |  |  |
| rear <br> connect (RC) <br> plug-in (PM) | bolt stud | 0 | - | 0 |  | - | 0 |  |
|  | flat bar stud | - | - |  |  | - |  |  |
|  | for switchboard | 0 | - | 0 |  | - | 0 |  |
| draw-out (DO) for distribution board |  | - | $\underline{\square}$ | 0 |  | - | 0 |  |
|  |  | - | $\underline{\square}$ |  |  | $\underline{-}$ |  |  |

## STANDARD FEATURES contact indicator <br> trip button

\section*{| Electronic type |
| :--- |
| Adjustable LTD, STD \& INST | <br> | Adjustable LTD, STD \& INST |
| :--- |
| Adjustable GFT or Adjustable PTA (option) |}

Trip indicators (option) (contacts)
Thermal-magnetic type
thermal and fixed magnetic trips
thermal and adjustable magnetic trips
adjustable thermal and fixed magnetic trips
adjustable thermal and magnetic trips


5-2
(7) TERASAKI

## Standard TemBreak circuit breaker Selection guide




MCCB operational characteristics \& dimensions
Page

| Thermal - magnetic MCCB characteristics | 7-2 to 7-4 |
| :---: | :---: |
| Time / current characteristics thermal - magnetic MCCBs | 7-5 to 7-10 |
| Electronic MCCB characteristics - settings | 7-11 to 7-14 |
| PTA - Pre-trip alarm option | 7-15 to 7-19 |
| GF - Ground fault / 4th CT option | 7-16 to 7-19 |
| LED trip indication options | 7-18 to 7-19 |
| Time / current characteristics electronic MCCBs | 7-20 to 7-22 |
| OCR checker for electronic MCCBs | 7-23 |
| TemCurve selectivity software | 7-24 |
| MCCB dimensions with and without motors fitted | 7-25 to 7-50 |
| AC Watts loss - 3 pole MCCBs | 7-51 |



## MCCB Technical data

## Thermal Magnetic MCCBs

Thermal-Magnetic MCCBs are available from 125 AF to 800 AF. Depending on the type of MCCB thermal and/or magnetic trip setting may be adjustable.

| MCCB type | Fixed <br> thermal | Adjustable <br> thermal | Fixed <br> magnetic | Adjustable <br> magnetic |
| :--- | :---: | :---: | :---: | :---: |
| XS125CS, XS125NS | - | - | - | - |
| XS125CJ, XS125NJ | - | - | - | - |
| XH125NJ, XH125PJ, TL100NJ | - | - | - | - |
| XH160PJ | - | - | - |  |
| XE225NC | - | - | - | - |
| XS250NJ, XH250NJ | - | - | - |  |
| XH250PJ | - | - | - |  |
| XS400CJ, XS400NJ, XH400PJ, TL250NJ | - | - | - |  |
| XS630CJ, XS630NJ, XH630PJ | - | - | - | - |
| XS800NJ | - | - | - | - |
| XH800PJ |  | - | - | - |

## Note: - Yes

- No

Access to setting dials
From 125 AF to 250 AF the thermal adjustment is visible from the front of the MCCB. At 400 AF and above a protective cover must be removed to gain access to the settings. To achieve access to the settings, the cover screw under the 'sealed' label must be removed. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver. Once set, secure the cover and apply a new sealing label.


[^2]

## MCCB Technical data

## Thermal Adjustment

TemBreak MCCBs have a wide thermal adjustment range, one of the largest on the market. The rated current ' l ' is continuously adjustable from $63 \%$ to $100 \%$ of its nominal current ' 1 n'. There are three main points of calibration marked at $63 \%, 80 \%$ and $100 \%$, as shown in the diagram below.

## Magnetic Adjustment

The magnetic adjustment is available on MCCBs of 400 AF and above. The magnetic setting ' 1 m ' is continuously adjustable from $500 \%$ to $1000 \%$ of its rated current 'In'. There are five main points of calibration marked as multiples of $\mathrm{In}_{\mathrm{n}} ; 5,6,7.1,8.5$ and 10 . These are shown in the diagram below.


## Examples

1. XS125NJ/125A MCCB set at $\mathrm{I}_{\mathrm{r}}=0.8$, the rated current is calculated as $125 \times 0.8=100 \mathrm{~A}$
2. XS400NJ/400A MCCB set at $\mathrm{Im}_{\mathrm{m}}=6$, the magnetic setting is calculated as $400 \times 6=2400 \mathrm{~A}$
3. $\mathrm{XS} 630 \mathrm{NJ} / 630 \mathrm{~A}$ MCCB set at $\mathrm{I}_{\mathrm{r}}=0.8$ and $\mathrm{Im}_{\mathrm{m}}=5.0$

The rated current is calculated as $630 \times 0.8=504 \mathrm{~A}$
The magnetic setting is calculated as $630 \times 5=3150 \mathrm{~A}$
Note that the magnetic setting is a multiple of the nominal current In and not the rated current Ir. All thermal and magnetic trip settings are expressed as AC RMS values.
All MCCBs are calibrated at $45^{\circ} \mathrm{C}$ unless otherwise specified.
Breakers with adjustable magnetic trip

|  | Rated <br> current (A) |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Breaker | Scale 10 | $\mathbf{8 . 5}$ | $\mathbf{7 . 1}$ | $\mathbf{6}$ | $\mathbf{5}$ |  |
| XS400CJ | 250 | 2500 | 2125 | 1775 | 1500 | 1250 |
| XS400NJ | 400 | 4000 | 3400 | 2840 | 2400 | 2000 |
| XH400PJ | 400 | 4000 | 3400 | 2840 | 2400 | 2000 |
| XS630CJ | 400 | 4000 | 3400 | 2840 | 2400 | 2000 |
| XS630NJ | 630 | 6300 | 5355 | 4473 | 3780 | 3150 |
| XH630PJ | 630 | 6300 | 5355 | 4473 | 3780 | 3150 |
| XS800NJ | 800 | 8000 | 6800 | 5680 | 4800 | 4000 |
| XH800PJ | 800 | 8000 | 6800 | 5680 | 4800 | 4000 |

[^3]
## MCCB Technical data

## Time/current characteristic curves



Ambient compensating curves


## Example 1

The XS250NJ set at its maximum thermal setting of 250A experiences an overload of 1000A. What would be the tripping time?

## Solution

As the axis are 'percent' rated current the overload as a percentage to rated current is

$$
\frac{100 \mathrm{~A}}{250}=400 \%
$$

The maximum and minimum on the curve are the tolerance bands. Therefore at $400 \%$ overload the tripping time would be as follows:
Maximum trip time $\approx 30$ seconds
Minimum trip time $\approx 10$ seconds
Average trip time $\approx 20$ seconds
Due to strict quality control of the manufacturing and calibration processes, the characteristic curve of most MCCBs will follow the 'average' curve within the tolerance band.

## Example 2

The XS250NJ is calibrated at 250 A for $45^{\circ} \mathrm{C}$ ambient. If the temperature rose to $55^{\circ} \mathrm{C}$ what effect would this have?

## Solution

At $55^{\circ} \mathrm{C}$ the ambient compensating factor is $93 \%$, i.e. $250 \times 0.93=232.5 \mathrm{~A}$

In other words the XS250NJ would act as an MCCB set at 232.5 A , in $55^{\circ} \mathrm{C}$.

## MCCB Technical data

## XS125CS, XS125NS

Time/current characteristic curves


Ambient compensating curves


XS125CJ, XS125NJ, XH125NJ, XH125NJ
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## XE225NC

Time/current characteristic curves


XH160PJ, XS250NJ, XH250NJ
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

```
XH250PJ, XS400CJ, XS400NJ, XH400PJ
```

Time/current characteristic curves


Ambient compensating curves


XS630CJ, XS630NJ, XH630PJ

Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

XS800NJ, XH800PJ
Time/current characteristic curves


Ambient compensating curves


XM30PB
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## TL30F

Time/current characteristic curves


Ambient compensating curves


## TL100NJ

Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## TL250NJ

Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## Microprocessor based characteristics and adjustments

## Characteristics

The standard microprocessor based MCCB from Terasaki has the most flexible characteristics on the European market. In addition to the standard overload and short circuit protection, there are a number of options available to meet specific applications.


Note:

- Standard
- Optional
- Not available
${ }^{1}$ ) Includes TL400NE \& XV400NE
${ }^{2}$ ) Includes TL630NE to TL1250NE
${ }^{3}$ ) Includes XV630, 800 \& 1250
Legend Application

| LTD | Long Time Delay | Overload protection, True RMS |  |  |
| :--- | :--- | :--- | :--- | :--- |
| STD | Short Time Delay | Short circuit protection and selectivity |  |  |
| INST | Instantaneous | Short circuit protection, fast acting |  |  |
| I2t RAMP |  | Provides easier grading with downstream fuses |  |  |
| TemBreak all |  |  |  |  |
| Pick-up LED |  | Microprocessor <br> MCCBs |  |  |
| Test Port |  | Lights on LTD overload, flashes on PTA pick-up |  |  |
| PTA | Pre-Trip Alarm | Useful for loadshedding application |  |  |
| GFT | Ground Fault Trip | Protection against ground faults |  |  |
| LEDs | Light Emitting Diodes | Indication of fault for faster diagnosis |  |  |
| HI-INST | High Instantaneous | High inrush applications, increased selectivity |  |  |

## Access to setting dials

To adjust the settings on the microprocessor TemBreak, the sealed label must be broken and the cover fixing screws removed. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver. Align the setting required between the black dots marked on the dial.


## MCCB Technical data

## Microprocessor based characteristics adjustments, operation, settings

Standard time current curves


Standard microprocessor adjustments


Each part of the characteristic curve can be independently adjusted. This unique adjustability of LTD, STD and INST enables the standard microprocessor MCCB to achieve more than 200,000 permutations of its time/current characteristic.

This makes the TemBreak microprocessor range one of the most flexible on the market.

To complement this range, NHP have developed TemCurve selectivity analysis software, which contains the full range of TemBreak MCCBs on database. This software package highlights the full benefit of having highly adjustable microprocessor MCCBs when involved with difficult selectivity problems.

The $1^{2} \mathrm{t}$ ramp switch, which is provided as standard, assists in discrimination with downstream fuses.

With the switch off, the STD operates with a definite time characteristic: L with the switch on, the characteristic alters to a ramp: $\measuredangle$, cutting off the corner which poses a potential selectivity problem.

| Setting Dial |  | Available adjustments |  |
| :--- | :--- | :--- | :--- |
| Base current setting | $I_{0}$ | $0.63-0.8-1.0 \times \mathrm{I}_{\mathrm{n}}$ | Amps |
| LTD pick-up | $\mathrm{I}_{1}$ | $0.8-0.85-0.9-0.95-1.0 \times \mathrm{I}_{0}$ | Amps |
| LTD setting | $\mathrm{T}_{1}$ | $5-10-15-20-25-30\left(\right.$ at $\left.\mathrm{I}_{1} \times 600 \%\right)$ | Secs |
| STD pick-up | $\mathrm{I}_{2}$ | $2-4-6-8-10 \times \mathrm{I}_{0}$ | Amps |
| STD setting | $\mathrm{T}_{2}$ | $0.1-0.15-0.2-0.25-0.3$ | Secs |
| INST pick-up | $\mathrm{I}_{3}$ | $3-12-\times \mathrm{I}_{0}$ (continuously adjustable) | Amps |

[^4] available. Please contact NHP for details.

## MCCB Technical data

## Adjustment of TemBreak (electronic type) tripping characteristics

Electronic models of TemBreak come standard with an 8-bit microprocessor overcurrent relay (OCR). It is the OCR which provides the functions necessary for protection, while maintaining a high level of reliability.

Note: The ground fault trip and pre-trip alarm cannot be used simultaneously in a single breaker.

The wide OCR adjustment range allows the circuit breaker to be set-up in order to trip under certain conditions. Adjustments can be made to the tripping current as well as the tripping time of the breaker.

Front view


Figure 1. Electronic OCR adjustment possible (with label removed).


## Adjustment method

Remove the sealing label, loosen and remove the cover fixing screws and remove the cover. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver.

Note: Align the groove (end marked with dots) between the bands for the required setting.
For example, the diagram right shows $\mathrm{l}=1.0$.
The INST and GFT pick-up currents are continuously adjustable.


Secure the cover and apply the sealing label.

## MCCB Technical data

## Microprocessor based characteristics - adjustments, operation and examples

Overload adjustment
The rated current of the microprocessor based TemBreak is adjusted using two current multipliers. This process achieves high accuracy adjustment from $50 \%$ to $100 \%$. These are the LTD pick-up dial ( 11 ) and the Base Current ( 10 ) selector switch. The rated current (LTD pick-up) is achieved as follows:
$I_{\text {Rated }}=\ln \times \operatorname{lox} \ln$
In the example shown on the right the rating would be:
Iratied $=1250 \times 1.0 \times 1.0=1250 \mathrm{~A}$
In total there are 15 possible increments of adjustment between 50 and $100 \%$ as shown below.


Base current


100

Current dial

## Breaker

 rated current

Example - Settings
In the example shown on the right, what are all the settings in Amps?

## Solution

Irating LTD pick-up $=\ln \times l_{0} \times l_{1}$
$1250 \times 0.8 \times 0.9=900 \mathrm{~A}$
STD pick-up $=\ln \times 10 \times l_{2}$
$1250 \times 0.8 \times 4=4000 \mathrm{~A}$
INST pick-up $=\quad \ln \times 10 \times l_{3}$
$1250 \times 0.8 \times 12=12,000 \mathrm{~A}$
GFT pick-up $=\ln \times I_{G}$
$1250 \times 0.1=125 \mathrm{~A}$
(Note that GFT is a function of $\mathrm{In}_{\mathrm{n}}$ and not I 0 )


Example - Time/Current curves



7-14

## MCCB Technical data

## Options (electronic type) TemBreak

Pre-trip alarm (PTA)
The PTA continuously monitors the true RMS value of the load current. When the load current exceeds the pre-set current (Ip) an LED gives local alarm that the MCCB is approaching an overioad situation.
Should the current Ip be exceeded for 40 secs a (N/0) contact will close to provide remote indication and/or load shedding.

## PTA specifications

Pick up current (A): [lp]


Adjustable steps of $70,80,90,100 \%$ of the selected rated current [17].
Setting tolerance $\pm 10 \%$
Note: The long time-delay trip does not operate 'first' when the pick-up current is adjusted to $100 \%$ of the rated current [ [1].

PTA characteristics


Operating time (s) [Ip] Output contact

40 secs (fixed definite time-delay) setting tolerance is $\pm 10 \%$
Normally open contact, (1a) Integral lead is standard length ( 450 mm )

|  |  | Resistive load | Inductive load |
| :--- | :--- | :--- | :--- |
| Rating of <br> contact | 250 V AC | 125 VA (2 A max) | 20 VA (2 A max) |
|  | 220 V DC | 60 W (2 A max) | 10 W (2 A max) |
|  | Pick-up LED flickers |  |  |

## MCCB Technical data

## Adjustment of TemBreak electronic type OCR with ground fault

Ground fault trip
The GFT pick-up current is continuously adjustable from $10 \%$ to $\mathbf{4 0} \%$ of the rated CT current.
Notes: The ground fault trip and pre-trip alarm cannot be used simultaneously in a single breaker. XS400SE, XH400SE are not available with ground fault function.
When a three pole breaker is used in a 3 phase, 4 wire system, a separate CT is required for the neutral line. (refer NHP).
GFT specifications

Pick-up current (A): [IG]


Continuously adjustable from 10 to $40 \%$ of the rated CT current (Ict) setting tolerance is $\pm 15 \%$
la X Igt
Time-delay (S): [TG]


The GFT has a definite time-delay characteristic and is
adjustable in steps of $0.1,0.2,0.3,0.4,0.8 \mathrm{~s}$. Total clearing time is +50 ms and resettable time is -20 ms for the preset

To SEC
time delay.
GFT characteristics
.


4th CT for GFI
Rating (A) Type

| 2500 | UXOY0007A |
| :--- | :--- |
| 2000 | UXOYO006A |
| 1600 | UXOYO005A |
| 1250 | UXOY0004A |
| 1000 | UXOY0003A |
| 800 | UXOY0002A |
| 630 | UXOY0001A |



| Rating (A) | A | B | C | D | E | F | H | CH | M | N |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2500-1000$ | 140 | 110 | 50 | 10 | 80 | 85 | 145 | 75 | 85 | 35 |
| $300-630$ | 105 | 100 | 40 | 8 | 50 | 75 | 110 | 57 | 50 | 20 |

7-16

## MCCB Technical data

## TemBreak electronic type with ground fault

External neutral sensor (4th CT)
External neutral sensors are required whenever optional earth fault is used on 3 phase 4 wire systems

The position and direction of 4th CT


The direction of 4th CT

## DIRECTION LINE SIDE



## (4) TERASAKI

## MCCB Technical data

## Trip indicators

The LEDs when lit, indicate which trip function tripped the breaker eg, long-time-delay (LTD), short-time delay/ instantaneous (STD/INST) or ground fault (GFI) (control power required).

Trip indicator display (1250 AF and above)


Trip indicator display ( 400 AF to 800 AF ) and OCR controller example: XS, XH400
An optional feature available with TemBreak electronic type are An external trip indicator box is required with 400AF models. fault indication contacts - these are voltage free and provide a signal of the cause of a trip (long time, STD/INST).


Notes: For dimensions of XS/XH800SE and PE refer to pages 7 - 40 and 7 - 41, add dimensions of OCR controller and trip indication box (above).

## MCCB Technical data

OCR controller (PTA and trip indication)

OCR controller mounting position


Dimension table (mm)

| Ampere <br> frame | Type of <br> MCCB | With UVT <br> controller | Without UVT <br> controller | B |
| :--- | :--- | :---: | :---: | :---: |
| 400 | XS400 | 34 | 97 | 48 |
| $\mathbf{4 3 0}$ | XH400/TL400NE | 34 | 97 | 48 |
| $\mathbf{X S 6 3 0 / X V}$ | 64 | 151 | 60 |  |
|  | XH630 | 64 | 151 | 60 |
| $\mathbf{1 2 5 0}$ | XS800/XV | 64 | 151 | 60 |
| $\mathbf{1 6 0 0}$ | XS800 | 64 | 151 | 60 |
| $\mathbf{2 0 0 0}$ | XS1600SE/TL-NE | 51 | 114 | 92 |
| $\mathbf{2 5 0 0}$ | XS2000NE | 54 | 180 | 115 |

OCR controller (PTA and trip indication)
The OCR controller is installed in the left hand side of the breaker (standard). This can also be installed externally to the breaker (please specify when ordering).
OCR controller specifications
Control power source
Rated voltage $100-120 \mathrm{~V} \mathrm{AC}$ or $200-240 \mathrm{~V} \mathrm{AC}$
Consumption 2 VA

Note: The permissible range of control power is $85-110 \%$ of the rated voltage.

OCR controller connection diagram $\left.{ }^{1}\right)^{2}$ )


OCR controller dimensions
(Installed external to the breaker)


Notes: ${ }^{1}$ ) Standard torque for the terminal screws M3.5-0.88~1.18 Nm (9~12 Kgf.cm). ${ }^{2}$ ) Connected cable size - Max $2.0 \mathrm{~mm}^{2}$.

## MCCB Technical data

## Time/Current curves

 XS400, XH400, TL400NE, XV400Time/current characteristic curves


Overcurrent tripping characteristics

| CT rated current ( $A$ ) ( $\mathrm{l}_{\text {a }}$ ) | 250, 400 |
| :---: | :---: |
| Base current setting (A) ( 10 ) | ( 1 ) $\times$ (0.63-0.8-1.0) |
| Long time-delay pick-up current (A): ( 1 ) | (10) $\times$ (0.8-0.85-0.9-0.95-1.0) Non-tripping at <br> (h) setting $\times 105 \%$ and below. Tripping at $125 \%$ and above. |
| Long time-delay time settings (S) ( $\mathrm{T}_{1}$ ) | (5-10-15-20-30) at ( 11 ) $\times 600 \%$ current. <br> Setting tolerance $\pm 20 \%$ |
| Short time-delay pick-up current (A): ( $\mathrm{I}_{2}$ ) | (10) $\times$ (2-4-6-8-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings (S) ( $\mathrm{T}_{2}$ ) | Opening time ( $0.1,0.15,0.2,0.25,0.3$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time - 20 ms for the timedelay setting |
| Instantaneous trip pick-up current (A) (13) | Continuously adjustable from (10) $\times$ ( 3 to 12 ) <br> Setting tolerance $\pm 20 \%$ |
| - Pre-trip alarm pick-up current (A) (la) | (h) $\times(0.7,0.8,0.2,1.0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarn time setting (S) (Tr) | 40 fixed definite time-delay. Setting tolerance $\pm 10 \%$ |

## Note:

- Optional.

Underlined values will be applied as standard ratings unless otherwise specified when ordering.

XS630, XH630, XS800, XH800, XV630, XV800
Time/current characteristic curves


Overcurrent tripping characteristics

| CT rated current (A) (h) | 630, 800 |
| :---: | :---: |
| Base current setting (A) ( l ) | ( $\mathrm{l}_{\text {l }} \times$ (0.63-0.8-1.0) |
| Long time-delay pick-up current (A): (l) | (l) $\times$ ( $0.8-0.85-0.9-0.95-1.0)$ Non-tripping at ( 1 ) setting $\mathrm{x} 105 \%$ and below. Tripping at $125 \%$ and above. |
| Long time-delay time settings (S) ( $\mathrm{T}^{\text {) }}$ | (5-10-15-20-30) at (l) $\times 600 \%$ current. <br> Setting tolerance $\pm 20 \%$ |
| Short time-delay pick-up current (A): (k) | (1) $\times$ (2-4-6-8-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings (S) ( $\mathrm{T}_{2}$ ) | Opening time ( $0.1 .0 .15,0.2,0.25,0.3$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time - 20 ms for the time-delay setting |
| Instantaneous trip pick-up current (A) (b) | Continuously adjustable from (1) $\times$ ( 3 to 12) Setting tolerance $\pm 20 \%$ |
| - Pre-trip alarm pick-up current (A) (b) | (h) $\times(0.7,0.8,0.21 .0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarm time setting (S) (T) | 40 fixed definite time-delay. Setting tolerance $\pm 10 \%$ |
| - Ground fault trip pick-up current (A) (la) | Continuously adjustable from ( 1 l ) $\times(0.1$ to 0.4$)$ Setting tolerance $\pm 15 \%$ |
| - Ground fault trip time setting (S) (T) | Opening time ( $0.1-0.2-0.3-0.4-0.8$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time is $\mathbf{- 2 0} \mathbf{~ m s}$ for the time-delay settings |

Note: - Optional.
Underlined values will be applied as standard ratings unless otherwise specified when ordering.

## MCCB Technical data

Microprocessor based characteristics and adjustments
XS1250SE, XS1600SE, XS2000NE, XS2500NE, TL630NE, TL800NE, TL1250NE \& XV1250
Time/current characteristic curves


Overcurrent tripping characteristics

| CT rated current (A) ( $\mathrm{L}_{2}$ ) | 1000, 1250, 1600, 2000, 2500 |
| :---: | :---: |
| Base current setting (A) (1a) | (L) $\times$ ( $0.63-0.88-1.0)$ |
| Long time-delay pick-up current ( $A$ ) : ( l ) | (b) $\times$ (0.8-0.85-0.9-0.95-1.0) Nontripping at (h) setting $x 105 \%$ and below. Tripping at $125 \%$ and above. |
| Long tine-delay time settings (5) ( $\mathrm{T}_{\text {1 }}$ ) | (5-10-15-20-30) at ( 1 l$) \times 600 \%$ current. <br> Setting tolerance $: 20 \%$ |
| Short time-delay pick-up curent (A): (1, | (b) $\times$ (2-4-6-2-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings (5) ( $\mathrm{T}_{2}$ ) | Opening time ( $0.1,0.15,0.2,0.25,0.3$ ) in the definite time delay. Total clearing time is +50 ms and resettable time - 20 ms for the time-delay setting |
| Instantaneous trip pick-up current ( | Continuously adustable from (10) $\times$ ( 3 to 12) <br> Setting tolerance $\pm 20 \%$ |
| - Pre-trip alam pick-up current (A) (b) | (h) $\times(0.7,0.8,29,1.0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarm time setting (5) (T) | 40 fiued definte time-delay. Seting tolerame $\pm 10 \%$ |
| - Ground fault trip pick-up current (A) (k) | Conthuously adustable from ( $\mathbf{2}$ ) $\times(0.1$ to 0.4$)$ <br> Setting tolerance $\pm 15 \%$ |
| - Ground foult trip time setting (5) (T) | Opering time (0.1-0.2-0.3-0.4-2.8) in the defirite time-delay. Total clearing time is +50 ms and resetable time is -20 ms for the time-delay settings |

Note: - Optional.
Underlined values will be applied as standard ratings unless otherwise specified when ordering.

## MCCB Technical data

Time/Current curves - Mathematical analysis

## MCCB curves

A microprocessor MCCB has three major regions on its overcurrent tripping characteristic, namely Long Time Delay (LTD) for overload protection, Short Time Delay (STD) and Instantaneous (INST), both for short-circuit protection.
The following is an insight into how these curves interact and could act as a guide for hand-drawing the curves. TemCurve Selectivity Analysis Software is available for computerised generation of curves (refer to page 7-24).
Firstly consider the following basic characteristic curve shown in figure 1. The LTD takes the form of a curve and has the following characteristic equation:

$$
(12-1) \cdot t=k
$$

where ' $k$ ' is a constant. To determine $k$, the calibration point of the LTD should be used, i.e. $t=T_{1}$ at $I_{1}=6(600 \%)$.
IEC - 60947-2 states that a breaker must not trip below $105 \%$ of its rated current, and always trip at $130 \%$ of its rated current.
Terasaki microprocesssor MCCBs however are calibrated to trip between $105 \%$ and $125 \%$. giving them a higher degree of accuracy. If the middle point is taken then the pick-up of the MCCB is $115 \%$ of its rated current.
The STD and INST parts of the curve can be drawn more easily as they are simply a series of horizontal and vertical lines determined by the $\mathrm{I}_{2}$ and $\mathrm{T}_{2}$ settings for the STD, and $\mathrm{I}_{3}$ setting for the INST.

## Example

If we assume that we have:
XS1250SE with 1250A CTs and
$\mathrm{I}_{0}=1, \mathrm{I}_{1}=0.8, \mathrm{~T}_{1}=30$ secs.
$\mathrm{I}_{2}=8, \mathrm{~T}_{2}=0.2 \mathrm{sec}$ and
$\mathrm{I}_{3}=1_{2}$ (dial setting on OCR)
then the characteristic curve can be constructed as follows.
To draw the LTD we firstly need to determine the constant $k$, as follows:
$\mathrm{k}=\left(\mathrm{l}^{2}-1\right) \mathrm{t}=\left(6^{2}-1\right) \quad 30=1050$
giving the characteristic equation:
$\left(\mathrm{I}^{2}-1\right) \mathrm{t}=1050$
By simple arithmetic the tripping times for each level of overload can now be determined.
For $400 \%$ overload (for the example this is equivalent to $1250 \times 1.0 \times 0.8$ $\times 4=400 \mathrm{~A}$ ).

$$
t=\frac{1050}{\left(1^{2}-1\right)}=\frac{1050}{\left(4^{2}-1\right)}=70 \text { secs }
$$

The STD and INST can be constructed as follows with
$I_{2}=I_{n} \times I_{0} \times I_{2}$
$I_{3}=I_{n} \times I_{0} \times I_{3}$
Please note that 20 ms is taken as an average time for the INST trip of the MCCB as it is the maximum time it will take the MCCB to trip. In practice the breaker will open much faster, particularly at high faults where the current limiting qualities of the MCCB become more effective.

Fig. 1




## MCCB Technical data

## OCR checker, inspection and maintenance



The TemBreak (Electronic) OCR checker. Type TNS-1, is a portable easy-to-use instrument for field testing the trip functions.

It checks the pick-up current and tripping time value of the LTD, STD, INST and GFT functions.

| Power source | 100-110 V, 220-240 V AC single phase $50 / 60 \mathrm{~Hz}$ |
| :---: | :---: |
| Power consumption | 30 VA |
| Application | LTD function check (set current and trip time values) |
|  | STD function check (set current and trip time values) |
|  | INST function check (set current value) |
|  | GFT function check (set current and trip time values) |
| Measurement of set | Display 3-digit digital display |
| current values | Range $\quad 0.900 \mathrm{~mA}$ |
| Measurement of tripping time values | Range 0.00-99.9 seconds |
| Outline dimensions ( mm ) | $200 \mathrm{~W} \times 84 \mathrm{H} \times 130 \mathrm{D}$ |
| Weight | 2.7 kg |

## NH: <br> TERASAK

## TemCurve

## Selectivity Analysis Software

Our objective is to provide you with the tools necessary to ensure your time is managed as effectively and efficiently as possible.

TemCurve has been developed wholly by NHP for the Australian market, but will also be used within the Terasaki organisation throughout the world.

Circuit breaker selection and set-up can be a laborious and time-consuming task. NHP has ensured that TemCurve 4.0, for "Windows ${ }^{\text {™ }} 98$, 2000, NT and XP is now even simpler to operate. Hence, accurate results can be gained in a matter of minutes.

The database within TemCurve holds the characteristic curves for all Terasaki devices presently available from NHP. In addition to this, the extensive database of non-Terasaki devices allows you to produce accurate grading from the transformer primary side to the point of final distribution.

High quality prints can be output, including the characteristic curves for each chosen device. as well as a complete list of device settings.

## For further information please contact your local NHP office or agent.

## MCCB Technical data

TemBreak XM30PB


ASL: Arrangement standard line
H: Handle frame centre line

Drilling plan


Rear connected (optional)

$\$ 15$ for accessory wing when necessary

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

## Plug-in (optional)

Drilling plan


## MCCB Technical data

TemBreak XS125CS, CJ, NS, NJ, XH125NJ, PJ and TL30F MCCBs


Rear connected (optional)
Drilling plan


Panel cut-out


Drilling plan


## MCCB Technical data

TemBreak TL100F/TL100EM - TL100NJ
ASL: Arrangement standard line H : Handle frame centre line Outline dimensions ( mm )


Rear connected
Bold stud type

$\$ 15$ for accessory wiring when necessary

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

Note: Interpole barriers standard on TL100NJ.

## MCCB Technical data

Motor operators (XMB type) for XS125, XH125, TL100NJ, TL30F $\left.{ }^{1}\right)^{2}$ )

Outline dimensions ( mm )

Front connected (standard)


ASL: Arrangement standard line H: Handie frame centre line


Drilling plan


Rear connected (optional)


Notes: ') For dimensions of 7MB-3BA2 used for TL100F refer to NHP.
${ }^{7}$ ) Dimensions for TL100NJ not showing length of MCCB. Refer page 7-27.
Above outline dimensions are for AC motors. Contact NHP for details for DC motors.

## MCCB Technical data

TemBreak XE225NC

## Outline dimensions (mm)

ASL: Arrangement standard line
Li: Handle frame centre line

## Front connected (standard)



Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.5 mm around the handle escutcheon.

## Rear connected (optional)



Note: In the standard shipment mode, terminals on both the line side and the load side are in a horizontal orientation.

## MCCB Technical data

## Motor operators for XE225NC



- Breakers with terminal bars available on request.

Rear connected (optional)


Note: In the standard selection mode, terminals on both the line side and load side are in a horizontal orientation.

## MCCB Technical data

TemBreak XS250NJ


Breakers with terminal bars available on request.


## MCCB Technical data

Motor operators (XMB type) for XS250NJ


- Breakers with terminal bars available on request.

Drilling plan

Rear connected (optional)

Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.


Plug-in (optional)



Note: For dimensions and selection of motors for TL225F refer to NHP.

## MCCB Technical data

## TemBreak XH160PJ and XH250NJ



Note: Breakers with terminal bars available on request.


Note: In the standard shipment mode, terminals on both the line side and the load side are in a horizontal orientation.

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.


## MCCB Technical data

Motor operators for XH160PJ and XH250NJ

Outline dimensions (mm)
ASL: Arrangement standard line
It: Handle frame centre line
Front connected (standard)


Rear connected (optional)

Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.

Plug-in (optional)


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## MCCB Technical data

TemBreak TL225F, TL250NJ


Front connected


## (1) TERASAKI

## MCCB Technical data

TemBreak XS400, XH400, XH250PJ, XV400

Outline dimensions (mm)
Front connected (standard)


Optional extension busbars

Rear connected (optional)


Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.

Drilling plan


ASL: Arrangement standard line
ㄴ: Handle frame centre line

Panel cut-out


Panel cut-out dimensions shown give an allowance of $\mathbf{1 . 0 ~ \mathrm { mm }}$ around the handle escutcheon.

Plug-in (optional)


## MCCB Technical data

TemBreak TL400NE

## Outline dimensions (mm)

ASL: Arrangement standard line ti: Handle frame centre line

Front connected


## Rear connected

Flat bar stud


Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

## MCCB Technical data

Motor operators (XMC type) for XS400, XH400, XV400, TL250NJ, TL400NE ${ }^{\text {' }}$ )

ASL: Arrangement standard line
ti: Handle frame centre line
Outline dimensions ( mm )

## Drilling plan



Rear connected (optional)


Panel cut-out
 shown give an allowance of 1.0 mm around the handle escutcheon.

Plug-in (optional)


Note: ") TL250NJ and TL400NE length dimension not shown.
Refer pages 7-35 and 7-37.

## MCCB Technical data

TemBreak 630 AF XS630, XH630


## (1) TERASAKI

## MCCB Technical data

TemBreak 800 AF XS800, XH800


Rear connected (optional)
Drilling plan


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

## Plug-in (optional)

Mounting block
Drilling plan


## MCCB Technical data

Motor operators (XMC type) for XS630, XH630, XS800, XH800

ASL: Arrangement standard line
T: Handle frame centre line
Outline dimensions ( mm )
Front connected (standard)


Drilling plan



Note: In the standard selection mode, terminals on both
the line side and the load side are in a horizontal orientation.

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the motor operator frame.

Plug-in (optional)


## MCCB Technical data

TemBreak XS1250, XV1250


Plug-in (optional)
Mounting block
Drilling plan


## MCCB Technical data

## Motor operators (XMD type) for XS1250, XV1250



## MCCB Technical data

TemBreak XS1600SE, TL630, TL800, TL1250NE


Rear connected with motor operator

Panel cut-out


Panel cut-out dimensions shown give an allowance of $\mathbf{1 . 5 ~ \mathbf { ~ m m }}$ around the handle escutcheon.

## Draw-out (optional)



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## MCCB Technical data

Motor operators for XS1600 TL630NE, TL800NE, TL1250NE

Draw out


## MCCB Technical data

TemBreak XS2000NE


## (1) TERASAKI

## MCCB Technical data

TemBreak XS2500NE

## ASL: Arrangement standard line <br> 4.: Handle frame centre line <br> Outline dimensions ( mm )

Rear-connected (RC standard, no FC version)


Panel cut-out


- Panel cut-out dimensions shown give an allowance of 2 mm around the handle escutcheon.

Note: RC - Rear connected, FC - Front connected.

TERASAKI

## MCCB Technical data

Motor operators (XMB type) for
MCCB accessories
XS2000NE \& XS2500NE

ASL: Arrangement standard line
H: Handle frame centre line

## Outline dimensions (mm)

Drilling plan


Rear connected (standard)



## (1) TERASAKI

## MCCB Technical data

Motor operators XMB types for XS2000NE \& XS2500NE

Outline dimensions ( mm )
Front connected (standard)


Note: ') Use non-magnetic angle
(SUS 304 etc)


## MCCB Technical data

AC power watts loss - 3 Pole MCCBs


Notes:
Standard terminal arrangements.
125-1600 front connection.
2000 and above rear connection.
${ }^{1}$ ) Watts loss figures are for 3 poles.
e.g. An XH125NJ operating at 125 A , will have a total watts loss of 41 watts.
${ }^{2}$ ) Watts loss values are approximate and will vary according to ambient conditions and switchboard construction.

## NH:

## NHP and PowerCad working together

PowerCad has established itself as the standard for electrical engineering design software for electrical engineering building services.
PowerCad contains a suite of electrical design software which provides solutions ranging from basic cable sizing up to complete electrical design and modelling. There are 5 software packages which have a stepped level of features. These are: QuickCable-LT™, QuickCable ${ }^{\text {mM }}$. PowerCalc ${ }^{m M}$, PowerCalc- $H^{T M}$, while the final and most powerful version is called PowerCad- $5^{\mathrm{Tm}}$.


The above is a typical screen representation providing a circuit schematic, along with an open window showing a protective device picture, its various device OCR settings, Cat. No, and other device details.

## PowerCad 5 - application

Starting with a network single line diagram, the designer is able to assign the loads in the system from which the software calculates maximum demands, determines the appropriate cable sizes, and selects suitable protective devices and can finally undertake a powerful harmonic modelling function of the entire system. In order for the software to accurately model the protective devices in the system, PowerCad includes various device characteristic data as a library within its software, including Terasaki circuit breakers.

[^5]

PowerCad 5 features:

- Maximum demand
- Cable sizing
- Conduit sizing
- Fault-loop impedance
- Cable voltage drop calculations
- Cable thermal stress
- Short circuit calculations
- Let-through energy
- Harmonic analysis
- Harmonic mitigation
- Power factor correction
- Network resonance
- L.V. Distribution Network Modelling
- Single Line diagram
- Single Line diagram export to AutoCad
- AutoCad interface for loads input
- Automatic mains \& submains cable selections
- Automatic final subcircuit cable sizing
- Circuit breaker selection
- Co-ordination time-current curves
- Co-ordination curve on screen CB adjustment
- Substation sizing
- Motor Libraries and light fitting
- Luminare Libraries
- Extensive reporting with print preview
- Direct online support
- Standards AS/NZS. IEC. BS and CP5
- Generator sizing
- Harmonic active filtering
- Reactor passive filtering
- Transfer switches


# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218

Westlake Drv
Equipment Type: Motor Contactors
Location: Motor Starter Section
Model Numbers:CA7-9
Manufacturer: Sprecher \& Schuh
Supplier:
NHP Pty Ltd
25 Turbo Drive
Coorparoo ..... QLD 4151
Ph: 0738916008
Fx: 0738916139

SP218 Westake Drive westake SPS Electical nsstaladion volume 2 OM Manual

## Attenti $\quad$ p prevent electrical shock, disconnect from

power: before installing or servicing. Install in suitable
...-C30 /...-30
enclosure. Keep free from contaminants.
...-C37 /...-37
Achtung: Vor Installations- oder Servicearbeiten Stromversorgung unterbrechen, um Unfälle zu vermeiden. Die Geräte müssen in einem passenden Gehäuse eingebaut und gegen Verschmutzung geschützt werden.
Attenzione: Per prevenire infortuni; togliere tensione prima dell'installazione o manutenzione. Installare in custodia idonea. Tenere lontano da contaminanti.
Attention: Avant le montage et la mise en service, couper l'alimentation secteur afin d'éviter tout accident. Prévoir une mise en coffret ou armoire appropriée. Protéger le produit contre les environnements agressifs.
Atención: Desconectar la alimentación eléctrica antes de realizar el montaje y la puesta en servicio, con el objeto de evitar accidentes. Instalado en una caja o armario apropiado. Proteger el producto de los ambientes agresivos.


IEC 60947-1/-4EN 60947-1/-4-1 UL 508; CSA 22.2 No. 14;


| $4$ |  |  | _ $\Delta^{r}$ ¢ |
| :---: | :---: | :---: | :---: |
| c [mm] | 34 | 53 | 56 |


| $1$ | $\square$ |  | (3) filiti $2,5 . .3,5 \mathrm{Nm}$ <br> $E D 2=\mathrm{NO}_{3}$ <br> Pozidriv No 2 |
| :---: | :---: | :---: | :---: |
|  | $\stackrel{5}{\pi}$ |  | (3) 筑 $\begin{aligned} & 1, \ldots 1,5 \mathrm{Nm} \\ & 8,9 . .13 \mathrm{lb}-\mathrm{in}\end{aligned}$ <br> $E D D=\mathrm{NO}_{3}$ <br> Pozidriv No 2 |


-Min. distance lateral to grounded parts or walls $=6 \mathrm{~mm}$
-Min. seitlicher Abstand zu geerdeten Teile oder Wände $=6 \mathrm{~mm}$
-Distance latéral min. enver pièces mises à terre ou parois $=6 \mathrm{~mm}$ - Distanza laterale min. verso pezzi a
massa o pareti $=6 \mathrm{~mm}$ -Distancia lateral min. a chasis paredes $=6 \mathrm{~mm}$


Technische Änderungen vorbehalten
22.221.950-01/05. 2007
Ausgabe 10

Ausgabe 10


# Broad current renge Compact dlinensions Maximum fillexilbilility 

## Series CA7 Contactors

## Reduces <br> Panel Space

Mechanically Linked Auxiliaries



Compact dimensions with maximum performance! Our CA7 contactors control motors up to 60 HP , in frame sizes ranging from $45 \mathrm{~mm}\left(1-3 / 4^{\circ}\right)$ to a maximum of $72 \mathrm{~mm}\left(2-3 / 4^{\circ}\right)$ wide.

Because of its modular design, CA7 is flexible and easy to use. All CA7 contactors use the same accessories, reducing the need to stock additional inventory. They are also mechanically and electrically compatible with Sprecher + Schuh's CEP7 electronic
overload relay and KT7 motor circuit controller. This provides easy, clean installation for a variety of motor starter applications.

Whether part of a system or for individual use, the CA7 is the right contactor for the job.

## Series CA7



## Save space, save money

The CA7 contactor series includes ten contactors within four frame sizes. The two smallest sizes house capacities up to 25 HP (@460V) and 30HP (@575V). They measure only $45 \mathrm{~mm}\left(1-3 / 4^{\prime \prime}\right)$ in width! Even the largest of the contactors - the CA7-85, controlling motors to 60 HP - measures only $72 \mathrm{~mm}\left(2-3 / 44^{\prime \prime}\right)$ wide. The space you save with CA7 translates to smaller panels and lower cost.


## Maximum flexibility

The CA7 contactor is designed for ultimate flexibility. Coil terminals can be supplied on the top or bottom, and are field-reversible to suit individual wiring needs. Auxiliary contacts can be mounted on the top and sides, for the most efficient use of panel space. In reversing applications where space may be tight, the mechanical interlock has a built-in auxiliary to save room.


Dual terminal technology provides additional wiring options, as well as increased reliability and a faster wiring process.
Dual wiring terminals speed installation

## State-of-the-art technology

CA7 contactors utilize the latest design technology. Combined with Sprecher + Schuh's CEP7 solid state electronic overload relay, the CA7 becomes the most accurate and reliable motor starter available. Mechanically linked contacts provide safety for all applications. In addition, snap-on electronic timers and a PLC interface are also available.


## Modular design

The CA7 contactor series includes universal accessories to fit every frame size. This provides incredible flexibility, and eliminates the need to purchase size-specific components.

Because of their modular design, CA7 contactors are easily joined to form complete starter combinations. The CA7 is specially designed for electrical and mechanical compatibility with our overload and motor circuit controllers.

## CA7 Selected Technical Data

| Catalog Number | $\begin{gathered} \text { AC-1 } \\ \text { Amp Rating } \\ 40^{\circ} \mathrm{C} \end{gathered}$ | Maximum Horsepower |  |  |  |  |  | Max.Aux.Contacts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Single Phase |  | Three Phase |  |  |  |  |
|  |  | 115 V | 230 V | 200V | 230 V | 460 V | 575 V |  |
| CA7-9 | 32 | $1 / 3$ | 1 | 2 | 2 | 5 | 7-1/2 | 9 |
| CA7-12 | 32 | 1/2 | 2 | 3 | 3 | 7-1/2 | 10 | 9 |
| CA7-16 | 32 | 1 | 3 | 5 | 5 | 10 | 15 | 9 |
| CA7-23 | 32 | 2 | 3 | 5 | 7-1/2 | 15 | 15 | 9 |
| CA7-30 | 50 | 2 | 5 | 7-1/2 | 10 | 20 | 25 | 9 |
| CA7-37 | 50 | 3 | 5 | 10 | 10 | 25 | 30 | 9 |
| CA7-43 | 85 | 3 | 7-1/2 | 10 | 15 | 30 | 30 | 8 |
| CA7-60 | 100 | 5 | 10 | 15 | 20 | 40 | 50 | 8 |
| CA7-72 | 100 | 5 | 15 | 20 | 25 | 50 | 60 | 8 |
| CA7-85 | 100 | 7-1/2 | 15 | 25 | 30 | 60 | 60 | 8 |

See Sprecher + Schuh's general catalog for complete information and pricing on CA7 contactors.

[^6]Sprecher + Schuh Canadian Division
3610 Nashua Dr., Unit 10, Mississauga, Ontario L4V 1 L2 Tel: (905) 677-7514; Fax: (905) 677-7663 www.sscdn.cc

## sprecher + schuh

## Contact Block

## Performance \& Selection

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## Contact Block Considerations

## Contact Material

## Contact Construction

A combination of many factors affect the dependability, life expectancy, and suitability of a contact block in any given application. Understanding the most important of those factors can help you select the best switch for your needs. In the pages that follow you'll gain a basic understanding of switch materials and properties, and how they affect switch performance.

The contact material forms the surfaces that come in contact with each other to establish an electrical circuit. Typical contact materials include fine silver, nickel-silver, and silver alloys. Fine silver provides low electrical resistance between the movable and stationary contact interface. Silver alloys form harder surfaces to reduce wear and help prevent contact welding.

In low voltage applications (below 48 V DC and 0.1 A , or below 24 V AC and 0.4 A ) where excess oil or dust is present, the use of more noble alloys (such as palladium, gold, and their alloys) in the contact material is recommended. These alloys are highly reliable in this type of environment.

Silver alloys are susceptible to chemical attack which can affect reliability at low voltages. Noble metals resist chemical attack, but are susceptible to frictional polymer formation, which can affect reliability. Combining gold and palladium will resist frictional polymer formation.

The perimeter of the contact is often shaped like a circle or rectangle and may have little effect on contact performance. The shape of the faces where the fixed and movable contacts meet is more important. This interface should not have two flat surfaces meeting. If one of the contacts has a flat surface, the other contact should be a rounded surface to provide a more defined and controlled touch point.

Figure 1. Bifurcated Spanner Example


The bifurcated style of construction provides a higher degree of reliability than the butt spanner because it divides each movable contact into two sections at the tip of the spanner. This minimizes the chance of foreign materials accumulating on contact surfaces and preventing the completion of the circuit. Even if foreign material accumulates on one of the contact tips, the second tip will most likely touch a clean spot establishing the circuit. Typically, the bifurcated spanner is designed for use in full voltage applications, where the arc between the spanner and stationary contacts will burn off small amounts of contamination in most cases. To aid contact cleaning the contact spanner is designed to flex, which wipes the stationary surface and allows each finger to act independently.

# Contact Block Considerations 

Figure 2. Pentafurcated and Quadfurcated Spanner Examples


In low voltage applications (below 48 V DC and 0.1 A or below 24 V AC and 0.4 A ) pentafurcated/quadfurcated styles of construction provide the highest degree of reliability because they divide each movable spanner contact side into separate flexible fingers. Every part in the system is corrosion-resistant and the flexible spanner is designed to wipe the stationary contacts clean every time the circuit is opened or closed. This is important since the absence of an arc in low voltage environments means that contaminants will not be burned off, but will be eliminated by the wiping action. Therefore, the pentafurcated or quadfurcated are the most reliable styles of spanners available.

Some manufacturers use protrusions such as bars or nibs raised on the face of either the movable or stationary contact to help establish the circuit under low power conditions. These raised surfaces will tend to penetrate non-conducting films that may be present on contact surfaces. They may also lessen the chance of foreign matter preventing completion of the circuit. Such protrusions may, however, quickly burn away under arcing or higher current conditions.

Base materials to which the contact material is attached include copper alloys and steel. Copper alloy is preferable because of its thermal conductivity, electrical conductivity, and corrosion properties.

## Contact Size/

Volume -
Stationary vs.
Movable

Contact size refers to the size of the face of the contact or the areas that meet to form the interface between the movable and stationary contacts. Volume is the total amount of contact material.

It is desirable to make one of the contacts smaller than the other so it stays within the perimeter of the other contact when switch action takes place. This arrangement provides greater assurance that alignment of contacts is maintained under repeated operation and resulting wear. Misalignment can cause severe contact wear and shorten switch life.

In the contact set, the movable contact is most often the smaller contact in both size and volume, so that its mass and resulting inertia can be minimized. Partly because of its low volume, the movable contact operates at a higher temperature than the stationary contact. Consequently, the stationary contact will also contribute to a greater rate of wear on the movable contact. The stationary contact is generally attached to a more massive base structure that provides a better heat sink than the movable contact structure.

In alternating current applications, the higher temperature of the movable contact can cause material to be expelled from the surface of the contact. The higher temperature can cause transfer of material to the cooler surface of the stationary contact as well. In direct current applications, the relative polarity of the contacts has a major effect on how the contact material is transferred from one surface to the other.

## Contact Block Considerations

Contact reliability pertains to the ability of contacts to establish a circuit across the interface between the stationary and movable contact set(s) each time the switch is operated. This reliability can be most often adversely affected by two conditions:

- Mechanical debris within the switch
- Non-conducting films that form on the contact surfaces

Mechanical debris or dirt can be introduced into the switch during assembly. Dirt and debris can also be interjected during installation or can be a product of switch action. The wear produced by internal switch components sliding past one another during operation can generate dirt. Care must be taken in the design of moving mechanisms to keep this wear to a minimum.

Non-conducting film and oxides can be formed from gaseous contaminants that enter the switch from an external environment as well as being formed from internally generated reactants. Sealing methods have been developed to isolate the switch interior from the external environment. An understanding of the relationship of all the material used in the construction of a switch is required to eliminate the internally generated reactants. This requires knowledge of the post curing outgassing of any plastics, elastomers, paint, and other components used in the construction of the system. Some gases will react in the presence of an electric arc to form non-conducting films that will cause reliability problems if deposited on the contact face. The tendency of many thermoset plastics to continue to outgas for a period of time after curing has led to the use of thermoplastic materials in switch interiors.

## Contact Resistance

Contact resistance pertains to resistance across the interface between a pair of movable and stationary contacts. The higher the value of this resistance, the more difficult it is to establish a circuit when the contacts close. This is especially true in low power circuits. Higher resistance also contributes to contact heating.

The initial contact resistance of both fine silver contacts and noble contact materials (gold, palladium, and their alloys) is $10 \ldots 15$ milliohms. However, the resistance of noble contact materials will remain relatively constant during their lifetime compared to silver contacts, which typically increase over time. These resistance values could vary with the ambient conditions in the vicinity of the contacts themselves

Sealed switches have slightly higher initial contact resistances compared to silver contacts ( $80 \ldots 150$ milliohms, depending on type), but they remain stable over the life of the device.

## Switch Design Considerations

In addition to the physical characteristics of the materials used in manufacturing, design considerations also affect the performance of a switching mechanism. In this section you'll gain an overview of those switch design fundamentals and how they affect switch performance.

## Single Break vs. Double Break

Figure 3. Single Break Design


Figure 4. Double Break Design


Single break and double break refer to the number of contact pairs that are used to make or break the electrical circuit. Single break means the electrical circuit is controlled by one set of contacts. Double break means the electrical circuit is controlled by two sets of contacts in series.

In a single break design, the contact pair tends to repeatedly make and break the circuit on the same spot on the contact faces. This helps to keep the contact touch point clean, enhancing the contact reliability.

The double break design provides twice the length of air gap in the electrical circuit using the same stroke of the actuating member as with the single break design. The result is the electrical arc that is created by the opening of the circuit will be extinguished sooner and with less actuator movement as compared to a single break design.

Also, since the energy in the arc created upon contact opening is distributed across two air gaps, there is less tendency for the contacts to weld in the double break design.

On the other hand, because of the nature of the double break design, the contact points of the spanner may vary slightly with each actuation. This variation may, over time, affect switch reliability.

Contact motion refers to the relative motion of the contact faces as they begin to touch one another. Various design techniques are utilized to increase the reliability of the contacts establishing the circuit as they meet.

A wiping or sliding action will help clear surfaces of dirt and oxides and break any nonconducting film that may have formed on contact surfaces. This type of action must be carefully controlled, especially with precious metal contacts, to avoid excessive mechanical wear of the contacts.

Contact tips on the end of the spanner must be capable of flexing and twisting to establish a seat on the surfaces of bifurcated/quadfurcated/pentafurcated stationary contacts. A sliding action of one contact against the other could cause continuity interruptions if the moving contact slides up over a piece of debris.

## Switch Design Considerations

## Spring Force

## Overtravel

The spring force discussed in the following paragraphs is the force provided within the contact block that returns the contact structure to its normal or unoperated state when the extemal force applied to the device operator is removed. This force holds the contact structure in its normal state until an external force is again applied to the device operator.

The amount of spring force is determined by the force required to insure contact reliability under the conditions in a variety of applications. Sufficient force is required to break through contaminants that may be present on the contact faces on the normally closed (N.C.) contacts. The force should insure that contacts stay stable under possible shock and vibration. Light welds created by contact arcing on the normally open (N.O.) contacts should be able to be broken by spring force. The spring force required to maintain circuit reliability is dependant on the contact material hardness. Greater force is required for harder materials.

Spring force directly affects the external force required to operate and to some extent contribute to internal switch friction. Consideration must be given to these factors when determining the spring force used.

Overtravel in a switch pertains to the amount of travel occurring in a switch beyond what is required to operate. Overtravel allows for wear within the switch mechanism. It helps to insure the switch will continue to function as the contacts wear or erode. Overtravel also provides contact stabilization under conditions of shock and vibration.

Contact Underlap vs. Contact Overlap

Contact underlap and overlap refer to the relative action of the N.O. and N.C. contacts when the switch is actuated.

Underlap is the more common type of switch action. As the device operator is moved from its rest position to initiate switch action, the following events take place in order:

1. The N.C. contact opens.
2. There is a duration where no electrical continuity is present.
3. The N.O. contact closes.

In overlap type switch action, the N.O. contact makes its circuit before the N.C. contact breaks its circuit. There is never a period of time when electrical continuity is absent:

1. The N.O. contact closes.
2. There is a duration where both circuits are active.
3. The N.C. contact opens.

The type of switch action selected is dependant on the requirements of the specific user circuit application.

## Switch Design Considerations

## Direct Drive

Contact Action

NFPA 79 and EN 418 both require that emergency stops must be a direct drive design. A direct drive design switch will have continuous mechanical linkage from the external operating member to the contact carrier. It will not employ the use of any resilient members or springs in the mechanical actuating path to open the N.C. contacts.

A special case of direct drive design is a switch that complies with IEC 60947-5-1. It is designed so that contact separation will take place even though the contacts may have been welded or "sticking" during fault circuit conditions. A direct drive switch is designed to allow contact separation even if the contacts have been lightly welded during fault circuit conditions. The manufacturer provides the fusing level requirements needed to protect these contacts from welding. The actuator movement and actuator force required affecting contact separation are specified by the switch manufacturer.

This type of switch construction is used to help ensure that contact action takes place when the external operating member is actuated. By avoiding the use of any springs in the actuating path, a solid connection is provided directly from the external mushroom operator to the contacts.

Contact opening should always take place at the same point in the actuating stroke and with the same operating force. By their nature, these types of switches fall into the slow break/slow make category of devices although some special designs have been developed that provide positive opening in snap action devices. With increased awareness of safety concerns and the movement toward designing devices that are used globally, greater emphasis has been placed on the direct drive feature.

Contact action refers to how contacts make and/or break the electrical circuit they intend to control. There are two basic types of contact action: slow make/slow break and snap action.

In slow make/slow break action, the contact carrier and contacts move at the same rate of travel as the actuating mechanism. This action is most often obtained with direct drive switch designs. Since the rate of movement of the contacts is solely dependant on the speed of the external actuator, it can result in slow separation of contacts and create a condition called "teasing".

In the teasing condition, the air gap created to break the electrical circuit opens so slowly that arcing occurs between the faces of the stationary and moveable contacts. This arcing is detrimental to the contacts because of accelerated contact wear and material transfer and can cause the contacts to weld rather than separate. The arcing can also cause circuit problems by introducing noise.

Snap action design incorporates a resilient member or springs between the actuator and contact carrier. The springs cause the contacts to move independently of the actuating mechanism. The mechanism is designed so that when actuator movement takes place, not only does the contact carrier movement take place, but energy is also built up in the spring system. Prior to the point in the travel of the actuator where contact separation takes place, the contact carrier and spring system are designed to go into an overcenter mode.

## Switch Design Considerations

## Mechanically Linked Contacts

Time Delay

Stacking

At the overcenter point, sufficient energy is available in the spring system allowing the carrier to move independently of any further actuator motion and the contacts snap open. This rapid opening prevents teasing and minimizes contact welding. Some snap action devices also incorporate direct opening action. The direct opening action occurs slightly later in the travel than the normal snapover point if the contacts were slightly welded.

This construction has also been known as "positively guided contacts". It combines a N.C. and N.O. contact combination to prevent N.C. and N.O. contacts from closing at the same time. This nomenclature is generally applied to control relays, but is also applicable to push buttons, pressure and temperature switches, and other control circuit devices. It is generally used for checking control circuit functions.

Time delay of a switching device is the interval between the time when the external operator of the switching device is actuated and the time when the contact action actually occurs.

In a switching device where time delay is provided, contact action takes place at a predetermined time interval after physical action has taken place to displace the external operator in a sufficient manner to operate the device. This time delay is fixed in some devices and adjustable in others to meet circuit requirements. Pneumatic timers are commonly used to perform this function.

A switching device that has been designed for stacking has provisions for attaching multiple contact elements to the operator.

Stacking provides a means for multiple circuits to be actuated from a single external operator. A switching device with this capability can perform multiple functions or combinations of functions depending on the type of external operator. A selector switch type operator with several positions in combination with multiple contact elements is one example of this type of device.

## Switch Design Considerations

Wiring Termination
The following are examples of some of the more common methods of termination used.

## Binding Head Screw

This screw has a larger than normal head. The underside of the screw head has a groove where the wire seats and is secured when the screw is tightened. It is most effective when used with solid wire. A cup washer can be added to accommodate stranded wire, but care must be exercised to ensure that all strands are secured

## Saddle Clamp

This is a U-shaped clamp with a screw in the center. The screw threads into a flat conductor on the switching device and the legs of the $U$ slide over the edges of the flat conductor in order to trap the wire.

Figure 5.


The saddle clamp should be designed so it tilts to securely clamp a single wire on one side or a different wire size on each side of the clamp.

Barrel Type - This is similar to the saddle clamp design, but instead of a U-shaped clamp, the clamp is rectangular.

Figure 6.


The screw is not threaded into the flat conductor but rather bears against its top surface. This causes the barrel to be drawn upward clamping the wire between the undersurface of the flat conductor and the lower portion of the barrel. A major advantage is the wire is easy to insert into the clamping area.

## Pressure Plate

A pressure plate is essentially a flat piece of material with a screw in the center. As with the saddle clamp, the screw threads into the flat conductor on the switching device. Even though the pressure plate is flat, it is designed to force the individual strands of wire to the center of the face plate that comes in contact with the conductor on the switching device where they are restrained. In addition, features are often designed into the body of the switching device that prevent any wire strands from escaping the pressure plate clamping action.

## Switch Design Considerations

## Stab Type

This type of termination is often termed quick-connect, push-on, fast-on, etc. The connection between the switching device and the wire is made with special complementary connection parts. The male part is normally built into the switching device and the female part is mechanically attached to the wire end. Termination is accomplished by mating the connector parts. This method provides a quick way to attach wires to the switching device and it is easy to remove the wires for service.

## PC Pin

These are switching devices that can be soldered directly to a printed circuit board or plugged with pin connectors into receptacles mounted on the board.

## Lugs and Ferrules

These devices are mechanically secured to the wire end. They make it easier to attach the wire to the switch terminal. They are normally used with stranded wire.

- Lugs provide a flat projection that is usually shaped like a fork or ring. The projection can be inserted under the head of the screw, inserted into saddle clamps, or slipped under pressure plates.
- Ferrules provide a pin type projection well suited for use with saddle clamps, pressure plates, and barrel type terminals.


## Solder

Solder can be applied to the end of stranded wire to prevent the individual strands of wire from separating. The end of the wire becomes solid when soldered and can be used with saddle clamps, pressure plates, and barrel type terminals. It should be noted that the solder end will be quite hard and will resist the crushing effect of clamping means. Because of the irregular shape obtained through soldering, only partial contact between the wire and the terminal could result.

## Spring-Clamp

This termination style is designed to minimize wiring time. The optimized spring-clamp is designed to reduce stress relaxation while maintaining contact force. An opening force is applied by a lever. The wire is then inserted and the opening force is removed. Upon force removal, the spring-clamp closes on the wire. This design is good for vibration environments.

Because of the large variety of termination options and the importance of establishing and maintaining a reliable connection between the switching device and the circuit, standards have been developed to address this area. The Underwriters Laboratories Pullout and Secureness test is used to insure that termination methods have sufficient strength to retain the wire under conditions of use. This test also determines if the wire strands have been damaged during the wiring process or are susceptible to breakage under conditions of use.

## Switch Design Considerations

Finger-Safe
A finger-safe device provides a degree of protection from accidental, casual contact of live electrical parts by personnel. Only those components meeting or exceeding the requirements of IEC standard IP2X (listed under IEC 529) can be considered finger-safe.

Those standards describe a model test finger, along with guidelines for the manner in which the test finger is to be manipulated in the vicinity of the wiring terminals to determine if the switching device provides the required degree of protection.

Some switching devices achieve the finger-safe condition by basic device design while others require an external attachment.

The finger-safe feature is becoming more prevalent as safety issues take on added importance. Higher voltage levels pose a greater risk of injury and liability. A concern of finger-safe design is it may provide a false sense of security to personnel who have access to the area where electrical terminations are made.

## Special Considerations

## Environmental <br> Considerations

Every switch serves as just one element in a complete system. Where and how that system operates plays a significant role in which switch will deliver the most cost-effective performance over time. In the section that follows, you'll gain a better understanding of some of the extraordinary issues involved in switch specification.

Careful consideration of the environment to which the switching device is subjected will help ensure proper operation and acceptable service life. Consideration of external environmental conditions of the operators includes temperature and humidity, shock and vibration, and exposure to washdown, cutting fluids, etc., encountered during operation.

In installations where an unfriendly external environment exists, the switching device should be housed in an enclosure designed to isolate it from the environment. Various enclosure ratings have been developed for use in specific environments and these ratings are regulated by industry standards. The external environment of the switching device can have a profound effect on the operation of the device and on its service life.

Conditions generated within enclosures can also have a negative effect on switch operation and life. Condensation, internally generated chemicals, or trapped dirt are some of the more common problems. In addition, since each switching device is made of a variety of materials, each produces its own internal environment. Caution must be taken during the design of the switching device to ensure the materials selected are proper for this kind of device and are compatible with one another.

The following information points out some key intemal and external conditions affecting switching devices, as well as their effects.

## Temperature

All electrical devices have a maximum operating temperature rating and this rating is generally understood by the user. The maximum storage temperature and the effects of low temperature are not as well-understood.

Exceeding the high temperature limits can cause degradation of materials within the switch. This degradation can weaken switch parts or release gases from plastics and elastomers. A change in physical dimensions may occur, affecting operational travel and force. A very low temperature environment can cause sticking of the actuator and compromise the retum action provided by the internal springs within the switching devices. Great care should be taken to exclude freezing liquids from the vicinity of the external operator or the switch may be inoperative under available levels of operating force.

Large fluctuations in temperature can lead to condensation of water or other liquids, and result in the problems relating to humidity, chemicals, and gases listed below (in those cases it is generally helpful to ventilate the enclosure).

## Humidity

Moisture can cause the formation of rust and corrosion on metallic parts as well as contribute to electrical problems such as arc tracking.

## Chemicals and Gases

This class of contaminants can cause degradation of material used in the product in a

## Switch Design Considerations

variety of ways. Corrosion of metallic parts and the degradation of physical properties of plastics and elastomers are among the most common effects. The formation of conductive films on the surface of the insulation can cause arc tracking.

## Dirt and Debris

Whether originating internally from wear or damage, or externally, this material can cause friction between moving parts, increase wear, and reduce switch life. Dirt on contacts increases resistance and contributes to contact reliability problems.

## Shock and Vibration

Consideration must be given to the shock and vibration to which the switching device is subjected. Severe shocks can cause unintended momentary contact operation that could result in circuit malfunction. Long term exposure to vibration can cause premature wear of the switch elements and generation of internal dirt. Even a poorly designed panel door can repeatedly subject a switching device to damaging shock and vibration.

It's also important to handle a switch with care during installation to avoid damaging shock.

## Physical Abuse

Improper handling of the switching device during shipping or installation can cause damage to device components that could affect operation.

## Environmentally Sealed Devices

An environmentally sealed device isolates the contact area from the environment.
The most common type of construction has the contacts hermetically sealed within a glass envelope. Prior to sealing, the interior of the glass envelope is filled with an inert gas that keeps the environment around the contacts stable. This construction keeps out explosive gases or contaminants that could affect contact reliability. Since the contacts are not accessible for actuation by mechanical means, they are operated by means of magnetic flux.

A special version of the sealed switch known as a logic reed is used in logic circuits. The logic reed is characterized by very short contact bounce, typically less than 0.5 milliseconds.

Contact isolation can also be accomplished by mechanical means such as a flexible diaphragm. These methods do not, however, provide a true hermetic seal, and are more susceptible to wear and degradation.

Switch Design Considerations

## Standards and Approvals

Standards have been developed by industry groups and governmental units to help ensure that switching devices meet certain requirements with regard to installation criteria, safe operation, load carrying ability, minimum mechanical and electrical life, etc.

Once a particular design has met the requirements of a specific standard, a marking may be affixed to devices constructed according to that design indicating that the standards of that particular agency have been met.

Users need to be aware of which standards pertain to the products used in their locations and which approvals are required. Requirements vary depending on the application and the governmental unit having jurisdiction. Some of the standards that apply to switching devices are listed below:

- UL 508
- NEMA ICS 5 part 1
- IEC 60947-5-1
- CSA 22.2 No. 14

Switch lile can be defined in a variely of ways. It can be defined as the time when the switch physically fails and can no longer provide contact action. It can also be defined as the point when the operating characteristics change to such a degree that switch action is no longer reliable or the parameters fall outside those required for that application. Examples of the latter would be an increase in operating force or excessive travel to obtain contact action.

A switching device may wear out due to mechanical considerations. Repeated operations cause physical wear of parts due to friction, shock, and stress, and can lead to eventual component failure. Dirt and debris generated by the moving mechanism can cause binding and can be a source of contact contamination.

The electrical life of a switch is not necessarily related to its mechanical life. The electrical life of a switch is primarily load dependant, because the electrical load is the main source of heating in - and damage to - current carrying components. High current loads can also contribute to arcing at the contacts during contact action. This arcing action results in contact erosion and deformation and can lead to welding of the contacts. As a result, it is good practice to evaluate both mechanical and electrical life ratings before selecting a switching device.

The switch environment can cause corrosion. This may lead to friction, physical failure of components, and dirt or corrosion in the contact areas.

Low level switching and infrequent use may allow buildup of film on contact faces, affecting contact reliability. Logic reed switches or switches with precious metal contacts are ideal in these applications.

## Shock and Vibration

Shock and vibration refer to the physical conditions that are present in the environment where the switch operates. These conditions often introduce undesirable motion into the device mechanism.

Sources of shock can be the normal motion of the equipment where the device is mounted or the expected movement of the entire control system. Such motion may be repetitive in nature or may occur only periodically under specific situations such as startup, etc. The user may try to anticipate random, abnormal conditions which could result in a high shock situation. One-time mishandling during shipping and installation can cause damage that will affect operation.

Another source of high shock is the slamming of control panel doors where the switching devices are mounted. In order to minimize the effect of known vibration, the axis of actuation of the switching device should not lie on the same plane as that of the direction of normal equipment vibration.

Contact reliability can be affected by shock and vibration. Continual vibration causes mechanical wear and under load conditions, arcing can lead to welding of contacts. A severe shock can cause unintended, momentary contact operation that could result in circuit malfunction.

The mechanical wear caused by long term exposure to vibration can result in the generation of dirt and debris which affects contact reliability and causes added friction in the sliding portions of the mechanism.

Dielectric Strength
Dielectric strength is a measure of the ability of the insulation used in the switching device to withstand the application of a voltage across its surface or through its mass. This will determine the maximum electrical rating of the device.

Degradation of the dielectric strength of insulation can lead to failure of the device. Unintended electrical continuity may be established between circuit elements and ground. In either case, the result is a failure of the switch to perform its intended function.

The most common type of failure is due to arc tracking across the surface of the insulation. The combination of a particular insulation and environmental conditions such as moisture and/or certain gases in the presence of an electrical arc can result in the buildup of a conducting path.

## Special Considerations

Contact Block Ratings

The contact block rating of a switching device is the electrical load that the device is capable of switching. This rating is expressed in voltage and current and typically refers to the maximum values that can be switched in a specified number of operations. Although contact blocks are usually rated for maximum conditions, there is a practical low load limit that the contacts will switch in a reliable manner.

Exceeding the high loads can cause burning and pitting of the contacts leading to welding and contributing to arc tracking. If the load to be switched is of a very low energy level, any contaminants or non-conducting films on the contacts may prevent a circuit from being established when the contacts are operated. If loads below 48 V DC and 0.1 A , or below 24 V AC and 0.4 A , are to be switched, the user must be cautious when selecting the contact materials. If the switching is within a typical Type $4 / 4 \mathrm{X} / 13$ environment, the quadfurcated/ pentafurcated blocks should be used for ultimate reliability. If the switching is within Class 1 and 2 Division 2 environment, without a sealing well or a conduit seal off, logic reed, sealed switch, or stackable sealed switch contact blocks should be used. If this type of switch is used at the high end of the rating, then caution should be exercised if these contacts are used for switching low energy loads. The feature built in for establishment of low energy loads may have been burned away during high load switching operations.

Due to the growing popularity of solid-state devices being used in control circuits, the trend in industry is toward lower energy loads.

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# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type:<br>Surge Diverter<br>Location:<br>Model Numbers:<br>Manufacturer:<br>Supplier:<br>Energy Correction Options PO Box 431<br>Kelvin Grove, QLD. 4059<br>Ph: 0733560577<br>Fx: 0733561432<br>Web: www.ecoptions.com.au

## TDS

## CRITEC Transient Discriminating Surge Diverters



## Surge Protection And Surge Ratings

The stress, which an SPD will experience under surge conditions, is a function of many complex and interrelated parameters. These include:

- Location of the SPD(s) within the structure - are they located at the main distribution board or within the facility at secondary board, or even in front of the end-user equipment?
- Method of coupling the lightning strike to the facility for example, is this via a direct strike to the structures LPS, or via induction onto building wiring due to a nearby strike?
- Distribution of lightning currents within the structure for example, what portion of the lightning current enters the earthing system and what remaining portion seeks a path to remote grounds via the power distribution system and equipotential bonding SPDs?
Type of power distribution system - the distribution of lightning current on a power distribution system is strongly influenced by the grounding practice for the neutral conductor. For example, in the TN-C system with its multiple earthed neutral, a more direct and lower impedance path to ground is provided for lightning currents than in a $T T$ system.
- Additional conductive services connected to the facility - these will carry a portion of the direct lightning current and therefore reduce the portion which flows through the power distribution system via the lightning equipotential bonding SPD.
- Type of waveshape - it is not possible to simply consider the peak current which the SPD will have to conduct, one also has to consider the waveshape of this surge. It is also not possible to simply equate the areas under the current-time curves (also referred to as the action integral) for SPDs under different waveshapes.
AAany attempts have been made to quantify the electrical wironment and "threat level" which an SPD will experience at different locations within a facility. The new IEC ${ }^{\text {wi }}$ standard on lightning protection, IEC 62305-4 "Protection against lightning - Part 4: Electrical and electronic systems within structures" has sought to address this issue by considering the highest surge magnitude which may be presented to an SPD based on the lightning protection level (LPL) being considered. For example, this standard postulates that under a LPL I the magnitude of a direct strike to the structure's LPS may be as high as 200kA $10 / 350$. While this level is possible, its statistical probability of occurrence is approximately $1 \%$. In other words, $99 \%$ of discharges will be less than this postulated 200 kA peak current level.

An assumption is made that $50 \%$ of this current is conducted via the building's earthing system, and 50\% returns via the equipotential bonding SPDs connected to
a three wire plus neutral power distribution system. It is also assumed that no additional conductive service exists. This implies that the portion of the initial 200 kA discharge experienced by each SPD is 25 kA .

Simplified assumptions of current dispersion are useful in considering the possible threat level, which the SPD(s) may experience, but it is important to keep in context the assumptions being made. In the example above, a lightning discharge of 200kA has been considered. It follows that the threat level to the equipotential bonding SPDs will be less than 25kA for 99\% of the time. In addition, it has been assumed that the waveshape of this current component through the SPD(s) will be of the same waveshape as the initial discharge, namely $10 / 350$, while in reality the waveshape have been altered by the impedance of building wiring, etc.

Many standards have sought to base their considerations on field experience collected overtime. For example, the IEEE* guide to the environment C62.41.1 and the recommended practice C62.41.2 present two scenarios of lightning discharge and different exposure levels under each of these depending on the location where the SPD is installed. In this standard, Scenario II depicts a direct strike to the structure, while Scenario I depicts a nearby strike and the subsequent conducted current into a structure via power and data lines. The highest surge exposure considered feasible to an SPD installed at the service entrance to a facility under Scenario I is $10 \mathrm{kA} 8 / 20$, while under Scenario II it is considered to be 10kA 10/350 (exposure Level 3).

From the above, it is apparent that the selection of the appropriate surge rating for an SPD depends on many complex and interconnected parameters. When addressing such complexities, one needs to keep in mind that one of the more important parameters in selecting an SPD is its limiting voltage performance during the expected surge event, and not the energy withstand which it can handle.


Mrotection zones defined by spedific product application.

## Advanced Technologies - The ERICO ${ }^{\circ}$ Advantage

## Transient Discriminating Technology

To meet the fundamental requirements of performance, longer service life and greater safety under real world conditions, ERICO has developed Transient Discriminating (TD) Technology.

This quantum leap in technology adds a level of "intelligence" to the Surge Protection Device enabling it to discriminate between sustained abnormal over-voltage conditions and true transient or surge events. Not only does this help ensure safe operation under practical application, but it also prolongs the life of the protector since permanent disconnects are not required as a means of achieving internal over-voltage protection.

## Traditional Technologies

Conventional SPD technologies utilize metal oxide varistors and/ or silicon avalanche diodes to clamp or limit transient events. However, these devices are susceptible to sustained $50 / 60 \mathrm{~Hz}$ mains over-voltage conditions which often occur during faults to the utility system. Such occurrences present a significant safety hazard when the suppression device attempts to damp the peak of each half cycle on the mains over-voltage. This condition can cause the device to rapidly accumulate heat and in turn fail with the possibility of inducing a fire hazard.

## The Core of TD Technology

The secret to ERICO's Transient Discriminating Technology is its active frequency discrimination circuit. This patented device can discriminate between a temporary over-voltage (TOV) condition


and a very fast transient, which is associated with lightning or switching-induced surges. When the transient frequencies are detected, the patented Quick-Switch within TD activates to allow the robust protection to limit the incoming transient. The frequency discriminating circuit that controls the Quick-Switch helps ensure that the SPD device is immune to the effects of a sustained 50 or 60 Hz TOV. This allows the device to keep operating, in order to help provide safe and reliable transient protection, even after an abnormal over-voltage condition has occurred.

## Meeting \& Exceeding UL* Standards

The CRITEC* range of surge protection devices from ERICO ${ }^{*}$ employing TD Technology has been specifically designed to meet and exceed the new safety requirements of UL 1449 Edition 3. To meet the abnormal over-voltage testing of UL 1449 Edition 3, many manufacturers of SPD devices have incorporated fuse or thermal disconnect devices which permanently disconnect all protection from the circuit during an over-voltage event. Transient Discriminating Technology on the other hand will allow the SPD device to experience an abnormal overvoltage up to twice its nominal operating voltage and still remain operational even after this event! This allows the device to help provide safe, reliable and continuous protection to your sensitive electronic equipment. TD Technology is especially recommended for any site where sustained over-voltages are known to occur, and where failure of traditional SPD technologies cannot be tolerated.

The UL 1449 testing standard addresses the safety of an SPD device under temporary and abnormal overvoltage conditions, but does not specifically mandate a design that will give a reliable, long length of service in the real world. Specifically, UL 1449 tests that the SPD remains operational at $10 \%$ above nominal supply voltage, allowing SPD manufacturers to design products that permanently disconnect just above that. Most reputable manufacturer's designs allow for up to a $25 \%$ overvoltage, while ERICO's TD Technology gives even greater overhead.


$\square$

## Features

- CRITEC TD Technology with thermal disconnect protection
- Compact package, modular DIN rail mounting for limited space requirements
- Three modes of protection: L-N, L-PE \& N-PE Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 15kA $8 / 20 \mu$ s surge rating per mode
- CE, UL ${ }^{\circ} 1449$ Edition 3 Listed


## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS 130 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS130 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. The TDS130 is specifically designed for the protection of single phase power supplies within instrumentation and control applications. They are conveniently packaged for easy installation on 35 mm DIN rail within control
 panels.
CRITEC ${ }^{\bullet}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of life. A visual indicator flag provides user-feedback in the event of such operation. The TDS130 provides a set of optional voltagefree contacts for remote signaling that maintenance is required.


The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.

| Model | \|TD5130|TR150 | TDS1301TR240 |
| :---: | :---: | :---: |
| Item Number for Europe | 702421 | 702422 |
| Nominal Voltage, $\mathrm{U}_{\mathrm{n}}$ | 120-150 VAC | 220-240 VAC |
| Max Cont. Operating Voltage, $\mathbf{U}_{5}$ | 170VAC | 275 VAC |
| Stand-off Voltage | 230VAC | 440VAC |
| Frequency | - $0-100 \mathrm{~Hz}$ |  |
| Nominal Discharge Current, ${ }_{6}$ | 8kA $8 / 20$ /s per mode |  |
| Max Discharge Current, Imar | $\begin{aligned} & \text { 15kA 8/20رs L-N } \\ & \text { 15kA 8/20us L-PE } \end{aligned}$ |  |
| Protection Modes | L-G, L-N, N-G |  |
| Technology | TD Technology with thermal disconnect |  |
| Short Circuit Current Rating, 1. | 200kAIC |  |
| Back-up Overcurrent Protection | 63AgL, if supply > 63A |  |
| Voltage Protection Level, $\mathrm{U}_{\text {p }}$ | $\begin{aligned} & 500 \mathrm{~V} \text { e 3kA }(\mathrm{L}+\mathrm{N}-\mathrm{G}) \\ & 800 \mathrm{~V} \text { e 3kA }(\mathrm{L}-\mathrm{N}) \end{aligned}$ | $\begin{aligned} & \text { 800V e 3kA (L+N-G) } \\ & 1500 \mathrm{~V} \text { e 3kA }(\mathrm{L}-\mathrm{N}) \end{aligned}$ |
| Status | N/O, N/C Change-over contact, 250V-/0.5 Mechanical flag/remote contacts (R mod | max $1.5 \mathrm{~mm}^{2}($ (314AWG) terminals lonly) |
| ModuleWidth | 1 M |  |
| Dimensions H $\times \mathrm{D} \times$ W: mm (in) | $90 \times 68 \times 18(3.54 \times 2.68 \times 0.71)$ |  |
| Weight: kg (ibs) | $0.12(0.26)$ |  |
| Enclosure | DIN 43880, UL94V-0 thermoplastic, IP 20 | EEMA-1) |
| Connection | $\qquad$ |  |
| Mounting. | 35 mm top hat Din rail |  |
| Temperature | $-40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}\left(-40^{\circ} \mathrm{F}\right.$ to $\left.1766^{\circ} \mathrm{F}\right)$ |  |
| Humidity | 0\% to 90\% |  |
| Approvals | CE, IEC 61643-1, UL 1449 Ed 3 Recogniz | Component Type 2 |
| Surge Rated to Meet | ANSPIEEE C62.41.2 Cat A, Cat B IEC 61643-1 Class II UL' 1449 Ed3 $\ln 3 \mathrm{kA}$ mode |  |
| Replacement Module | TDS130M150 | TDS130M240 |
| Replacement Module (Europe) | 702432 | 702424 |

## TDS 150

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS 150 Series

## Features

- CRITEC ${ }^{\text {© }}$ TD

Technology with thermal disconnect protection

- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design
facilitates
replacement of a failed surge module
- $50 \mathrm{kA} 8 / 20 \mu \mathrm{~s}$ maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL® 1449

Edition 3 Listed

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS150 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.
CRITEC ${ }^{\text { }}$ TD technology helps ensure reliable and continued operation during sustained and abnormal
 over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A visual indicator flag provides userfeedback in the event of such operation. As standard, the TDS150 provides a set of voltage-free contacts for remote signaling that maintenance is required.
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


| Model | TDST1501SR150 | TDST1501SR240 | \|TDST501SR277 | TDS1501SR560 |
| :---: | :---: | :---: | :---: | :---: |
| Item Number for Europe | 702404 | 702406 | 702407 | 702408 |
| Nominal Voltage, $\mathrm{U}_{n}$ | 120-150 VAC | 220-240 VAC | 240-277 VAC | 480-560 VAC |
| Max Cont. Operating Voltage, $\mathbf{U}_{s}$ | 170VAC | 275VAC | 320VAC | 610 VAC |
| Stand-off Voltage | 240VAC | 440VAC | 480VAC | 700VAC |
| Frequency | O-100Hz |  |  |  |
| Short Circuit Current Rating, $\mathrm{L}_{5}$ | 200kAIC |  |  |  |
| Back-up Overcurrent Protection | 125 AgL , if supply > 100A |  |  |  |
| Technology | TD with thermal disconnect |  |  |  |
| Max Discharge Current, ${ }_{\text {max }}$ | 50kA 8/20us |  |  |  |
| Nominal Discharge Current, $\mathrm{I}_{9}$ | 25kA 8/20/5s [20kA $8 / 20$ |  |  |  |
| Protection Modes | Single mode (L-G, L-N or N-G) |  |  |  |
| Voltage Protection Level $\mathrm{U}_{p}$ | $\begin{aligned} & 400 \mathrm{~V} \text { e } 3 \mathrm{kA} \\ & 1.0 \mathrm{kV} \text { In } \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} 93 \mathrm{kA} \\ & 1.2 \mathrm{kV} \mathrm{e} \mathrm{in} \end{aligned}$ | $\begin{aligned} & 800 \mathrm{~V} \Theta 3 \mathrm{kA} \\ & 1.6 \mathrm{kV} \mathrm{©} \mathrm{In} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.8 \mathrm{kV} @ 3 \mathrm{kA} \\ & 2.4 \mathrm{kV} \text { In } \end{aligned}$ |
| Status | N/O, N/C Change-over contact, $250 \mathrm{~V} \sim / 0.5 \mathrm{~A}$, max $1.5 \mathrm{~mm}^{2}$ (\#14AWG) terminals <br> Mechanical flag/remote contacts ( R model only) |  |  |  |
| Dimensions H $\times \mathrm{D} \times \mathrm{W}$ : mm (in) | $90 \times 68 \times 18(3.54 \times 2.68 \times 0.69)$ |  |  |  |
| Module Width | 1 M |  |  |  |
| Weight: kg ( $\mathrm{b}^{\text {s }}$ ) | 0.12 (0.26) |  |  |  |
| Enclosure | DIN 43880, UL94V-0 thermoplastic, IP 20 (NEMA-1) |  |  |  |
| Connection | $\begin{aligned} & 525 \mathrm{~mm}^{2} \text { (AAWG) stranded } \\ & \leq 35 \mathrm{~mm}^{2} \text { ("2AWG) solid } \end{aligned}$ |  |  |  |
| Mounting | 35 mm top hat DIN rail |  |  |  |
| Temperature | $-40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}\left(-40^{\circ} \mathrm{F}\right.$ to $\left.176{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
| Humidity | 0\% to 90\% |  |  |  |
| Approvals | CE, IEC 61643-1, UL 1449 Ed 3 Recognized Component Type 2 |  |  |  |
| Surge Rated to Meet | ```ANSIथIEEE C62.41.2 Cat A, Cat B, Cat C ANSI%/IEEE` C62.41.2 Scenario II, Exposure 2, 50kA 8/20\mus IEC 61643-1 Class II UL* 1449 Ed3 In 20kA mode``` |  |  |  |
| Replacement Module | IDSI50M150 | ITDS150M240 | ITDS150M277 | ITDS150M560 |

## Features

- CRITEC ${ }^{\circ}$ TD Technology with thermal disconnect protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches common circuit preakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- $100 \mathrm{kA} 8 / 20 \mu \mathrm{~s}$ maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL -1449 Edition 3 Listed


## TDS1 100

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS 1100 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS1100 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.
CRITEC ${ }^{\circ}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior
 at end-of-life. A visual indicator flag provides user-feedback in the event of such operation. As standard, the TDS1100 provides a set of voltage-free contacts for remote signaling that maintenance is due.

The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


| Model | TDSTIT023R150 | [TDSTIT002SP280 | [TDSTIT022SR277 | [TDSTIC0238560 |
| :---: | :---: | :---: | :---: | :---: |
| Item Number for Europe | 702409 | 702411 | 702412 | 702413 |
| Nominal Voltage. $\mathrm{V}_{5}$ | 120-150 VAC | 220.240 VAC | 2402271 VAC | 0.560 VAC |
| Max Cont. Operating Voltage, Lt. | 170VAC | 275 VAC | 320 VAC | 610VAC |
| stand-oft Votage | 240 VAC | 140 VAC | 480 VAC | 700VAC |
| Frequency | 0-100 Hz |  |  |  |
| Short Crout Current Rating, 1 | 200.AAIC |  |  |  |
| Eackup Overcurment Protection | 125 AOL lif supp | 100 A |  |  |
| Technology | T0 with thermal | sconnect |  |  |
| Max Discharse Current hes | 100kA82015 |  |  |  |
| Impuse Current Los | 12.5kA 10/350/us |  |  |  |
| Wominal Discharge Current, ${ }^{\text {a }}$ | 5013882015 | 140kA 8200 s |  |  |
| Protection Modes | single mode (l-G | L-Nor $\mathrm{N}-\mathrm{G}$ |  |  |
| Voltage Protection Level, $\mathbf{W}_{\text {, }}$ | $\begin{aligned} & 400 \mathrm{~V} 3 \mathrm{kA} \\ & 1.0 \mathrm{kV} \text { e } 20 \mathrm{kA} \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} \text { e3kA } \\ & 1.2 \mathrm{kv}=20 \mathrm{kA} \end{aligned}$ | $\begin{aligned} & 800 \mathrm{Ve} 3 \mathrm{kA} \\ & 1.6 \mathrm{kV} e 20 \mathrm{kA} \end{aligned}$ | $\begin{aligned} & 1.8 \mathrm{k} \cdot \mathrm{~V} 3 \mathrm{kA} \\ & 124 \mathrm{kV} 202 \mathrm{kA} \end{aligned}$ |
| Status | NO, NC C Cange Mechanical flag | $\begin{aligned} & \text { over contact, } 250 \mathrm{~V} \\ & \text { remote contacts ( } \mathrm{R} \end{aligned}$ | $\begin{aligned} & \text { I.5A max } 1.5 \mathrm{~mm}^{2} \\ & \text { odel only) } \end{aligned}$ | 14AWG) termina |
| Dimensions $\mathrm{H} \times \mathrm{DXW}$ : mm ( (in) | $90 \times 68 \times 353$ | $\times 2.68 \times 1.38)$ |  |  |
| Modulewidth | 2 M |  |  |  |
| Weight: kg ( $\mathrm{b}_{\text {a }}$ ) | $0.24(0.53)$ |  |  |  |
| Encosure | DIN 43850, U1\% | -0thermoplastic, | O(NEMA-1) |  |
| Connection | $\begin{aligned} & \frac{25 \mathrm{~mm}^{2}(44 A W C}{35 \mathrm{~mm}^{2}(\# 2 A W C} \end{aligned}$ | stranded solld |  |  |
| Mounting | 35 mm tophat 1 | rrail |  |  |
| Temperature | $40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}(-4$ | fo 176\% |  |  |
| Humidity | 0\% to $90 \%$ |  |  |  |
| Approvals | CE, IECC $61643-1$ | $1{ }^{\circ} 1449$ Ed 3 Reco | zed Component | pe 2 |
| Surge Rated to Meet |  | 1.2 Cat $A$ Cat $B, C$ 1.2 Scenarlo Il, Exp and Class II kA mode | re 3 , 100kA 820 | 10kA 10/350 |
| ReplocementMoVModule | IOSIS0M150 | ITDS150M240 | [10S150M27] | IIDSI50M560 |

## Features

- CRITEC ${ }^{\circ}$ TD Technology with thermal disconnect protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 50kA $8 / 20 \mu \mathrm{~s}$ maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL ${ }^{\odot} 1449$ Edition 3 Listed


## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS350 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
CRITEC ${ }^{\circ}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A
 visual indicator flag provides user-feedback in the event of such operation. As standard, the TDS provides a set of voltage-free contacts for remote signaling that maintenance is due.
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


7


# TECHNICAL DATA SHEET 

## For <br> SEWAGE PUMP STATION SP218 <br> Westlake Drv

## Equipment Type:

Location:

Model Numbers:

Manufacturer:

Supplier:

Surge Filter

Main Incomer

TDF-10A-240V

Critec

Energy Correction Options
PO Box 431
Kelvin Grove, QLD. 4059

Ph: 0733560577
Fx: 0733561432
Web: www.ecoptions.com.au

## Features

- CRITEC ${ }^{*}$ Transient

Discriminating
(TD) Technology
provides increased service life

- In-line series protection
- High efficiency low pass sine wave filtering - ideal for the protection of switched mode power supplies
- Three modes of protection: L-N, L-PE \& N-PE
- 35 mm DIN rail
mount - simple installation
- LED status indication and opto-isolated output - for remote status monitoring
- CE, UL 1449 Ed. 3 Listed


## CRITEC ${ }^{\circledR}$ Transient Discriminating Filter

The TDF series has been specifically designed for process control applications to protect the switched mode power supply units on devices such as PLC controllers, SCADA systems and motor controllers. Units are UL ${ }^{*}$ Recognized and available for 3A, 10A and 20A loads and suitable for $\mathbf{1 1 0 - 1 2 0} \mathrm{V}$ acdc and $\mathbf{2 2 0 - 2 4 0} \mathrm{Vac}$ circuits.
The TDF is a series connected, single phase surge filter providing an aggregate surge
 and N-PE. The low pass filter provides up to 65 dB of attenuation to voltage transients. Not only does this reduce the residual let-through voltage, but it also helps further reduce the steep voltage rate-of-rise providing superior protection for sensitive electronic equipment.


| Model | TDF3A120V | ITDF3A240V | TDF10AT20V | TDF 10A240V | \|TDF20A120V | DF20A240V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| tem Number for Europe | 700001 | 700002 | 700003 | 700004 | 700005 | 700006 |
| Nominal Voltage, $\mathrm{U}_{5}$ | 110-120 | 220-240 V | 110-120V | 1220-240 V | 110-120 | $1220-240 \mathrm{~V}$ |
| Distribution System | TIN-C.S. TN-S |  |  |  |  |  |
| Max Cont. Operating | 170VAC | 3 3 VAC | 170 VAC | 340 VAC | 170 VAC | 340VAC |
| Voltage, Uc |  |  |  |  |  |  |
| Stand-off Voltage | 240 V | 400 V | 240 V | 400 V | 240 V | 400 V |
| frequency | $0-60 \mathrm{~Hz}$ | 5060 Hz | 0.60 Hz |  |  | 50/60 Hz |
| Max Line Current, $k$ | 3 A |  | 10A |  | [20A |  |
| Operating Current OU, | 135 mA | $\underline{250} \mathrm{~mA}$ | 240 mA | 1480 mA | 240 mA | 1480 mA |
| Max Discharge Current, |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Protection Modes | All modes protected |  |  |  |  |  |
| Iechnology | In-line series low pass sine wave filter TD Technology |  |  |  |  |  |
| Voltage Protection Leve, | 500VO 500A | 700 V 500A | 1500V 500A | 700V 500A | 1500Ve 500A | 700V 500A |
|  | 250 V e 3kA | 600 V e 3kA | 250 V - 3kA | 600 V e 3kA | 250 V e 3kA | 600 Ve 3 kA |
| Filtering | -62d8 100 kHz |  | -65dB e 100 kHz |  | -53dBe 100kHz |  |
| status | Green LED. On $=0 \mathrm{k}$. Isolated optocoupler output |  |  |  |  |  |
| Dimensions $\mathrm{H} \times \mathrm{DxW}$ : | $\begin{aligned} & 90 \times 68 \times 72 \\ & (3.54 \times 2.68 \times 2.83) \end{aligned}$ |  | $\begin{aligned} & 90 \times 68 \times 144 \\ & (3.54 \times 2.68 \times 5.67) \end{aligned}$ |  |  |  |
| mm (in) |  |  |  |  |  |  |
| Module Width | 4 M |  | 8 M |  |  |  |
| Weight: kg ( lbs ) | 0.7 (1.54) |  | 1.48(3.25) |  | 11.57 (3.46) |  |
| Enclosure | DIN $43880, \mathrm{U}$ [94V-0 thermoplastic, $1 P 20$ (NEMA ${ }^{\text {a }}$-1) |  |  |  |  |  |
| Connection | $1 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ ( 18 18WG to $\# 10$ ) |  |  |  |  |  |
| Mounting | 35 mm top hat DIIN rail |  |  |  |  |  |
| Back-up Overcurrent | 3 3 |  | 10 A |  | 20 A |  |
| Protection |  |  |  |  |  |  |
| Temperature | -35 ${ }^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}(-31 \%$ to 131\%) |  |  |  |  |  |
| Humidity | 0\% to 90\% |  |  |  |  |  |
| Approvals | C-Tick CE (NOM 3A 120V), CSA 22.2, U0 ${ }^{\circ} 1283$, UL 1449 Ed 3 Recognized Component Type 2 |  |  |  |  |  |
| Surge Rated to Meet | ANS ${ }^{\text {PheEE }}$ C 62.41 .2 Cat A, Cat B, Cat C |  |  |  |  |  |

(1) Opto-coupler output can be connected to DINUNE Alarm Relay (DAR275V) to provide Form C dry contacts.


## Features

- In-line series protection
- EMI/RFI noise filtering - protects against industrial electrical noise
- Compact design
- fits into motor
control and
equipment panels
- Three modes of protection: L-N, L-PE \& N-PE
- 35 mm DIN rail mount - simple installation
- LED power indicator


## CRITEC ${ }^{\circledR}$ Dinline Surge Filter

The "two port" DSF series has been specifically designed for process control applications to protect the switched mode power supply units on devices such as PLC controllers, SCADA systems and motor controllers. The $\mathbf{3 0 V}$ unit is suitable for 12 V and $\mathbf{2 4 V a c} / \mathrm{dc}$ signaling and control systems.
The 6A DSF series incorporates a space efficient, low pass, series filter which provides attenuation to high frequency interference. The larger 20A model provides status indication and a higher surge rating, making this ideal for the protection of higher risk equipment.


| Model | IDSF6A30V | [DSF6A150V | [D5F6A275V | DSFF20A275V |
| :---: | :---: | :---: | :---: | :---: |
| tem Number for Europe | 702090 | 701000 | 701030 | 701020 |
| Nominal Voltage, $\mathrm{U}_{\mathbf{n}}$ | 24 | 110-120V | 220-240 V |  |
| Distribution System | $1 \mathrm{Ph} 2 \mathrm{~W}+\mathrm{G}$ |  |  |  |
| System Compatibility | TN-S, TN-C.S |  |  |  |
| Max Cont: Operating Voltage, Uc | 30VAC, 38VDC | 150VAC | 275VAC |  |
| Frequency | 0-60Hz | 50160Hz |  |  |
| Max Line Current, $\frac{1}{}$ | 6 6A |  |  | 20A |
| Operating Current ${ }^{\text {O }} \mathrm{U}_{\mathrm{n}}$ | 7 mA |  |  |  |
| Max Discharge Current, ${ }_{\text {Ima }}$ | 4kA $8 / 20 \mu 5$ | 16kA8/20/5 |  | $\begin{aligned} & \text { 15kA } 8 / 20 \mu \mathrm{LL} \mathrm{~L} \\ & \text { 15kA } 820 \mu \mathrm{~L} \text { L-PE } \\ & \text { 25kA } 8 / 20 \mu \mathrm{~N} . \mathrm{N}^{2}-\mathrm{PE} \end{aligned}$ |
| Protection Modes | All modes protected |  |  |  |
| Fechnology | $\begin{aligned} & \text { In-line series filter } \\ & \text { MOV } \\ & \hline \end{aligned}$ |  |  |  |
| Voltage Protection Level, $\mathrm{U}_{8}$ | 110Ve3kA | 1400Ve 3 kA | 750Ve 3 kA | 710Ve 3kA |
| Filtering | -3d8e 300kHz |  |  | -308Be 62 kHz |
| Status | LED power indicator |  |  | Status indicator |
| Dimensions $\mathrm{H} \times \mathrm{D} \times \mathrm{W}$ : mm (in) | $\begin{aligned} & 90 \times 68 \times 36 \\ & (3.54 \times 2.68 \times 1.42) \end{aligned}$ |  |  | $\begin{aligned} & 90 \times 68 \times 72 \\ & (3.54 \times 2.68 \times 2.83) \end{aligned}$ |
| Module Width | 2M |  |  | 4M |
| Weight: kg ( l ) | 0.2(0.441) |  |  | 0.7 (1.543) |
| Endosure | DIN 43880, UL94V-0 thermoplastic, PP 20 (NEMA-1) |  |  |  |
| Connection |  |  |  |  |
| Mounting | 35 mm top hat DIIN rail |  |  |  |
| Back-up Overcurrent Protection | 6A |  |  | 20A |
| Temperature | -35 ${ }^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}\left(-31^{\circ} \mathrm{F}\right.$ to 1310\%) |  |  |  |
| Tumidity | 0\% to 90\% |  |  |  |
| Approvals | C-Tick, CE, NOM, U[0 1449 Ed 3  <br> Recognized Component Type 2  |  |  |  |
| Surge Rated to Meet | ANSIHEEE C6241.2 Cat A, Cat 8 |  |  |  |

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## WARNING

ERICO products shall be installed and used only as indicated in ERICO's product instruction sheets and training materials. Instruction sheets are available at wwwerico.com and from your ERICO customer service representative. Improper installation, misuse, misapplication or other failure to completely follow ERICO's instructions and warnings may cause product malfunction, property damage, serious bodily injury and death.

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## INSTALLATION INSTRUCTIONS



MODEL NUMBER<br>TDF-3A-120V<br>TDF-10A-120V<br>TDF-20A-120V<br>TDF-3A-240V<br>TDF-10A-240V<br>TDF-20A-240V

## 1. PREPARATION



DANGER: Electrical shock or burn hazard. Installation of this Transient Voltage Surge Suppressor should only be made by qualified personnel. Failure to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections to this electrical panel be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.

## CAUTION NOTES:

1. The installation of this Surge Protector should follow all applicable electrical codes, such as the National Electrical Code, or the Canadian Electrical Code.
2. Check to make sure line voltage does not exceed Surge Protector voltage requirement.
3. Prior to installation ensure that the TDF is of the correct voltage, current, and frequency rating for your application.
4. The earth terminal must be connected to a low impedance earth (< 10 ohms) for correct operation.
5. Do not perform a "Flash Test" or use a Mega-Ohm Meter (Megger) to test circuits that are protected with TDF modules. Damage may occur to the TDF modules.
6. Follow all instructions to ensure correct and safe operation.
7. Do not attempt to open or tamper with the TDF units in any way as this may compromise performance and will void warranty.

## 2. INTRODUCTION

Transient Discriminating Filters (TDF) are packaged in "DIN 43 880 " profile enclosures for simple installation onto 35 mm DIN
rails. They can be selected for use on distribution systems with nominal RMS voltages of 120 Vac or 240 Vac at frequencies of $50 / 60 \mathrm{~Hz}$. The 120 Vac unit also operates on nominal 125 Vdc supplies.

## 3. QUICK INSTALLATION OVERVIEW

Install in the following manner:

1. Ensure that power is removed from the area and the circuits that will be connected.
2. Snap lock the TDF module to the DIN rail.
3. Install the appropriate upstream overcurrent protection.
4. Connect wiring to the indicated $i / p$ and $o / p$ terminals.
5. Apply power and observe correct operation of the Status Indication, and alarm facilities if provided - see Section 11.

## 4. PROTECTION CONCEPTS

To optimize effectiveness of the TDF protection, the unprotected and protected wiring should be separated. Wiring from the exposed transient source to the TDF should be considered unprotected and kept approximately $12^{\prime \prime}$ ( 300 mm ) from all other wiring wherever possible. Wiring on the equipment side of the TDF should be considered protected.

The separation of protected and unprotected wiring is recommended to minimize the risk that transients conducted on unprotected wiring may cross couple onto protected circuits, and diminish the level of protection available from the TDF module.

The terminals on the TDF module are labeled "INPUT/LINE" (unprotected side) and "OUTPUT/LOAD" (protected side) assuming that the source of the transients is on the input side of the TDF module.
For applications where the transient source is on the load side of the TDF module, the TDF should be reverse connected with the INPUT/LINE terminals connected to the load side, toward the source of the transients.

## 5. MOUNTING

TDFs are designed to clip to 35 mm DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the TDF module spring clips to the bottom and the label text the correct way up.

NOTE: TDFs must be installed in an enclosure or panel that:

- prevents the TDF unit temperature from exceeding $122^{\circ} \mathrm{F}\left(50^{\circ} \mathrm{C}\right)$
- provides adequate electrical and safety protection
- prevents the ingress of moisture and water
- allows TDF status indicators to be inspected


## 6. GROUND FAULT CIRCUIT INTERRUPTION (GFCI)

Where GFCI protectors ( $\mathrm{RCDs} / \mathrm{ELCBs}$ ) are used, it is preferable that the TDF modules be installed prior to these devices (i.e. upstream). If this is not done, nuisance tripping of the GFCls may occur during transient activity.

## 7. CONDUCTOR TERMINATION

Each TDF terminal is designed to accept wire sizes from 10 to 18 AWG ( $1.5 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ ) solid or stranded conductor. The wire insulation should be stripped back $5 / 16^{\prime \prime}(8 \mathrm{~mm})$.
NOTE: Do not use greater than ginlbs (1Nm) of torque when tightening the terminals. For UL compliance, where two wires may need to be terminated into one terminal, the permissible wire size is 18AWG each.

## 8. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of every TDF to provide protection to the unit itself, the load and the wiring in case of fault situations. The current rating of the breaker or fuse used should be determined according to below. However, the current rating should be less than the rating of the wiring. For example, if a 20A TDF were installed in a circuit with wiring that can carry 15A, then a 15A overcurrent device must be installed upstream to protect both the TDF and wiring from overload.

| MAX FUSE SIZES: | TDF RATING | FUSE RATING |
| :---: | :---: | :---: |
|  | 3 A | 4 A |
|  | 10 A | 10 A |
|  | 20 A | 20 A |

## 9. STATUS INDICATION

TDF modules have a single Status Indicator on the front panel. When power is applied and full surge capacity is available, the Status Indicator will be illuminated. Should power be applied and the indicator fail to illuminate, the TDF should be replaced, as optimum protection is no longer provided.

## 10. MAINTENANCE \& TESTING

Before removing a TDF module from service, ensure that the power has been removed from the module. Replacement of a

TDF module should only be undertaken by qualified personnel.
NOTE: TDF units should be inspected periodically, and also following any periods of lightning or transient voltage activity. Check the Status Indicator and replace the module if it is not illuminated as detailed in Section 9 STATUS INDICATION.

## 11. DINLINE ALARM RELAY (DAR)

The TDF status monitoring circuit which provides the visual Status Indicator, also provides a low voltage opto-coupler alarm output circuit. Should voltage free alarm contacts be required, the ERICO Inc, DINLINE ALARM RELAY (DAR) should be used.

The DAR module provides a fully isolated dry contact alarm output. One DAR can be used per TDF, or up to 16 TDFs can be connected in series to one DAR to provide a common dry contact alarm output.
Ensure that the voltage rating of the alarm wiring is rated in accordance with the other voltages present in the equipment. This would normally be the same voltage rating as that used for the TDF module input wiring.
It is recommended that the DAR unit be powered from the output/load side of the TDF being monitored, however the DAR can be powered from other circuits. This allows for example, one DAR unit to be connected to separate TDFs which are protecting a three phase circuit.
NOTE: Depending upon the usage of the DAR output contacts, failure of power to the DAR may be interpreted as a failure of one or more TDFs. Visual inspection of the DAR and TDF Status Indicator is required to clarify this situation.

## 12. USE OF OTHER INTERFACES

ERICO, Inc. DAR units are recommended for the interfacing of equipment to the TDF opto-coupler alarm output circuit. The direct connection of other equipment to the TDF opto-coupler alarm output circuit may not provide sufficient isolation or exceed the opto-coupler specifications. This may damage the TDF and/or the connected equipment. Warranty may be voided under such circumstances. However, the specifications for TDF alarm output has been provided for those who desire to use the TDF opto-coupler output directly.
The TDF alarm opto-coupler output is available on terminals 3 and 5 . Terminal 3 is the positive and 5 is the negative side. This output is an open collector transistor output of the optocoupler. When the opto-coupler is driven on, it should be arranged to have 2 mA flowing through it. For use with 24 Vdc circuits, a $12 \mathrm{k} \Omega$ current limiting burden resistor is required. For use with 12 Vdc circuits, a $5.6 \mathrm{k} \Omega$ current limit resistor is required. For use with 5 Vdc circuits, a $2.2 \mathrm{k} \Omega$ current limit resistor is required.
NOTE: In connecting to the TDF opto-coupler alarm output, do not reverse the + -connections or exceed the maximum permissible ratings ( 30 Vdc ) as damage may occur.

# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218

Westlake Drv

| Equipment Type: | Surge Filter Alarm Relay |
| :--- | :--- |
| Location: | Main Incomer |
| Model Numbers: |  |
|  | DAR-275V |
| Manufacturer: | Critec |
|  |  |
| Supplier: | Energy Correction Options |
|  | PO Box 431 |
|  | Kelvin Grove, QLD. 4059 |
|  | Ph: 07 3356 0577 |
|  | Fx: 07 3356 1432 |
|  | Web: www.ecoptions.com.au |

## INSTALLATION INSTRUCTIONS



## MODEL NUMBER

DAR 275 V

## 1. PREPARATION



DANGER: Electrical shock or burn hazard. Installation of this device should only be made by qualified personnel. Failure to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.

## CAUTION NOTES:

1. The installation of this device should follow all applicable electrical codes, such as the National Electrical Code.
2. Check to make sure line voltage does not exceed DAR275V voltage ratings.
3. Follow all instructions to ensure correct and safe operation.
4. Do not attempt to open or tamper with the DAR in any way as this may compromise performance and will void warranty. No user serviceable parts are contained.

## 2. INTRODUCTION

Selected DSD, TDS \& TDF DINLINE Surge Protection Devices include status monitoring circuits which provide visual status display of device capacity. They may also provide a low voltage opto-coupler alarm output circuit that can be connect to the DAR to provide potential free (Form C) change-over contacts. The DAR alarm contacts may be used to provide output to external alarm systems or remote monitoring circuits.

One DAR can be used per DSD/TDS/TDF opto-coupler alarm or up to 16 DSD opto-coupler alarms can be connected in series to the one DAR to provide a common output. It is recommended that the DAR be powered from the same power circuit that feeds the device(s) being monitored, however the DAR can be powered from other circuits. This allows for example, one DAR unit to be connected to separate SPDs that are protecting a three phase circuit.

Note. Depending upon the usage of the DAR output contacts, failure of power to the DAR may be interpreted as a failure of one or more of the SPDs being monitored. Visual inspection of the DAR and SPDs status displays would determine this.

## 3. MOUNTING

The DAR is designed to clip to 35 mm (top hat) DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the DAR module spring clips to the bottom and the label text the correct way up.
NOTE: The DAR must be installed in an enclosure or panel that:

- prevents the DAR temperature from exceeding $131^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$
- provides adequate electrical and safety protection
- prevents the ingress of moisture and water
- allows DAR status indicators to be inspected


## 4. ELECTRICAL CONNECTION

The interconnecting wiring should:

- be of size \#10 to \#14 AWG ( $2.5 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ ) solid or stranded conductor.
- The wire insulation should be stripped back $5 / 16^{\prime \prime}(8 \mathrm{~mm})$.
- NOTE: Do not use greater than 9inlbs ( 1 Nm ) of torque when tightening the terminals.


## CONNECTION TO TELECOMMUNICATIONS NETWORKS

The DAR is approved for use in Australia where the alarm contacts may be connected to private lines or building cabling associated with the telecommunications network. NO direct connection to the public switched network should be made.

## INSTALLATION INSTRUCTIONS

## 5. INTERCONNECTION

When connecting the DAR to a single opto-coupler output the + terminal of the SPD should connect to the + terminal on the DAR. The - terminal should connect to the-terminal.


When connecting the DAR to multiple opto-couplers the optocouplers should be connected in series with + terminal of one connected to the - terminal of the next. The DAR + terminal should connect to + SPD terminal at one end of the series connection and the - DAR terminal connect to the - SPD terminal at the other end of the series connection.

+/-terminal connections are polarity sensitive. Do not reverse.

## 5. STATUS INDICATION



## 6. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of the power supply to the DAR to provide protection to the unit itself and the wiring in case of fault conditions.

The fuse rating should be based on the wiring size used to connect to the DAR Ph \& N terminals. Australian regulations AS3000-1991, Table B2 specifies the following upstream protection for single phase circuits, unenclosed in air.

| Cable Size | HRC Fuse or | CB Rewirable Fuse |
| :--- | :---: | :---: |
| $1.5 \mathrm{~mm}^{2}$ | 16 A | 12 A |
| $2.5 \mathrm{~mm}^{2}$ | 20 A | 16 A |
| $4 \mathrm{~mm}^{2}$ | 25 A | 20 A |
| $6 \mathrm{~mm}^{2}$ | 32 A | 25 A |

Where overcurrent protection of the appropriate rating or smaller is already fitted in the upstream circuit, overcurrent protection at the DAR will not be required

## 6. MAINTENANCE \& TESTING

Before removing a DAR unit from service, ensure that the power has been removed. Maintenance, testing and replacement should only be undertaken by qualified personnel.
Testing of a DAR unit which is connected to a fully functional DSD unit can be accomplished by removing power to the DSD only. The DAR Status indication and output contacts should alter from the Normal to Fault condition.

Testing of the DAR unit alone may be accomplished by disconnecting the $+/$-connections to the unit. When power is applied the DAR "Fault" Status Indicator should be illuminated. By connecting the $+/$ - terminals together, the "Normal" Status Indicator should be illuminated. The output contacts should alter to the appropriate state.

## 7. USE OF OTHER INTERFACES

Only DAR units are recommended for the interfacing of equipment to the DSD, TDS \& TDF opto-coupler alarm output circuit(s). The direct connection of other equipment to these opto-coupler alarm outputs may not provide sufficient isolation or exceed the opto-coupler specifications. This may damage the SPD and/or the connected equipment. Warranty may be voided under such circumstances.
NOTE: In connecting to the SPD opto-coupler alarm output(s), do not reverse the +/- connections as damage may occur?

# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218

## Westlake Drv

Equipment Type: Phase Failure Relay
Location:Common Control
Model Numbers: ..... 252-PS GW
Manufacturer: Crompton
Supplier:
Crompton Instruments.PO Box 5108Minto Business CenterMinto NSW, 2566
Ph: 0296032066Fx: 0296039335

## Page 1 of 2

Ref: IW250PMSH - Rev 6 - March 02

## Modets Covered

| 252-PMM | $252-P M T$ | $252-\mathrm{PSF}$ |
| :--- | :--- | :--- |
| $253-\mathrm{PH} 3$ | $252-\mathrm{PMM}$ | $252-\mathrm{PMT}$ |

## Introduction

Thermistior Trip Relay (252-PMM 8 252-PMT).
The trip inputs are monitored within settable limits. In the event of the inptit moving outsidethese fints, the unit will initiate a trip signal via a doude pole crängeover relay. An illuminated green LED indicates when the themistor' temperature is within nomal working limits. The unit is designed such that the atarm relay is energised when normal temperatures are reached.
Model 252-PMM has the facility for manual resetting, so that the trip condition remains after normal operating temperature is reached, until manuad intervention occurs.

Phase Balance Relay (252-PSF 8 252-PSG)
Trip inputs are monitored within settable limits. In the event of the input moving outside these limits, the unit will initiate a trip signal via a double pole changeover relay. An illuminated red LED indicates that the supply is within limits.

Speed Sensing Retay (253-PH3)
Tip inputs are monitored within settable limits. In the event of the input moving outside these limits, the unit will initiate a. trip signal. The ituminated red LED's indicates that the single pole output relays are in an energised state and at normal running speed all three relays should be energised. Units are factory adjusted for normal unning speed $=0.75 \mathrm{~mA}$. output. The meter adjust pot on the product front is used for this requirement; which also ensures the trip levels are set to the calibrated values. Terminal 8 is connected to terminal 5 internally. Terminals 15 and 16 give a $0 / 1 \mathrm{~mA}$ signal proportional to speed.

No. 1 Relay energises on rising speed
No. 2 Relay energises on rising speed
No. 3 Relay de-energises on rising speed
This product is designed for use conly with magnetic coil inductive sensors.

## Waming

- Duñing normal operation, voltages hazardous to life may be present at some of the teiminals of this unit. Installation and servicing shoutd be performed only by qualified, properly trained personnef abiding by local regulations. Ensure all supplies are de energised betore attempting connection or other procedures.
- It is recommended adjustments be made with the. supplies de-energised, but il this is not possible, then extreme cautioñ shöuld be exercised.
$\therefore$ Terminals stiould not be user accessible after instatlation and extemal installation provisions must be sufficient to prevent hazards under fault conditions.
- This unit is not intended to function as pant of a system providing the sole means of fault protection - good engineering practice dictates that any critical function be protected by at least two independent and diverse means.
Never open circuit the secondary winding of an energised current transformer.


## Protector Trip Relays

DIN Rail \& Wall Mounted 250 Series Thermistor Trip, Speed Sensing 8 Phase Angle
Installation
The Protector should be installed in a dry position, not in direct sunlight and where the ambient temperature is reasonably stable and will not be outside the range 0 to 60 degrees Celsius. Mounting will nomally be on a veitical surface but other positions will not affect the operation: Vibration should be kept to a-minimurn:-The Protectors are designed for mounting on a 35mm, rail to DIN 46277. Alternatively they may be screw fixed; a special adaptor is supplied to mount 252 types.

To moumt a protection on a.DIN rail, the top edge of the atiout on the beick is hooked over one edge of the rail and the botbom edge carrying the release clip clicked into place. Check thet the unt is fimfy fixed. Removal or repositioning may be actioved by tevering down the retease ctip and liting the urit up and of ter rail.

Connection diagrams stould be carefully followed to erisire correct podarity and phase rotation where applicabte. Externat vodiage transtomers may be used on 252-PSF and 252.PSG to extend the range.

252-PMM, 252-PaT 8 253-PH3
Pick up, input and ounfat teads shoutd be kept separate from any okter wivita

Setting Controls (252-PSF, 252-PSG)
These products have two calibration facitios that can beset
to suft operating requirements and they are factory calibrated as follows:-

1. \% unbalance sot poinis

Voltages of and below 380 vots $L i$ are caftrirated to
$1.0 \%$ class index of rated voltage. Vottages above 380 volts L-L are calibrated to $1.5 \%$ class index of rated voltage.
2. Time Delay

For all voltage ranges $10 \%$ maxinum delay.
3. Voltage Withstand

Continuous overload $=1.35 \times$ rated voltage
Setting Up (all other models)
The calibration marks around the comtrols are provided as a guide if the installer does not have access to accurate equiprnent. The maximum error of the calibration marks is typically $10 \%$ of the span of the control concemed.

## Maintenance

The unit should be inspected to normal standards for this ctass of equipment. For example remove accumulations of dust and check all connections for tightness and corrosion. In the unlikely event of a repatr being riecessary it is recommended that the unit be retumed to the factory or to the nearest Cromptori Instruments Service Centre

Electromagnetic Compatibility
This unit has been designed to provide protection against EM (electro-magnetic) interference in line with requirements of EU and other regulations. Precautions necessary to provide proper operation of this and adjacent equipment will be installation dependent and so the following can only be general guidance:-

- Avoid routing wiring to this unit alongside cables and products that are. or could be, a source of interference.


# Ref: IW250PMSH - Rev 6-March O2 <br> Protector Trip Relays DIN Rail \& Wall Mounted 250 Series Thermistor Trip, Speed Sensing \& Phase Angle 

- The auxiliary supply to the unit should not be subject to excessive interterence. In some cases, a supply line filter may be required.
- To protect the prodüct against incorrect operation or permanent damage, surge transients must be controlled. It is good EMC practice to suppress differential surges to 2 kV or less'at the source. The unit has been designed to automatically recover from typical transients, however in extreme circumistances it may be necessary to temporanily disconnect the auxiliary supply for a peniod of greater than 5 seconds to restore correct operation.
.- Screened communication and small signal leads are recommended and may be required. These and other connecting leads may require the fitting of RF suppression components, such as ferrite absorbers, line filters etc., if RF fields cause probtems.
-inis good practice to install sensitive electronic instruments that are performing critical functionsin-EME enclosures that protect against electrical interference causing a disturbance in function.


The Information contained in these installation instructions is for use onty by installers trained to make electrical power installations and is intended to describe the correct method of Installation for this product. However. Tyco Electronics has no control over the fletd conditions, which influence product installation.
It i' sser's responsibility to determine the suitability of the installation method in the users fietd conditions. Tyco Electronics' only abitgations are those in Tyco El Les' standard Conditions of Sale lor this product and in no case will Tyco Electronics be liable for any other incidental, indirect or consequential damages ar' .- om the use or misuse of the products. Crompton is a trade mark.

# TECHNICAL DATA SHEET 

## For <br> SEWAGE PUMP STATION SP218 <br> Westlake Drv

| Equipment Type: | Level Relay |
| :---: | :---: |
| Location: | Common Control |
| Model Numbers: | MTR 240VAC |
| Manufacturer: | Multitrode |
| Supplier: | Multitrode Pty Ltd 130 Kinston Road Underwood. QLD 4119 <br> Tel: 0733407000 Fax: 0733407077 |

## 1 Introduction

The MultiTrode level control relay is a solid-state electronic module in a hi-impact plastic case with a DIN rail attachment on the back, making a snap-on-snap-oft installation. Any number of relays can be easily added to the DIN metal rail then wired together to form a complex pumping system that other wise may have to be controlled and operated by a programmed PLC.

The relay is normally matched with the MultiTrode probe which works in conjunction with the relay and uses the conductivity of the liquid to complete an electrical circuit.

## 2 Electrical Overview



Thereare 10 screw terminalson the unit Facingthe trayas shown, we look at the bottom terminals (left to right):

- Lo - (Charge mode). This is the point when the probe is dry: the relay will tum on.
- Lo - (Discharge mode). This is the point when the probe in the tank is dry the relay will tum off.
- Hi - (Charge mode). This is the point when the probe in the tank is wet a relay will tum off
- $\mathrm{Hi}-$ (Discharge mode). This is the point when the probe in the tank is wet a relay will turn on.
- C - is common earth. All earth boriding must be terminated here for correct operation.
- " $L$ " is "live" (240V AC)
$0-\mathrm{Na}$ neutral" (240VAC)

If the tank is plastic, or if you are conducting tests in a plastic bucket, or the vessel has no earth point inside, you must install an earth rod within the tank, vessel or bucket ard make sure that it is borided back to $C$ on the relay unit.

## 3 DIP Switches

### 3.1 DIP Switches

## (See Wining Diagram for full program functions.)

### 3.1.1 DIP 1 \& 2

DIP 1 and 2 control the Sensitivity, in other words the cleaner the liquid the higher the sensitivity setting must be. Concentrated acids; minerals are by their own chemical composition highly conductive, so a low level of sensitivity is required, purified water is almost an insulator against electrical current flow so a higher sensitivity inside the relay is required.

### 3.1.2 DIP 3; 4 \& 5

DIP switches 3, 4 and 5, control delay on activation. For example, in discharge mode with DIP switches 3.4 and 5 set to 10 seconds, when the Hi point becomes wet it will activate the motor and it will take 10 seconds of continual coverage of the probe sensor to make the relay close and start the pump. This is invaluable when the probe is in a turbulent part of a well where fluid is splashing around touching the sensors momentarily, and false activation cannot be tolerated.

### 3.1.3 DIP 6

DIP switch 6 controls the charge/discharge function. Set "ON" for charge, and "OFF" for discharge

### 3.2 Relay Contacts \& their Applications

### 3.2.1 Contacts $15,16 \& 18$

Contacts 15, 16, and 18 are used for electronic or visual notification of a change in state at the pump itself. Contacts 15, 16, and 18 are used for more advanced applications because they are a changeover relay, their state may be the same as contacts 25,28 or the opposite. Both sets of contactors are triggered simultaneously. An example is when in discharge mode, (see Figure 1).
You have a gravity flow coming in so the fluid reaches the lower sensor PB1, contacts 15 and 18 are open ( 15 being common to both contact 16 and 18) contacts 25 and 28 are also normally open but contacts 1516 in this current situation are closed, whether PB1 is wet or dry is of no concern all will stay the same. The level now rises to PB2 and both relays change state, contacts 25 and 28 close to turn on the pump, contacts 15 and 16 are open, with 15 and 18 closed.
In advanced applications this state change may be fed into a logic device to indicate the pump is running or the pump has stopped and perhaps light an LED or incandescent light source for visual confirmation that a change has occurred in the relay.

### 3.2.2 Contacts 25 \& 28

Contacts 25 and 28 are used to control pump states. Contacts 25 and 28 are mostly used for turning on motors via a starting relay or solenoid, so, these sets of contacts react to the rising or falling levels of the fluid inside the tank, they will operate to turn on a pump in discharge mode when the top sensor is wet and in charge mode turn on the pump when the bottom sensor is dry.

## 4 Practical Overview

### 4.1 Discharge Mode - DIP switch 6 set to "OFF"



Figure 1 - Discharge Mode
Figure 1 shows two probes, (PB1 connected to Lo and PB2 connected to Hi). The pit is mostly underground and there is a gravity-fed inlet at the top left-hand side. The pit is empty with PB1 completely dry. Dipswitch 6 is set to "OFF."

| \%ex |
| :---: |
| SEM 18 |
| DETM A A |
| obat |
| ch/olsc - ${ }^{\text {a }}$ |

The relay operation depends on the electrical conductivity of liquid in the pit, i.e. no liquid $=$ no current flow. The level starts to rise and covers PB1.
This is a discharge operation so we do not want the relay to close and start a pump until the well is full so as the water rises it reaches PB2, the relay closes and the pump starts. The level now drops below PB2

### 4.2 Charge Mode - DIP switch 6 set to "On"



Figure 2-Charge Mode
Note: "C" is connected to common bonded earth. The unit will not operate correctly if not earthed.
Let's look at the same relay but in a tank that is charging (DIP 6 is now on). See Figure 3 , where liquid is being pumped into a tank, and discharging through a gravity feed, the tank is on steel stands " $x$ " metres above the ground.


With the tank full, PB1 and PB2 will be wet, the relay is off, and the pump has stopped. Water is slowly fed out from the bottom, and now as PB2 (HI) becomes dry nothing happens; the water now drops to below PB1 (Lo), and the pumps restarts to fill the tank.
The pump will continue to fill the tank until PB2 (HI), becomes wet again.

### 4.3 MTRA Relay with Alarm (Discharge Applications Only)



Figure 3-MTRA Operation

The MTRA relay works in the same way as the MTR relay except the MTRA has a separate alarm output, and does not have a charge mode. The planned application is to close a contact to illuminate a warning alarm light. . Various other applications have included introducing a third probe to latch another relay.
In Figure 2 we see three probes in a pit that is plastic, note the steel rod in the tank. (In a plastic vessel a steel rod must be used to create an earth return in the liquid so probes can function.) PB1, PB2, and PB3 are dry, and the relay power LED is on. When water enters the pit and wets PB1, nothing happens, water now reaches PB2 causing contacts 13 and 14 to close, the pump LED to light, and the water to drop.

If, for example, the pump has its inlet partially blocked, the level continues to rise and wets PB3. This closes a separate relay that can activate a red flashing light, an audible fog horn or send a 5 volt pulse into another device with the common cause to wam human beings that a spill is due to occur. If the pumps become unclogged and PB3 becomes dry the alarm opens again and breaks the circuit that stops the light from flashing or the foghorn from sounding.

## 5 Most Common Installation Problems

The relay requires a path between the probes to earth through the liquid. If you are testing in a plastic bucket, have installed the probe in a plastic tank or have no good earthing in the vessel you will need to install a separate earth and make sure all earth bonding comes back to the $C$ terminal. Most problems like these are traced back to a lack of or poor earthing, or open circuits in the probe wiring.
Now is the time to check the relay by using "the bridge testing line technique" remember you must simulate a fluid flow to correctly ascertain a good relay or a bad one. (All DIPswitch settings from 1 to 6 should be off.)
Cut two pieces of insulated flexible copper wire one black one red 250 mm long, strip both ends back 10 mm on both cables, and join one black end and one red end. Insert the joined ends into C on the relay box, observing all safe electrical practises. You should have one black wire and one red wire free.

Set your relay for discharge mode (DIP switch 6 is off) with no sensors connected to the unit, connect the red wire to Lo - nothing should happen (if It does return the relay for replacement or repair"). Now connect the black wire to the Hi terminal the relay activated LED should light instantly (if it does not, the relay should be returned for repair${ }^{\star}$ ).

## 6 Troubleshooting

| I have checked all the DIPswitches and settings <br> but in discharge mode as soon as the bottom <br> sensor gets wet the pump turns on then turns off <br> almost straight away. | -This is the most common problem encountered with relay set up <br> and commissioning, the probe in the bottom of the tank is wired <br> into the Hi terminal instead of the Lo terminal. <br> The installation went fine but now and again the <br> pump will not turn on even though I am sure the <br> probe is wet. <br> Check the sensitivity level set on the relay, some times the level is <br> set for foul water but due to changes in the flow the water <br> becomes grey or clear, try changing the setting from 20K $\Omega$ <br> $80 \mathrm{~K} \Omega$ and monitor the results carefully. <br> All wiring is complete and all DIPswitches have <br> been checked but the pump will not turn on at all. <br> - If you have completed the test schedule for the relay and it passed <br> then check the wiring to the sensors - for this is now where the <br> problem lies or in the earthing arrangements. If possible check <br> the resistance between the sensor cable and the steel sensor on <br> the probe to prove a solid connection. |
| :--- | :--- |

[^7]
# TECHNICAL DATA SHEET 

## For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type: ..... Radio
Location: RTU Section
Model Numbers: DR900-06A02-D0
Manufacturer: ..... Trio
Supplier:Brisbane Water

# TC－900DR USER GUIDE 

ロ円T円CロM
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## GENERAL

The Trio DataCom TC－900DR is a full duplex 900 MHz Radio featuring a fully integrated 4800／9600 bps data radio modem and antenna diplexer．Configuration of the unit is fully programmable，with parameters held in non volatile memory（NVRAM）．All configuration parameters are accessible using the TC－DRPROG installation package， consisting of a programming lead，manual and software which will run on a PC under Windows $95 / 98 / \mathrm{NT}$ ．It is essential that each unit is programmed to suit individual requirements prior to operation．For detailed information refer to the TC－900DR Handbook．

## DATA CONNECTION

The data connection is via a DB9 connector labeled＇Port $A^{\prime}$（shown below），which is wired as a DCE．

## User Serial＂Port A＂Pin Assignment．

## EXTERNAL VIEW OF＇PORT A

NOTE：Pin 6 and pin 9 provide a dual function which depends on the mode that the TC－900DR is operating in．


## User Serial＂Port B＂Pin Assignment．

Port $B$ can be used as a secondary data steam （independent of Port $A$ ）once configured by the programmer．Port B also has one connection that may be of use for installation．This connection（Pin 9）is Receive Signal Strength Indicator（RSSI）output． $0-5 \mathrm{~V}$ where 1.5 V typically indicates -110 dBm and every 0.5 V increase indicates an improvement of $» 10 \mathrm{dBm}$ ．
EXTERNAL VIEW OF＇PORT B＇


VOTE：Port B Pin 9 output has a high impedance of zround 50 K OHMS and loading will decrease accuracy of the RSSI measurement．

## POWER CONNECTIONS

The power required is 13.8 VDC nominal，at $600 \mathrm{~mA}(\mathrm{Tx})$ nominal．If the POWER LED indicator is not illuminated once power is applied，check the internal 1Amp fuse fitted within the unit．


The auxiliary connector is primarily for use with the optional audio handset．The connections to this auxiliary 6 pin RJ11 connector are as follows：

| PIN NUMBER | FUNCTION | External view <br> of socket |
| :--- | :--- | :--- |
|  | 8 VOLTS |  |
| 2 | AUDIO OUT |  |
| 3 | GROUND |  |
| 4 | MIC INPUT／SENSE |  |
| 5 | GROUND |  |
| 6 | MANUAL PTT | 6 |

The optional audio handset is recommended as an aid in checking installations for radio path viability．This audio handset will only function when fitted prior to applying power to the unit．
The modem upon power up will check the presence of the handset and will inhibit data being transmitted so that voice communications can be established．
Once the path tests have been conducted the audio handsets MUST be REMOVED and the unit powered up with the handset removed before data communication can commence．

## USER INDICATIONS

The TC－900DR provides 4 LED＇s that show status information to the user－POWER，RXSIG，SYNC，and TXMIT indications．
The POWER is indicated by a green LED and simply signifies that power has been applied to the unit．
The RXSIG LED（yellow）indicates the level of RSSI signal from the radio IF strip，compared to a threshold level set in the configuration data programmed by the user．If the signal is above the threshold，then the LED indicator is turned on．
In all operation modes except＂Programmer mode＂，the SYNC LED（yellow）indicates when the modem has detected a valid data stream．The SYNC LED is activated， when the modem detects a valid HDLC flag sequence，and remains active until an invalid sequence of seven or more consecutive＂ 1 ＂bits is detected．
The SYNC LED will not be turned on if the RSSI signal strength（as indicated by the RXSIG LED）is below the minimum threshold．This prevents false SYNC detection from noise．
The TXMIT LED（red）indicator is connected directly to the modem＇s PTT output transistor．Whenever the radio is transmitting，this TXMIT．LED indicator will be on．

## SPECIAL MODES OF OPERATION

Part of the power-up/reset initialisation phase of the TC-900DR are tests to determine if the modem should enter one of 3 "special operation" modes. In these modes the TC-900DR won't operate in its standard run mode.

- Programmer mode.
- Bit error rate test mode.
- Handset mode.

These modes are only entered if the required setup conditions are present at power up. An error mode of operation can also be entered into, if during normal operation, an error condition occurs.

## PROGRAMMER MODE

CABLE - Pins 2, 3, 4, 5 straight through with Pin 6 on the DB9 connector of Port A, connected to pin 5. When the modem is powered up with this fitted, the controller senses this and attempts to enter "Programmer mode" and the "SYNC" LED will flash approx. once per second. (Note, the TC-DRPROG programming software and lead has the required connections). Failure to supply the correct password in time, will cause the modem to abandon the "Programmer mode" attempt, and go on with it's normal power-up procedure.

## BIT ERROR RATE TEST MODE

Pin 9 of the DB9 connector of Port $A$, is normally the Ring Indicate output line. However, if this pin is driven positive (connecting it to pin 6 [DSR] and pin 7 [RTS]), then the modem's data transmitter and receiver will enter the BER test mode. This will activate the RF transmitter, and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic " 1 " level in the unscrambled data. Any errors in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a "0" bit.
Note: As the TC-900DR is full duplex this test can operate in both directions simultaneously.
Every error bit detected, will activate the SYNC LED. For error rates of 1 in $10^{3}$ and above, the SYNC LED will be ON most of the time. A 1 in $10^{4}$ error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for installation purposes. Note: Error count messages
( $E T: X X X X$ ) for every 10,000 bits are presented to Port $A$ for the user. If pin 9 ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

## HANDSET MODE

The DFM4-9 modem tests for the presence of a handset plugged into the handset auxiliary port at power up. If a handset is plugged in, the modem will not generate a data stream. However, it will continue to indicate received RF signal strength. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED. It is essential to remove the handset from the unit and reapply power to the unit in order to return to normal operation.

## ERROR INDICATION MODES

There are 3 error conditions that cause the RXSIG \& SYNC LEDs to be used for error indications and not their normal purpose. Two are fatal conditions, that cause the modem to restart after the duration of the error indication shase.

## TRANSMIT POWER LOW

While the modem activates the radio transmitter, it periodically checks the transmit power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately 4 times per second. The TXMIT LED will also be on during this process. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function. Factory set to 100 milliWatts.

## NVRAM READ ERROR

The DFM4-9DR modem accesses the non-volatile memory as part of it's initialisation phase, to read programming configuration data. If the communication protocol with the device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED operates ON and OFF twice, then the other. A total of five cycles of this occurs, then the modem restarts initialisation.

## SYNTHESISER LOCK DETECT ERROR

If at any time during normal operation, BER mode, or handset mode, the TBB206 frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting.
One LED is turned ON (O), the LEDs are swapped, then both turned OFF ( $\bullet$ ). Then the latter LED ON again, swap LEDS, and then OFF. This will give the appearance of a sweeping motion between the LEDs. The following table shows all error condition displays.

| Tx PWR Err |  | NVRAM Err |  | SYNTH Err |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | $\bullet$ | 0 | $\bullet$ | 0 | $\bullet$ |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ | 0 |
| 0 | $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ | 0 |
| 0 | $\bullet$ | $\bullet$ | 0 | 0 | $\bullet$ |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ |
| 0 | $\bullet$ | $\bullet$ | 0 |  | repeat |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ |  |  |

## MOUNTING AND ANTENNA CONNECTION

The TC-900DR should be.mounted in a cool, dry, vibration free environment, whilst providing easy access to screws and connections. There are 4 mounting holes on the unit. The antenna should be an external yagi antenna but can be a ground independent dipole mounted via a feeder to the antenna connector (SMA type) for short range applications. However the whole radio modem should be clear of the associated data equipment to prevent mutual interference.

## ASSEMBLY OF POWER LEAD

A small plastic bag containing a molex connector (M5557-2R) and two pins (M5556-TL) is provided in the packing box.
The pins are designed to take 18-24 (AWG) wire size with insulation range 1.3-3.10mm.

## TC-900DR

## 900 MHz

Full Duplex Data Transceiver

## User Manual

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## IMPORTANT NOTICE

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This handbook is for the installation, operation and maintenance of the TC-900DR. The specifications described are typical only, and are subject to normal manufacturing and service tolerances.

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## Modifications

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|  | Removed Filter Alignment Setup Diagram |
|  | Inserted RSSI Level of Received Signal (typical) |
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|  | Addition of section 5.2.6.1 and 5.2.6.4 |
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Change of Company Name

## SECTION 1

## INTRODUCTION

## 1 INTRODUCTION

### 1.1 GENERAL

The TC-900DR is a Full Duplex 900 MHz Radio, featuring a fully integrated 4800 or 9600 bps data modem.

The entire unit is housed in a robust metal enclosure that provides a compact and transportable means for the transmission of data over radio.

The product has been fully designed and developed in Australia, by an Australian owned and managed company.

The TC-900DR meets the ACA SP4/89 specification which covers radio data transmissions over point-to-point and point-to-multipoint systems.

It is ideally suited for applications such as :
, Transaction Processing.
, Public Utility Telemetry Systems.
, Alarm Monitoring.
, Supervisory Control and Data Acquisition.
, Energy Distribution.
, Inventory Control
, Common Carrier Data Services.
, Temporary Installations
The modem provides byte oriented packet data communications over narrow band FM systems, using digital filtered binary FSK modulation.
The TC-900DR can be supplied for use with $12.5 \mathrm{kHz}, 15 \mathrm{kHz}, 25 \mathrm{kHz}$ or 30 kHz channel spacings. Its operational parameters can be programmed with the TC-D Series installation programmer. This is a separate software package that runs on an IBM compatible PC under Windows 95/98/NT.

### 1.2 FACTORY QUALITY ASSURANCE

The TC-900DR has been designed and manufactured with particular emphasis placed on the following points :
\{ State of the art design techniques.
\{ Simple assembly/disassembly.
\{ Minimal alignment requirements.
\{ Manufactured using quality components.
All units have been manufactured using automated assembly procedures. This assures attention to detail and a high level of quality control.

All components used are of high quality, and conform to Trio DataCom's required specifications. The component suppliers provide batch, date and manufacturing criteria that are required to meet quality control standards.

Each unit is individually tested with an inbuilt self diagnostic program. It is then passed through a set of automatic test procedures with minimal human intervention. This ensures a consistently manufactured and performing product. Many of the alignments are factory set and should not require re-alignment in the field.

Trio DataCom's quality control does not finish here. Once each unit has passed its individual tests, it is placed in a cyclic heat/cooling chamber. This chamber is automatically cycled from $-10^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$, twice, over a twenty hour period. During this time, the modem controller - using external precision calibrated test equipment - monitors and stores frequency stability versus temperature data. The TC-900DR uses this information to achieve its temperature compensated, frequency stability level of 1 ppm .

Power output is measured during the temperature cycling. This is achieved by having the unit connected to a PC and various test equipment via a GPIB. Units that fail any of these tests are reported by the test program and corrective action taken before going through the complete cycle once again. Each unit shipped from the factory comes with a factory alignment printout which details:
" Configuration.
" Transmit frequency.
" Receive frequency.
" Receiver sensitivity.
" Transmitter power output.
, Transmitter modulation.
In most cases, the radio transmitter as shipped from the factory will require no re-alignment.

It is this care and quality control that ensures that the purchaser of a TC-900DR radio modem, obtains a consistently manufactured and performance specified product, which has been "burned in" to minimise any operational failures.

### 1.3 FEATURES

Advanced microwave and digital techniques were employed during the design phase of the TC-900DR, ensuring an innovative and state of the art product.

Features include :
\{ Fully integrated full duplex radio and modem
\{ Built in antenna diplexer
\{ Power output +30 dBm (1 Watt nom) at antenna connector
\{ Radio meets ACA SP4/89 requirements 2/90
\{ In-built transparent remote diagnotics capability.
\{ Custom single chip modem - digital signal processing
\{ 4800 \& 9600 bps transfer rates, full duplex
\{ Selectable 110..19k2 asynchronous RS-232 host interface
\{ Unique collision avoidance facilities
\{ Integrated supervisory signalling channel
\{ Software selectable configuration parameters
\{ Configurable bit error rate testing
\{ Excessive temperature power fold-back
\{ Auxiliary port for use with an optional supervisory audio handset

### 1.4 SPECIFICATIONS

### 1.4.1 RADIO SECTION

Rx frequency range
Tx frequency range
Channel spacing

Frequency stability : $1 \mathrm{ppm}\left(-10^{\circ} \mathrm{C}\right.$ to $65^{\circ} \mathrm{C}$ amb), $\left[\right.$ opt $-30^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ ], aging $<=1$ ppm/Annum

Power output : $+30 \mathrm{dBm} \pm 1 \mathrm{dBm}$ ( 1 W nom)
at Antenna connector
switchable under software control $200 \mathrm{~mW} / 1 \mathrm{~W}$
Duty cycle
Output impedance
Timeout timer
Tx key up time
Rx sensitivity

Rx intermodulation
$R x$ spurious responses
Continuous
50 Ohms
Programmable from 1 sec . to 28 minutes (max)
: $\quad<=$ to 1 mS (output_1dB of power).

Tx spurious emissions : <=-65 dBc (ref unmodulated carrier).
Full duplex with single antenna.

Note 1. The reciprocal frequency option for point-to-point operation or point to multi-point base repeaters is available as follows:

- Rx frequency range 847 MHz to 857 MHz .
- Tx frequency range 923 MHz to 933 MHz .

Note 2. The transmitter is normally supplied, with its frequency offset from the receiver by 76 MHz .

### 1.4.2 MODEM SECTION

| User Ports | $:$ | DB-9 connector, EIA RS232, DCE, serial <br> asynchronous, 300..19k2 baud, 7/8 bit, <br> no/odd/even parity. |
| :--- | :--- | :--- |
| Data Rate | $:$ | $4800 / 9600$ bps Full Duplex. |
| BER | $:$ | Less than 10E-6 @ -105dbm measured at antenna port |
| Data Format | $:$ | Narrow band digital filtered binary FSK Modulation, <br> using Trio DataCom's DFM4-9 digital modem chipset, <br> including Trio's unique supervisory signalling channel |
| C/DSMA collision avoidance scheme. |  |  |

### 1.4.3 RADIO AND MODEM SECTIONS COMBINED

Occupied bandwidth : $\quad$| Meets ACA SP4/89 guidelines for point-to-point and |
| :--- |
| point-to-multipoint assignments. |

| Mean deviation | $\pm 1.5 \mathrm{kHz}$ ( 4800 bps ), <br> $\pm 2.75 \mathrm{kHz}$ ( 9600 bps ) |
| :---: | :---: |
| Power requirements | 14 Volts AC 10VA or 13.8 Volts DC ( 11 to 16 V Max). |
| Transmit current | < to 600 mA . |
| Receive current | 175 mA . |
| Size | $241 \mathrm{~mm} \times 161 \mathrm{~mm} \times 65 \mathrm{~mm}$. |
| Weight | 1.3 Kg . |

### 1.4.4 CONNECTORS

| User RS-232 Connection | DB9 female wired as DCE (modem). <br> (AMP Part \# 747844-5) |
| :---: | :---: |
| Mating connectors | DB9 male solder type. <br> (AMP Part \# 747983-3) <br> Backshell to suit. <br> (AMP Part \# 205729-1). <br> Optional supplied to order |
| Antenna Connection | Gold plated SMA female bulkhead. <br> (E.F.JOHNSON Part \# 142-0701-501) |
| Mating connector | SMA male to RG223 crimp type. <br> (E.F.JOHNSON Part \# 142-0407-006) <br> Optional supplied to order |
| AC/DC Power Connector | 2 pin locking (9A rating). <br> (PCB SOCKET MOLEX Part \# M5569-2A2) |
| Mating connector | (RECEPTACLE MOLEX Par\# M5557-2R) (RECEPT PINS MOLEX Part \# M5556-TL) Supplied with standard unit. |
| Supervisory Audio |  |
| Handset Connector | 6 pin modular jack. <br> (AMP Part \# 520250-3) |
| Mating connector | 6 pin modular jack plug. <br> (AMP Part \# 5-641337-3). <br> Supplied with optional audio handset. |

### 1.5 OPTIONAL ACCESSORIES

Trio stock a large range of ancillary devices including coax cables, RF connectors, antennas, lightning protection, power supplies, etc.

Please contact Sales for futher information.

## SECTION 2

## HARDWARE TECHNICAL DESCRIPTION

## 2 HARDWARE TECHNICAL DESCRIPTION

### 2.1 GENERAL

The TC-900DR is a 900 MHz full duplex radio complete with radio modem and antenna diplexer. In this and subsequent descriptions to follow, references have been made to block diagrams, circuit diagrams and component loading diagrams.

These can be found in appendix $A$, at the rear of this manual.
The unit can be divided into five major sub-blocks :
Radio section.
Antenna diplexer section.
Audio handset.
Modem section.
Unit housing assembly.

### 2.2 RADIO SECTION

The radio section is built on a single PCB with approximate dimensions of $193 \mathrm{~mm} \times$ $152 \mathrm{~mm} \times 1.6 \mathrm{~mm}$.

This section consists of the following main blocks :
Receiver.
Transmitter.
Frequency control.
Interfaces.
Each of these blocks can be further broken down as follows :
Receiver.
Pre-amplifier.
Mixer.
45 MHz I. F. filter.
FM I.F. \& Demodulator
Audio processing.

- Data.
- Voice.

RSSI processing.
Transmitter.
Audio processing.

- Data.
- Voice.

Modulator.
Multiplier.
Mixer.
Power amplifier.
Control.

- PTT.
- Power.

Frequency control
Synthesiser.
Local oscillator.
AFC
Interfaces
Modem section.
Antenna diplexer.
Audio handset.

### 2.2.1 RECEIVER

The general form of the receiver circuitry is shown in diagrams "DR9 Macro Block Diagram" (drawing number TC01-05-19 sheet 3/3), and " 900 MHz Radio - Block Diagram" (drawing number TC01-05-19 sheet $2 / 3$ ).

### 2.2.1.1 PRE-AMPLIFIER

The receiver pre-amplifier obtains signal direct from the antenna diplexer port connector X 2 . It consists of two stages. The first stage is optimised to give a low noise figure, while the second is optimised to produce gain.

The central devices used are MRF5711 high frequency transistors. They provide the basis for a wide band amplifier that can receive from the lowest band frequency range of 852 to 854 MHz to the higher band frequency range of 928 to 930 MHz .

The RF selectivity is provided by the diplexer filter.
Strip line impedance matching networks are employed to ensure optimum performance of the amplifier.

The overall gain of the pre-amplifier is set to 20 dB .

### 2.2.1.2 MIXER

The receiver mixer consists of a 180 "rat race hybrid ring" followed by a passive Schottky mixer diode.

The mixer injection frequency is set 45 MHz from the required receive frequency, (high side injection for 930 MHz receive and low side for 850 MHz receive). This results in an I.F. frequency output of 45 MHz .

The level of the injection is set to 6 dBm by the amplifier stage Q3.

### 2.2.1.3 FIRST I.F. STRIP FILTER

The required receiver mixer product is filtered by the first I.F. filter. The filter is a bandpass crystal controlled device, centred on 45 MHz , and provides image rejection for the second IF Mixer.

The filter is aligned for optimum response by adjustment of inductors L4,L3 and L5.

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### 2.2.1.4 FM IF and DEMODULATOR

The heart of the demodulator section is an NE615D high performance low power mixer FM IF system IC.

This device incorporates a mixer/oscillator, two limiting intermediate frequency amplifiers, a quadrature detector, muting circuitry, logarithmic RSSI, and a voltage regulator.

The input to the device is from the output of the 45 MHz first IF strip filter. This is applied at $R F_{\text {in }}$ and $R F_{\text {bypass }}$ pins (U2-p1,p2).

This signal is applied internally to a Gilbert cell mixer, which is set to convert the signal down to 455 kHz .

The mixer injection is supplied by an internal oscillator, which is driven by an external oscillating signal applied at the XTAL OSC pins (U2-p3,p4).
The basic injection frequency is governed by the 44.545 MHz crystal XTAL1. This produces a mixer output product of 455 kHz .

The output of the mixer is available at MIXER OUT (U1-p20). This is applied to a 455 kHz centred bandpass filter. This acts as the "front end" filter, CF1.

The bandwidth and rolloff characteristics of this filter are set, depending on the required baud rate of the data being used on the modem, and the required channel spacing. Refer to Circuit Diagram for filter types.
The filtered output is then applied to the input of the internal IF amplifier, IF AMPIN (U1-p18). The bandwidth of the amplifier is about 40 MHz , with a gain of about 39 $\mathrm{dB}(\mathrm{uv})$. C10 and C11 provide IF amplifier decoupling.

The output is available at IF AMP OUT (U1-p16). This is applied to a 455 kHz centered bandpass filter. This acts as the "rear end" filter, CF2.

Again the filter selection depends on the required bandwidth. Refer to Circuit Diagram for filter types.

The filtered output is then applied to the input of the internal IF limiter, LIMITER IN (U1-p14). The bandwidth of the limiter is about 28 MHz , with a gain of about 62 dB (uv). C13 and C14 provide IF limiter decoupling.

The signal from the second limiting amplifier is passed to an internal Gilbert cell quadrature detector, as well as to LIMITER OUT (U1-p11).

One of the Gilbert cell ports is driven directly by the IF, the other by a tuned quadrature network, which is driven by the IF signal from LIMITER OUT. The tuned network is based around a ceramic resonator CF3. The Q of the network is varied depending on the required baud rate used by the modem. For 9600 baud the link LK3 is inserted, giving a higher damping factor than that required for 4800 baud, where the link is removed.

This gives the two input signals applied to the Gilbert cell a 90 degree phase relationship, the output of which is the demodulated audio/data signal.

The output signal is available at UNMUTED AUDIO OUT (U1-p9). A gated output is also available at MUTED AUDIO OUT (U1-p8).

### 2.2.1.5 AUDIO PROCESSING

### 2.2.1.5.1 DATA

The demodulated data signal output has been assigned to the UNMUTED AUDIO OUT pin (U1-p9). This ensures no interruption to the flow of data.

The signal is filtered by the $\mathrm{C} 22, \mathrm{R} 20, \mathrm{R} 29$ and C 23 filter network. This is to remove any high frequency components produced at the output of the quadrature detector.

It is then amplified and DC level shifted by op-amp $\cup 1: C$. The amount of $D C$ bias applied to the signal can be varied by the potentiometer VR2. For correct processing by the modem, this level is set to 2 V . The $A C$ level of the signal is set to about $1 \mathrm{~V}_{\mathrm{p} \text {-p }}$

### 2.2.1.5.2 AUDIO

The demodulated audio signal output has been assigned to the MUTED AUDIO OUT pin (U1-p8). This allows switching control of the audio passed to the handset earpiece.

The signal is filtered by R23 and C17. This is to remove any high frequency components produced at the output of the quadrature detector.

It is then buffered, amplified and level shifted by op-amp U1:D, and presented to the handset via coupling capacitor C20 and connector X3-p2.

The mute control signal is applied to the NE615 (FM IF system IC) MUTE IN pin (U2-p5). When active, the audio output signal from the IC is attenuated by greater than 60 dB .

### 2.2.1.6 RSSI

The RSSI output is presented by the NE615 at RSSI OUT (U2-p7). This signal is logarithmic with an output range greater than 90 dB . It is used for audio mute processing, and by the modem section as a data qualifier signal.

The signal is first passed through a unity gain buffer, op-amp $U 1: B$, before it is split.
The RSSI level is compared with the setting of "audio mute adj" potentiometer VR1, by op-amp U1:A. The result is passed to the MUTE IN pin of the NE615.

This allows a suitable mute cutoff point to be set for the received audio sent to the handset earpiece.

The RSSI signal is also passed to the modem section for processing via R19 and connector X1-p21.

### 2.2.2 TRANSMITTER

The general form of the transmit circuitry is shown in diagrams "DR9 Macro Block Diagram" (drawing number TC01-05-19 sheet 3/3), and "900 MHz Radio - Block Diagram" (drawing number TC01-05-19 sheet 2/3).

### 2.2.2.1 AUDIO PROCESSING

### 2.2.2.1.1 DATA

The transmit data signal enters the radio section via connector J*3-p13, from the modem section. It is biased via R68 and R75 to a DC level of about 0.86 V . The signal is then passed through a level setting potentiometer VR2, used to set the level of transmit deviation.

It is then presented to the input of the modulator circuit.

### 2.2.2.1.2 VOICE

The transmit voice signal enters the radio section via connector $\times 3$-p4, from the microphone in the handset. The pre-amp in the microphone circuit is given some bias via R76.

The signal is first passed through a clipping circuit. This consists of back to back clamping diode pair D2, AC-coupled via C154. This ensures that a maximum transmit deviation level is imposed.

The modulator circuitry is based around a low power FM transmitter system IC,MC2833. Included in this device is a microphone amplifier and clipper. The audio is passed to the amplifier via R76 at the MIC AMP INPUT pin (U7-p5).
Feedback for gain is supplied by R76, and band limiting by C50. The amplifier output is presented at MIC AMP OUTPUT (U7-p4).
Further low pass filtering is provided by the network of R71, C49, R59.. and C42... C43 provides a rising response below 100 Hz . This filtering is needed to shape the base band signal, so as the transmit frequency spectrum stays within channel boundaries.
The audio is coupled into the modulator circuit at the MODULATOR INPUT pin of the MC2833 (U7-p3).

### 2.2.2.2 MODULATOR

The heart of the modulator section is an MC2833 low power FM transmitter system IC. This device is a one chip FM transmitter subsystem designed for FM communication equipment. It includes a microphone amplifier, a variable reactance modulator, a voltage controlled oscillator, and two auxiliary transistors.

Data is fed directly to the input of the reactance modulator at the MODULATOR INPUT pin (U7-p3). The audio channel is fed via an inbuilt clipper amplifier in the MC2833. The output of this variable reactance circuit is used to modulate the FM carrier.

The carrier frequency of the modulator is provided by an internal oscillator, which is driven by an external oscillating signal applied at the RF OSC pins (U7-p15,p16).

This oscillating signal is governed by the 20.166 MHz crystal XTAL3. The actual applied frequency is set by the modulating signal, which slightly varies ("pulls") the crystal frequency. This is achieved by connection of the crystals circuit to the output of the variable reactance circuit VARIABLE REACTANCE OUTPUT (U7-p1). This output is coupled to the crystal via a frequency trimming coil L6.

The output FM signal is presented at the RF OUTPUT pin (U7-p14).

### 2.2.2.3 MULTIPLIER

The output of the modulator is passed to a frequency tripler stage employing auxiliary transistor TR2. This places the carrier frequency at 60.5 MHz .

It then passes to a frequency doubler stage employing auxiliary transistor TR1, where the carrier is moved up to 121 MHz .

The signal is amplified through these stages to a level of about -4 dBm at 121 MHz .

### 2.2.2.4 MIXER

The transmit FM signal at 121 MHz when mixed with the VCO frequency by U8 produces a transmitter signal 76 MHz from the receiver frequency.

The mixer employed is an MCL SBL-1X monolithic doubly balanced mixer (U8).
The transmit VCO signal is amplified to a level of about +6 dBm by Q2, and applied to the "L" input of the mixer. The 121 MHz signal is applied to the "I" input of the mixer.

To select the correct mixing product for the transmitter, a tunable filter using C78 and a coupled stripline circuit is used.

The output signal is then buffered by two MRF5711 transistors Q4 and Q5, to provide about +4 dBm of signal level, which is applied to the final amplifier section.

### 2.2.2.5 POWER AMPLIFIER

The power amplifier provides an overall gain of about 30 dB . This is achieved by three stages of amplification.

The first stage uses an MRF5711 transistor (Q8). This device is primarily designed for high gain, low-noise, small signal amplifiers, and is ideal for a transmitter pre amplifier. This stage provides about 13 dB of gain. The power control circuit acts on this stage to provide constant power at the PA. output connector.

The second stage uses an MRF8372 transistor (Q9). This device is primarily designed for wideband, large signal predriver stages, in the 800 MHz range. This provides a further 10 dB of gain.

The final stage uses two MRF8372 transistors (Q10, Q11) in a parallel configuration to provide the final output power. Each of these stages provides about 10 dB of gain. The output impedance is matched to 50 ohms via the use of balanced impedance strip lines.

The transmitted signal is presented at connector X4, at a level of about +32 dBm , where it is passed to the diplexer section.

### 2.2.2.6 CONTROL

### 2.2.2.6.1 PTT

PTT must be activated for the TC-900DR to transmit an RF signal. There are two sources of PTT, the audio handset, and the modem section.

PTT from the audio handset is referred to as "manual PTT". It enters the radio section via connector X3-p6. It is passed to the PTT control switch transistor Q12. PTT is active LOW, and turns on Q12 when applied.
PTT from the modem section enters the radio section via connector X1-p12, "/PTT". It is connected to the PTT control switch transistor Q12.

When PTT is not activated the transmitter is totally disabled. All stages of the transmit chain are turned off. This is to ensure that power consumption is kept to a minimum.

The PTT signal connects to the start of the transmit chain at the multiplier stage.
The internal transistors of the MC2833 IC, TR1 and TR2 have their bases effective grounded, turning off the devices. Similarly the mixer output buffer and amplifier transistors Q4 and Q5 are turned off as are the final amplifier stages employing Q8, Q9, Q11 and Q10.

When the PTT is activated, bias is applied to all these stages and transmission is possible.
Note : Tx enable must also be active to allow transmission.

### 2.2.2.6.2 TRANSMIT ENABLE

Transmit enable is a further control placed on the transmitter circuits. No transmission is possible unless the transmit enable signal is active. The signal enters the radio section via connector $\times 1-\mathrm{p} 11$, "ITX EN", from the modem section.

This signal basically enables the PTT switching transistor Q12, thus providing VCC for the 20.166 MHz oscillator section of the MC 2833 modulator $I C$, and bias to the handset microphone.

### 2.2.2.6.3 POWER

The RF power output of the TC-900DR can be set to two levels. Low power level is 200 mW , and high power is 1 W .

This level is controlled by two dc levels. One signal is a control level from the modem section, the other from an RF detector located at the output of the transmitter itself. These two signals are used in conjunction to hold the output power constant.

The signal from the modem section enters the radio section via connector $\times 1-\mathrm{p} 10$, "TXPWR". The signal is fed to an op-amp comparison circuit U9:A, via level setting potentiometer VR4.

The level is compared to that actually detected at the output of the transmitter, by the circuit based around diode D3. The comparator output is then used to bias the first stage of the P.A. section (Q8) of the transmitter, hence varying the transistor gain performance and ultimately the output RF power. This basic feedback network is required to keep the power at a constant level, regardless of any external conditions.

The detected output power level is also fed back to the modem section for monitoring and analysis via connector X1-p9, "TXPWR SENSE".

### 2.2.2.6.4 TEMPERATURE SENSE

A temperature sensing device is included in the radio section. The device used is an LM335 precision temperature sensor, U6. It is operated as a two terminal zener diode, with a breakdown voltage directly proportional to absolute temperature, with an output of +10 mV per degree kelvin.

The temperature data output is passed to the modem section for analysis and processing via connector $\times 1-\mathrm{p} 14$, "TEMP SENSE".

During the "Burn In". cycle, that the TC-900DR is passed through during production, the unit calibrates the output of the sensor to the test temperature. In particular it stores the hottest temperature reached by the test cycle (about 65C).

If the unit reaches this maximum temperature setting while operating in the field, the modem section of the TC-900DR will automatically signal the power control circuit to place the transmitter into low power mode $(200 \mathrm{~mW})$.

This low level of output power is retained until the temperature sensor signals the modem section, that the temperature has fallen back below the maximum temperature. When this occurs the transmitter is placed back to its previous power setting. A hysteresis is built into the microprocessor control circuitry to stop power jitter.

This scheme is referred to as "High Temperature Fold Back". It is used to protect the transmitter final power transistors from any damage that may be encountered under extreme temperature conditions.

### 2.2.3 FREQUENCY CONTROL

### 2.2.3.1 SYNTHESISER

The synthesiser section provides a local oscillator for use by the receiver and transmitter sections.

The synthesiser circuitry is based around a TBB206 PLL frequency synthesiser IC.
This device is a complex PLL circuit in CMOS technology for processor controlled frequency synthesis. The processor resides in the modem section, and three basic control lines are used to interface to the device. The enable "EN", data "DA" and clock "CL" control signals are passed to the TBB206 via connector $\times 1-\mathrm{p} 16, \mathrm{p} 17, \mathrm{p} 18$ respectively.

The reference frequency for the synthesiser is applied to the "RI" pin of the TBB206 (U3-p2). This reference is provided by a 12.000 MHz voltage adjustable temperature compensated crystal oscillator (VTCXO), XTAL2. This input has a sensitive preamplifier for a 16-bit (R)eference divider. C33 provides AC coupling for the input.

The VCO frequency is applied to the "FI" input pin of the TBB206 (U3-p8). This input has a highly sensitive preamplifier for a 12-bit N divider and a 7-bit A divider. C29 provides AC coupling for the input.

The actual signal applied to the "FI" input is from the output of a TBB202 dual modulus divider IC (U4-p4). This is to transform the actual VCO frequency of between 786 MHz and 996 MHz , down to a frequency acceptable for use by the "FI" input.

The divider ratio selected by the TBB202 is determined by the state of the "MOD" input pin (U4-p6). If the signal is HIGH, then a ratio of $1: 128$ is used. If the signal is LOW, a ratio of $1: 129$ is used. The state of this signal is controlled by the TBB206 synthesiser "MOD" output pin (U3-p7). The TBB206 drives this output LOW at the beginning of a cycle. When the A divider has reached its set value, the "MOD" output is set to HIGH. When the N divider reaches its set value, the output is set LOW again and the cycle is repeated.

The input to the TBB202 divider is from the VCO output via a strip line impedance matching network. The signal is applied to the "I1" pin (U44-p1).

The TBB202 can be placed into standby mode, when not in use. This is achieved by connection of the "STB" pin (U4-p7), to the multi function output port of the TBB206 synthesiser (U3-p6). This port is driven by the DFM4-9 modem IC located in the modem section.

The phase detector signal is provided on the "PD" pin of the TBB206 (U3-p12). This signal has especially short anti backlash pulses to avoid any "dead zones", and to neutralise any small phase deviations. This signal is passed to the loop filter of the VCO circuit.

A lock detect indication is given by the TBB206 synthesiser at the "LD" output pin (U3-p14). This signal is filtered and shaped by the network using R47 and C36, and presented to the modem section for monitoring and processing, via connector X1-p19.

### 2.2.3.2 VCO

The VCO used is an MQC309 series VCO. The exact device used depends on the required frequencies that the unit has to work with.

Two types are used:
A. MQC309 798 - Frequency range of 784 MHz to 816 MHz

Gives unit frequency ranges of :

- Transmit : 905 MHz to 937 MHz
- Receive : 829 MHz to 861 MHz
B. MQC309 978 - Frequency range of 962 MHz to 994 MHz

Gives unit frequency ranges of :

- Transmit : 841 MHz to 873 MHz
- Receive : 917 MHz to 949 MHz

The 798 type employs low side injection to the mixers, whereas the 978 type employs high side injection.

The loop filter consists of R44, C40, C41 and R43.
The output of the VCO is passed to the receiver mixer via RXMIX, and to the transmitter mixer via TXMIX signal lines. Each of these is impedance matched by strip line circuits for optimum performance.
The layout and selection of all these components has been done in such a way so as to minimise VCO noise being impressed onto either the transmitted or received RF signals.

### 2.2.3.3 VCO TEMPERATURE COMPENSATION

Frequency temperature compensation is provided for by an input to the reference oscillator circuit.

During the "Burn In " cycle, that the TC-900DR is passed through during production, the unit calibrates the output of the temperature sensor to the test temperature and to any frequency variations that occur, and stores the results.

When the unit is operating in the field, the temperature of the unit is constantly being analysed. Should a frequency offset be required based on the calibration measurements, the modem section signals to the 12.000 MHz reference oscillator to vary its frequency slightly. This signal is passed to the radio section via connector X1-p15, "TEMP COMP". The voltage on this line "pulls" the reference oscillator XTAL2 onto a new frequency, which corresponds to the correct offset required.

Note : Because the temperature compensation for the installed VTCXO is held in the NVRAM of the modem it is imperative that modems and radio boards are maintained as matched pairs. Should either the VCO or NVRAM require replacement it is highly recommended that the unit be retumed to the manufacturer for re-calibration.

### 2.2.3.4 RECEIVER AFC

Automatic frequency control is provided for the received signal. The control signal is applied to the radio section from the modem section via connector X1-p22, "AFC CTL".

The basic injection frequency to the front end mixer of the NE615 FM demodulator IC (U2), is governed by the 44.545 MHz crystal XTAL1. The actual applied frequency can be set by the level of the AFC signal, which slightly varies ("pulls") the XTAL1 crystal frequency via the varactor diode DV1.

The modem section monitors the average DC level of the received signal (DATA signal X1-p13), which gives an indication of received frequency drift.

From this the modem section calculates the required compensation necessary and applies it to the "AFC CTL" signal line.

A reference signal is passed back to the modem section from the radio section via connector X1-p23, "AFC REF". This is processed by the modem section, and used to help determine the level of AFC signal level.

### 2.2.4 INTERFACES

### 2.2.4.1 MODEM SECTION

The radio section interfaces to the modem section via connector X 1 . Attached permanently to this connector is a 90 mm length of 26 way ribbon cable, fitted with a female 26 way connector at the other end. This attaches to connector JX3 on the modem section PCB.

Refer to interface diagram "RADIO MODEM INTERFACE", drawing number TC01-05-18 sheet $1 / 3$.

## CONNECTOR $\times 1 / J \times 3$ SIGNAL DESCRIPTION PIN NUMBERS

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26

13V8 POWER SUPPLY RAIL 13V8 POWER SUPPLY RAIL 13V8 POWER SUPPLY RAIL GROUND
GROUND
GROUND
8V POWER SUPPLY 8 V POWER SUPPLY TXPWR SENSE (o/p- TRANSMIT POWER SENSE) TXPWR (i/p-TRANSMIT POWER LEVEL)
TX EN ( $\mathrm{i} / \mathrm{p}-\mathrm{TRANSMIT}$ ENABLE)
/PTT

## DATA

TEMP SENSE
(i/p - PRESS TO TALK)
(o/p-TEMPERATURE SENSOR)
TEMPCOMP (i/p-TEMPERATURE COMPENSATION)
EN
DA
CK LD DATA OUT
RSSI AFC CTL SUPPLY/MIC TEST1 (i/p - ENABLE FOR SYNTH)
(i/p - DATA FOR SYNTH)
(i/p-CLOCK FOR SYNTH)
(o/p - LOCK DETECT FROM SYNTH)
(o/p - RECEIVED DATA)
(o/p - RSSI SIGNAL)
(i/p - AFC CONTROL)
(UNUSED)
(UNUSED)
TEST2
(UNUSED)
(UNUSED)

### 2.2.4.2 ANTENNA DIPLEXER

The interface between the radio section and the antenna diplexer section is via coaxial connectors $X 4$ and $X 2$, and low loss coaxial cables.

| CONNECTOR | SIGNAL DESCRIPTION |
| :--- | :--- |
| X4 | TRANSMITTER OUTPUT |
| X2 | RECEIVER INPUT |

### 2.2.4.3 AUDIO HANDSET

The interface between the radio section and the audio handset is via the modular- 6 pin connector X3.

CONNECTOR X3 PIN NUMBERS

6

SIGNAL DESCRIPTION

8 V POWER SUPPLY
AUDIO OUT (o/p-AUDIO TO EARPIECE)
GROUND
MIC (i/p - MICROPHONE AUDIO)
GROUND
MANUAL PTT (i/p-HANDSET PTT)

### 2.3 ANTENNA DIPLEXER SECTION

### 2.3.1 GENERAL

The antenna diplexer section of the TC-900DR is a separate plug in module, that "piggy backs" the radio section PCB.

The diplexer performs two major tasks. Firstly it couples both the transmit and receive RF paths to the antenna while providing high isolation between them, and secondly it provides image and spurious rejection for each of these paths, with high $Q$ bandpass filters.

The isolation between the transmit side and the receive side is greater than 50 dB .
The diplexer consists of two teflon PCB's bonded together using a critical temperature and pressure process. The top and bottom outer layers are connected via brass eyelets, that are pressed through the PCB. This eliminates the need for through hole plating of Teflon, which requires the use of dangerous chemicals.

The design is essentially two continuous ground planes, filled in between, with laminate dielectric, and stripline filter tracks which are centrally located between these ground planes.

The etching of the filter tracks is closely monitored and controlled to ensure an accuracy of better than $0.001^{\prime \prime}$ in track width and spacing.

The diplexer has been factory tested to ensure bandpass and performance characteristics are met. The diplexer has approximately 3 dB of loss at 930 MHz and 2 dB of loss at 850 MHz .

This diplexer requires no alignment in the field.

### 2.3.2 INTERFACES

The antenna diplexer connects to the radio section via low loss coaxial cables and connectors, and to the units antenna via a SMA connector.

Two versions of the diplexer are available, depending on the transmit and receive frequencies used. The difference between the two is the loading of the SMA connector.

TYPE-A CONNECTIONS (Transmit frequency $=930 \mathrm{MHz}$ range)

DIPLEXER CONNECTOR
850 MHz port
930 MHz port
ANT port

SIGNAL DESCRIPTION AND DESTINATION
RF RECEIVE - RADIO SECTION X2
RF TRANSMIT - RADIO SECTION X4
ANTENNA

TYPE-B CONNECTIONS (Transmit frequency $=850 \mathrm{MHz}$ range)

DIPLEXER CONNECTOR
850 MHz port
930 MHz port
ANT port

SIGNAL DESCRIPTION AND DESTINATION
RF TRANSMIT - RADIO SECTION X4
RF RECEIVE - RADIO SECTION X2
ANTENNA

### 2.4 AUDIO HANDSET SECTION

### 2.4.1 GENERAL

Refer to diagram "MTCU HANDSET MAIN PCB \& MIC PCB CIRCUIT DIAGRAM", drawing number 5015-A200-50.

The handset provides an audio link between units, to assist in link setup and commissioning. It is not intended for general use and the equipment is not licensed for voice operation only.

Caution: When the handset is inserted into the TC-900DR, reliable data transmission or reception is not possible. Unintentional voice traffic on a point to multi point system may cause data corruption to other units.

The data transmission section of the modem is totally disabled, if the handset is plugged in when the TC-900DR is turned on.

The handset contains two PCB's, a receive board and a microphone board, which are connected by a 10 way ribbon cable. Acoustic padding is also included in the handset for improved performance.

The microphone board contains an ECM30 electret microphone, along with a common emitter preamplifier stage (Q1), to provide transmit voice audio.

There are four indication LED's that are not used by the TC-900DR.
The receiver board contains a 78 L05 5 V voltage regulator (REG1). This is used to supply power to the LF353 receive amplifier (U2-p7), which drives a DH32-30 ohm earpiece.

The sidetone circuit provided by U2-p1 is disabled and not used by the TC-900DR. Similarly, the LED drivers are disabled.

The PTT switch places a ground connection onto its output signal line, for processing by the radio section.

### 2.4.2 INTERFACES

The audio handset connects directly to the radio section via the RJ11 connector, X3. Attached to the handset is an 8 way flexible curly cord.
$\left.\begin{array}{lllll}\text { PIN NUMBER } & \begin{array}{l}\text { HANDSET } \\ \text { CONNECTOR }\end{array} & & \begin{array}{c}\text { X3 PIN } \\ \text { NUMBER }\end{array} & \end{array} \begin{array}{l}\text { RADIO SECTION } \\ \text { CONNECTOR X3 }\end{array}\right]$

### 2.5 MODEM SECTION

The modem section is built on a single PCB with approximate overall dimensions of $165 \mathrm{~mm} \times 152 \mathrm{~mm} \times 18 \mathrm{~mm}$.

It consists of the following main blocks :
Modem control

- DFM4-9 modem.
- Reset and watchdog.
- Memory.
- External NVRAM.
- External RAM.

Host interface.
Radio interface.
Transmit signal conditioning.
Receive signal conditioning.

- Data recovery.
- Clock recovery.

User indications.
Power supply
Interfaces.

- Radio section.
- Port A.
- Port B.
- Power.

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### 2.5.1 MODEM CONTROL

### 2.5.1.1 DFM4-9 MODEM

The modem section is controlled by a DFM4-9 Trio DataCom modem IC, (U5).
This device is specifically designed to provide data communications from a host computer over a radio channel.

The DFM4-9 is capable of full duplex operation, at data rates of 4800 baud or 9600 baud over the radio channel. The transmitter and receiver data rates may be set independently. The host computer interface provides two RS232 asynchronous serial ports, configurable for a variety of baud rates, and data formats.

In the standard delivery format of the modem, only one asynchronous serial port is operational. (Port A).

Advanced data recovery techniques are employed to ensure excellent performance in both good and noisy signal environments.

The data transmission method used, employs advanced optimal waveform shaping techniques. This maximises the recovered signal at the destination receiver, while remaining within the allocated RF channel bandwidths. The method uses computer generated Finite Impulse Response (FIR) techniques, to derive the transmitted waveform data.

The modem features a unique supervisory signalling channel, which embeds low speed data in the primary bit-stream, and is transparent to the user of the primary channel.

To drive the DFM4-9 modem clocking circuits, an external resonator is required. A 19.6608 MHz crystal (XTAL1) is applied to the OSC pins (U5-p9,10) of the device to achieve this.

A 4 way DIP switch is supplied to set up some configuration parameters of the modem. These are only read by the DFM4-9 at device power up. They connect to the "ESx" pins of the device (U5-p3,p5,p6,p7). Switches 1 and 2 are presently unused, switches 3 and 4 are defined in section 4.5.1.

### 2.5.1.2 RESET AND WATCHDOG

A MAX690 reset and watchdog IC (U3), is used to perform a variety of ancillary functions. This device provides a fixed length reset pulse for the proper initialisation of the modem chip on power up and reinitialisation. The MAX690 monitors the level of the VCC power supply line. If the voltage moves out of specification, the reset output is activated. This ensures that the modem chip recovers correctly in the event of a power failure. The reset signal is applied to the "RESET" pin of the modem (U5-p8).

The MAX690 provides a power monitoring function, which gives advance warning of imminent power supply failure. The DFM4-9 modem checks this signal, applied to its "PF" pin (U5-p2), before performing any transactions with the non-volatile memory, thus preventing accidental corruption of the contents of this memory. This "advance warning", is the length of time that the power supply capacitors hold their charge, after loss of power, before the Vcc supply rail drops below its cutoff level, and a reset pulse is generated.

The MAX690 also includes a "watchdog" timer. This timer must be strobed at a minimum rate, to prevent a reset pulse being generated. The DFM4-9 provides this signal at its "WDO" pin (U5-p22). Should the DFM4-9 modem operation go astray for some reason, it is probable that it will no longer perform this strobing function correctly. This condition is treated as irrecoverable and the MAX690 will timeout on its watchdog function and re-initialise the modem.

### 2.5.1.3 MEMORY

### 2.5.1.3.1 EXTERNAL NVRAM

The DFM4-9 modem, has a wide variety of configurable operating parameters, all of which are stored in an ST24C04 NVRAM IC, (U4). These parameters are read at power up, and determine the operating characteristics of the modem.

The NVRAM has 4096 bits of memory: It is accessed using the standard $I^{2} C$, two wire, bus interface. A feature of this particular device, is a write protect function for one area of the memory.

This write protect feature prevents configuration data being inadvertently corrupted should some anomaly in modem operation occur. A hardware signal line is used to override this write protection feature, so that the configuration data may be changed by manual means. This signal can be accessed via the front panel connector, and is used when the TC-DFM9IP modem programmer is connected.

### 2.5.1.3.2 EXTERNAL RAM

External RAM is used to store data frames.
The RAM used may be either a $6264-8 \mathrm{~K}$ or $62256-32 \mathrm{~K}$ byte IC (U9). The standard TC-900DR is supplied with an 8K package. The DFM4-9 modem, tests the size of the attached RAM on power up.

All of the externally connected RAM is used to store packet data, and is allocated evenly between transmit and receive data. This memory is connected to the modem chip, by an 8 bit bus, and 3 control lines.

Two 8 bit 74HC573 latches (U8 and U10), are used to latch the memory address off the bus, before the data read or write cycle. The read/write control line to the RAM, is passed as the top address line in the MSB address latch.

The RAM read cycle operates as follows :

- The modem sets the two latch control lines, LADR_EN and HADR_EN, high.
- The high-address/R_select is then placed on the 8 bit bus.
- The HADR_EN line is set low to latch the data into U8.
- The lower eight address bits are placed on the bus.
- The LADR_EN line is set to low to latch the data into U10.
- The modem bus port is set to input mode.
- The RAM CE line is set low.
- The modem reads the data off the bus.

The RAM write cycle operates as follows:

- The modem sets the two latch control lines LADR_EN and HADR_EN, high.
- The high-address $W_{\text {_ }}$ select is then placed on the 8 bit bus.
- The HADR_EN line is set low to latch the data into U8.
- The lower eight address bits are placed on the bus.
- The LADR_EN line is set to low to latch the data into U10.
- The modem bus port is set to output mode.
- The modem writes the data to the bus.
- The RAM CE line is set low to write the data into the RAM.


## Note: WARNING

A modem containing a $32 K$ RAM package will not be compatible with a modem containing an $8 K$ RAM package if end to end flow control is being used over the data link.

### 2.5.2 HOST INTERFACE

The host interface is provided by two RS232 ports, configured as DCE. These ports are presented to the user as 9 way female DMIN connectors, designated as PORT A and PORT B.

With the standard TC-900DR, only PORT A is operational.
The RS232 level translation is performed by two LT1081/MAX232 line transceivers (U1 and U 2 ). These require a single five volt supply, and include internal charge pumps to generator the required +10 V and -10 V rails.

The four input and four output lines implement one full duplex serial port with RTS/CTS/DTR and DCD. This is PORT A. A second full duplex port with no handshake lines is provided on PORT B.

### 2.5.3 RADIO INTERFACE

The interface to the radio is via a 26 pin PCB header connector, $X 4$.
The modem section has full control over the connected radio transceiver. It provides :

- Four lines for synthesiser control (used for RF channel selection).
- RSSI detection.
- Temperature sense input.
- Transmit power sense input.
- Temperature compensation for the synthesiser reference frequency.
- Receiver AFC.
- PTT control.
- Analogue lines for receive and transmit data signals.
- Regulated +13.8 V and +8 V power supplies.

Input to the receiver signal port, RXSIG, is offset by 2.0 V DC, with a signal level of $1 \mathrm{Vp}-\mathrm{p}$ AC.

The transmit signal output, TXSIG, has a signal level of $1 \mathrm{Vp}-\mathrm{p}$ for 4800 BPS , and $2 \mathrm{Vp}-\mathrm{p}$ for 9600 BPS , with a nominal DC offset of 2.0 V . This offset may vary by $\pm 1 \mathrm{v}$ according to the modulator temperature compensation requirements.

An ADC0834 four channel ADC (U6), is used to monitor various analogue quantities within the radio. The DFM4-9 modem communicates with the ADC by controlling 3 lines. An active high chip select, "ADCS" line (U5-p33), a data clock, "DCLK" line (U5-p35), and a serial data, "SD" line (U5-p36).

The state of the data line from the ADC is clocked into internal registers of the DFM4-9 on the rising edge of the clock line. The data stream consists of a four bit preamble, which includes the channel address. From the 5th clock pulse onward, the ADC drives the data line with the data of the conversion, MSB first. The transaction is terminated with the CS line being set to inactive low.

The first channel is used to monitor temperature, by measuring the voltage from an LM335 monolithic temperature sensor U6. The LM335 is situated in the radio section, adjacent to the 20.1666 MHz XTAL and VCXO synthesiser reference oscillator, and is fed into the modem section via connector X4-p14, ADC0.

The second channel is used to monitor RSSI, by measuring the RSSI output of the NE615 IF circuit. This signal is fed to the modem section from the radio section via connector X4-p21, ADC1.

The third channel is used to monitor the power level output by the RF transmitter, by measuring a voltage derived in the power control section of the radio. This is used to determine the "health" of the radio transmitter. This signal is fed to the modem section from the radio section via connector $\mathrm{X} 4-\mathrm{p} 9, \mathrm{ADC2}$.

The fourth channel of the ADC, is used to measure the voltage of the +13.8 volt supply rail and to sense the presence of the audio handset at power up. The handset derives microphone bias from the modulator stage, and the voltage at this point is measured and compared with a fixed nominal value, to determine if the handset is connected at the time of TC-900DR power up. This signal is fed to the modem section from the radio section via connector $\mathrm{X} 4-\mathrm{p} 24$, ADC3. This 4 th $A D C$ channel is also multiplexed to measure the AFC control voltage so that an indication of received signal frequency can be made. U14:D is used to perform this switching function.

An auxiliary latch (U11) is provided to supply some of the output control to the radio section.

The latch receives data from the same data buss as the RAM. The lower six bits are fed to an R/2R ladder network DAC (RN2), which is used to present an analogue voltage to the radio's local oscillator synthesiser frequency reference. This correction voltage provides for excellent temperature stability of the radio. This signal is fed to the radio section via connector X4-p15, TEMP COMP.

The two top bits of the latch, drive auxiliary functions within the radio section.
Bit 6 is used to control the power of the RF transmitter in the radio section. This can be set to a HIGH level of 1 W , or to a LOW level of 200 mW . This signal is fed to the radio section via connector X4-p10, TXPWR.

Bit 7 provides the RF transmitter enable signal to the radio section. No RF signal can be transmitted unless this signal is set to active. This signal is fed to the radio section via connector X4-p11, TX EN.

### 2.5.4 TRANSMIT SIGNAL CONDITIONING

The transmit section of the DFM4-9 modem, outputs a byte of data, four times per bit period, on the "TDx" pins (TD1..TD7, U5-p56..49).

The parallel data is presented to an eight bit R/2R ladder network (RN1). This is a simple DAC which produces the transmit waveform at its output.

This signal is fed into opamp (U13:C) for amplification and filtering. This stage is a single pole low pass filter, used to attenuate clocking noise in the waveform. Two more filter stages follow, U13:B and U13:D.

By using 4 samples per bit, and an 8 bit resolution, precise control of the waveform shape is possible.

The gain and pole frequency of amplifier stage U13:C is switched by the DFM4-9 modem, via a 74 HC 4066 CMOS FET switches (U14:A). This is to produce the required waveform for the two data rates currently available. The bit rate output signal, "BRO" is provided at U5-p44.

For 4800 baud, components C43 and R45, are "included" in the feedback loop of the amplifier stage. When 9600 baud is selected, switch U14:A is turned OFF, and the components are "excluded" from the circuit.

### 2.5.5 RECEIVE SIGNAL CONDITIONING

The data receiver, consists of several functional blocks. Some of these are implemented by internal functions of the modem IC, and the remainder by external circuitry.
The incoming analogue signal, is routed to two separate sections of circuitry. One to process the received clock, the other to process the received data.

### 2.5.5.1 DATA RECOVERY

The data recovery is based around an "Integrating Data Slicer" circuit.
This circuit consists of a non-inverting, resetable integrator (U16:A, U12:C and U15:D), a dual peak detector ( $\mathrm{U} 12: \mathrm{A}, \mathrm{B}$ ) and a reference divider.

The received signal is passed into the modem section from the radio section via connector X4-p20, "RXSIG".

The signal is integrated by the non-inverting integrator formed by $U 16: A$, and $U 12: C$, and then forwarded on to a comparator ( $\mathrm{U} 7: \mathrm{B}$ ), where it is "squared up", ready to be read by the DFM4-9 modem.

An output signal is provided by the modem IC, to indicate the sampling point. In fact this signal, called "RxCLKOUT", is pulsed high immediately after the sampling operation has taken place.

The integrator is reset at the end of each bit period, by the 74 HC 4066 FET switch, U15:D, after the value of the bit has been read. The DFM4-9 provides this reset signal at the reset integrator "RxCLKOUT" pin (U5-p19).

The integrated receive signal, is then fed to the dual peak detector, where the positive and negative peaks of the integrated signal are detected, and stored on the capacitors C28 and C27.

The peak detector's attack time is determined by the output resistance of the opamps (U12:A,B) and the bulk resistance of the diodes (D7, D4). The decay time however is determined by the values of the hold capacitors (C28, C27) and the summing resistors (R24, R25).

Four diodes (D5, D6, D8, D9) are used to clamp the reference rail. If the incoming signal has a large DC shift, this clamping arrangement ensures that the data slicer reference level is quick to settle somewhere near its final operating point. This clamp however does impose a maximum allowable input signal level. Exceeding this level will cause the integrated signal to directly modulate the reference rail. The derived reference voltage level, is amplified and output back to the radio section, where it is used for AFC in the receiver.

### 2.5.5.2 CLOCK RECOVERY

The received clock signal is presented to the DFM4-9 modem at its "RXCLK" input (U5-p4).
Within the DFM4-9, a phase-locked-loop is used for data clock recovery, which relies on level transitions in the data signal.

This mechanism maintains the data sampling point in the center of the bit cells by comparing the signal's level transitions with an internal clock.

An error in the relative phase of the RXCLK signal and the internal clock, causes the internal clock to increase or decrease in speed, to bring the phase error to zero.

The phase-locked-loop clock recovery mechanism within the DFM4-9 modem, maintains the sampling point in the center of the bit cells, but the use of the integrator demands that this take place at the end of the bit cell. This means that the signal fed to the DFM4-9 modem RXCLK input must be delayed by half a bit period.

To obtain this, the received signal is passed through a half bit delay, low-pass filter (U16:D, U12:D, U7:A). The delay characteristics of this filter, are switchable between the available data rates of 4800 and 9600 baud operation, by five 74 HC 4066 FET switches. These switches are controlled by the "BRO" output of the DFM4-9.

### 2.5.6 USER INDICATIONS

There are four indication LED's supplied for user information. POWER, TXMIT, SYNC and RXSIG. The POWER LED is green, TXMIT LED is red and the other two are yellow.

The POWER LED (LED4), is driven from the 13V8 power supply line. When supply is present the LED is activated.

The TXMIT LED (LED3), is activated when PTT is present. It is driven when the switching transistor Q3 is turned ON by the DFM4-9 modem "PTT" output going active (UX3-p38).

The SYNC LED (LED2), is activated when a valid data stream has been detected. It is driven when the switching transistor Q2 is turned ON by the DFM4-9 modem "SYNC" output going active (U5-p43).

The RXSIG LED (LED1), is activated when the received signal level is at a usable level. It is driven when the switching transistor Q1 is turned ON by the DFM4-9 modem "RXSIG" output going active (U5-p43).

### 2.5.7 POWER SUPPLY

The power supply is based around the use of three voltage regulators that supply +13 V 8 , +8 V and +5 V .

The incoming power is applied to a bridge rectifier (BR1). Normally two legs of this bridge are linked out, so it provides only reverse polarity protection shunt diodes. A special manufacturing option allows for $A C$ input, where the links are removed. A 2200uF electrolytic capacitor (C2), provides filtering for $A C$ inputs.

This is then applied to an LT1086 low dropout regulator (REG1). The output of this is set to 13 V 8 and feeds the RF final amplifier, and the following two regulators.

The 8 V regulator (REG2) takes it's input directly from the 13 V 8 rail, its output is routed to the radio section, and provides supply for one of the amplifier devices.

The 5 V regulator (REG3) provides the supply rail for the modem section logic circuits. It takes it's input from the 13 V 8 rail via diode D1. Extra filtering capacitance is provided by C7.

### 2.5.8 INTERFACES

### 2.5.8.1 RADIO SECTION

The modem section interfaces to the radio section via connector JX3. The physical link between the two sections is achieved via a 90 mm length of 26 way ribbon cable.

Refer to interface diagram "RADIO MODEM INTERFACE", drawing number TC01-05-18 sheet $1 / 3$.

## CONNECTOR JX3

SIGNAL DESCRIPTION
PIN NUMBER

| 1 | 13V8 POWER SUPPLY RAIL |  |
| :---: | :---: | :---: |
| 2 | 13V8 POWER SUPPLY RAIL |  |
| 3 | 13V8 POWER SUPPLY RAIL |  |
| 4 | GROUND |  |
| 5 | GROUND |  |
| 6 | GROUND |  |
| 7 | 8V POWER SUPPLY |  |
| 8 | 8V POWER SUPPLY |  |
| 9 | ADC2 | (i/p - TRANSMIT POWER SENSE) |
| 10 | TXPWR | (o/p - TRANSMIT POWER LEVEL) |
| 11 | TXXEN | (o/p - TRANSMIT ENABLE) |
| 12 | /PTT OUT | (o/p - PRESS TO TALK) |
| 13 | TXSIG | (o/p - TRANSMIT DATA) |
| 14 | ADC0 | (i/p - TEMPERATURE SENSOR) |
| 15 | TEMPCOMP | (o/p- TEMPERATURE COMPENSATION) |
| 16 | EN | (o/p - ENABLE FOR SYNTH) |
| 17 | DA | (o/p - DATA FOR SYNTH) |
| 18 | CK | (o/p - CLOCK FOR SYNTH) |
| 19 | LD | (i/p - LOCK DETECT FROM SYNTH) |
| 20 | RXSIG | (i/p - RECEIVED DATA) |
| 21 | ADC1 | (i/p - RSSI SIGNAL) |
| 22 | AFC CTL | (o/p - AFC CONTROL) |
| 23 | SPARE | (UNUSED) |
| 24 | ADC3 | (FOR SUPPLY/HANDSET) |
| 25 | TEST1 | (UNUSED) |
| 26 | TEST2 | (UNUSED) |

### 2.5.8.2 PORT A

The modem section interfaces to the host user via the 9 way female DMIN type connector JX1.

## CONNECTOR JX1 SIGNAL DESCRIPTION

PIN NUMBER

| DATA CARRIER DETECT | (DCD) |
| :--- | :---: |
| RECEIVE DATA OUTPUT | (RXD) |
| TRANSMIT DATA IN | (TXD) |
| DATA TERMINAL READY | (DTR) |
| COMMON | (COM) |
| DATA SET READY/prog mode | (DSR) |
| REQUEST TO SEND | (RTS) |
| CLEAR TO SEND | (CTS) |
| RING INDICATE/BER Test Mode | (RI) |

Note: Pin 6 and pin 9 provide a dual function which depends on the mode that the TC-900DR is operating in.

### 2.5.8.3 PORT B

For the standard delivery version of the TC-900DR, port $B$ is normally not enabled. This port provides no handshake lines except DCD (parallel connected with DCD on Port A) and DSR which is wired active.

## CONNECTOR JX1 <br> PIN NUMBER

1
2
3
4
5
6

7
8
9 RECEIVE SIGNAL STRENGTH INDICATOR (RSSI)

Pin 9 is used to output the RSSI signal for external measurement.
The RSSI output ranges from 0 to 5 Volts, where 5 volts indicates the strongest signal. It is important to note that this port output has a high impedance of around 50 K ohms and loading will decrease accuracy of the recorded measurement.

### 2.5.8.4 POWER

Power is supplied to the modem section via connector X 1 . Typically +13.8 V DC is applied to the top pin, with the common connected to the bottom pin.

## SECTION 3

## OPERATIONAL DESCRIPTION

## 3 OPERATIONAL DESCRIPTION

### 3.1 GENERAL

The Trio DataCom TC-900DR radio modem, is a full duplex 4800/9600 bits per second device, which converts digital data into an analogue form suitable for transmission over a radio channel. It uses specially filtered direct binary frequency modulation techniques to achieve this. It conversely, converts the analogue signal derived from a radio channel into a digital data signal.

The heart of the unit is the DFM4-9 modem IC. This performs all waveform shaping, randomising and de-randomising, NRZ/NRZI conversion, clock recovery, and HDLC framing and CRC error generation and checking. These functions are performed simultaneously, allowing full duplex operation at up to 9600 bps .

The modem is fully HDLC compatible. The user is provided with two RS232 compatible ports, which may each be configured with a standard PAD interface or SLIP/KISS protocol driver. The unit may also be configured for repeater operation.

It may be configured to use RS232 handshake lines, or XON/XOFF flow control on Port A.

The modem features a unique supervisory signalling channel, which embeds low speed data in the primary bit-stream, and is transparent to the user of the primary channel.

The supervisory signalling channel can be disabled if not required. It could be used to pass low speed data such as $E$ and $M$ status or CIDSMA control schemes.

The data rate of the supervisory signalling channel can be set independently for transmit and receive. It can range from about 40 to 533 bps with the primary channel rate at 4800 baud, and 80 to 1067 bps at a primary channel rate of 9600 baud.

NOTE: with the supervisory signalling channel active, the bit-stream is not compatible with standard HDLC interface devices (such as 8530).

The host user port may be configured for baud rates of 300 to 19 K 2 , with 7 or 8 bit character size, 1 or 2 stop bits, and parity off/odd/even.

The DFM4-9 modem includes several data tables which are used to generate waveforms with different characteristics. This is primarily for optimum performance at differing baud rates. A custom data table can be placed into the NVRAM of the modem, for specialised applications.

Configuration of the modem is fully programmable, with parameters held in non-volatile memory. All configuration parameters are accessible with the TC-DFM9IP Installation Program.

Configuration parameters include but are not limited to:
Supervisory Signalling Channel rate.
XON/XOFF or RTS/CTS/DTR/DCD handshake mode.
Default transmitter lead in delay.
Constant specifying minimum RF RSSI for valid receive.
Constant specifying minimum Tx power level.
Asynchronous serial port parameters.
User interface operating mode :

- User port interface protocol
- PAD Parameters


### 3.2 TC-900DR MODEM FIRMWARE REVISION VA2.3.0

### 3.2.1 FUNCTIONAL CHANGES AND ADDITIONS

The Diagnostics "M" command (serial port Mode) completed. The implementation of this command was not finished in time for VA2.2 release. This command is used to configure either of the two user ports, for character length, number of stop bits, parity odd/even/off.

1 Bit 7 is used to address which port is being referenced (set to " 0 " for Port $B$, or set to "1" for Port A).

2 Bit 6 determines the character size. Set to " 0 " for 8 bit, or "1" for 7 bit character size.

3 Bit 5 is set to " 1 " to enable parity, " 0 " to disable parity.
4 Bit 4 determines Odd (set bit to "1"), or Even (set bit to " 0 ") parity if Bit 5 is set.
5 Bit 3 determines the number of stop bits. Set to " 0 " for 1 stop bit, or set to " 1 " for 2 stop bits.

6 Bits 2, 1, and 0 are used to select the baud rate. The following table shows the available rates. The 19.2 K baud selection should only be made for Port A if Port $B$ is disabled. The last selection of 110 baud may be deleted from future firmware revisions.

| Bit | Bit 1 | Bit 0 | Baud Rate |
| :---: | :---: | :---: | ---: |
| 0 | 0 | 0 | 300 |
| 0 | 0 | 1 | 600 |
| 0 | 1 | 0 | 1,200 |
| 0 | 1 | 1 | 2,400 |
| 1 | 0 | 0 | 4,800 |
| 1 | 0 | 1 | 9,600 |
| 1 | 1 | 0 | 19,200 |
| 1 | 1 | 1 | 110 |

Channel Access Strategy 3 is now defined. This is selected by setting bits 1 and 0 (TxCtrl1 and TxCtrl0) in "Config1", both to "1". This mode forces a randomly generated delay before transmission begins, even if the channel is perceived to be clear. This delay mechanism is similar to that used in Channel Access Strategy 2 when the channel is perceived to be busy. This operating mode is useful in systems that include remote terminals that generate reports at regular fixed intervals. In such a system, slight differences in this interval between two remotes, would cause them to become synchronised for some time, and thus transmissions from them would consistently
collide. Inserting a randomly generated delay before all transmissions will reduce the incidence of this effect.

The RS232 DCD handshake line now becomes active only during output of received data. Formerly, the DCD line indicated real time SYNC status of the modem data receiver. To facilitate the use of RS232 to RS422/RS485 converters, the DCD line is driven active a short time (approximately 0.5 mS ) before the received data is output to the user port, and lingers for approximately 2 to 3 character times (i.e. is proportional to baud rate of user port). The modem generates only one DCD function, which is available on pin 1 of both Port A and Port B. Thus the DCD pin of both user ports will be activated when either port is outputting received data.

### 3.2.2 OTHER ENHANCEMENTS

Improvements in handling of the RS232 RTS line (Port A), makes the modem more tolerant in the timing of rapid OFF transitions of this handshake line, immediately after the end of the last character of a message. It has been observed that communications drivers in many PLCs turn their RTS output line OFF very shortly after the end of a message, resulting in the loss of the last character of the message with previous modem firmware revisions. This revision does not suffer this problem.

The random number generator used for the Channel Access Timer, has been improved to make it more random.

### 3.3 FACILITIES AND CONFIGURATION INFORMATION FIRMWARE VERSION 2.2

### 3.3.1 GENERAL

The TC-900DR provides fully transparent remote diagnostics facilities, and expanded data stream switching, which supports advanced stream trunking applications.

The diagnostics core, supports the reporting of current analogue conditions, including temperature, RSSI (Received Signal Strength Indication), RF transmitter power, AFC (i.e. received signal frequency offset), and supply voltage. Also, an extensive range of operating parameters may be changed remotely, including remote (RF) channel change.

Configuration options, allow various system topology's, so that the location of the system's diagnostics controller is flexible.

The data stream switching mechanism has been upgraded to allow either MUX/DeMUXing or multi-stream routing functions, independently for each port.

A few other minor upgrades to previous revisions of firmware are:

* Two different "ticker clocks" implemented, one running at 1 mS , and used for a) PAD Character Input Timers, and b) Channel Access Timer when running in Collision Avoidance mode. The other "ticker clock" runs at 10 mS , and is used for the PTT timer, and a host of other internal functions, not accessible by configuration programming.
* When XON/XOFF flow control is enabled on PortA, the CTS output line continues to operate correctly, indicating the flow control state. XON/XOFF characters are generated in addition to, and reflect state changes on this line. As before, the DTR input line is ignored while XON/XOFF flow control is set, and the RTS line is not required to be true to validate transmit data.
* The modem stores data for transmission in buffer memory, which is limited. It also keeps track of frame boundaries of the stored data, and the number of frames it can manage is also limited by the amount of memory used to record the position of the frame boundaries. Thus it is possible that the modem can approach overflow before exhausting data buffer space, if frames are small. This flow control state is activated when the "frame boundary memory" approaches half full, for similar reasons used in data buffer management.
* If the Supervisory Signalling Channel is enabled in both transmit and receive directions, and PortA is configured in Repeater Mode, then the received Supervisory Signalling Channel data is also repeated, by being copied from the Supervisory Signalling Channel receiver to the Supervisory Signalling Channel transmitter.
* RSSI measurements are full eight bit conversion, so the "min_RSSI" configuration parameter lies in the range $0-255$ (decimal). This is only important when setting this parameter without the aid of the DRPROG programmer.


### 3.3.2 INTERNAL DATA STREAM ROUTING

Essentially, all data streams travelling in both directions (transmit and receive), are examined and tested for a match with the diagnostics receive SID header code. If this match test is successful, then the data frame is copied into a buffer for the diagnostics core to process. The data frame also continues in the original direction as well. Thus diagnostics frames received from the radio channel (receive data), and from the stream switcher (transmit data, from one of the physical ports), are copied as they pass between the HDLC "device" and the data stream "switcher". Messages generated by the diagnostics core in response to received commands, are always sent back to the source of the command. That is, if a status request is received from the radio channel side of the modem, then the response is directed back out of the radio channel.

This dual access structure, allows the diagnostics controller to be located on either side of the modem, and thus supports any system topology.

### 3.3.3 DIAGNOSTICS REPEAT FUNCTION

Some applications will require that the "base" unit in a point to multi-point system repeats diagnostics frames. This will be the case where the system diagnostics controller is attached to a remote terminal in the system, and polls the system population from this point. The "base" unit must re-transmit diagnostics frames which are not addressed to itself. A "diagnostics repeat" configuration bit enables this function.

### 3.3.4 DIAGNOSTICS FRAME STRUCTURE

Diagnostics data frames, are structured according to a defined protocol. A frame consists 1st of the SID header code, which would normally (but not necessarily) be 00 . Following this is a three byte address of the destination unit, followed by a three byte source address. An addressed unit responding to a diagnostics command, will swap these two address fields around, in the response frame. The destination address in a diagnostics frame to a TC-900DR unit, is in fact the unique (factory) serial number of the unit. By convention, the diagnostics controller (a DOS based PC), will use a unique address for itself, outside the range of permissible TC-900DR addresses (e.g. 000000). Following the two address fields, is a single character command/response code, which is in turn followed by any operands that may or may not be required for the command/response. Total frame size is limited to 17 bytes. After the SID header, address fields, and command/response mnemonic, this allows up to nine bytes of data to be transferred per diagnostics frame.

### 3.3.5 DIAGNOSTICS COMMAND SET

The following is a list of the command set recognised by the diagnostics core in the TC-900DR Firmware. Also is tabulated the response to each command. The following examples use address 123456 for the TC-900DR unit address, and 000000 for the address of the system diagnostics controller. For the purposes of clarity only, each byte in the example messages is separated by a comma. Mnemonics are represented in quoted form to indicate an ASCII character (e.g. "C" is actually binary byte h'43).

## B Warm Boot Command.

This command forces the addressed unit to perform a "warm boot". Previous to this, the unit will have been halted (see " H " command), and one or more parameters changed with "P" and "W" commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " B "$
Response:- $\quad 00,00,00,12,34,56, " b "$

## C Calibration Constant Poll.

This command requests the addressed unit to reply with it's internal Analogue To Digital Converter (ADC) calibration constants. These are necessary to accurately interpret the data sent in Status Poll ("S") replies. This command has no operands, and the response mnemonic is " $c$ ". The form of the command and reply is:

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " C "$
Response:- $\quad 00,00,00,12,34,56, " c ", t t, r r, p p, f f, s s$
Where:-
$\mathrm{tt}=$ Temperature calibration code
rr = RSSI calibration code
pp = Transmit Power calibration code
$\mathrm{ff}=$ Received Frequency Offset calibration code
ss $=$ Power Supply calibration code

## D Powered Up Response

This command is sent from the modem to the controller in response to a status poll ("S") immediately after the modem has been powered up. The modem will continue to send this command in response to a status poll until the controller acknowledges the command with a "d". The modem will then respond normally to a status poll.

This mechanism is used by the controller to determine whether it requires calibration data from the modem.

Syntax:-
Command:- $\quad 00,00,00,12,34,56$ "D $^{\prime \prime}$
Response:- $\quad 12,34,56,00,00,00 " d "$

## F Set New RF Synthesiser Frequency.

This command forces the unit to set the RF synthesiser to a new frequency, thus selecting another radio channel. This command has one operand, which defines the source of the synthesiser data. A value of zero, indicates that the frequency data has already been set with a parameter set command. Values from one to four select one of the channels stored in the NVRAM of the modem configuration. The addressed unit responds with an " $f$ " reply, before executing the channel change command (i.e. on the old channel).

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " F ", n n$
Response:- $\quad 00,00,00,12,34,56,{ }^{\prime \prime} f^{\prime \prime}$
Where:-
$\mathrm{nn}=00$ to 04 to select data source .

## H Halt Command

This command forces the addressed unit to halt all internal operations, except diagnostics processing. This is necessary, when changing some parameters, before a warm boot command is issued to the re-configured unit.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " H "$
Response:- $\quad 00,00,00,12,34,56, " h "$

## M

Set Serial Port Mode.
This command forces the addressed unit to change the operating mode of one or both serial ports. Parameters such as character size, number of stop bits, parity etc. are changed with this command. It should be noted, that data may be lost while the operating mode of the serial ports is changed.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " M ", x x$
Response:- $\quad 00,00,00,12,34,56, " m "$
Where:-
$\mathrm{xx}=$ Serial port address bit and mode data

## P Parameter Set command.

This command stores the contents of the operand string to a storage buffer. No other action is taken. This command should be immediately followed by a "W" command. See "W" command below. The parameter may be either a bit quantity, a byte quantity, a word quantity, or a string quantity. The diagnostics core in the modem firmware determines this from the parameter indentifier, which indexes an internal lookup table. String quantities are of indefinite length, and determined by the length of the operand string in the received "P" command. The "P" command response ("p"), echoes the complete received string. This is unique to the " P " and " W " commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " P ", n n, a a, b b, c c, \ldots$
Response:- $\quad 00,00,00,12,34,56, " p ", n n, a a, b b, c c, \ldots$
Where:-
$\mathrm{nn}=$ parameter identifier
$\mathrm{aa}, \mathrm{bb}, \mathrm{cc}, \ldots$ are data value(s) for selected parameter

## R Parameter Readback command

This command forces the addressed unit to read the state of the addressed parameter, and send this data back the the command originator (diagnostics controller) in a reply message. Again the size of the parameter (bit, byte, word, or string) is determined by the parameter identifier. String parameters are returned as a string of eight consecutive bytes.

Syntax:-
Command:- 12,34,56,00,00,00,"R",nn
Response:- 00,00,00,12,34,56,"r",nn,aa,bb,...hh

## S Status Poll

This command requests the addressed unit to reply with the current value of analogue quantities, present temperature, last/present received RSSI, transmit power of last transmission, received frequency offset of last/present received signal, and present supply voltage.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " S "$
Response:- $\quad 00,00,00,12,34,56, " s ", t t, r r, p p, f f, s s$
Where:-
$\mathrm{tt}=$ Temperature conversion code
rr = RSSI conversion code
$p p=$ Transmit Power conversion code
ff $=$ Received Frequency Offset conversion code
ss = Power Supply conversion code

## T Diagnostics Watchdog Timer command.

This command forces the addressed unit to (re)set a special watchdog timer. The operand value is a word (16_bit) quantity. A zero value will disable the timer. A non-zero value will initialise the timer. This timer, while non-zero, will be decremented periodically. If the timer is decremented to zero, then the TC-900DR will perform a cold boot, thus restoring operating parameters from the NVRAM configuration memory. This command should be used in conjunction with parameter set and write commands. If a parameter change renders the unit in-operable, then either it will not continue to receive further " T " commands to reset the timer, or the system diagnostics controller may cease to send the timer reset commands, thus will eventually cause the unit to cold boot.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " T ", n n n n$
Response:- $\quad 00,00,00,12,34,56, " t "$
Where:-
nnnn = timer reset value (16 bit value)

V Request Firmware Version String command.
This command requests the addressed unit to reply with a string indicating it's firmware version number. Future firmware versions may provide further facilities that may then be used, by sending appropriate commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " V "$
Response:- 00,00,00,12,34,56,"v","A2.2.0"

## W Write Parameter command.

This command is used in conjunction with the "P" parameter set command. This parameter write command must be identical to the previous parameter set command. Providing they are identical (excepting the command mnemonic), then the operand is written to the selected modem operating parameter. Changing some parameters while normal operation continues could produce improper operation, possibly resulting in corrupted parameters, so the unit should be halted with a HALT command before such parameters are changed.

Syntax:-
Command:- $\quad 12,34,56,00,00,00$, ' $W$ ', nn, $a a, b b, c c, \ldots$
Response:- $\quad 00,00,00,12,34,56, " w ", n n, a a, b b, c c, \ldots$
Where:-
nn = parameter identifier
$a a, b b, c c, \ldots$ are data value(s) for selected parameter

### 3.3.6 PARAMETER SET

The following is a list of parameters which may be remotely set. Parameters marked with a "*", should only be changed while the unit is in a halted state, followed by a warm boot command. Parameters marked with a "\#", may only be referenced in an "R" readback command. Attempts to change these with " P " and " W " commands may produce unpredictable results.

| Parameter Identifier | Parameter Type(Size) | Parameter Name |
| :---: | :---: | :---: |
| 00 (^@) | undefined | not defined, reserved to facilitate future expansion |
| 01 (^A) | undefined | not defined, Trio DataCom test use only |
| 02 (^B) | byte | Drift_Offset |
| 03 (^C) | word | PTT_Time |
| 04 (^D) | string | Synthesiser Data for channel change |
| 05 (^E) | byte | min_RSSI |
| 06 (^F) | byte | Tx_LID |
| 07 (^G) | byte | Slot_Num |
| $08(\wedge)$ | byte | Slot_Time |
| 09 (^1) | word | SIDA1 and SIDA2 |
| OA (^J) | word | SIDB1 and SIDB2 |
| OB (^K) | word | SIDD1 and SIDD2 |
| OC ( ${ }^{\wedge}$ ) | byte | KISS_adrA |
| OD (^M) | byte | KISS_adrB |
| 0 E (^N) | byte | EOMA_code |
| $0 \mathrm{~F}\left({ }^{\wedge} \mathrm{O}\right)$ | byte | EOMB_code |
| 10 (^P) | byte | input_timeA |
| 11 (^Q) | byte | input_timeB |
| 12 (^R) | byte | frame_sizeA |
| 13 (^S) | byte | frame_sizeB |
| 14 (^) | bit * | SLIP/KISS_mode portA |
| 15 (^U) | bit* | SLIP/KISS_mode portB |
| 16 (^V) | bit | EOM_enable portA |
| 17 (^W) | bit | EOM_enable portB |
| 18 (^X) | bit * | KISS_mode portA |
| 19 (^Y) | bit * | KISS_mode portB |
| $1 \mathrm{~A}{ }^{\wedge} \mathrm{Z}$ ) | bit | RTS/CTS_interlock portA |
| 1 B ( ${ }^{\text {l }}$ ) | bit * | PORTB_enable |
| 1C (^) | bit * | Repeat_Enable portA |
| 1D (^) | bit * | Repeat_Enable portB |


| 1 E (^^) | bit * | (Not defined, reserved for Error Recovery Enable) |
| :---: | :---: | :---: |
| 1 F (^) | bit * | (Not defined, reserved for Error Recovery Enable) |
| 20 () | bit | LiveFrame porta |
| 21 (!) | bit | LiveFrame port |
| 22 (") | bit | XonXoffMode port |
| 23 (\#) | bit | XonXoffMode portB |
| 24 (\$) | byte | PORTA_Config |
| 25 (\%) | byte | PORTB_Config |
| 26 (8) | bit | diags_repeat |
| 27 (') | bit | TxPWR_HI/LOW |
| 28 () | bit | SID_Enable |
| 29 ()) | bit | RTS2PTT |
| 2A (*) | bit | SYNC2PTT |
| 2B(+) | bit | SCDO_Default |
| 2C() | bit | SupChnFunc |
| 2D (-) | bit | TxCtrl1 |
| 2 E (.) | bit | TxCtrI0 |
| $2 \mathrm{~F}(\mathrm{n}$ | byte | Config1 |
| 30 (0) | byte \# | SMR1 (portA serial port mode) |
| 31 (1) | byte \# | SMR0 (portB serial port mode) |
| 32 (2) | byte \# | BRR1 (portA serial port baud rate) |
| 33 (3) | byte \# | BRR0 (portB serial port baud rate) |
|  |  | Additions for version A2.3.0 |
| 34 (4) | byte | err_limit (Frame Error output for Base Station) |
| 35 (5) | byte | err_flags |
| 36 (6) | word | good_cnt |
| 37 (7) | word | bad_cnt |
| 38 (8) | word | lost_sync_cnt |
| 39 (9) | word | lost_RSSI_cnt |
|  |  | Additions for version A2.3.1 |
| 3A (:) | byte | DCD_timeA |
| 3B (;) | byte | DCD_timeB |
| 3 C (<) | byte | Diags_Delay |

### 3.3.7 ADVANCED STREAM ROUTING FUNCTIONS

The TC-900DR provides advanced stream routing functions. For each port, there is allocated two SID (Stream IDentifier) codes, and a configuration flag that determines how these two codes are used.

With the flag off, SIDx1 (where x is A or B for portA and portB respectively) defines the SID code of received frames that are de-multiplexed to the port, and SIDx2 defines the SID code that is inserted by the modem at the front of every frame it transmits. Thus only one data stream passes through the port, and the modem manages the insertion and extraction of SID header codes.

With the configuration flag on, SIDx1 and SIDx2 define a range of streams that will be passed from the received data to the port. SIDx1 defines the lowest stream, while SIDx2 defines the highest stream. The SID header codes remain on the received frames, and are passed to the port. For transmit data, the modem assumes that the SID header codes are already in place, being inserted by some external device, and no processing is performed on the transmit data. For this application, it is highly desirable that a SLIP (or KISS) driver be employed so that frame boundaries are defined.

These functions are independent for each port, so it is possible to construct (say), a multi-drop, multi-hop repeated data system, where one stream can be "peeled off" at each repeater site. There are many other possibilities, the TC-900DR product simply requiring suitable configuration to construct a vast range of network topologies.

### 3.4 FACILITIES AND CONFIGURATION INFORMATION VERSION 2

### 3.4.1 GENERAL

The TC-900DR, provides two independent user data streams, which are multiplexed onto the radio channel data stream. The stream switching protocol also provides for an embedded remote diagnostics facility.

The two (asynchronous) user ports can be configured for a variety of baud rates, character sizes, parity, and stop bits.

Flow control on user Port_A may be set to use RTS/CTS/DTR/DCD handshake lines, or XON/XOFF characters. Flow control for Port_B may be set to use XON/XOFF characters, or no flow control. Port_B is not supported by RTS/CTS/DTR handshake lines.

Data is transported in (HDLC) frames, protected by a 16 bit CRC error checking sequence, conforming to the CCITT standard. Received frames found to contain errors are discarded. The TC-900DR does not release received data frames to the user port, until completely received, and error checked.

Maximum frame size is configurable for each port independently, and may be set to any value between 4 and 255 . Frame size limiting is disabled by setting this parameter to zero (0).

Each user port, is supported with PAD functions conforming to $\times 3$, or SLIP*1 or KISS* protocol interface.

For Point To Multipoint applications, a unique collision avoidance mechanism is available, with configurable channel access parameters.

All configuration parameters are held in a non-volatile memory. Normally, this memory can only be written when the radio modem is connected to a programmer.

### 3.4.2 BRIEF OVERVIEW OF MODEM INTERNAL OPERATION.

### 3.4.2.1 DATA TRANSMITTER

Each physical user port, is supported by a "driver", in this case a PAD (Packet Assembler/Dis-assembler) or SLIP/KISS. This function transfers the data from the port, to a buffer memory. This buffer not only stores the raw user data, but also keeps track of frame boundaries. Another functional block, retrieves that stored data, and feeds it to a third mechanism, which generates the data waveform which is applied to the radio transmitter modulator.

[^8]
### 3.4.2.2 DATA RECEIVER.

The receiver extracts data frames from the received signal, and stores the contents of the frames into buffer memory. It may also perform a steering function, if more than one port is enabled. A second function is to retrieve the stored data, and send it to the user port(s), consistent with some flow control regime.

### 3.4.3 SELECTING FRAME SIZE

The selection of maximum frame size is a compromise between channel through-put and data propagation time over the link.

The receiving modem collects and stores the incoming data frame, and on detecting the end of the frame, checks if an error has occurred. If not, then the stored data is released for transfer to the user data port. If an error has occurred, then the stored data is "flushed" from the data store. Thus a delay is introduced between the time the frame data begins to enter the destination radio modem, and the time this data begins to emanate from the user port. This delay is effectively the length of the data frame, which consists of the user's data, plus the framing overhead. This overhead will include at least 24 bits for the HDLC Flag and FCS (error checking data), plus another 8 bits if SID (Stream IDentifier) codes are enabled (refer to detailed description elsewhere in this document), plus the duration of the transmitter Lead-In-Delay, if the radio transmitter had to be started up to send the data. Thus larger frames reduce the proportional overhead, but increase the end to end propagation delay.

On the assumption that the radio transmitter was already on, and that the frames include the SID header, then every frame includes 32 bits of overhead.

Assuming that the user port is configured for 8 bit character size ( 8 bit data no parity, or 7 bit data and parity), and 1 stop bit, then each character is carried as a 10 bit sequence on the asynchronous user channel. On the radio channel data stream, user data is stripped of the start and stop bits used on the asynchronous user port, and transmitted as eight bit "octets", and so the character rate is $1 / 8$ th of the bit rate, while on the asynchronous user port, the character rate is $1 / 10$ th of the bit rate. For every 16 user characters 32 bits are stripped off, so if the maximum frame size parameter is set to 16 , and the nominal baud rates are the same, then the effective character rates on the asynchronous user channel and the synchronous radio data channel will be the same. This also assumes that the supervisory signalling channel is not enabled; and does not allow for the overhead introduced by the HDLC "dummy zero" stuffing mechanism.

### 3.4.4 CONFIGURING PAD PARAMETERS

The Packet Assembler/Dis-assembler (PAD) can be configured with a variety of parameters. Each user port is supported by an identical but independent PAD.

The configuration parameters of the PAD, control how the user data (to be transmitted) is framed. There are three distinct mechanisms that can cause the frame that will carry the user data to be closed.

The first of these is the Maximum Frame Size parameter, already discussed above. As each character is input to the modem, a counter is incremented, and when this counter reaches the set maximum frame size, the data storage mechanism that operates within the modem, will close the frame. This function may be disabled, by setting the parameter to zero.

The second mechanism, is the use of a specified End Of Message (EOM) character. This function is enabled/disabled by a flag in a configuration byte for the port driver. The EOM character may be any 8 bit character. When the EOM function is enabled, all incoming user data is compared to the selected EOM character code, and in the event of a match, the current frame is closed. Note that this match only triggers the frame closure mechanism. The matching character is not deleted from the user data stream, and in fact becomes the last user character in the frame.

The third mechanism, is the implementation of a timer. If the timer is enabled, each character received from the user port re-starts the timer. If the time duration between successive user characters allows the timer to expire, then the frame closure mechanism is invoked. The timer counts in units of "ticker clocks", which is a time interval generated by the modem internally, and is approximately 2.5 mS . The reload value for the timer can be set from 1 to 255 ticker clocks. The timer mechanism is disabled by setting the PAD timer parameter to zero.

There is a single bit configuration flag, that allows the radio modem to begin transmitting user data, even before the frame is deemed to be complete. In this case, as soon as there is any data in the storage buffer, the modem begins the transmission procedure. Providing that the input character rate is greater than or equal to the character rate on the synchronous radio channel, then there is no danger of an under-run condition, where the modem transmitter runs out of data before the PAD deems a frame end. However, should this occur, the modem data transmitter function simply closes the frame itself. Further data is carried in the next frame. This may or may not cause problems elsewhere in a system context. If higher protocol layers are employed (e.g. X. 25, AX. 25 etc.), where address and control fields normally occupy fixed positions in data frames, then the above scenario should not be allowed to occur.

The major advantage of allowing the radio modem to begin the transmission procedure before the frame is deemed to be complete, is that it avoids a (store and forward) delay in the modem transmitter, similar to that required in the receiver. For applications where a transparent point to point link is all that is required, this mode provides the most time efficient transport mechanism.

In fact with the immediate transmission function enabled, there is little necessity to enable the EOM or timer functions of the PAD.

### 3.4.5 SUPERVISORY SIGNALLING CHANNEL: APPLICATIONS \& CONFIGURATION.

The reader is referred to drawing number TC01-05-18, which provides a diagramatic view of this section.

The Supervisory Signalling Channel (SSC) is implemented by the insertion of extra data bits in the primary bit-stream on the synchronous radio channel. These extra bits are inserted between primary data octets, at a rate which can be set to range from once every octet, to once every 15 octets. The SSC operates independently for transmit and receive directions, and can be disabled by setting the rate variable to zero.

The SSC, when enabled, can be configured either to provide end-to-end flow control for Port_A data, or implement the collision avoidance mechanism.

### 3.4.5.1 PORT_A END TO END FLOW CONTROL APPLICATION.

In this configuration, the SSC is used to carry flow control information for data on Port_A at each end of the link.

SSC data inserted into the transmitted bit-stream, relates to the flow of the primary data stream received. When handshake lines are employed, the DTR line locally controls the flow of receive data to the user port. The state of this line is also logically combined with the "fill" state of the receive buffer, and the result is then sent as SSC data in the transmit data stream. Thus the state of the transmitted SSC data bit is one ("1") if the DTR line is in a "false" state, OR the receive buffer is more than half (approximately) full. In the case where XON/XOFF flow control is used, the DTR line input is instead replaced with the state of the last received XON or XOFF control character.

SSC data extracted from the received bit-stream, is logically combined with the "fill" state of the transmit buffer, and the result is output to the CTS line of the modem. The CTS output line is set to "false" if the transmit buffer is more than half (approximately) full, OR the received SSC data bit is a one ("1"). Thus the CTS line is set to "false" if the local transmit buffer is more than half (approximately) full, OR the remote receive buffer is more than half full, OR the remote DTR input line is "false" (or equivalent XOFF received).

Data flow control is exercised only at the user port. No flow control is used on the radio channel, so once data is entered into the transmit buffer, it will be transmitted. This is the reason why the buffers are only allowed to become half full before the flow control mechanism engages. If the flow of receive data is stopped by deactivating the DTR line, the remaining data in the transmit buffer will not overflow the receive buffer. It should be noted that some hysteresis is used in the buffer occupancy tests, to prevent the CTS line from changing state too often, as some hosts (e.g. DOS machines) appear to get confused when this happens.

If the SSC is not configured for end to end flow control, or is disabled, then the flow control mechanisms still operate at a local level. That is, the CTS line (or equivalent XON/XOFF control regime) reflects the fill state of the local transmit buffer.

### 3.4.5.2 COLLISION AVOIDANCE APPLICATION.

When the SSC is allocated to transporting collision avoidance data, the transmitted SSC data reflects the state of the radio receiver. Other processes in the modem, measure the RSSI signal from the radio receiver, and compare this measurement to a preset threshold level. This threshold value is also held in the non-volatile configuration memory. The result of the comparison is copied to the modem pin that drives the RXSIG LED. The transition of the RXSIG signal from off to on, (re)starts an internal timer. This time is a fixed value of $35 \pm 5 \mathrm{mS}$. The SSC data transmitted, is simply a copy of the RXSIG pin state, until the timer terminates, and there-after, the modem data receiver must be "SYNC'd" to maintain the "1" state of the SSC transmit data. Thus the SSC data transmitted by the modem will indicate that the radio channel receiver is busy, using only RSSI for the first $35 \pm 5 \mathrm{mS}$, but after this time, data receiver SYNC is used to qualify this state. This prevents low level RF interference from effectively blocking the channel.

At the receiving end, the recovered SSC data is used by the radio modem to determine when the receiver of the destination station is free. This data can then be used to control it's channel access strategy. Channel access strategies are dealt with in more detail elsewhere in this document.

In such a data transport system, there is a single unit which performs the function of Master, and two or more stations which operate as Slaves. The SSC need only operate in one direction, that from Master to Slaves. In the reverse direction, the SSC can be disabled. That is the SSC in the Slaves is enabled in the data receiver only, while in the Master, it is enabled only in the data transmitter.

### 3.4.5.3 RECEIVED SSC DATA DEFAULT STATE

The received SSC data bit is stored in an internal latch. This latch is updated each time a SSC data bit is extracted from the incoming bit-stream. However, if the radio receiver looses signal, then a default state is forced into the latch. This default state is configurable.

For applications which use the SSC for collision avoidance, this configuration bit would normally be set to "1", so that the remote station would not attempt channel access while the signal from the base is lost.

For applications which use the SSC for end to end flow control, setting the default state of the SSC receive data latch to "0", would cause the CTS output line to indicate local flow control status only, until the destination unit enables it's transmitter, where-upon the received SSC data would reflect the state of the destination receive buffer and DTR input line. Alternatively, setting the default state to "1", would ensure that the CTS output line would be in a "FALSE" state, until the destination unit enables it's transmitter, where-upon the received SSC data would reflect the state of the destination receive buffer and DTR input line.
An associated configuration bit, is one that allows the automatic activation of the radio transmitter, whenever the data receiver attains SYNC. When this configuration bit is set to " 1 ", the modem will automatically activate the radio transmitter's PTT control line when the data receiver is SYNC'd. This could be used at the base end of a small point to multipoint network, using the SSC for flow control, and would not require the host connected to base, to specifically activate the radio transmitter to establish the end to end link.

### 3.4.6 SLIP/KISS PROTOCOL DRIVERS

In addition to a generic PAD, two other host interface protocols are supported, "Serial Line Interface Protocol", SLIP, which hails from the world of UNIX(tm), and an extension of SLIP, KISS "Keep It Simple Stupid", (a rather unfortunate phrase in the present context, but a protocol standard proposed by Phil Kahn, USA, specifically for the control of radio connected data terminals) which includes a facility to send commands which are addressed to the DCE device itself. These commands set operating parameters of the radio-modem DCE, such as transmitter lead-in delay, or radio channel (RF frequency).

Neither of these protocol standards, specify anything about the construction of data packets on the radio channel. Allocation of address, control, and information fields is the user's responsibility.

As standard, the modem is equipped with an 8 K ( 8192 bytes, 32 K optional) data storage memory to hold transmit and receive data. This memory is divided equally between transmit and receive buffer space, and equally between the two user ports, so the largest frame size is 4095 bytes, if only PortA is enabled, (or 2047 bytes each if both user ports are enabled), before the frame check sequence (FCS)is appended.

Additionally, the modem can store up to sixty four separate frames for each direction, again split between the two user ports if both are enabled, though the total byte count is still limited to 8192 total.

### 3.4.6.1 SLIP Protocol Description/Definition

The SLIP protocol, is a data transport protocol, originated and used extensively in UNIX(tm) based systems, and thus also closely associated with TCP/IP networked systems. Although not truly a "standard" it is so widely used that it has become the defacto standard for serial interface in UNIX and many other networked systems. SLIP is a method of framing messages containing binary data, on asynchronous channels. The asynchronous serial channel is configured for eight bit character size, no parity, and one stop.

A specific binary code called FEND (Frame End, hexadecimal value $=C 0$ ) is reserved to define a frame boundary. Should this same code occur in the data message to be transferred across the channel controlled under SLIP, then an escape sequence is used so that the message byte will not be confused for a FEND. This escape sequence, involves replacing the message hexadecimal C 0 code with a two byte sequence FESC , TFEND. FESC (Frame Escape) is the binary code hexadecimal DB, and TFEND (Transposed FEND) is binary code hexadecimal DC. Likewise, if the FESC character ever appears in the user data, it is replaced with the two character sequence FESC, TFESC (Transposed FESC). The TFESC is the binary code hexadecimal DD. The following table clarifies this.

| ABBREVIATION | DESCRIPTION | HEX.VALUE |
| :---: | :--- | :--- |
| FEND | Frame end | C0 (192) |
| FESC | Frame escape | DB (219) |
| TFEND | Transposed frame end | DC (220) |
| TFESC | Transposed frame escape | DD (221) |

As characters arrive at the SLIP receiver, they are appended to a buffer containing the current frame. Receiving a FEND marks the end of the frame, and consequently, succeeding bytes are considered part of the next frame.

Receipt of a FESC code puts the SLIP receiver into "escaped mode", causing it to translate a following TFESC or TFEND back to a FESC or FEND code, appending it to the buffer, and resuming it's normal state. Receipt of any byte other than TFESC or TFEND while in escaped mode, is an error. No translation occurs, and the SLIP receiver leaves escaped mode. A TFESC or TFEND received while not in escaped mode is treated as an ordinary character and stored accordingly. Reception of consecutive FEND characters, causes no action to be taken (i.e. is not interpreted as zero length frames).

An example of a typical SLIP frame is shown below. The message consists of the string DA,C4,C0, $55, D B, 20, B D, D C, D D$. The SLIP frame will be:-

$$
\begin{aligned}
& <\text { FEND }>, D A, C 4,<F E S C>,<T F E N D>, C 5,<F E S C>,<T F E S C>, 20, B D, D C, D D,<F E N D> \\
& ==>\quad C 0, D A, C 4, D B, D C, C 5, D B, D D, 20, B D, D C, D D, C 0
\end{aligned}
$$

### 3.4.6.2 KISS Protocol Description/Definition

The KISS protocol is an extension of SLIP. It uses the same method of framing packets, using FEND, FESC, TFEND, and TFESC codes. However, the first byte in each frame is reserved as a control code, that defines the function/content of the frame, and also contains an address.

This addressing scheme allows up to sixteen "Terminal node controllers" (TNC's), to share a multidrop buss. The top nibble of the control code carries the TNC address, and the lower nibble carries the command code. Normally the address is set at zero for installations containing only one TNC. Note that some extensions have been proposed for the KISS protocol, that properly support addressed multidrop line operation of multiple TNCs, that the present TC-900DR modem firmware does not implement. The following table shows the commands defined by KISS, and the comment column indicates how the TC-900DR modem interprets them.

| COMMAND | FUNCTION | COMMENTS |
| :---: | :---: | :---: |
| 0 | Data Frame | The rest of the frame is data to be transmitted. |
| 1 | TxDelay | The next byte is the RF transmitter key-up delay in octets. |
| 2 | Slotnum | The next byte is the Slotnum parameter. |
| 3 | Slot-Time | The next byte is the "Slot" interval in "ticker clocks". |
| 4 | TxTail | The next byte is the time to hold up the RF transmitter after the closing FLAG has been sent. This command is obsolete, and not implemented in the TC-900DR. |
| 5 | FullDuplex | The next byte is zero for half duplex, non-zero for full duplex. This command is not implemented in the TC-900DR, as it always operates in full duplex mode. |
| 6 | SetHardware | Specific for each TNC. This parameter has values between 00 and 03 , and commands the TC-900DR to set RF channels 0 to 3 . Values above 3 are ignored by the present modem firmware, but may be used in future versions. |
| F | ExitKISS | Exit KISS and return control to higher level TNC control program. This command is not implemented in the TC-900DR. |

### 3.4.7 RF TRANSMITTER CONTROL AND CHANNEL ACCESS STRATEGIES

There are three conditions which cause the modem to activate the radio transmitter. These are: a) receiver SYNC if enabled, as described above; b) RTS if enabled, as described below; and c) the existence of a data frame ready for transmission. The first two mechanisms are absolute, and if enabled, cause an immediate activation of the radio transmitter. There are two configuration bits that control how the availability of a data frame, will activate the radio transmitter, and thus gain access to the channel. For the purposes of this description, these are referred to as Modes $\mathrm{A}, \mathrm{B}$, and C .

In Mode A, channel access is immediate. The radio transmitter is activated, and the modem then proceeds to send a preamble sequence, followed by the data. The preamble sequence is necessary for receiver synchronisation, and the length is a configuration parameter. Further discussion of these aspects of the modem configuration are dealt with elsewhere in this document.

In Mode B, the modem will attempt channel access only if the radio receiver is NOT receiving a signal (i.e. the measured RSSI level is below the minimum RSSI threshold as described elsewhere in this document). This method could be used for small point to multipoint systems, where the base station would enable it's radio transmitter on receiving a transmission. Typically this would be done at the base unit by enabling the SYNC-PTT function, as described above. This implements a basic collision avoidance system, without the use of the Supervisory Signalling Channel, which then remains available for flow control applications.

In Mode C, the modem will attempt channel access only if the data receiver is SYNC'd, and the SSC data is "0" (i.e. base receiver free). This is the full Collision Avoidance system as described in detail above.

In the latter two cases, if another data frame is ready for transmission at the time the present one is ending, then it is automatically appended as another frame, and the transmission continues. Obviously since the radio transmitter is already enabled, no preamble is required or sent. The modem itself does not limit the number of consecutive frames it will transmit. If data continues to be input to the modem, once channel access is gained, it continues to be transmitted. It is the responsibility of the user to manage any maximum channel access time in overall system design. However; if the PTT timer is enabled (dealt with in detail elsewhere in this document), and the set time is reached, then the modem will disable the radio transmitter PTT line. User data will now be lost.

For the two latter strategies, if channel access fails (i.e. signal at radio receiver in the former case, or $\mathrm{SSC}=1$ in latter case), then the modem uses a timed delay mechanism before testing for channel availability again.

### 3.4.7.1 SELECTING "SLOTIME" AND "SLOTNUM" VALUES

This delay time is necessary to prevent multiple remotes from attempting to gain access to the channel as soon as it is signalled to be clear after another transmission has finished, as this would result in the transmissions from all these remotes colliding. Instead, when a modem fails to gain channel access, it generates a randomly selected delay time, and when this time has expired, it again tests for channel availability.

There are two parameters which are used to generate the delay time. The "Slotime" parameter defines the size of the time increment used in selecting the delay. This value defines a time counted in "ticker clocks" (approximately 2.5 mS ), and has an allowable range of 0 to 255 . The "SlotNum" parameter defines the upper limit of the random number generator. The random number generator selects an integer between one and the value of "SlotNum", and then multiplies this by the value of "Slotime" to derive the delay time. The "SlotNum" parameter has a maximum allowable range of 1 to 16 .

These two parameters together provide a very flexible method of tuning the channel access characteristics of a system, and should be regarded as system tuning parameters. In the absence of any knowledge of a system configuration, Trio DataCom's set default values for these to parameters to 4 and 16 for "Slotime" and "SlotNum" respectively.

### 3.4.7.2 PTT CONTROL BY RTS LINE

Applications relying on establishing a point to point link before data is transferred, would normally require some "manual" method of activating the radio transmitter. A configuration bit enables the RTS input line to be used as a PTT control. The modem is always generating a data signal. During the time when no user data is available, the modem continually generates an "idle" bit-stream of HDLC FLAGs. This sequence produces no data output at the receiving radio modem.

### 3.4.8 SELECTING FLOW CONTROL REGIMES

The type of flow control to be used on the radio modem port(s), depends on the user's application and capabilities of the equipment which the user interfaces to the TC-900DR.

Port_A, which is always active, can be configured to use the standard RS232 handshake lines RTS/CTS/DTR, or use XON/XOFF protocol.

### 3.4.8.1 PORT_A, HARDWARE HANDSHAKE FLOW CONTROL

If hardware handshake lines are configured, then RTS must be active to validate characters input to the modem for transmission. As each character is received (i.e. at the end of each character bit sequence) the state of the RTS input line is tested to validate the character. If the RTS line is tested "true", then the character is stored ready for transmission. If "false", then the character is discarded. The modem provides flow control of transmit data with the CTS line. The CTS line is set "false" to indicate that no more transmit data should be input. Normally, most terminals or hosts will still send one or two more characters after the CTS line is set "false", and this is normal and allowed for in the CTS control logic. In fact the modem will continue to accept and store transmit data (providing the RTS line is still active) even though it has set the CTS line to "false", however the user then risks the occurrence of an overflow condition. If the transmit buffer becomes full, then further data is discarded.

A configuration bit, further controls the state of the CTS output line in relation to the RTS input line. If the bit is clear, then the CTS output will always indicate the flow control state, regardless of the state of the RTS input. If the bit is set, the CTS line is conditional on the state of the RTS input. If the RTS input is "false", then the CTS output is also "false". If the RTS input is "true", then the CTS output indicates the flow control state. This latter configuration is typical of a "wired" modem.

The modem's internal data store holds both the raw user data, and records the position of frame boundaries (as defined by PAD operation) in the data. A limited amount of memory is allocated to storing the frame boundary data. When this memory space is full, the modem sets the CTS output to false, even though the character storage space may not be full. The frame boundary storage space is sufficient to hold data for 64 frames. If the modem has both ports (Port_A and Port_B) enabled, then this space is evenly divided between the two, or if Port_B is disabled, then up to 64 frames can be stored for Port_A. If data continues to be input when the CTS line has been set to "false" because no more frame boundaries can be recorded, then the frame closure mechanism may abort. This has the effect that a frame will not be closed when defined by PAD configuration. An example of this, is where the PAD is configured to close the frame on receiving a <CR> (carriage return) EOM. If the frame boundary space is full, when a $<C R>$ is input, then the subsequent characters will be appended to the same frame. Another attempt to create a new frame will not occur until the same or another frame close condition (as defined by PAD configuration) occurs, in this case another <CR>. This logic avoids the unnecessary loss of data.

Situations where the data storage space or frame boundary storage space become full, would be rare, and would only be likely to occur if the transmitter could not gain access to the channel, or the input data rate exceeds the channel transmission rate for some time.

Normally the TC-900DR is manufactured with an 8 kilobyte memory for data storage. This memory space is divided equally between transmit and receive data storage. If both user ports are enabled, then each half is equally divided between the ports (i.e. 2K/2K/2K/2K for Port_A transmit, Port_A receive, Port_B transmit, Port_B receive). If Port_B is disabled, then 4 K is available for each of the transmit and receive data storage functions for Port_A.

The DTR line controls the flow of receive data to the user port. While the DTR input line is "true", available received data is output from the port. If the DTR input is "false", then receive data output ceases.

### 3.4.8.2 PORT_A XON/XOFF FLOW CONTROL PROTOCOL

When XON/XOFF flow control is configured for Port_A, the CTS line is set "true", the RTS input line is not required to validate input data, and receive data is not dependent on the state of the DTR line. Instead of controlling the CTS line, the modem sends XON/XOFF characters (embedded in the receive data stream), to the port. The flow of receive data is controlled by the receipt of XON/XOFF characters in the transmit data stream. These control characters are trapped out of the transmit data stream, and are not transmitted.

The underlying flow control logic is the same as RTS/CTS/DTR control. An XON is sent instead of a "false" to "true" transition of the CTS line, and an XOFF is sent instead of a "true" to "false" transition on the CTS line. A received XON is recorded by an internal flag that emulates a "true" state on the DTR line, and a received XOFF is recorded by the flag to emulate a "false" state on the DTR line.

This method of flow control would be considered to be less reliable, since a lost XON or XOFF control character could cause either an overflow condition, or data flow to stop altogether.

### 3.4.8.3 PORT_B FLOW CONTROL

User Port_B can be configured for no flow control, or XON/XOFF flow control. When XON/XOFF flow control is configured, it operates identically to Port_A, except that this port has no CTS line to set "true". Flow control on Port_B operates at a local level only, since end to end flow control via the SSC is available only for Port_A.

If XON/XOFF flow control is disabled, then no flow control is used on Port_B, as there are no RTS/CTS/DTR lines implemented on Port_B. Users should be careful to avoid overflow conditions, to avoid loss of data.

It will now be obvious that the RTS input line on Port_A can be used by more than one function in the modem. RTS can have no function, or be used in Port_A flow control, and/or provide a manual PTT facility.

### 3.4.9 SETTING MINIMUM RSSI LEVEL

The data receiver of the modem is continually running. It will be in one of two states. It is not SYNC'd, and thus looking for HDLC FLAGs in the radio receiver signal, or it is SYNC'd, and recovering frame data to be checked and stored. If the radio receiver is not receiving a signal, then the recovered signal applied to the data receiver of the modem, will consist only of noise. To prevent the modem from erroneously locking onto noise, a minimum RSSI level must be present to validate the recovered signal applied to the modem data decoder. This threshold level, is stored in the non-volatile configuration memory. It should be set by applying a signal to the radio receiver, which produces a desired SiNaD result, a desired bit error rate, or more crudely, a predetermined absolute signal level into the antenna connector of the TC-900DR. The modem (operating in Test/Program mode) is then commanded to measure the RSSI level, which produces a response of a message indicating the measured level, in hexadecimal. This process should be repeated several times, then an average taken. The analogue to digital conversion performed in this way, is an eight bit conversion. In normal operation, the modem performs a six bit conversion when measuring the RSSI level, so the average of the levels measured in the test mode should now be divided by four. The result should now be stored in the configuration memory, at the address reserved for it.

### 3.4.10 SETTING PTT TIMER

The modem implements a PTT timer. This timer can be disabled entirely by setting the PTT Timer configuration value to zero. The timer value is a 16 bit number, that counts in "ticker clocks". If the timer is enabled, whenever the modem activates the PTT control to the radio transmitter, it initialises the timer with the configured value. The timer is decremented while the PTT control remains active, and if it terminates, the PTT control is deactivated. No other action is taken, and all other functions within the modem are oblivious to this condition, so data frames continue to be output, and thus lost. The PTT timer is to be considered an emergency override mechanism only, in case an error occurs in the operation of the user's host equipment and/or software. To reset this time-out state, conditions must be met that would cause the modem to normally deactivate the PTT control. The PTT timer will then be re-initialised the next time the PTT control is activated. The time-out period may be set in "ticker clock" ( 2.5 mS ) increments to over 160 seconds.

### 3.4.11 DATA STREAM SWITCHING, SELECTING AND ENABLING SID CODES

The TC-900DR radio modem includes a feature that provides data stream switching. This is achieved by placing a Stream Identifier code (SID) at the beginning of every frame. This code functions as a simple addressing function. If both user ports of the TC-900DR are enabled, then SID codes should also be enabled, so that data frames carry a code which identifies the originating port ( $A$ or $B$ ), thus the port to which the frame data should be directed when the frame is received at the destination station.

However this stream switching mechanism is not only confined to this simple application. The SID codes for each user port, are contained in the configuration memory, and are thus "soft". It would be possible to engineer a small (up to 256 stations) network using an individual SID code for each remote station. Since the modem receiver will discard frames which are headed by an SID code which is not recognised, only frames specifically addressed would be stored and passed on to the attached host. The SID code is allocated to the port, so the modem uses the same SID code both for transmission and receipt of frames. Therefore in such a system, the master would be configured with SID codes disabled. The host attached to the master would preface each message with the eight bit address of the destination remote. The message from the remote emanating from the port will have the SID code removed. A message received from a remote, will have the SID code of the sending station at the beginning as the first byte. The remote modem itself places this code at the head of the frame.

Another application of the stream switching feature, is a remote diagnostics facility. This is a facility which is planned for release in the next firmware version. A reserved SID code will be used to address a diagnostics function within the modem. A command/addressing protocol is being developed that employs the units own unique serial number for addressing. "Stay tuned for further updates!".

The SID code is placed in the first octet of each frame. This provides up to 256 unique codes. However, to avoid possible future compatibility problems where higher level protocols are in use on the same channel (e.g. AX.25, etc.), it is suggested that the SID codes used have bit0 set to "1". Such higher level protocols normally use extended addressing where more than one octet is used to carry the destination/source address. A frame using an SID code with bit0 set, will fail an address test and be discarded by such systems. Conversely, if this modem receives a frame containing a higher level protocol, bit 0 of the first octet will normally be set to " 0 ", so will not match any SID code stored in the configuration memory, and be discarded.

By default, Trio DataCom sets the SID codes to 03 and 05 for ports $A$ and $B$ respectively. We have also reserved SID code 00 for the diagnostics facilities.

### 3.4.11.1 Separate Tx And Rx SID Codes. (Firmware Revision V2.1 onwards)

Firmware revision V2.1.0 onwards allows the Transmit and Receive SID codes to be different. Normally the RxSID and TxSID parameters (separate for each port) would be programmed the same. By programming them to be different, means that a TC-900DR unit will receive frames carrying a SID code that matches the configured RxSID code, but transmit frames which carry a SID code that is specified by the TxSID code configuration parameter. Applications for this feature are in small point to multipoint systems, using a central "community" repeater.

### 3.4.11.2 Repeater Operation Mode. (Firmware Revision V2.1 onwards)

The TC-900DR radio modem may also be configured in a repeater mode. The repeater function is enabled as a protocol driver on a port. Thus each user port driver can individually be configured for repeater operation. Essentially, what this does is automatically routes the received data frames back to the transmitter. If SID codes are enabled, then the original SID codes are stored as part of the data frame, and thus the retransmitted frame is identical to that received. Note that only frames received error free will be repeated.

When a port driver is configured for repeater operation, the RxSID and TxSID codes stored in configuration data in the NVRAM are used to define a range of streams to be repeated. The RxSID code configuration parameter defines the lowest SID stream to be repeated, and the TxSID code configuration parameter defines the highest SID stream that will be repeated. Thus it is possible to configure a unit to perform a repeater function for two separate ranges of streams, by configuring both user ports with a repeater driver, or to configure one end of a data link to also be a repeater for a range of other streams.

### 3.4.12 SETTING TRANSMITTER LEAD_IN_DELAY

Whenever the radio transmitter is activated a timer is started. No data frames are transmitted until this timer terminates, so that the destination unit receiver has time to synchronise it's data receiver before frame data is begun. The radio transmitter is very fast, reaching final output power and frequency stability in a matter of a few hundred microseconds (other sections of this document deal with the receiver synchronising aspects). This timer counts in octets, not "ticker clocks" as most other timed functions do, so the actual time elapsed is a function of the radio channel bit rate. However, the synchronisation time is primarily a function of the number of bits to the receiver. Trio DataCom would suggest a value of 25 to 50 (decimal) for this parameter, but it's final value will depend on signal strength and quality at the receiving point, and should best be determined by test.

### 3.5 FACTORS AFFECTING MODEM SYNCHRONISATION TIME

### 3.5.1 (UN)SCRAMBLER AND HDLC STATE MACHINE

It can be shown, that the un-scrambler in the receiving unit will synchronise to the scrambler in the sending unit in 17 bits maximum.

The receiving unit must then detect an HDLC FLAG, which will take another 15 bits maximum. Thus the HDLC state machine and unscrambler should be synchronised in 32 bits maximum.

### 3.5.2 PHASE LOCKED LOOP

Before valid data can be read for the unscrambler, the phase locked loop (PLL) must lock. The time required for this to occur is affected by signal quality and content. The PLL relies on level transitions of the binary signal, on which to lock. It essentially compares the phase of an internal counter, with the phase of the incoming data bits. A detected phase error, will cause the internal counter to speed up or slow down, to reduce the phase error. The greater the error, then the greater the speed adjustment to the internal counter.

If the incoming data stream has few transitions, then the internal counter will "catch up" to it quicker, since it's speed is adjusted less often. The PLL will synchronise to within $90 \%$ of the correct phase (from 0\%), in 16 to 36 bits time, depending on the number of transitions.

In practice, even though the PLL has not reached $90 \%$ lock, meaningful data will still be obtained as long as a good strength, clean signal is available.

### 3.5.3 ERROR CONTROL

Having recovered the raw data, the modem then applies the bit-stream to a de-ramdomiser, which is based on a recursive tapped shift register, described by the polynomial:

$$
X^{17}+X^{12}+1
$$

The output of the de-randomiser is then fed through another conversion function, to convert the NRZI data to NRZ.

The data is now an HDLC data stream, conforming to ISO3309. It is then applied to a function which detects HDLC FLAGs, and extracts "dummy zeros", which were inserted by the transmitter. Frame boundaries are detected at this point.

The modem calculates and appends a 16 bit Cyclic Redundancy Checksum (CRC) word to the end of each frame. This calculation uses the polynomial:

$$
X^{16}+X^{12}+X^{5}+1
$$

This is sometimes referred to as CRC-CCITT since it is a CCITT standard.

The 1's complement is taken of the calculation result and this FCS is appended to the end of the data frame and sent MSB first. (Refer to ISO 3309 for more information)

At the receiver, this calculation is repeated on the received data, and the result checked. A detected error, will cause the receiver to discard the entire frame. A higher protocol level (determined by the user) will detect the lost packet, and initiate a re-send of the packet.

In terms of the reliability of this FCS, it can be claimed that the following will be detected: 2

All single bit errors.
All double bit errors.
Any odd number of errors.
Any burst error less than 16 bits long.
Most large burst errors.
From here emanates the original frame data, provided the FCS was correct. If not then the frame data is discarded. The data is stored in externally addressed memory, connected to the modem IC. Maximum data packet size is determined by the amount of available memory. Normally the modem is fitted with an 8K CMOS RAM, of which half (4096 bytes) is allocated to the receiver. The modem can be fitted with an external memory up to 32 K with no other modifications. The receiver section of the modem can store up to 32 separate data packets.

How this data is handled from this point on, depends on the user protocol implemented by the modem on the user interface.

### 3.5.4 TRANSMISSION FORMAT AND TIMING

The data to be transmitted is input to the modem, via the user interface protocol implemented on the user interface. The modem stores the data packet(s) in externally addressed memory, connected to the DFM4-9 modem IC. Maximum data packet size is determined by the amount of available memory. Normally the modem is fitted with an 8 K CMOS RAM, of which half ( 4096 bytes) is allocated to the transmitter. The modem can be fitted with an external memory up to 32 K with no other modifications. The transmitter section of the modem can store up to 32 separate data packets.

Most of the transmitter functions are performed internally in the modem IC, with only a DAC (Digital to Analogue Converter) and final low pass filter implemented by external circuitry.

The data is placed into an HDLC frame (consistent with ISO3309), complete with dummy zeroes where required. During transmission, a CRC calculation (CRC-CCITT) is performed, and when the end of the data packet is reached, this FCS (Frame Check Sequence) is appended to the end of the frame, before the closing HDLC FLAG.

Where two or more consecutive frames are sent, only one FLAG octet is used to delimit the frames. All frames are composed of an integral number of octets.

[^9]Data from the HDLC formatting stage is fed through a function, to convert the NRZ data to NRZI format.

The NRZI encoded data stream is now fed to a data randomiser, to ensure that there is no DC component to the data stream. This is based on a recursive seventeen bit shift register with two taps.

### 3.5.5 COLLISION AVOIDANCE SCHEME

The unique supervisory signalling channel facility available in this product is ideally suited to the implementation of a highly effective collision avoidance mechanism. This is a highly desirable feature in a multipoint data network, in that it allows vastly increased usage of the available channel capacity.

For instance, take a point-to-multipoint network, with a central base station, and a large number of remote data terminals scattered around the central station.

This is a split frequency duplex channel, where the central station is able to transmit on frequency F1, and simultaneously receive on frequency F2. Remote stations transmit on frequency F2, and receive on frequency F1.

If a transmission by one remote station is "crashed" by a transmission by another remote station, then the base station may not get the message correctly, and thus not acknowledge it. If there is no control over when the remote stations transmit, then because the remote stations cannot "hear" each other, their transmissions will begin to collide more often as the data traffic increases. This type of system will suffer a total blockage as the total traffic requirement approaches about $50 \%$ of the channel capacity.
Now, if the base station could quickly inform all other remote terminals, when the base receiver is busy because one of the remote terminals is transmitting, then this message can be delivered to the base receiver without being "jumped on" by another terminal blindly "crashing in". The next terminal can then deliver it's message when the receiver is signaled to be free. Of course collisions are still possible, but the occurrence of these can be dramatically reduced by this type of scheme.

Now to implementation specifics. The supervisory signalling channel in the modem, can be set independently for transmit and receive directions. For the purposes of this collision avoidance scheme, the supervisory signalling channel is only required in the base transmit direction. In the reverse direction, the supervisory signalling channel is disabled. The base transmitter is active full time, sending only FLAGs when it has no real data to send. The base controller, then indicates to the whole population of remote terminals, the current status of the base receiver, in the value of the supervisory signalling channel data bits.

The remote data terminals are programmed so that they will not begin a transmission if the received supervisory signalling channel data indicates that the base receiver is currently busy. This would result in remote terminals queuing for access to the base receiver. To prevent all these remote terminals all beginning a transmission as soon as the base indicates a free receiver, a "windowed" timing mechanism would be implemented, with a random factor added in the terminal's selection of a "window".

There are many factors that would determine the quantification of system variables, but this short description serves to illustrate a basic approach.

### 3.6 TEMPERATURE COMPENSATION

Periodically, the modem controller reads the voltage on the temperature transducer mounted on the radio section. This value is then used in a table look-up procedure, to derive correction data to be applied to the modulator circuitry via a transmit waveform offset voltage. This is provided by the output of the six bit DAC (UX8/RN2), which is fed to the correction voltage input of the 12 MHz reference oscillator.

The offset table is constructed in the temperature calibration cycle performed during the factory testing procedure. The radio-modem is temperature cycled twice from -10C to +65 C . During this time, the necessary data is determined to correct the temperature induced frequency errors. At the end of the cycle, the final database is constructed and written to the non-volatile memory.

### 3.7 USER INDICATIONS

The TC-900DR provides three LED's that show status information to the user - RXSIG, SYNC, and TXMIT indications.

In all operation modes of the modem except "Programmer mode" (see the section below on special modes of operation), the RXSIG LED indicates the level of the RSSI signal from the radio IF strip, compared to a threshold set in the configuration data read from the non-volatile memory. If the signal is above the threshold, then the LED indicator is turned on. There is no hysteresis applied in this process.

In normal operation, the SYNC LED indicates when the modem has detected a valid data stream. The SYNC LED is activated, when the modem detects a valid HDLC flag sequence, and remains active until an invalid sequence of seven or more consecutive "1" bits is detected. The SYNC LED will not be turned on if the RSSI signal strength (as indicated by the RXSIG LED) is below the minimum threshold. This prevents false SYNC detection from noise. While the modem is SYNC'd, it does not continue to measure RSSI levels.

The TXMIT LED indicator is connected directly to the modem's PTT output transistor. It is active whenever the PTT line to the radio section is active low.

### 3.8 SPECIAL MODES OF OPERATION

### 3.8.1 GENERAL

Part of the power-up/reset initialisation phase of the TC-900DR modem, is a set of tests to determine whether the modem should enter a special operation mode.

There are three of these "special" modes. Whilst in these modes the TC-900DR will not operate in its standard run mode.

- Programmer mode.
- Bit error rate test mode.
- Handset mode.

These modes are only entered if the required setup conditions are present at power up of the TC-900DR. An error mode of operation can also be entered into, if during normal operation of the TC-900DR modem, an error condition occurs.

### 3.8.2 PROGRAMMER MODE

Pin 6 on the DB9 connector of Port A, is normally the DSR line. This pin is pulled high by a resistor to +13.8 v , so that to a connected DTE the DSR signal implies that this DCE is ready.

However, if this pin is connected to pin 5 when the modem is powered up, the controller senses this, and attempts to enter "Programmer mode". The modem sends out of the serial port, an ASCII "?" (question mark) character, and waits for the programmer to reply with a password. The SYNC LED toggles on and off with every output of the "?" prompt until the correct password is entered. This mode is sustained for approximately 30 seconds. Failure to supply the correct password in time, will cause the modem to abandon the "Programmer mode" attempt, and go on with it's normal power-up procedure. This password protection scheme provides some defense against unauthorised tampering with the TC-900DR modems configuration data.


### 3.8.3 BIT ERROR RATE TEST MODE

Pin 9 of the DB9 connector of Port A, is normally the Ring Indicate output line. The modem includes a resistive pulldown to ground to show a negative condition on this line. However, if this pin is driven positive (typically by connecting it to pin 6), then the modem's data transmitter and receiver will enter the BER test mode.

It will activate the RF transmitter and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic "1" level in the unscrambled data.

A test point on the modem section PCB, is available to monitor this point with a frequency counter. (In fact this test point is always active, and may be used to monitor the received data decoded by the DFM4-9 modem IC at any time). Any errors in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a " 0 " bit.

An internal timer is used to generate a time equivalent to 1000 bits. Every error bit detected, will activate the SYNC LED, and restart the timer. If and when the timer expires, the SYNC LED is deactivated. Thus, for error rates of 1 in 103 and above, the SYNC LED will be ON most of the time. A 1 in 104 error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for installation purposes.

Other functions performed in this state include RXSIG indication, and temperature compensation. The state of pin 9 is constantly monitored in this mode. If the pin ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

### 3.8.4 HANDSET MODE

The DFM4-9 modem tests for the presence of a handset plugged into the handset audio port at power up.

This is done by measuring the voltage on channel 4 of the analogue to digital converter (UX10-p6). This signal is passed into the modem section from the radio section via connector X4-p24, "ADC3".

If a handset is plugged in, then the measured voltage will be about 2 V , but if it isn't installed, then the voltage will be about 4 V . The measured voltage is compared to 3 V to determine whether the handset is plugged in. If this test succeeds, then the modem will not generate a data stream. However, it will continue to indicate received RF signal strength, and perform temperature compensation. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED.

### 3.8.5 ERROR INDICATION MODES

### 3.8.5.1 GENERAL

There are three error conditions that will cause the RXSIG and SYNC LEDs to be used for error indications and not their normal purpose. Two of these are fatal conditions, that cause the modem to restart after the duration of the error indication phase.

### 3.8.5.2 TRANSMIT POWER LOW

While the modem activates the radio transmitter, it periodically checks the transmit power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately four times per second. The TXMIT LED will also be on during this process. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function.

### 3.8.5.3 NVRAM READ ERROR

The DFM4-9DR modem accesses the non-volatile memory as part of it's initialisation phase, to get configuration data. If the communication protocol with the device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED operates ON and OFF twice, then the other. A total of five cycles of this occurs, then the modem restarts it's initialisation from scratch.

### 3.8.5.4 SYNTHESISER LOCK DETECT ERROR

If at any time during normal operation, BER mode, or handset mode, the TBB206 frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting. One LED is turned ON ( 0 ), the LEDs are swapped, then both turned OFF (*). Then the latter LED ON again, swap LEDS, and then OFF. This will give the appearance of a sweeping motion between the LEDs.

The following table shows all error condition displays for comparison.

| Tx PWR Error |  | NVRAM Error |  | TBB206 Error Synthesiser |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | - | 0 | - | 0 | - |
| - | 0 | - | $\bullet$ | - | 0 |
| 0 | - | 0 | $\bullet$ | - | - |
| - | 0 | - | - | - | 0 |
| 0 | - | - | 0 | 0 | - |
| - | 0 | $\bullet$ | - | - | $\bullet$ |
| 0 | - | - | 0 |  | repeat |
| - | 0 | $\bullet$ | $\bullet$ |  |  |
| continue |  |  | repeat |  |  |

### 3.9 SYNCHRONOUS OPERATION MODE FIRMWARE REVISION: V2.1

### 3.9.1 GENERAL

The TC-900DR when operating in Synchronous mode, implements a V. 24 like interface. The unit uses a special wiring harness that converts the two 9 pin "D" connectors on the end panel of the TC-900DR to a standard 25 pin "D" connector for user interface.

Synchronous Mode implements a bit level interface. Data is carried on a bit by bit basis. No framing or error detection is performed. Modem operation is full duplex.

Current implementations of SYNC mode, do not provide a DCD signal in the 25 pin RS232 interface.

### 3.9.2 DATA RECEIVER

While sufficient RF signal is present into the radio receiver, the data decoder is continually extracting data bits from the received signal, and outputting these to the user interface connector. If the received RF signal into the radio receiver falls below the minimum threshold, then the data decoder stops.

### 3.9.3 SETTING MINIMUM RSSI LEVEL

The data decoder of the modem is continually running while sufficient RF signal is present into the radio receiver. If the radio receiver is not receiving a signal, then the recovered signal applied to the data decoder of the modem, will consist only of noise. To prevent the modem from erroneously locking onto noise and producing "garbage" at the RxD pin, a minimum RSSI level must be present to validate the recovered signal applied to the modem data decoder. This threshold level, is stored in the non-volatile configuration memory. It should be set by applying a signal to the radio receiver, which produces a desired bit error rate, a desired SiNaD result, or more crudely, a predetermined absolute signal level 'into the antenna connector of the TC-900DR. The modem (operating in Test/Program mode) is then commanded to measure the RSSI level, which produces a response of a message indicating the measured level, in hexadecimal. This process should be repeated several times, then an average taken. The analogue to digital conversion performed in this way, is an eight bit conversion. In normal operation, the modem performs a six bit conversion when measuring the RSSI level, so the average of the levels measured in the test mode should now be divided by four. The result should now be stored in the configuration memory, at the address reserved for it. The DR9_PRGM programmer available from Trio DataCom Pty Ltd facilitates this process.
*Use a signal generator modulated with a sine wave frequency of half the nominal bit rate of the unit (e.g. for a 4800 BPS unit, use 2400 Hz modulation).

### 3.9.4 DATA RECEIVER CLOCK OUTPUT

The receive section of the modem, includes a clock line driven by the modem. This signal is used to synchronise the transfer of receive data to the user system. The RCO (Rx_Clock_Output, pin17 in the DB25 connector) line changes from ON (TRUE) to OFF (FALSE) as the RxD (Receive_Data, pin3 in the DB25 connector) line outputs the next bit, and from OFF (FALSE) to ON (TRUE) in the nominal centre of the bit cell. This conforms to the V. 24 specification.

### 3.9.5 OTHER RS232 RECEIVER CONTROL LINES

The DSR (Data_Set_Ready) line is driven true by the modem. This line is in fact merely tied to the internal +13.8 volt rail via a 4 K 7 resistor. The DTR (Data_Terminal_Ready) input is unused in Synchronous mode.

### 3.9.6 DATA TRANSMITTER

The transmit data input is continually sampled and coded for transmission. This process consists of sampling the data input, randomising the bit pattern so that the DC component of the transmitted stream is zero, and generating a waveform suitable for application to the modulator of the FM radio transmitter.

### 3.9.7 DATA TRANSMITTER CLOCKS

The modem transmit data interface, includes two clock lines. One clock line, TCO (Transmit_Clock_Out, pin15 in DB25 connector) is driven by the modem, the other, TCl (Transmit_Clock_In, pin24 in the DB25 connector) can be enabled to allow the external user to supply a transmit data clock. This is implemented by synchronising the internal clock generator to the user's clock (within a small frequency range). This function is essentially a Phase Locked Loop, and effectively adjusts the phase of the internal clock to match that of the input clock. If the user clock source stops, then the modem will continue to generate the internal clock at it's nominal rate. In accordance with specification V.24, the state of the transmit data line (TxD, pin2 in the DB25 connector) is sampled on the ON to OFF transition of the clock, the bit cell boundary occurs with the OFF to ON transition of the clock.

### 3.9.8 TRANSMITTER RTS/CTS LINES

Two other control lines are included in the transmitter interface. The RTS (Ready_To_Send) input line, is used to control the radio RF transmitter. The CTS (Clear_To_Send) output line is driven by the modem, to indicate that the modem transmitter is ready to accept transmit data. The RTS to CTS time is determined by an internal timer. A configuration parameter is used to load the internal timer when the RTS line is activated, which must expire before the modem activates the CTS line. This time is necessary to allow the remote receiver to settle and synchronise to the data stream, before the user at the transmitting end begins sending data. However it should be noted, that the CTS signal does not perform any flow control function within the modem.

### 3.9.9 PHASE SYNCHRONISM WITH GLOBAL CLOCKS

When data is transferred over more than short distances, and synchronism must be maintained to some external global master clock (e.g. Telecom DDN network), then the propagation delay, and thus phase shift of the data becomes significant. A facility is provided, to introduce a phase delay in the transmitted data stream, of up to $3 / 4$ of a bit, in $1 / 4$ bit steps. This delay is adjusted so that minimum phase offset results at the receiver of the destination station.

### 3.9.10 TRANSMIT TIMER

The modem implements a transmit (PTT) timer. This timer can be disabled entirely by setting the PTT Timer configuration value to zero. The timer value is a 16 bit number, that counts in increments of 2.5 milliseconds. If the timer is enabled, whenever the modem activates the PTT control to the radio transmitter, it initialises the timer with the configured value. The timer is decremented while the RTS line remains active, and if it terminates, the PTT control is deactivated. No other action is taken, and all other functions within the modem are oblivious to this condition, including the CTS line, so data continues to be "carried", and thus lost. The PTT timer is to be considered an emergency override mechanism only, in case an error occurs in the operation of the user's host equipment and/or software. To reset this timeout state, the RTS line must be taken from ON to OFF. The PTT timer will then be re-initialised the next time the RTS line is activated. The timeout period may be set in 2.5 mS increments to over 160 seconds.

### 3.9.11 LED INDICATORS

### 3.9.11.1 Received Signal Strength Indication. RXSIG LED

In all operation modes of the modem except "Programmer Mode" (see section below on special modes of operation), the RXSIG LED indicates the level of the RSSI signal from the radio IF strip, compared to a threshold set in the configuration data read from the non-volatile memory. If the signal is above the threshold, then the LED indicator is turned on. There is no hysteresis applied in this process.

### 3.9.11.2 Data Carrier Detect Indication. SYNC LED

In "Synchronous" operation mode (V2.1.x), prior to modem hardware revision "D", and firmware revision "V2.1.4", the SYNC LED is superfluous and not driven.

## Note that firmware revision V2.1.5 onwards should only be used in SYNC mode.

From modem hardware Revision D onwards, the SYNC LED drive is used to generate a DCD function in the user interface connector, and requires firmware revision V2.1.4 onwards (i.e. firmware revision V2.1.4 onwards drives the SYNC LED ON 20 mS after the "leading edge" of the RxSig LED).

This means that the SYNC LED drive should always show this function and not be allowed to show low Tx Power (see Error indication modes section 3.8.5.2). To facilitate this the Min Tx Pwr parameter in the TC-900DR modem should be set to zero, when the modem is built for synchronous operation.

### 3.9.11.3 Radio Transmitter Active Indication. TXMIT LED

This LED indicator is connected directly to the modem's PTT output drive. It is illuminated whenever the PTT line to the radio board is active.

### 3.9.12 SPECIAL MODES OF OPERATION

### 3.9.12.1 Programmer Mode

Part of the power-up/reset initialisation phase of the modem, are tests to determine whether the modem should enter a special operation mode. The first, is a test for "Programmer Mode". Pin6 on the DB9 connector of Port A, is normally the DSR line. To this end, this pin is pulled high by a resistor to +13.8 v , so that to a connected DTE this signal says that this DCE is ready. However, if this pin is connected to pin5 (Com) when the modem is powered up, the modem senses this, and attempts to enter "Programmer Mode". The modem sends out of PORTA, an ASCII "?" (question mark) character, and waits for the programmer to reply with a password. Failure to supply the correct password in time, will cause the modem to abandon the "Programmer Mode" attempt, and go on with it's normal power-up procedure. This password protection scheme provides some defence against unauthorised tampering with the radio/modem's configuration data.

### 3.9.12.2 Bit Error Rate Test Mode

The next test, is one for "Bit Error Rate Test Mode". Pin9 of the DB9 connector of Port A, is normally the Ring Indicate output line. The modem includes a resistive pulldown to Gnd to show a negative condition on this line. However, if this pin is driven positive (typically by connecting it to pin6), then the modem's data transmitter and receiver will enter the BER test mode. It will activate the RF transmitter and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic "1" level in the unscrambled data. A test point on the modem PCB, is available to monitor this point with
a frequency/event counter. (In fact this test point is always active, and may be used to monitor the received data decoded by the modem IC). Each error bit in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a " 0 " bit. An internal timer is used to generate a time equivalent to 1000 bits. Every error bit detected, will activate the SYNC LED, and restart the timer. If and when the timer expires, the SYNC LED is deactivated. Thus, for error rates of 1 in $10^{3}$ and above, the SYNC LED will be ON most of the time. A 1 in $10^{4}$ error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for installation purposes. Other functions performed in this state include RXSIG indication, and temperature compensation. The state of pin9 is constantly monitored in this mode. If the pin ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

### 3.9.12.3 Order_Wire/Handset Mode

Failure of the BERT Mode test, brings the modem to test for the presence of a handset plugged into the handset audio port. This is done by measuring the voltage on channel 4 of the analogue to digital converter. If a handset is plugged in, then the measured voltage will be about 2 volt, but if it isn't installed, then the voltage will be about 4 volt. The measured voltage is compared to 3 volt to determine whether the handset is plugged in. If this test succeeds, then the modem will not generate a data waveform to the radio transmitter. However, it will continue to indicate received RF signal strength, and perform temperature compensation. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED.

### 3.9.12.4 Error Indication Modes

There are three error conditions that will cause the RXSIG and SYNC LEDs to be used for error indications and not their normal purpose. Two of these are "fatal" conditions, that cause the modem to restart after the duration of the error indication phase.

### 3.9.12.5 Transmit Power Low

While the modem activates the radio transmitter, it periodically checks the level of the radio transmitter output power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately four times per second. Of course, the TXMIT LED will also be on in this case. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function. The user should be aware that from Revision D of the modem PCB, this state will cause incorrect operation of the DCD output line. As stated above, the Min Tx Pwr parameter should be set to zero.

### 3.9.12.6 NVRAM Read Error

The modem accesses the non-volatile memory as part of it's initialisation phase, to get configuration data. If the communication protocol with the memory device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED winks on and off twice, then the other. A total of five cycles of this occurs, then the modem restarts it's initialisation from scratch.

### 3.9.12.7 Radio Frequency Synthesiser, Lock Detect Error

If at any time during normal operation, BERT mode, or handset mode, the frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting. One LED is turned ON, the LEDs are swapped, then both off. Then the latter LED ON again, swap LEDS, and OFF. This will give the appearance of a sweeping motion between the LEDs. The following table shows all three modes for comparison.

| Tx PWR Error |  | NVRAM Error |  | TBB206 Error Synthesiser |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | - | 0 | - | 0 | - |
| - | 0 | - | - | - | 0 |
| 0 | - | 0 | - | - | - |
| - | 0 | - | - | - | 0 |
| 0 | - | - | 0 | 0 | - |
| - | 0 | - | - | - | - |
| 0 | - | - | 0 |  | repeat |
| - | 0 | - | $\bullet$ |  |  |
| continue |  |  | repeat |  |  |

### 3.9.13 WIRING ADAPTOR HARNESS FOR TC-900DR SYNCHRONOUS MODEL

| PORT A | 1 (DCD) | (RCO) |  | DB25F |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 (RxD) | $(\mathrm{R} \times \mathrm{D})$ | 3 |  |
|  | 3 (TxD) | (TxD) | 2 |  |
|  | 4 (DTR) | (DTR) | 20 |  |
|  | 5 (Com) | (Com) | 7 |  |
|  | 6 (DSR) | (DSR) | 6 |  |
|  | 7 (RTS) | (RTS) | 4 |  |
|  | 8 (CTS) | (CTS) | 5 |  |
|  | 9 (RI) |  |  |  |
| PORT B | 1 (DCD) | (DCD) | 8 |  |
|  | 2 (RxD) | (TCO) | 15 |  |
|  | 3 (TxD) | (TCI) | 24 |  |
|  | 4 |  |  |  |
|  | 5 (Com) |  |  |  |
|  | 6 (DSR) |  |  |  |
|  | 7 |  |  |  |
|  | 8 |  |  |  |
|  | 9 (RSSI) |  |  |  |

## SECTION 4

## ALIGNMENT PROCEDURE

## 4 ALIGNMENT PROCEDURE

### 4.1 GENERAL

This section details operational performance and alignment procedures that may be required for the TC-900DR. During servicing it may also be necessary to measure specific performance parameters as a means of verifying the presence of a fault condition.

### 4.2 TEST EQUIPMENT REQUIRED

The following list of test equipment is required to carry out all of the procedures detailed below.

- Frequency counter accurate to better than 100 Hz at 1 GHz
- $\quad \mathrm{FM}$ Signal generator. 455 kHz to $1 \mathrm{GHz} .-120 \mathrm{dBm}$ to +10 dbm . Synthesised in 100 Hz steps.
- Spectrum analyser 10 MHz to 1 GHz . Dispersion down to $2 \mathrm{kHz} / \mathrm{cm} .80+$ dB dynamic range. $\mathrm{IF} \mathrm{b} / \mathrm{w}$ down to 1 kHz .
- RF Power meter to $1 \mathrm{GHz} .-20$ to +30 dbm . Accuracy $\pm 0.25 \mathrm{~dB}$.
- Digital volt meter.
- HP3406 RF Millivoltmeter or similar.
- RF Test leads, MCX male and SMA male.
- Audio noise and distortion test set.
- Audio oscillator.
- Surface mount repair tools.


### 4.3 TEST POINT LOCA TIONS

Both the radio section PCB and the modem section PCB contain numerous test points. They are easily located on the PCB's, and are detailed below.

### 4.3.1 MODEM SECTION PCB

| TEST POINT |  | SIGNAL |  |
| :--- | :--- | :--- | :--- |
| TP1 |  | DESCRIPTION |  |
| TXCLK |  | Transmit clock |  |
| TP2 |  | TxCR TST |  |
| TP3 |  | SYR test output |  |
| TP4 |  | RxCLKOUT | Synchronised output |
| TP5 | RxCLK | Integrator reset |  |
| TP6 | RxDATA | Receive clock |  |
| TP7 | DATA OUT | Receive data |  |
| TP8 | INTEGRATOR | Transmit data |  |
|  |  | Rxintegrator reset |  |

### 4.3.2 RADIO SECTION PCB

| TEST POINT | SIGNAL | DESCRIPTION |
| :---: | :---: | :---: |
| FINAL PA SECTION |  |  |
| TP31 | TXPW | R-2 Bias to Q8 |
| TP25 | TXPV | R-3 Bias to Q8 |
| TP27 | TXPW | R-4 Bias to Q9 |
| TP14 | +8v | Power Supply |
| TP15 | TXEN | Transmit enable |
| TP20 | RxMI | XOUT Rxmixer bias |
| TP28 | TXPA-1 | Bias to Q10 |
| TP29 | TXPA-2 | Bias to Q11 |
| TP26 | +13V8 | Power supply |
| TP33 | PWR CONT | Power control supply |
| TP30 | PTT+8V | Press to talk |
| 121 MHz SECTION |  |  |
| TP13 | DATA | Tx data input |
| TP17 | 60.5 MHz | Modulated 60.5 MHz |
| TP16 | 121 MHz | Output of doubler |
| TP18 | 121 MHz | Modulated 121 MHz |
| TP32 | MIC | Tx Mic audio input |
| NE615 IF SECTION |  |  |
| TP6 | 415kHz I/P | 455 filter input/second mixer output |
| TP9 | QUAD | Quad detector |
| TP8 | DATA | Rx data out |
| TP10 | AUDIO | Rxaudio out |
| TP7 | RSSI | RSSI output |
| TP4 | MUTE | Mute control output |
| TP1 | 2nd L.O | Second Xtal oscillator |
| TP2 | 2nd L.O | Second Xtal oscillator |
| TP3 | IF Input | 45 MHz IF filter input |
| TP5 | IF Output | 45 MHz IF filter output |
| TP19 | Vco | VCO oscillator injection |
| SYNTHESISERNCO SECTION |  |  |
| TP12 | LOCK DET | Synthesiser lock detect |
| TP11 | +5V | Synthesiser +5 v supply |
| AUXILIARY HANDSET INTERFACE SECTION |  |  |
| TP21 | MIC | Tx mic audio input |
| TP22 | PTT | Manual press to talk |
| TP23 | +8V | Handset +8 V supply |
| TP24 | AUDIO OUT | Rx audio output |

### 4.4 ADJUSTMENT POINTS

All adjustment points are located on the radio section PCB. The following is a list of these adjustable components.

| COMPONENT | ADJUSTMENT |
| :--- | :--- |
| XTAL2 | VCO reference frequency |
| VR3 | Deviation level set |
| L10 | Tripler filter |
| L9 | Doubler filter |
| L7 | 121 MHz filter |
| L8 | 121 MHz final filter |
| L6 | Tx frequency set (121MHz Osc) |
| VR4 | Tx power control adjust |
| C78 | Tx mixer tunable filter |
| VR1 | Rx audio mute adjust |
| VR2 | Rx data DC BIAS offset adjust |
| L3 | 45 MHz filter alignment |
| L1 | 44.545 oscillator adjust |
| L4 | 45 MHz filter alignment |
| L5 | 45 MHz filter alignment |

### 4.5 LINK OPTIONS

Several options are set in the TC-900DR modem by the setting of links on the radio section PCB. Listed below is an option table for the various combinations.

| LINK NUMBER | SETTING |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| LK2 |  |  |  |  |
|  | IN |  | AFC option disabled |  |
|  | OUT | AFC option enabled | (factory standard) |  |
| LK4 | IN | PWR control disable |  |  |
|  | OUT | PWR control enabled |  |  |

### 4.6 HOUSING

The TC-900DR has been designed with the serviceability of the unit in mind. Construction of the unit is robust yet easily dismantled. The unit is primarily assembled in an aluminium extrusion with a central chassis that is fixed to the front panel.

### 4.6.1 DISASSEMBLY PROCEDURE

To disassemble the unit, simply remove the two silver screws on the underside of the unit and the six black screws located on the front panel (the front panel of the unit has the two DB9 connectors protruding from it). Ensure you do not loose the attached nylon washers, as these prevent the Lexan front panel label being damaged upon replacing and tightening the six screws. Simply slide the unit out of the extrusion clasping front panel and the complete unit is exposed to you.

Caution : When re-assembling be careful not to foul the ribbon cable against the case when sliding the unit into its case as this may inadvertently damage the cable.

### 4.6.2 MODEM AND POWER SUPPLY PCB

All components and connections to the modem section PCB are accessible without removing the PCB from the chassis. If access to the rear of the PCB is required, firstly remove two nuts that clamp the C TO-220 power supply regulator to the front panel. Once this is removed, simply remove the four screws securing the PCB to the chassis.

The PCB is now free to work on, and can be folded out so as to service the unit in an open accessible condition whilst still connected to the radio section PCB. If required, the modem section PCB can be separated from the radio section PCB by simply unplugging the ribbon cable.

NOTE: Regulators will need to have heat-sinks fitted if unit is to be operated in this condition for excessive time periods.

### 4.6.3 ANTENNA DIPLEXER

The antenna diplexer is mounted on top of the radio section PCB. It is easily removed by firstly disconnecting the two miniature RF connectors (MCX type) from the PCB.

Care should be taken when unplugging these connectors so as not to damage them, it is important to remove and insert connectors in a vertical direction.

Secondly, remove the nut securing the antenna output connector from the central mounting chassis. The last two remaining screws must be removed which secure the diplexer to two metal PCB standoffs on the radio section PCB. The diplexer can now be removed.

Testing of the radio section PCB can be continued without the antenna diplexer, by connecting to the receiver and transmitter ports separately.

Miniature MCX RF Connectors are available from Trio DataCom if required.

### 4.6.4 RADIO SECTION PCB

The radio section consists of a two sided PCB which has surface mount components on one side and conventional components on the other. Several critical test points are accessible on the component side of the PCB which minimises removal of the PCB from the chassis.

To remove the PCB from the chassis, fifteen screws must be removed. Upon removal of these screws, the PCB can be manoeuvred from the chassis and once again can fold out so as to be serviceable as a complete unit.

NOTE : It is essential that all RF Deck mounting bolts are fitted and secure upon reassembly as many of these bolts provide inter-stage isolation and secure grounding ensuring the product meets all specifications.

Once service of the unit is complete, reassembly is simply the reversal of the above procedures.

Care should be taken when sliding the complete chassis assembly back into the extrusion. Ensure that the ribbon cable connecting the modem and radio section PCB's is carefully "tucked" away within its designated slot so as not to damage the cable.

### 4.7 ALIGNMENT DESCRIPTION

CAUTION - As the TC-900DR is capable of full duplex operation, care should be taken to avoid damage to sensitive test equipment such as signal generators or spectrum analysers. It is recommended that a 30 db 2 Watt pad be connected between the unit and any test equipment prior to testing.

This section is for alignment/adjustment of the RF Deck and should be read in conjunction with Section 2 (Hardware Technical Description) and Section 7 (Fault Finding) if faults or difficulties are experienced.

For initial alignment, proceed in the following order :
Reference oscillator \& synthesiser.
121 MHz Tx modulated injection oscillator.
Tx final stage/Power control.
Receiver and audio mute

### 4.7.1 REFERENCE OSCILLATOR AND SYNTHESIZER

1 Check VCXO (XTAL2) for reference frequency o/p at a level of 550 mV rms with an RF Millivoltmeter, and the VCO o/p for an RF level of around 150 mV rms.

2 Check that the TBB202 dual modulus prescaler (U4) is producing an output of approximately 7 MHz and a level of 550 mV rms at the "IF" $\mathrm{i} / \mathrm{p}$ to the TBB206 synthesiser I.C.(U3-p8)

3 Ensure that the synthesiser has been programmed to a frequency within the range of the VCO, and check that the VCO is locked by observing a high ( 5 V ) level on Lock detect output of the synthesiser I.C.(U3-p14). Note that very short duration pulses to ground is normal.

4 Program the synthesiser with the following VCO frequencies according to VCO type and ensure lock occurs at both ends of the frequency range. These frequencies are 2 MHz beyond the published specification.
VCO TYPE: MQC-798
Maximum 786 MHz VCO $=907 \mathrm{MHz}$ Tx or 831 MHz Rx
Minimum 814 MHz VCO $=935 \mathrm{MHz}$ Tx or 859 MHz Rx
VCO TYPE: MQC-978
Maximum $\quad 996 \mathrm{MHz}$ VCO $=875 \mathrm{MHz}$ Tx or 951 MHz Rx
Minimum $\quad 960 \mathrm{MHz} \mathrm{VCO}=839 \mathrm{MHz}$ Tx or 915 MHz Rx
5 Program the VCO to a given frequency within the range as specified above and measuring the VCO o/p frequency, adjust the 12 MHz (VCXO) reference trimmer to bring the frequency within 250 Hz of the VCO frequency.
Note: Unit is temperature compensated at factory and no field adjustment of Ref. Oscillator is possible. If VCO frequency is not correct ( $\pm 1500 \mathrm{~Hz}$ ), consult factory for service advice.
Note ensure that the VCXO control input is within its active range (1-4 Volts).

6 Check the VCO power o/p by monitoring the Rx mixer bias at TP20, where approximately 200 mVDC should be measured.

7 With a spectrum analyser set to the VCO frequency and a dispersion of about 5 or 10 kHz per cm , check that the reference sidebands are less than -60 dBc in the adjacent channel.

8 Check VTCXO Reference frequency is $\mathrm{F}(\mathrm{tx})+121 \mathrm{MHz}$ for 853 remote units or $\mathrm{F}(\mathrm{tx})-121 \mathrm{MHz}$ for master units. If Reference is out by more than $\pm 1.5 \mathrm{kHz}$, drift offset should be applied via the programmer or unit should be returned for factory service. attempting to alter Reference trimmer will void temperature compensation process and should only be done in an emergency and as a temporary measure.

### 4.7.2 121 MHZ MODULATOR

Note - make sure the transmitter is loaded with a suitable attenuator on the antenna or Tx o/p socket before energising

1. For Initial alignment set all coil cores to their nominal positions as per the table below :

Miller coils
L9 5 turns from top of coil can
L10 2 turns
L7 4 turns
L8 5 turns
L6 0 turns
To prevent the final transmitter stages from producing excessive power whilst low level stages are being aligned, it is suggested that the Tx post mixer tunable filter be de-tuned. Energise the transmitter via manual PTT from the auxiliary handset.
2. Tune L 7 through L 10 for peak $\mathrm{o} / \mathrm{p}$. For initial alignment this can be done by monitoring the 121 MHz level at TP18 initially and then at the input to the SBL-1X transmit mixer (U8), where a level of about 75 mV should be measured by an RF millivoltmeter (e.g HP11960).

Typical RF millivoltmeter readings for each stage are :

| TP17 | $125 \mathrm{mVRF}=0.25 \mathrm{VDC}$ on HP11960 probe. |
| :--- | :--- |
| TP16 | $40 \mathrm{mVRF}=0.06 \mathrm{VDC}$ on HP11960 probe. |
| TP18 | $550 \mathrm{mVRF}=1.0 \mathrm{VDC}$ on HP11960 probe. |
| 121 MHz i/p to mixer | $75 \mathrm{mVRF}=0.13 \mathrm{VDC}$ on HP11960 probe. |

Note: The signal at TP17 is present as long as "Tx En" is active. The subsequent test points require PTT to also be active.

If the complete transmit chain is known to be operative then the $121 \mathrm{MHz} \mathrm{o/p} \mathrm{can}$ be peaked by first de-tuning C78 on the tunable Tx filter until the Tx power o/p is less than 100 mW and then tuning Inductors L7 to L10 for maximum output at the Tx frequency.
3. With the radio section links set for the desired data rate (see link table above), set the peak deviation as per the chart below with VR3, and center frequency to 121.000 MHz with L6.

NOTE : THESE ADJUSTMENTS ARE INTERACTIVE. ENSURE ALL COILS ARE SECURE BAUD RATE 4800 bps

DEVIATION LEVEL
$\pm 1.5 \mathrm{kHz}$ peak
$9600 \mathrm{bps} \quad \pm 2.75 \mathrm{kHz}$ peak
4. Note that temperature compensation is applied to the 121 MHz oscillator so attempting to adjust either VR3 or L6 will upset compensation and should only be done as a temporary measure. Return unit to factory for repair if errors $> \pm 500 \mathrm{~Hz}$ are detected.

### 4.7.3 TX FINAL

NOTE: It is essential that all RF Deck mounting bolts are fitted and secure upon reassembly as many of these bolts provide inter-stage isolation and secure grounding ensuring the product meets all specifications.

1 Ensure the 121 MHz Tx injection is operating correctly.
2 Check Q2,4,5,8, are all biased correctly as per the voltage chart.
Temporarily disable the Tx power control circuitry by shorting LK4 located on the top side of the board near the ribbon cable.
Energise the transmitter via the manual PTT on the auxiliary handset.
3 Tune the Tx filter tuning capacitor C78 for a peak output power measured at Antenna port or X4.
4 With full drive, Q9 driver collector current as seen across TP26//TP27 should be approximately $45 \mathrm{~mA}(100 \mathrm{mVDC})$, and NOT MORE THAN $55 \mathrm{~mA}(120 \mathrm{mVDC})$.
5 With full drive at Q9 each final transistor should be drawing around 175 $\mathrm{mA}(385 \mathrm{mVDC})$ as seen across TP26/TP29 or TP28. The output power measured directly at the final connector should be between +32 and +34 dbm without power control.

6 Re-enable the power control circuitry and with the 'Txpwr' control line set at +5 VDC , set VR4 for $+32 \mathrm{dbm}+/-0.25 \mathrm{~dB}$ at the tx o/p socket X4. Check that the current in EACH final collector does NOT EXCEED 225 mA .

7 Check with the spectrum analyser that the $T x o / p$ is free from spurious signals.
Note 1 . Prior to the diplexer the VCO level is nominally about -20 dbc .

> Note 2. Close in mixing products (less than $+/-30 \mathrm{MHz}$ ) must be greater than 65 db below the carrier, as they are not attenuated by the diplexer filters.

## D.C. Voltages of Radio Section

RF Output Power set to +32 dbm at X4 (diplexer input) with 13.8 VDC supply

| Transistor | Base | Emitter | Collector |
| :--- | :--- | :--- | :--- |
| Q2 | 1.66 VDC | 0.92 VDC | 6.96 VDC |
| Q4 | 1.79 VDC | 1.06 VDC | 6.46 VDC |
| Q5 | 1.80 VDC | 1.08 VDC | 7.51 VDC |
| Q8 | 1.05 VDC | 0.31 VDC | 4.02 VDC |
| Q9 | 0.47 VDC | 0 VDC | 13.35 VDC |
| Q10 | 0.28 VDC | 0 VDC | 13.05 VDC |
| Q11 | 0.29 VDC | 0 VDC | 13.16 VDC |
| Q12 | 7.17 VDC | 7.97 VDC | 7.88 VDC |
| Q1 | 7.29 VDC | 7.97 VDC | 7.91 VDC |
| Q13 | 4.56 VDC | 3.84 VDC | 7.97 VDC |
| Q7 | 1.14 VDC | 0.41 VDC | 6.68 VDC |
| Q6 | 1.13 VDC | 0.40 VDC | 7.52 VDC |
| Q3 | 1.06 VDC | 0.33 VDC | 7.59 VDC |

### 4.7.4 RECEIVER

The receiver section requires little or no alignment once factory aligned.

### 4.7.4.1 No AFC Models (Xtal $1=\mathbf{4 5 . 4 5 5 M H z}$ )

1 Adjust L1 for 45.455 MHz measured with pickup loop near L1.
2 In emergency adjust coils L3, L4 and L5 for best SINAD at TP8.
3 Adjust audio mute VR1 to mute handset audio at 10dB SINAD
4 Adjust VR2 for 2.0 VDC at TP8 whilst receiving data off-air.

### 4.7.4.2 AFC Models

Monitor 44.545 MHz with pickup at L1. Test for $44.545 \pm 1.5 \mathrm{KHz}$
Consult factory for alignment or service information.

## SECTION 5

## INSTALLATION AND COMMISSIONING

## 5 INSTALLATION OVERVIEW

All Data Radio Modem devices needs to be properly installed and commissioned in order to function reliably. It is important that installers are familiar with RF products / installations and are geared up with appropriate tools necessary to confirm the ongoing reliability of a communications system.

This chapter is intended as a short form checklist to ensure such radio devices are installed correctly and that important tests are made and recorded at each site for future reference should a problem eventuate.

Installers should check that each data radio has been programmed to suit their specific requirements before installation.

### 5.1 GENERAL

Installations play a critical role in network performance. Although this is a known fact, installations are often performed poorly or given little regard. It is essential that the installation is performed in a professional manner with careful attention and consideration to the following items :

1. Adequate primary power cable - relative to the length of cable to minimise voltage drop.
2. Shielded data cable between the unit and any external data equipment.
3. Low loss coax used for antenna feed line.
4. Careful termination of RF connectors.
5. A suitable antenna for the requirement.
6. Suitable placement of the antenna.
7. Adequate signal strength from the base station / other radio communications device.

### 5.2 INSTALLATION

The following information should assist when installing and commissioning data radio systems.

### 5.2.1 DATA CONNECTION

In industrial environments connection to any external device should be by shielded data cable with the shield connected to the connector shell to minimise data corruption, and/or radio interference.

### 5.2.2 MOUNTING

The radio modem should be mounted in a cool, dry, and vibration free environment. Mounting of the unit should be in a location providing easy access to screws and all connections.

### 5.2.3 POWER CONNECTIONS

The power required for $5 \mathrm{Watt}(\mathrm{Tx})$ at 13.8 VDC , is typically 2.0 Amps. As the $T x$ key up current is significant, the gauge of primary power wiring should be considered. It is suggested that a minimum of 18 gauge stranded copper wire be used for distances of up to two metres and a minimum of 14 gauge for longer distances up to 5 metres.

Ensure correct polarity to avoid costly repairs.

### 5.2.4 COAX CABLE CONNECTION

It is important to select the correct cable and connectors for each application as a poor selection can seriously degrade the performance of the unit.

As an example, for each 3 dB of cable and connector loss, half the transmitter power is lost and twice the receiver signal power is required to produce the same bit error rate.

In some installations where strong signals are present, a compromise of cable and connector cost may be acceptable.
It is essential that all connector terminations are performed as per the manufacturers specifications (especially at 900 MHz and above) and if connectors are to be used outside, it is essential that a sealant such as amalgamating tape be used to seal connectors. DO NOT use acetic cure silicon to seal the connectors.

It is also important that coax cables are not stressed by tight bends, kinking or excessive flexing. Ensure that coax cables have sufficient strain relief and are secure. If large diameter rigid or semi rigid cable is used, it is recommended to use a short length of high quality RG58 or RG223 cable between the unit and main cable feed.

The following chart is a guide to losses in various types of coaxes at 400 MHz and 900 MHz over distance, please consider this when installing the unit.

| CABLE TYPE | LOSS RELATIVE TO DISTANCE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 dB |  | 3 dB |  | 6 dB |  | 9 dB |  |
|  | 450 MHz | 900 MHz | 450 MHz | 900 MHz | 450 MHz | 900 MHz | 450 MHz | 900 MHz |
| RG58C/U | 2.3m | 1.6m | 7 m | 5 m | 14m | 10 m | 20 m | 15m |
| RG223/U | 3.1 m | 2.3m | 9 m | 7m | 18m | 14m | 28m | 21m |
| RG213/U | 6.1 m | 4 m | 18m | 12m | 37 m | 24m | 55m | 37m |
| $\begin{array}{\|l\|} \hline \text { HELIAX } \\ \text { LDF4-50A } \end{array}$ | 19m | 14m | 57m | 43m | 114m | 87m | 171m | 130m |
| $\begin{array}{\|l\|} \hline \text { HELIAX } \\ \text { LDF5-50A } \end{array}$ | 38m | 25m | 114m | 75m | 229m | 150m | 343m | 225m |

### 5.3 ANTENNA INSTALLATION

The selection of antennas and their placement is one of the most important factors when installing a radio based network. People often use a simile, it is like putting square wheels on a Mercedes Benz..... very true comparison.

Antennas are generally mounted to a vertical pole with either vertical or horizontal polarisation as per the licence requirement.

Antennas should be mounted as high as practical and away from metal surfaces which can cause reflections.

Determining the type of antenna is very important and as a typical generic example, Point to Multipoint (PTMP) systems generally employ high gain ( 3,6 , or 9 dB gain) omni directional antennas at the base station sites and either omni directional whips (unity gain) or preferably high gain directional yagi antennas ( 9 or 14 dB gain) at the remote sites.

### 5.3.1 YAGI ANTENNAS

Yagi antennas not only provide signal gain and directivity, but also provides protection from interfering signals which are outside the beam width of the antenna. Yagi antennas are essential when communicating over very long distances.

Yagi antennas are polarised and must be mounted either vertically (elements pointing from the ground to the sky) or horizontally (elements in parallel with the horizon).

As a general rule, Point to Multipoint remote units are vertically polarised, while Point to Point links are horizontally polarised.

When mounting yagi antennas with vertical polarisation, it should be noted that the dipole (loop section of antenna) has a drain hole. The small drain hole on one end of the dipole must be pointed towards the ground so that water will drain out of the antenna.

### 5.3.2 OMNI DIRECTIONAL ANTENNAS

Omni directional antennas provide a radiation pattern of equal strength through $360^{\circ}$ in the horizontal plane. This makes them ideal for base antennas in point to multipoint systems because they can reach the remote antennas.

Omni directional antennas are also used at remote sites (although yagi antennas are preferred) and are typically ground independent "whip" type antennas. The main reason for using whips at remote sites is for aesthetics as they are far less obtrusive than a yagi.

Regardless of the type, antennas need to be mounted properly and in a suitable location as covered below.

### 5.3.3 ANTENNA PLACEMENT

Antenna placement is of paramount importance and plays a big part of the antennas and in turn systems performance.

When choosing antenna locations the aim is to find the largest path of unobstructed space and locate the antennas within that space. It is important to locate antennas as high as possible and definitely clear of any moving obstructions.

Where possible it is important to avoid mounting antennas:

1. Against or adjacent to steel structures.
2. In an area which will have constant intermittent obstructions - people walking past, vehicles driving past etc. That is, mount antennas well above such moving obstructions.
3. Near any electrical equipment.
4. Near metal beams, structures etc.
5. Inside any metal enclosures, tin sheds / warehouses etc. - note meshed wire fences act like a "brick wall" to RF transmissions.
6. Away from guard rails or support beams.

Note: Sometimes installations in such environments are unavoidable and where this is the case, certain care can be taken to still ensure a reliable installation. Please consult Trio for assistance on a case by case basis.

If tests indicate poor signal strength then the antennas at one or both ends of the link should be raised, and/or moved clear of obstructing objects, or if directional antennas are employed they should be checked for correct directional orientation and polarisation (horizontal or vertical signal orientation).

### 5.3.4 REFLECTIONS AND OUTPUT POWER

Ideally, the propagation path should be clear Line of Site (LOS).
The biggest problem with UHF radio when used within "steel" buildings or obstructed paths is the large presence of signals randomly reflected from the surrounding obstructions or "steel" walls. These signals cannot be eliminated, but by maintaining a 10 to 20 dB margin between the wanted and unwanted signals, problems should not be experienced. The simplest way to do this is to use directional gain antennas.

These antennas will provide attenuation to all signals arriving from a direction other than the direct path. Where steel walls or structure exist immediately behind the antenna location, the high front to back ratio of such antennas will negate such high level reflections. Power output should be set at the minimum level required to achieve a 25 dB fade margin, in order to minimise the amount of RF being reflected, and to avoid saturating the receiver front end and therefore reducing the margin between wanted and unwanted signals.

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### 5.4 COMMISSIONING - RSSI LEVEL

When commissioning a data radio network, it is important to ensure that the incoming received signal strength (RSSI) is adequate to provide reliable communications.

Note: A good signal path should allow for approximately 30 dB fade margin.
Received signal strength (RSSI) of the incoming signal is available as an analogue output on Trio data radio modems. This RSSI output ranges from 0 to approx 4 Volts, where 4 Volts indicates the strongest signal. The actual values of received signal strength can be determined by comparing the output voltage against the calibrated graph supplied in the handbook.

By referring to the RSSI chart alignment of aerials can be optimised to achieve the greatest signal strength (highest output voltage).

Note: Be sure to stand clear of aerials when measuring this output voltage, touching or standing in close proximity to aerials will give inaccurate readings.

### 5.4.1 CHECKING DATA COMMUNICATIONS

If the host computer and remote equipment are capable of performing data integrity tests then connect the host and terminal data equipment to the radio modems.

Remove and re-apply power to each radio modem to ensure they are both in data comms mode, and run data tests on the link.

### 5.4.2 BIT ERROR RATE (BER) TESTING

If the connected data equipment is NOT capable of running data integrity tests then the TC-450DS modems can be put into a BER test mode, whereby the data channel can be tested in each direction to a reasonable level without external test equipment. To run a link test with the radio modems themselves, they must BOTH be put into BER test mode.

To place the unit in BER mode connect pin 6 and pin 9 of port A together and apply power..

The transmitter can be activated by driving the RTS pin (7) of port A positive. The unit will then send a predefined pseudo random sequence which is tested for accuracy by the receiving unit and any errors displayed on the front panel 'SYNC' lamp.

Each error bit will illuminate the lamp for approximately 1000 bits duration, therefore error rates above 1 in 1000 will show an almost constant error indication.

To return the unit to normal data transmission mode simply power it up without pin 9 connected to pin 6.

For further information on radio path problems please contact Trio DataCom for detailed advice.

Note : BER testing is not viable in an operational point to multi-point environment as the BER test will interfere with other operative units.

### 5.4.3 OUTPUT POWER - VSWR

Upon installation of equipment an output power measurement should be done using a suitable power meter. Forward and reflected power should be measured at the antenna port and recorded for future reference. The reflected power measurement should be as a minimum 3:1 of the forward power. If this is not the case, investigate possible causes such as poor terminations, faulty antenna etc.

### 5.4.4 DATA CONNECTION

The data connection is via a DB9 connector labelled 'Port A', which is wired as a DCE as shown below. The port labelled 'Port B ' is not used for the standard configuration but can be enabled by the programmer for use as a totally independent second data channel. In industrial environments connection to the modem should be by shielded data cable with the shield connected to the connector shell to minimise data corruption, and radio interference.

## - User Serial "Port A" Pin Assignment

PIN NO. \& FUNCTION

1. DATA CARRIER DETECT (DCD)
2. RECEIVE DATA OUTPUT (RXD)
3. TRANSMIT DATA IN (TXD)
4. DATA TERMINAL READY (DTR)
5. COMMON (COM) $\qquad$
6. PROGRAM PIN (PGM)
7. REQUEST TO SEND (RTS)
8. CLEAR TO SEND (CTS)

## EXTERNAL VIEW OF 'PORT A'


9. BIT ERROR RATE PIN (BER)

NOTE: Pin 6 and pin 9 provide a dual function which depends on the mode that the TC-450DR is operating in.

## - User Serial "Port B" Pin Assignment.

Port B of the TC450DR is essentially unused in its standard configuration but can be enabled by the Programmer for use as a totally independent second data channel. This port is essentially used for specific applications and only has one connection that may be of use for installation purposes. This connection (Pin 9) is Receive Signal Strength Indicator (RSSI) output.
This RSSI output ranges from 0 to 5 Volts, where 5 Volts indicates the strongest signal. It is important to note that this Port output has a high impedance of around 10 K ohms and loading will decrease accuracy of the recorded measurement.

1. DATA CARRIER DETECT
2. RECEIVE DATA OIP (RxD)
3. TRANSMIT DATA O/P (TxD)
4. DATA TERMINAL READY (DTR)
5. COMMON
6. DATA SET READY (DSR)
7. REQUEST TO SEND (RTS)
8. CLEAR TO SEND (CTS)
9. RECEIVE SIGNAL STRENGTH

EXTERNAL VIEW OF 'PORT B'


### 5.5 GENERAL CHECKLIST

The following is a simple commissioning checklist which should be used at every site not only to ensure correct installation, but also as a reference list for problems which may eventuate.

| TRIO SITE COMMISSIONING CHECK LIST / RECORD |  |  |
| :--- | :--- | :--- |
| Company: | Operator: |  |
| Site Location: | Date: |  |
| Link to: | Serial \#: |  |
| Radio Type: | Config File Name: |  |
| Antenna Type / Gain | Path Distance |  |
| Tx Power at Radio | Measured RSSI Volts |  |
| Reflected Power | Fade Margin |  |
| VSWR | Line of Site to Base |  |
| Tx Power at Antenna | DC volts at Radio (Tx) |  |
| Site QA Inspection: |  |  |
|  |  |  |
|  |  |  |
| Notes: |  |  |
|  |  |  |

## SECTION 6

## FAULT FINDING

## 6 FAULT FINDING

This section is to assist with difficulties that may be experienced when installing or working on the TC-900DR.

### 6.1 MODEM/GENERAL

The following is a list of possible problem areas, and suggested checks that can be made to isolate any general problem that may have occurred.

1. POWER SUPPLY
a) Check for +13.8 Volts at supply input.
b) Check fuse on Modem PIS PCB (1 Amp SLO-BLOW).
c) Check supply volts:
$\begin{array}{ll}\text { Modem PIS } & \text { i) } 13.8 \text { Volts }\end{array}$
ii) 8 Volts
iii) 5 Volts

RF Deck i) 13.8 Volts
ii) 8 Volts
iii) 5 Volts

## 2. ANTENNA

a) Check antenna, cable and connectors for damage or water
b) Check forward and reflected power at antenna connector of unit.

VSWR should be $<=1.5: 1$

## 3. PROGRAMMING

Check programming information. e.g.
i) Transmit and receive frequencies are within the operating band of the unit
ii) User interface configuration.
4. INTERFACE
a) Check connections to Port A (DB9 Connector).
b) Check cable to host communications.
c) Interface commands to unit are incorrect or communications are not established correctly.

## 5. POOR TRANSMITTER PERFORMANCE

a) Check correct transmit frequency programmed.
b) Check transmitter carrier frequency.
c) Check transmitter deviation.
d) Check RF output power level.

## 6. POOR RECEIVER PERFORMANCE

a) Check correct receive frequency programmed.
b) Check receive sensitivity.
c) Check audio output level and DC bias to modem.
d) Check mute threshold.

### 6.2 RECEIVER

The following is a list of problem areas, and suggested checks that can be made to isolate any receiver specific problems that may have occurred.

### 6.2.1 RECEIVE SENSITIVITY LOW

1 Check mixer drive level by measuring DC bias developed across R27.
2 Check for correct DC bias conditions and supply volts on RF Amp, Local Osc buffer, and IF Strip, compared to voltage charts.

3 Ensure 44.545 MHz oscillator (part of NE615 IF IC) is within $\pm 250 \mathrm{~Hz}$. This is best carried out by using a communications test set such as an IFR1200 or similar in receiver mode with frequency error displayed.
4 Ensure that the local oscillator is netted to frequency by monitoring the Tx mixer injection with a pick up loop connected to a sensitive frequency counter of high stability. Adjust the VCXO frequency reference until correct L.O. frequency is observed. Note that the VCO and synthesiser use the VCXO as the frequency standard. Measure the Synthesiser LOCK signal to ensure the VCO is in phase lock.

5 With a 50 ohm signal generator tuned to 455 kHz , apply signal via a 1 nF capacitor to the inputs of the 1st and second IF Amp sections of the 615 IF IC and compare the level required to produce the correct RSSI level.

6 With a 50 OHM signal generator tuned to 45.000 MHz , apply signal to the points defined on the IF test chart and compare RF level required to produce the reference RSSI level as specified at TP4.

7 Apply signal frequency to the RF input connector at X2 and compare the level required to produce RSSI reference level at TP4 with that shown in the IF Level Chart.

8 Reconnect the Antenna Diplexer and apply the signal generator to the Antenna terminal of the diplexer. Adjust the generator level to provide the same Rx mixer bias from applied RF signal as was noted in 7) above. The level required should be no more than 3 dB ( Rx diplexer path loss) greater.

Note that the RSSI signal provided by the IF IC is a fairly accurate logarithmic scale between 0.5 and 4 VDC, providing about 0.5 VDC for each 10 dB of signal applied to the input of the IF Strip, and can be used as a reasonable measure of signal providing it is unmodulated and on center frequency at 455 kHz .

### 6.2.2 RECEIVER LEVEL CHART

The following chart lists the level (terminated) of a 50 OHM signal generator to produce 2.0VDC of RSSI at TP4 when applied as specified to the point shown and at the frequency indicated.

| FREQUENCY | CONNECTION POINT AND APPLICATION | NOM LEVEL |
| :--- | :--- | :--- |
| 455 kHz | Pin 20 of IC U2 NE615 via 1nF | -72 dBm |
| 455 kHz | Pin 18 of IC U2 NE615 via 1nF | -74 dBm |
| 455 kHz | Pin 1(i/p) of IF Filter CF2 via 1 nF | -58 dBm |
| 455 kHz | Pin 14 of IC U2 NE615 via 1nF | -43 dBm |
| 45 MHz | Rx i/p at X2 via coax direct | -49 dBm |
| 45 MHz | Mixer i/p following R.F. Amp | -62 dBm |
| 45 MHz | Mixer diode (D1) o/p across C100 | -61 dBm |
| 45 MHz | Junction of 1st \& 2nd 45 MHz crystal filter | -77 dBm |

### 6.3 TRANSMITTER

The following is a list of problem areas, and suggested checks that can be made to isolate any transmitter specific problems that may have occurred.

1. NO TRANSMIT
2. Check PTT circuit.
3. Check unit is programmed within its operational range.
4. Check if manual PTT (Rear Aux connector) keys transmitter.
5. Check if any transmitter output is present. Tuning required?

## 2. TRANSMITTER SPURIOUS EXCESSIVE

The probable cause is dependent upon the nature of the spurious as follows:
Carrier $\pm 910 \mathrm{kHz}$. - IF detector signal ( $2 \times 455$ ) modulating or mixing with carrier. Check 1 n bypass on reference $\mathrm{i} / \mathrm{p}$ to power control op-amp. Check bypasses on collectors and supply lines of low level transmitter stages, and L.O. buffer.

Carrier $\pm 20.166$ and/or 40.333 . - Excessive harmonics of 20.166 crystal oscillator in 121 MHz FM driver IC (U7). Check all pins of IC (U7) for correct DC conditions. Check all tuning inductors for 'normal Q', as 'soft' tuning will almost surely indicate an incorrect or faulty capacitor, or inductor.

Carrier $\pm$ VCXO reference frequency (approximately 7 MHz ). - Reference signal modulating VCO, or mixing with carrier in L.O.buffers. - Check Synthesiser supply bypasses, check for defective joints or components in and around the resistive divider at output of VCO.

Note that it is imperative that low frequency divider products be attenuated before they can reach the base/emitter junctions of the L.O. buffer transistors where they can mix with the VCO frequency.

Note also that poor SMD solder joints will provide nonlinear conductance and give rise to frequency mixing in this area. Check for faulty components or poor joints around the Synthesiser to VCO frequency control area, or VCO supply line bypassing.

Excessive Transmitter power radiated or conducted to the area of the VCO can also cause spurious effects and may enhance the levels of otherwise acceptable levels of spurious. If this is suspected, check that ALL chassis securing bolts are fitted and tight on the RF deck, and that ALL bypass capacitors and chokes are fitted and correct in and around the final $T x$ stages.
3. TRANSMITTER POWER LOW OR UNSTABLE :

1 Firstly - Ensure that ALL RF Deck mounting bolts are fitted and secure.
2 Check that the feed resistors used for current indication on all stages of the final are of correct value and firmly in circuit.

3 Check that the Tx L.O. buffer and post mixer buffers are correctly biased as per the voltage charts.

4 If necessary disconnect the final stages from the Tx post mixer buffers by removing the solder bridge between Q5 and Q8, and with an appropriate instrument measure the RF power available from the Tx buffers to the final pre-driver.
Note that the o/p impedance of the buffer is 50 OHM and must be measured by a 50 OHM instrument. It is highly recommended that a measuring spectrum analyser be used here as this instrument will also display the relationship between the wanted signal and other spurious or unwanted mixing products.
The nominal display seen at this point by a spectrum analyser is shown on the spectrum charts attached.

5 To test the final stages separate from the buffers - inject a signal from a 50 OHM generator at Tx frequency into pre-driver (Q8) via C122. The level required to drive the final to full output is shown on the Tx level chart.

6 Check that the current drawn by the driver transistor as measured across the feed resistor (TP28 to TP27) is within spec, and if not check and or replace the driver transistor or associated components as necessary.

7 Check that the current drawn by each final transistor as indicated by the voltage across the 2.2 OHM ( $2 \times 4.7$ ohm in parallel) collector feed resistors (TP26 to TP28 and TP29) is within the range stated in the voltage charts, and that both are within $10 \%$ of each other. If in error check components around final pair and replace final transistors as necessary.

NOTE it is possible for power transistors to be partly defective due to current or thermal abuse, and the fact that the devices are actually drawing current does not always indicate that they are producing full power at the collector.

## TX LEVEL CHART :

| Frequency | Connection Point \& Application | Level Remarks |
| :---: | :---: | :---: |
| Base band | Data from modem section TP13 (4800 baud) | 2 VD.C |
| Base band | Applied data signal to modulator U7 pin 3 (4800 baud level from modem) | $1 V_{p-p}$ |
| Base band | Audio signal to modulator TP32 | 0.84 VD.C <br> $60 \mathrm{mV}_{\mathrm{p}-\mathrm{p}}$ for VR3 set for maximum value $400 \mathrm{mV}_{\text {p.p }}$ for VR3 set for minimum value |
| Base band | Audio signal to modulator U7- pin 4 | $\begin{aligned} & 1.3 \mathrm{VD.C} \\ & 0.5 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} \end{aligned}$ |
| 121 MHz | Signal level at TP18:A | $-5 \mathrm{dBm}$ |
| Final Tx frequency | Output to diplexer connector X 1 | $3 W$ at maximum power setting |

## SECTION 7

## APPENDIX A

## DRAWINGS

## 7 APPENDIX A DRAWINGS

TC01-08-12 Data Radio Mounting Details
TC01-08-11 Data Radio Assembly Details
TC01-04-05 Data Radio Basic Modem 9K6/4K8 Component Loading Details
TC01-00-05 450DR / 900DR Packet Modem (2 sheets)
TC01-08-10 PWB Manufacturing Details 900DR Data Radio - Radio Board (2 sheets)
TC01-00-10 Data Radio Project Sheet
TC01-00-10 Data Radio Final PA (AFC Fitted)
TC01-00-10 Data Radio 121 MHz OSC (AFC Fitted)
TC01-00-10 Data Radio - Synthesiser - VCO (AFC Fitted)
TC01-00-10 Data Radio - NE6154K8/9K6 (AFC Fitted)
TC01-04-15 850-930 MHz Antenna Diplexer Component Side Assembly
TC01-05-10 Radio Board Top Side (C/S) Test Point \& Adjustment Location Details
TC01-05-10 Radio Board Bottom Side (S/S) Test Point \& Adjustment Location
Details
TC01-05-16 Duplex Radio BER/S $+\mathrm{N} / \mathrm{N}$ vs Sig
TC01-05-17 AFC Alignment Setup - Block Diagram
TC01-05-12 4800/9600 BPS Modem Functional Diagram
TC01-05-23 Asynchronous Modem Functional Diagram
TC01-05-19 Macro Block Diagram
TC01-05-18 Radio Section - Modem Section Interface
DR9-BLOK 900 MHz Radio Block Diagram
RSSI Level cf Received Signal (typical)

## SECTION 8

## APPENDIX B

## GLOSSARY of TERMS and ABBREVIATIONS

## 8 APPENDIX B GLOSSARY

ADC: Analogue to digital converter.
AFC: Automatic frequency control.
BER: Bit error rate.
bps: Bits per second.
C/DSMA: Carrier or data sense, multiple access scheme.
COM: Common.
CRC: Cyclic redundancy checksum.
CTS: Clear to send.
DAC: Digital to analogue converter.
DCD: Data carrier detect.
DCE: Data communications equipment.
DFM4-9: Trio DataCom digital modem chipset.
DIP: Dual in line package.
DOTAC: Department of Transport and Communications.
DSR: Data set ready.
DTR: Data terminal ready.
FCS: Frame check sequence.
FEND: Frame end.
FESC: Frame escape.
FIFO: $\quad$ First in first out.
FIR: $\quad$ Finite impulse response.

FM: Frequency modulation.
FSK: Frequency shift keying.
GPIB: General purpose interface bus.
HADR_EN: High address enable signal.
IC: Integrated circuit.
I.F.: Intermediate frequency.
i/p: Input.
KISS: Keep it simple stupid.
LADR_EN: Low address enable signal.
MSB: Most significant bit.
NVRAM: Non volatile RAM.
NRZ: Non return to zero.
NRZI: Non return to zero - inverted.
o/p: Output.
PCB: Printed circuit board.
PLL: Phase locked loop.
PMP: Point-to-multipoint.
ppm: Parts per million.
PTP: Point-to-point
PTT: Press to talk.
RF: Radio frequency.
RI: $\quad$ Ring indicate.
R_select: RAM read select signal.
SIO: Serial input/output.
RSSI: Receive signal strength indication.
RTS: Request to send.
Rx: Receive.
RXD: Receive data output.
SCADA: Supervisory control and data acquisition.
SLIP: Serial line interface protocol.

TC-900DR: Trio DataCom 900MHz full duplex data transceiver.
TC-DFM9IP: Trio DataCom TC-900DR parameter programming software suite.
TFEND: Transposed Frame End.
TFESC: Transposed Frame Escape.
TNC: Terminal node controller.
Tx: Transmit.
TXD: Transmit data in.
VCO: Voltage controlled oscillator.
W_select: RAM write select signal

# TECHNICAL DATA SHEET 

For<br>SEWAGE PUMP STATION SP218<br>Westlake Drv

Equipment Type: Impulse Suppressor
Location:
RTU Section
Model Numbers: ..... IS-50NX-C2
Manufacturer: Polyphaser
Supplier:

Brisbane Water



# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type:Radio/DC ConverterManufacturer:Powerbox
Supplier: Brisbane Water

## PBIH Series

## 15-150 WATTS DC/DC SINGLE OUTPUT

## Features

- Wide selection of models
- 4 input voltage ranges
- High efficiency
- Low output ripple
- Proven reliability
- Good thermal margins


| Specifications INPUT |  |
| :---: | :---: |
| Input voltage | 12VDC (9.2-16) |
|  | 24VDC (19-32) |
|  | 48VDC (38-63) |
|  | 110 VDC ( $85-140$ ) |
| Inrush current | 20A max. for 110V only |
| OUTPUT |  |
| Output voltage | See table |
| Voltage adjustment | $\pm 10 \%, \pm 5 \%$ for PBIH-F |
| Output current | See table |
| Ripple \& noise | Output Volts $\times 1 \%+50 \mathrm{mV}$ to - 100 mV pk -pk |
| Line regulation | $0.8 \%$ over input range |
| Load regulation | 0.9\%, 0\%-100\% load |
| Temperature coefficient | $0^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}, 0.03 \%$ per ${ }^{\circ} \mathrm{C}$ |
| Overvoltage protection | o.V. damp, PBIH-F <br> Output shutdown, PBIH-G, J, M, R-input must be switched off for at least $30 S$ to reactivate |
| Overcurrent protection | Fold back - PBIH-F <br> Current limiting, PBIH-G, , M, R (PBIH-R series is adjustable); PBIH110xxR models are not adjustable |
| Drift | Output $\mathrm{V} \times 0.5 \%+15(\mathrm{mV})$ per 8 hrs after 1 hr warm-up |
| Rise Time | $\begin{aligned} & 200 \mathrm{mS} \text { max. - PBIH-F, M, R } \\ & \left.100 \mathrm{mS} \text { max. }- \text { PBIH-G, J (at } 25^{\circ} \mathrm{C}\right) \end{aligned}$ |
| Holdup time | 10 mS (only 110 V input) |
| Remote sense | PBIH-R Series only |


| OPERATING |  |
| :---: | :---: |
| Efficiency | 70\%-89\% |
| Safety isolation (1 minute) | Type - 12, 24, 48V input Input - Output: 1500VAC Input-Case: 1500VAC Output-Case: 500VAC Type-110V input Input- Output: 2000VAC Input-Case: 2000VAC Output- Case: 500VAC |
| Insulation resistance | 50M (500VDC) Input - Case |
| Parallel operation | Consult sales office for details |
| Remote control | PBIH-R Series: <br> Open link: output normal Short link: output off |
| ENVIRONMENTAL |  |
| Operating temperature | $0^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ full load |
| Cooling | Convection cooled |
| Storage temperature | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Humidity | 85\% |
| Shock | 30G, PBIH-F, G and J |
| Vibration | ( $5 \mathrm{~Hz}-10 \mathrm{~Hz}, 10 \mathrm{~mm}$ ), $(10 \mathrm{~Hz}-50 \mathrm{~Hz}) 2 \mathrm{G}, \mathrm{PBIH}-\mathrm{F}, \mathrm{G}$ and J |
| STANDARDS AND APPROVALS |  |
| Safety | Designed to UL1950 |
| C-tick | AS/NZS CISPR11 Group 1, Class A |
| MECHANICAL |  |
| Weight | PBIH-F: 250g <br> PBIH-G: 380g <br> PBIH-J : 410 g <br> PBIH-M : 800g <br> PBIH-R: 1.4kg |

## PBIH Series

15-150 WATTS DC/DC SINGLE OUTPUT

## Selection Table

| MODEL <br> NUMBER <br> PBIH-1205F | $\begin{aligned} & \hline \text { INPUT } \\ & \hline 9.2-16 \mathrm{~V} \end{aligned}$ | OUTPUT |  | OUTPUT <br> POWER <br> $15 W$ |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 5 V | 3A |  |
| P8IH-1212F | $9.2-16 \mathrm{~V}$ | 12 V | 1.2A | 15W |
| P8th-1215F | $9.2-16 \mathrm{~V}$ | 15V | 1A | 15W |
| PBIH-1224F | 9.2 16V | 24 V | 0.62 A | 15W |
| PBIH-2405F | $19-32 \mathrm{~V}$ | 5 V | 3A | 15W |
| PBIH-2412F | 19.32 V | 12 V | 1.2A | 15W |
| PBIH-2415F | $19-32 \mathrm{~V}$ | 15V | 1A | 15W |
| PBIH-2424F | 19.32 V | 24 V | 0.62A | 15W |
| P81H-4805F | $38-63 \mathrm{~V}$ | 5 V | 3 A | 15W |
| PBIH-4812F | 38.63 V | 12 V | 1.2A | 15W |
| PBIH-4815F | 38.63 V | 15 V | 1A | 15W |
| PBIH-4824F | $38-63 \mathrm{~V}$ | 24 V | 0.62 A | 15W |
| PBIH-11005F | $85-140 \mathrm{~V}$ | 5 V | 3A | 15W |
| PBIH-11012F | 85.140 V | 12 V | 1.2A | 15W |
| PBIH-11015F | 85.140 V | 15 V | 1A | 15W |
| PBIH-11024F | $85-140 \mathrm{~V}$ | 24 V | 0.62A | 15W |
| PBIH-12056 | $9.2-16 \mathrm{~V}$ | 5 V | 5A | 25W |
| PBIH-1212G | 9.2 .16 V | 12 V | 2.1A | 25W |
| PBIH-1215G | $9.2-16 \mathrm{~V}$ | 15 V | 1.7A | 25W |
| PBIH-1224G | 9.2 .16 V | 24 V | 1.1A | 25W |
| PBIH-1248G | $9.2 \cdot 16 \mathrm{~V}$ | 48 V | 0.5A | 25W |
| PBIH-240SG | 19.32 V | 5 V | SA | 25W |
| PBIH-2.412G | 19.32 V | 12 V | 2.1A | 25W |
| PBIH-2415G | 19.32 V | 15 V | 1.7A | 25W |
| PBIL-2424G | 19.32 V | 24 V | 1.1A | 25W |
| PBIH-2448G | 19.32 V | 48 V | 0.5A | 25W |
| P8IH-4805G | 38.63 V | 5 V | 5 A | 25W |
| P8IH-4812G | 38.63 V | 12 V | 2.1A | 25W |
| PBiH-4815G | 38.63 V | 15 V | 1.7A | 25W |
| PBIH-4824G | 38.63 V | 24 V | 1.1A | 25W |
| PBIH-4848G | 38.63 V | 48 V | 0.5A | 25W |
| PBIH-11005G | 85-140V | 5V | 5A | 25W |


| MODEL <br> NUMBER <br> PBIH-11012G | $\begin{aligned} & \hline \text { IMPUT } \\ & \hline 85-140 \mathrm{~V} \\ & \hline \end{aligned}$ | OUTPUT |  | OUTPUT <br> POWER <br> $25 W$ |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 12V | 2.1A |  |
| PBIH-11015G | $85-140 \mathrm{~V}$ | 15V | 1.7A | 25W |
| PBIH-11024G | $85-140 \mathrm{~V}$ | 24V | 1.1A | 25W |
| PBIH-11048G | $85-140 \mathrm{~V}$ | 48V | 0.5A | 25W |
| PBIH-1205) | 9.2 -16V | 5 V | 8A | 50 W |
| PBIH-1212] | $9.2-16 \mathrm{~V}$ | 12V | 3.3A | 50 W |
| P8iH-1215 | $9.2-16 \mathrm{~V}$ | 15V | 2.7A | 50 W |
| PBIH-1224J | 9.2 -16V | 24 V | 1.7A | 50 W |
| P8IH-1248J | 9.2-16V | 48 V | 0.8A | 50W |
| PBIH-2405J | 19.32 V | SV | 10A | S0W |
| PBIH-2412] | 19.32 V | 12 V | 4.3A | S0W |
| PBIH-2415J | 19.32 V | 15 V | 3.4A | 50 W |
| PBIH-2424J | 19.32 V | 24 V | 2.5A | 50 W |
| PPIH-2448J | 19-32V | 48 V | 1A | 50 W |
| P8IH-4805 | 38-63V | 5 V | 10A | 50 W |
| P8IH-4812] | 38-63V | 12 V | 4.3A | 50 W |
| P8IH-4815 | 38-63V | 15 V | 3.4A | 50 W |
| P81H-4824 | 38-63V | 24 V | 2.5A | SOW |
| P8ITH-4848I | 38-63V | 48 V | 1 A | SOW |
| P8IH-11005! | 85.140 V | 5 V | 10A | SOW |
| P8IH-11012 | $85-140 \mathrm{~V}$ | 12 V | 4.3A | SOW |
| P8IH-11015 | $85-140 \mathrm{~V}$ | 15 V | 3.4A | SOW |
| P8[H-11024] | $85-140 \mathrm{~V}$ | 24 V | 2.5A | S0W |
| P8[H-11048] | $85-140 \mathrm{~V}$ | 48 V | 1 A | 50W |
| PBIH-1205M | 9.2-16V | 5 V | 18A | 100W |
| PBIH-1212M | 9.2-16V | 12 V | 9 A | 100W |
| PBIH-1215M | $9.2-16 \mathrm{~V}$ | 15 V | 7 A | 100W |
| PBIH-1224M | 9.2 .16 V | 24 V | 4.5A | 100W |
| PBIH-1248M | $9.2-16 \mathrm{~V}$ | 48 V | 2 A | 100W |
| PBIH-2405M | 19.32 V | 5 V | 20A | 100W |
| PBIH-2412M | 19.32 V | 12 V | 9 A | 100W |
| PBIH-2415M | 19.32 V | 15 V | 7A | 100W |


| MODEL NUMBER | IMPUT | OUTPUT |  | OUTPUT <br> POWER <br> 100 W |
| :---: | :---: | :---: | :---: | :---: |
| PBIH-2424M | 19.32 V | 24V | 5A |  |
| PBiH-2448M | $19-32 \mathrm{~V}$ | 48 V | 2A | 100W |
| PBIH-4805M | 38.63 V | 5 V | 20A | 100W |
| PBIH-4812M | 38.63 V | 12 V | 9A | 100W |
| PBIH-4815M | 38.63 V | 15 V | 7A | 100W |
| PBIH-4824M | 38.63 V | 24V | 5A | 100W |
| PBIH-4848M | 38.63 V | 48 V | 2A | 100W |
| PBIH-11005M | $85-140 \mathrm{~V}$ | 5 V | 20A | 100W |
| PBIH-11012M | $85-140 \mathrm{~V}$ | 12 V | 9A | 100W |
| PBIH-11015M | 85.140 V | 15 V | 7A | 100W |
| PBIH-11024M | 85.140 V | 24 V | 5 A | 100W |
| PBIH-11048M | 85.140 V | 48 V | 2 A | 100W |
| P8IH-1205R | $9.2-16 \mathrm{~V}$ | 5 V | 27A | 150W |
| PBIH-1212R | 9.2 .16 V | 12 V | 13A | 150W |
| PBIH-1215R | 9.2 -16V | 15 V | 10A | 150W |
| PBIH-1224R | $9.2-16 \mathrm{~V}$ | 24 V | 6.5A | 150W |
| PBIH-1248R | 9.2-16V | 48 V | 3.3A | 150W |
| PGIH-2405R | 19-32V | 5 V | 30A | 150W |
| PGIIH-2412R | 19.32 V | 12 V | 14A | 150W |
| Pgill-24158 | 19-32V | 15 V | 11A | 150W |
| P8IH-2424R | 19-32V | 24 V | 7 A | 150W |
| P8IH-2448R | 19-32V | 48 V | 3.5A | 150W |
| P8IH-4805R | 38.63 V | 5 V | 30A | 150W |
| P8IH-4812R | 38.63 V | 12 V | 14A | 150W |
| P8IH-4815R | $38-63 \mathrm{~V}$ | 15 V | 11A | 150W |
| PBIH-4824R | 38.63 V | 24 V | 7 A | 150W |
| P8IH-4848R | 38.63 V | 48 V | 3.5A | 150W |
| P8IH-11005R | $85-140 \mathrm{~V}$ | SV | 30A | 150 W |
| P81H-11012R | 85.140 V | 12 V | 14A | 150W |
| P8IH-11015R | $85-140 \mathrm{~V}$ | 15 V | 11A | 150W |
| PBIH-11024R | 85.140 V | 24 V | 7A | 150W |
| P8IH-11048R | 85-140V | 48 V | 3.5A | 150W |

## PBIL-F



## PBIN-G



| Terminal | Connection |
| :---: | :---: |
| 0 | FG |
| 1 | $\mathrm{DC}+\mathrm{V}$ in |
| 2 | OV in |
| 3 | LFG |
| 4 | NO |
| 5 | NO |
| 6 | -V out |
| 7 | +V out |

PBIH-J


| Terminal | Connection |
| :---: | :---: |
| 1 | FG |
| 2 | $\mathrm{DC}+\mathrm{V}$ in |
| 3 | OV in |
| 4 | LFG |
| 5 | -V out |
| 6 | +V out |
| 7 | NC |

PBIH-M


| Terminal | Connection |
| :---: | :---: |
| 1 | +V out |
| 2 | +V out |
| 3 | -V out |
| 4 | -V out |
| 5 | FG |
| 6 | -V in |
| 7 | +V in |

PBIH-R


| Terminal | Connection |
| :---: | :---: |
| 1,2 | +V out |
| 3 | +S |
| 4 | -S |
| 5,6 | -V out |
| 7 | Remote |
| 8 | Control |
| 9 | $\mathrm{DC}+\mathrm{V}$ in |
| 10 | DC OV in |
| 10 | FG |

# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type:Modem/Power SupplyLocation:RTU Section
Model Numbers: ..... PB251
Manufacturer: Powerbox
Supplier: Brisbane Water

## PB251 Series

## 220-330 WATTS DC UPS

## Features

- Ultra-low noise output
- Independent battery charging output
- DC output OK \& battery OK alarms \& LEDs
- Battery-LVD and alarm
- Over-temperature protection
- Battery fuse fail LED



## STANDARDS \& APPROVALS

| Specifications INPUT |  |
| :---: | :---: |
| Voltage: | 190 to 264 vac, or 190 to 400VDC |
| Line regulation: | 0.2\%typical |
| Current: | 1.4A maximum |
| Inrush current: | 10A maximum |
| Frequency: | 45 to 65 Hz |
| OUTPUT |  |
| Voltage | See table |
| Current | See table |
| Load regulation | 0.5\%typical |
| Current limit type - load cct | Constant current |
| Current limit type - batt. cct | Constant current |
| Short circuit protection | Indefi nite, auto-resetting |
| Over-voltage protection | 17.5 to 20 V latching ( 13.8 Vdc output) 31.5 to 39 V latching (27.6Vdc output) |
| Ripple \& noise 100 MHz bandwidth | $28 \mathrm{mVp}-\mathrm{p}$ ( 13.8 Vdc output) $55 \mathrm{mVp}-\mathrm{p}$ (27.6Vdc output) |
| ENVIRONMENTAL |  |
| Operating temperature | 0 to $70^{\circ} \mathrm{C}$ ambient with derating, $5 . . .90 \%$ relative humidity (non-condensing) |
| Over-temperature protection | Automatic \& auto-resetting |
| Cooling requirement | Natural convection |
| Efficiency | 80\% minimum |

## Selection Table

| MODEL NUMBER | OUTPUT |  |  | OUTPUT | Note: Non standard battery charging current available on request. ie PB251-12CM-H-10 for 10A. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | VDC | I Load | $\mathrm{I}_{\text {Batt }}$ | POWER |  |
| PB251-12CM | 13.8 V | 16A | 2A | 220W |  |
| PB251-12CM-H | 13.8 V | 20A | 2A | 275W |  |
| PB251-24CM | 27.6V | 11A | 2A | 300W |  |
| PB251-24CM-H | 27.6V | 12A | 2A | 330W |  |
| PB251-12RML | 13.8 V | 20A | 4A | 275W |  |
| PB251-12B | 13.8 V | 20A | 4A | 275W |  |
| PB251-24RML | 27.6V | 12A | 2A | 330W |  |

## PB251 Series

275-330 WATTS DC UPS

Technical Illustrations


# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218

Westlake Drv
Equipment Type: Level Probe
Location:Common Control
Model Numbers: ..... 020130FSP
Manufacturer: Multitrode
Supplier:
Multitrode Pty Ltd130 Kinston RoadUnderwood. QLD 4119Tel: 0733407000Fax: 0733407077

## The MultiTrode Probe


#### Abstract

MultiTrode probes are unsurpassed for rugged reliability, cost effectiveness and simplicity. Designed for the tough, turbulent conditions found in water, sewage and industrial tanks and sumps, the probes can be found in the simplest and the most complex water and wastewater management systems around the world.


- Low maintenance
- Simple installation
- Excellent in turbulence
- Short \& long term cost savings
- Environmentally friendly
- Safe, low sensing voltage
- Unaffected by fat, grease, debris and foam
- Positive pump cut-out
- Safe - MTISB Barrier


## Reliable in all conditions

Operation is unaffected by build up of fat, grease debris and foam, which causes other systems such as floats, bubblers, pressure and ultrasonic transducers to fail. Turbulence does not affect the probe operation. The rugged, streamlined design eliminates tangling and is ideal for confined spaces.

## Positive pump cut-out

Operational consistency is important to longevity, low maintenance and cost control. The positive pump cut-out ensures pumps are turned off at the same level every time. This avoids damage due to pump over run and the cost of additional control equipment.

## Safe for people and environment

The extra low sensing voltage ensures operators and maintenance staff are protected. All MultiTrode products are environmentally safe, containing no mercury or other harmful contaminants.

## Cost savings

The low cost of equipment, installation and maintenance makes MultiTrode one of the most efficient level control systems available. Plus robust construction and longevity ensures continued cost savings when compared to other systems on the market.

## MULTITRODE

MultiTrode Pty Ltd • Australia Brisbane Technology Park 18 Brandl Street PO Box 4633 Eight Mile Plains Qld 4113 Tel: +61 733407000 Fax: +61733407077 sales@multitrode.com.au

## Standard and custom probes

MultiTrode manufactures a wide range of standard probes, from a single sensor $(200 \mathrm{~mm})$ to a ten-sensor probe $(1000 \mathrm{~mm}$ increasing to a maximum of nine metres). Custom probes can be manufactured to suit your requirements.

## Installation

Installation is straightforward. Probes are easy to install without entering the wet area. The probe is simply lowered in from the top and suspended by its own cable, using the mounting kit supplied.

## MTAK-1 Mounting Kit (Supplied)

The mounting bracket is a standard accessory supplied with all multi-sensor probes (not standard with $0.2 / 1-\mathrm{xx}$ single sensor probe).
The MTAK-1 mounting bracket has an integral cleaning device. All metal components are stainless steel.


## MTAK-2 Mounting Kit (Optional extra)

This extended bracket provides up to 300 mm extra wall clearance. This bracket is not included as standard with probes.


Ordering Examples and Information

| Model <br> Code | Probe <br> Length <br> $(\mathbf{m} / \mathbf{i n})$ | Sensor <br> Separation <br> $(\mathbf{m m} / \mathrm{in})$ | Cable <br> Length <br> ( $\mathbf{~} / \mathrm{ft})$ | Number of <br> Sensors |
| :---: | :---: | :---: | :---: | :---: |
| $0.2 / 1-10$ | $0.2 / 8$ | $\mathrm{~N} / \mathrm{A}$ | $10 / 33$ | 1 |
| $0.5 / 3-10$ | $0.5 / 16$ | $150 / 6$ | $10 / 33$ | 3 |
| $1.0 / 10-10$ | $1 / 40$ | $100 / 4$ | $10 / 33$ | 10 |
| $1.5 / 10-30$ | $1.5 / 60$ | $150 / 6$ | $30 / 100$ | 10 |
| $2.0 / 10-30$ | $2 / 80$ | $200 / 8$ | $30 / 100$ | 10 |
| $2.5 / 10-30$ | $2.5 / 96$ | $250 / 10$ | $30 / 100$ | 10 |
| $3.0 / 10-30$ | $3 / 115$ | $300 / 12$ | $30 / 100$ | 10 |
| $6.0 / 10-30$ | $6 / 224$ | $600 / 24$ | $30 / 100$ | 10 |
| $9.0 / 10-30$ | $9 / 368$ | $900 / 40$ | $30 / 100$ | 10 |

[^10]```
MultiTrode Inc USA
6560 East Rogers Circle Boca Raton Florida 33487
Tel: +15619948090 Fax: +15619946282
sales@multitrode.net
```


## MultiTrode Probe Immersion Table

## multitrode <br> WATER • WASTEWATER • PUMP STATION • TECHNOLOGY

PVC and AVESTA 254-SMO stainless steel comprise the major, exposed surfaces of the MultiTrode probe, and have been operated and tested in the following chemicals.

| ACETIC ACID | 50\% Aqueous |
| :---: | :---: |
| ADIPIC ACID | Saturated Aqueous |
| ALUMINIUM SULPHATE | 27\% |
| AMMONIUM CARBONATE | 50\% Aqueous |
| AMMONIUM HYDROXIDE | All Concentrations |
| AMMONIUM PHOSPHATE | All Concentrations |
| AMMONIUM SULPHATE | All Concentrations |
| AMMONIUM SULPHIDE | All Concentrations |
| AMYL ALCOHOL |  |
| ANILINE HYDROCHLORIDE | All Concentrations |
| BARIUM HYDROXIDE | All Concentrations |
| BEER |  |
| BORAX | All Aqueous |
| BORIC ACID | All Aqueous |
| CALCIUM NITRATE | 50\% Aqueous |
| CHLORIC ACID | 10\% |
| CHROMIC ACID | 5\% |
| FORMIC ACID | Up to 50\% Aqueous |
| GELATINE | All Concentrations |
| GLUCOSE | All Concentrations |
| GLYCERINE | All Concentrations |
| HYDROBROMIC ACID | 50\% Aqueous |
| HYDROCYANIC ACID | 100\% |
| HYDROFLUORIC ACID | 1\% |
| HYDROGEN PEROXIDE | 30\% Aqueous |
| HYDROGEN SULPHIDE | Moist Gas or Saturated Aqueous solution |
| LACTIC ACID | 18\% Aqueous |
| LEAD ACETATE | All Concentrations |
| MERCURY | 100\% |
| MILK | Sour |
| NITRIC ACID | Up to 40\% Aqueous |


| OXALIC ACID | 5\% |
| :---: | :---: |
| PHOSPHORIC ACID | Up to 30\% Aqueous |
| POTASSIUM BICHROMATE | 25\% |
| POTASSIUM CHLORATE | 36\% |
| POTASSIUM CHROMATE | All Concentrations |
| POTASSIUM CYANIDE | All Concentrations |
| POTASSIUM PERMANGANATE | 5-10\% |
| POTASSIUM PERSULPHATE | Saturated |
| POTASSIUM SULPHATE | All Concentrations |
| SODIUM ACETATE | All Concentrations |
| SODIUM BICARBONATE | All Concentrations |
| SODIUM BISULPHATE | 5\% |
| SODIUM BISULPHITE | 10\% |
| SODIUM CHLORATE | 30\% |
| SODIUM FLUORIDE | 5-10\% |
| SODIUM NITRATE | All Concentrations |
| SODIUM PHOSPHATE | All Concentrations |
| SODIUM SILICATE | All Aqueous |
| SODIUM SULPHATE | All Concentrations |
| SODIUM SULPHIDE | 5\% |
| SODIUM SULPHITE | 50\% |
| SODIUM THIOSULPHATE | 16-25\% |
| SULPHUR DIOXIDE | Technically Pure Anhydrous |
| SULPHURIC ACID | 98\% |
| SULPHUROUS ACID | Saturated Aqueous |
| TANNIC ACID | All Aqueous |
| TARTARIC ACID | All Aqueous |
| TURPENTINE OIL | Technically Pure |
| VINEGAR | 4-5\% |
| YEAST | All Aqueous |

Unless stated otherwise, all aqueous solutions are 100\%.

Note: $\quad$ MultiTrode probes can be used in many other aggressive applications and the list above is by mo means complete.

## Materials:

| Sensors: | Avesta 254 SMO high grade stainless steel alloy |  |
| :--- | :--- | :--- |
| Casing: | uPVC premium quality extruded tube |  |
| Cable: | PVC/PVC multi-core, purpose-manufactured |  |
| Resin: | Fast cure, low viscosity, and solvent free |  |
|  | Compressive Strength (TM-45) 7 days at $25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$ | $=60 \mathrm{~N} / \mathrm{mm}^{2} \mathrm{r}^{2}$ |
|  | Elastic Modulus in Compression $(\mathrm{TM}-45) 7$ days at $25^{\circ} \mathrm{C}$ | $=60 \mathrm{~N} / \mathrm{mm}^{2}$ |
|  | Flexural Strength $(\mathrm{TM}-46) 7$ days at $25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$ | $=5 p e c i m e n ~ d i d ~ n o t ~ b r e a k ~ u n d e r ~ t e s t ~$ |
|  | TG $(\mathrm{TM}-22) 7$ days at $25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$ | $=30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$ |
|  | $32 \mathrm{~mm}(11 / 4$ in) diameter $\times$ specified length |  |
| Dimensions: | via the supplied suspension/cleaning bracket inside the wet well |  |

* Mounting bracket not supplied with single-sensor probes
Environmental Range: $\quad 0^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}\left(32^{\circ} \mathrm{F}\right.$ to $\left.+149^{\circ} \mathrm{F}\right)$

Cable:
Conductor Size
Strands/Conductor
Ohms/km
Ohms/mile

* Other multi-core cables are available for non-standard probes



# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type: Soft Starter
Location:Drive section
Model Numbers:MSF 2.0
Manufacturer: Emotron
Supplier:
Siemens Ltd.
885 Mountain HighwayBayswater Vic 3153
Tel: 137222
Fax: 1300360222

## Emotron MSF 2.0 Softstarter



Instruction manual English

Valid for the following softstarter models: MSF 2.0

## MSF 2.0

## SOFTSTARTER

## Instruction manual

Document number: 01-4135-01
Edition: rl
Date of release: 25-07-2007
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## Safety instructions

## Safety

The softstarter should be installed in a cabinet or in an electrical control room.

- The device must be inscalled by crained personnel.
- Disconnect all power sources before servicing.
- Always use standard commercial fuses, slow blow e.g. gl, gG types, to protect the wiring and prevent short circuiting. To protect che thyristors against short-circuic currents, superfast semiconductor fuses can be used if preferred. The normal guarantee is valid even if superfast semiconductor fuses are not used.


## Operating and maintenance personnel

1. Read the whole Instruction Manual before installing and purting the equipment into operation.
2. During all work (operation, maintenance, repairs, etc.) observe the switch-off procedures given in this instruction as well as any other operating instruction for the driven machine or system. See Emergency below.
3. The operator must avoid any working methods which reduce the safery of the device.
4. The operator must do what he can to ensure that no unauthorised person is working on the device.
5. The operator must immediately report any changes to the device which reduce its safery to the user.
6. The user must undertake all necessary measures to operate the device in perfect condition only.

## Installation of spare parts

We expressly point out that any spare parts and accessories not supplied by us have also not been tested or approved by us.
Installing and/or using such producrs can have a negative effect on the characteristics designed for your device. The manufacturer is not liable for damage arising as a result of using non-original parts and accessories.

## Emergency

You can switch the device off at any time with the mains switch connected before the softstarter (both motor and control supply voltage must be switched off).

## Dismantling and scrapping

The enclosure of the softstarter is made of recyclable material such as aluminium, iron and plastic. Legal requirements for disposal and recycling of these materials must be complied with.
The softstarter contains a number of components demanding special treatment, such as thyristors for example. The circuir boards contain small amounts of tin and lead. Legal requirements for the disposal and recycling of these materials must be complied with.

## General warnings



WARNINGI Make sure that all safety measures have been taken before starting the motor in order to avold personal injury.

WARNINGI Never operate the softstarter with the front cover removed.


WARNING! Make sure that all safety measures have been taken before switching on the power supply.

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## 1. General information

This manual describes the Emotron Softstarter MSF 2.0.

### 1.1 How to use the Instruction Manual

This instruction manual cells you how to install and operate the softstarter MSF 2.0. Read the whole Instruction Manual before installing and putcing the unit into operation.

Once you are familiar with the softstarter, you can operate it from the control panel by referring to chapter 5 . page 27.
This chapter describes all the functions and possible settings.

### 1.2 Integrated safety systems

The device is equipped with a protection system which reacts to:

- Over temperature
- Voltage unbalance
- Over- and under voltage
- Phase reversal
- Phase loss
- Motor overload protection thermal and PTC.
- Motor load monitor, protecting machine or process maximum or minimum alarm
- Starrs per hour limitation

The soffstarter is equipped with a connection for protective earch $\stackrel{\perp}{=}$ (PE).

All MSF 2.0 softstarters are IP 20 enclosed types, except MSF-1000 and MSF-1400 which are delivered as open chassis IPOO.

### 1.3 Safety measures

These instructions are a constituent part of the device and must be:

- Available to comperent personnel at all times.
- Read prior to installation of the device.
- Observed with regard to safety, warnings and information given.
The tasks in these instructions are described so that they can be understood by people trained in electrical engineering. Such personnel must have appropriate tools and testing instruments available. Such personnel must have been trained in safe working methods.

The safety measures laid down in DIN standard VDE 0100 must be guaranteed.

The user must obtain any general and local operating permits and meet any requirements regarding:

- Personnel safery
- Product disposal
- Environmental protection

NOTEI The safety measures must remain in force at all times. Should questions or uncertaintles arise, please contact your local sales outlet.

### 1.4 Notes to the Instruction Manual

NOTE: Additional Information as an ald to avoiding problems.


CAUTION: Failure to follow these instructions can result in maffunction or damage to the softstarter.


WARNING: Failure to follow these instructions can result in serious injury to the user in addition to serious damage to the softstarter.

Important
For all enquiries and spare parts orders, please quote the correct name of the device and serial number to ensure that your inquiry or order is dealt with correctly and swiftly.

### 1.5 Type number

Fig. 1, page 5 gives an example of the type code number used for an Emorron MSF Softstarter. With this code number the exact type of the softstarter can be determined. This identification will be required for type specific information when mounting and installing. The code number is located on the product label, on the front of the unit.

| MSF | -017 | 525 | 2 | $C$ | $V$ | $N$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |

Fig. 1 Type number.

Table 1

| Position | $\begin{array}{l}\text { Configuration } \\ \text { parameter }\end{array}$ | Description |
| :--- | :--- | :--- |
| 1 | Softstarter type | MSF 2.0 type, Fixed |
| 2 | Motor current | 017-1400 A |
| 3 | $\begin{array}{l}\text { Mains supply } \\ \text { voltage }\end{array}$ | $\begin{array}{l}525 \mathrm{~V} \\ 690 \mathrm{~V}\end{array}$ |
| 4 | $\begin{array}{l}\text { Control supply } \\ \text { voltage }\end{array}$ | $\begin{array}{l}2=100-240 \mathrm{~V} \\ 5=380-500 \mathrm{~V}\end{array}$ |
| 5 | $\begin{array}{l}\text { Control panel } \\ \text { option }\end{array}$ | $\begin{array}{l}\text { C=Standard, no external } \\ \text { control panel } \\ \text { H=External control panel }\end{array}$ |
| 6 | $\begin{array}{l}\text { Coated boards } \\ \text { option }\end{array}$ | $\begin{array}{l}\text { =No coated boards } \\ \text { V=Coated boards }\end{array}$ |
| 7 | $\begin{array}{l}\text { Communication } \\ \text { option }\end{array}$ | $\begin{array}{l}\text { N=No COM included } \\ \text { S=RS232/485 included } \\ \mathrm{D}=\text { DeviceNet included }\end{array}$ |
| $5=$ Profibus included |  |  |$\}$|  |
| :--- |

### 1.6 Standards

The device is manufactured in accordance with these regulations:

- IEC 60947-4-2
- EN 60204-1, Safery of Machinery, Electrical equipment of machines, part 1 , General requirements and VDE 0113.
- EN 61000-6-4, EMC, Emission standard for industrial environments
- EN 61000-6-3, EMC, Emission standard for residential, commercial and light-industrial environments
- EN 61000-6-2, EMC, Immunity for industrial environments
- GOST
- UL 508


### 1.7 Tests in accordance with norm EN 60204 standard

Before leaving the factory, the device was subjected to the following tests:

- Through connection of earthing system:
a) visual inspection.
b) check that earthing wire is firmly connected.
- Insulation
- Voltage
- Function


### 1.8 Transport and packing

The device is packed in a carton or plywood box for delivery. The outer packaging can be recycled. The devices are carefully checked and packed before dispatch, but transport damage cannot be ruled out.

Check on receipt
Check that the goods are complete as listed on the delivery note, see type no. etc. on the rating plate.

Is the packaging damaged?
Check the goods for damage (visual check).
If you have cause for complaint
If the goods have been damaged during transport:

- Contact the transport company or the supplier immediately.
- Keep the packaging (for inspection by the transport company or for returning the device).


## Packaging for returning the device

Pack the device so that it will resist shock and impact.

## Intermediate storage

After delivery or after it has been dismounted, the device can be stored before further use in a dry room.

### 1.9 Unpacking MSF-310 and larger types

The MSF 2.0 softstarter is attached to the plywood box/ loading stool by screws, and the softstarter must be unpacked as follows:

1. Open only the securing plates at the bottom of the box (bend downwards). Then lift up the box from the loading stool, both top and sides in one piece.
2. Loosen the three (3) screws on the front cover of the sofstarter unit, down by the lower logo.
3. Push up the front cover about 20 mm so that the front cover can be removed.
4. Remove the two (2) mounting screws at the bottom of the softstarter.
5. Lift up the softstarter unit at the bottom about 10 mm and then push backwards about 20 mm so that the softstarter can be removed from the mounting hooks* at the top. The hooks are placed under the bottom plate and cannot be removed until the softstarter is pulled out.
6. Loosen the two screws (2) for the mounting hooks and remove the hooks.
7. The hooks are used as an upper support for mounting the softstarter.


Fig. 2 Unpacking MSF-310 and larger models.

### 1.10 Glossary

### 1.10.1 Abbreviations

In this manual the following abbreviations are used:
Table 2 Abbreviations

| Abbreviation | Description |
| :--- | :--- |
| FLC | Full load current |
| DOL | Direct on-line |

### 1.10.2 Definitions

In this manual the following definitions for current, voltage, power, torque and speed are used:

Table 3 Definitions

| Name | Description | Unit |
| :--- | :--- | :--- |
| $I_{\text {nsoft }}$ | Nominal softstarter current | A |
| $P_{\text {nsoft }}$ | Nominal softstarter power | $\mathrm{kW}, \mathrm{HP}$ |
| $\mathrm{N}_{\mathrm{nsoft}}$ | Nominal softstarter speed | rpm |
| $\mathrm{T}_{\mathrm{n}}$ | Nominal motor torque | $\mathrm{Nm}, \mathrm{lbft}$ |
| $\mathrm{U}_{\mathrm{n}}$ | Nominal motor voltage | V |
| $\mathrm{I}_{\mathrm{n}}$ | Nominal motor current | A |
| $P_{\mathrm{n}}$ | Nominal motor power | $\mathrm{kw}, \mathrm{HP}$ |
| $P_{\text {normal }}$ | Normal load | \% of $\mathrm{P}_{\mathrm{n}}$ |

## 2. Description

In this chapter different starting methods for induction motors are explained and compared. The functionality of softstarters with torque control and their advantages and limitations compared to other starting methods are explained.
First a brief account of the background theory of starting induction motors will be given in section 2.1. Thereafter the different starting methods based on the usage of reduced voltage will be described and compared. This chapter will also cover softstarters with torque control. In section 2.3 some common starting methods based on other physical principles are explained. With this information some limitations of the reduced voltage starters will become clear. In section 2.4 there is a brief analysis of which applications may benefit from using a softstarter.

### 2.1 Background theory

The following two sections deal with motors with squirrelcage rotors. In contrast to a wound rotor, the squirrel-cage rotor consists of straight conductors, which are shortcircuited together at both ends.
When such a motor is connected directly to the line voltage it will typically draw a starting current of about 5 to 8 times its nominal current while the resulting starting torque will be about 0.5 to 1.5 times its nominal torque. In the following picture a typical starting characteristic is shown. The x axis represents the speed relative to the nominal speed while the y -axis shows the torque and the current respectively, even those normalized to their nominal values. The dashed line indicates the nominal values.


Fig. 3 Typical torque characteristics for the DOL start


Fig. 4 Typical current characteristics for the DOL start
For many industrial applications direct on-line starting is not convenient, as the supply in this case has to be dimensioned to deliver the unnecessarily high starting current. Moreover, most applications do not gain anything from the high starting torque. Instead there is a risk of mechanical wear or even damage because of the resulting jerk at speedup.
The acceleration torque is determined by the difference between motor and load torque. The figure below shows some typical torque characteristics for constant speed applications. For comparative purposes, the inducion motors' torque characteristic is added to the diagram.


Fig. 5 Typical load torque characteristics
Typical applications with constant load are elevators, cranes and conveyors. Linear load characteristics are found for calendar rollers and smoothing machines; quadratic correlation between speed and torque is typical for pumps and fans.

Some applications like conveyors or screws may need an initial torque boost. However, for many applications it can be seen that the torque needed is much lower than the torque delivered by the induction motor in a DOL start.

A common method to reduce both starting torque and current is to decrease the motor voltage during starting. The following figure shows how the motor's torque and current characteristics are changed when the supply voltage is reduced.


Fig. 6 Reduced voltage start
A general rule of thumb is that the torque at each operating point is roughly proportional to the square of the current. This means when the motor current is decreased by a factor of two by means of reducing the supply voltage, the torque delivered by the motor will be decreased by a factor of four (approximately).

$$
\begin{aligned}
& \mathrm{T} \sim 1^{2} \\
& \mathrm{I}_{\mathrm{LV}}=1 / 2 \mathrm{I}_{\mathrm{DOL}} \rightarrow \mathrm{~T}_{\mathrm{LV}} \approx 1 / 4 \mathrm{~T}_{\mathrm{DOL}} \\
& \mathrm{I}_{\mathrm{LV}}=1 / 3 \mathrm{I}_{\mathrm{DOL}}>\mathrm{T}_{\mathrm{LV}} \approx 1 / 9 \mathrm{~T}_{\mathrm{DOL}} \\
& \mathrm{LV}=\text { low voltage } \\
& \mathrm{DOL}=\text { Direct on line }
\end{aligned}
$$

This relationship is the base for any starting method using reduced voltage. It can be seen that the possibility of reducing the starting current depends on the correlation between the motor's and the load's torque characteristic. For the combination of an application with very low starting load and a motor with very high starting torque, the starting current may be reduced significantly by means of decreasing the voltage during start. However, for applications with high starting load it may - depending on the actual motor - not be possible to reduce the starting current at all.

### 2.2 Reduced voltage starting

This section describes different starting methods which are based on the reduced-voltage principle explained above. A pump and its quadratic torque characteristic are used as an example.

The star-delta starter is the simplest example of a reduced voltage starter. The motor phases are first star connected; at about $75 \%$ of nominal speed the phase connection is then changed to delta. To enable star-delta start, both ends of all three motor windings have to be available for connection. Moreover, the motor has to be dimensioned for the (higher) voltage in the delta connection. The following figure shows the resulting torque and current characteristics.


Fig. 7 Star-delta start

The disadvantage of the star-delta start is that it cannot be adapted to a special application. Both the voltage in star and in delta connection are defined by the supply, the resulting starting performance depends on the motor's DOL characteristic. For some applications the star-delta starter cannot be used as the resulting torque in star connection is too low to start rotating the load. On the other hand for low load applications further savings of starting current are impossible even though a big torque reserve is available. Moreover, the resulting abrupt rise of torque first at start and later when changing from star to delta connection may contribute to mechanical wear. The high transient currents during start-delta transition create unnecessary excess heat in the motor.
Better performance is achieved with a voltage ramp start, which a simple electronic softstarter can provide. The voltage is increased linearly from an initial value to the full supply voltage by means of phase angle control. The resulting torque and current characteristics are shown in the following figure.


Fig. 8 Soft starting - voltage ramp
Obviously a much smoother start is realized compared to the star-delta start and the starting current is decreased.

A softstarter $i$ often used to keep the starting current below a desired level. For the example above, setting a current limit of three times the nominal current may be desirable. The following figure shows the resulting torque and current characteristics.


Fig. 9 Soft starting - voltage ramp with current limit
Once again the figure illustrates that the resulting performance depends on the combination of motor and load characteristics. In the example above the motor torque is close to the load torque at about half speed. This means for some other applications with different load characteristics (for example a linear torque-speed correlation) this particular motor would need more than three times the nominal current to start.

The most sophisticated electronic softstarters use torque control, which results in an almost constant acceleration during the start. A low starting current is also achieved. However, even this start method uses reduced motor voltage and the quadratic correlation between current and torque described in the first section of this chapter is still valid. This means, the lowest possible starting current is determined by the combination of motor and load characteristics.


Fig. 10 Soft starting - torque control
For optimal starting performance, correct setting of the softstarter's parameters such as initial torque and end torque at start and start time is important. The choice of parameters is explained in detail in section 8.7, page 55.

### 2.3 Other starting methods

In contrast to the preceding sections of this chapter, which focused on squirrel-cage motors, slip-ring motors are dealt with later on. A slip-ring motor is equipped with a wound rotor; one end of each rotor winding is available for external connection via slip-rings. These motors are often optimized for rotor resistance starting, e.g. with short-circuited rotor windings they develop a very low torque at an extremely high current. For starting external resistances are connected to the rotor windings. During the start, the resistance value is decreased in several steps until the rotor windings are short-circuited at nominal speed. The following figure shows typical torque and current characteristics for a slipring motor during the start with an external rotor-resistance starter.


Fig. 11 Rotor-resistance starting
Because of the low starting torque it is often not possible to short-circuit the rotor windings and replace the rotor-resistance starter with a softstarter. However, it is always possible to use a frequency inverter instead. The following illustration shows how the torque and current characteristics are affected when the stator frequency is changed.


Fig. 12 Voltagelfrequency regulation
Thus, such a motor can be started with a quite simple frequency inverter with voltage-frequency regulation. This solution is even valid for all other applications, which for some reason (high load torque compared to motor torque etc.) cannot be started by a softstarter.

### 2.4 Use of softstarters with torque control

To determine if a specific application benefits from using a softstarter at all, the correlation between the motor's torque characteristic during the start and the load's requirements has to be evaluated. As it can be seen from the examples above, the application will only benefit from using a softstarter if the load torque during the start is clearly below the motor's starting capacity. However, even loads with a high initial release torque may profit from a softstarter. In this case an initial torque boost can be used, thereafter the start ramp is continued reducing the starting current considerably.
The profit can be maximized when using a softstarter with torque control. To be able to configure the torque control parameters for optimal performance, the load characteristics (linear, square or constant load, need of initial release torque) must be known. In this case a proper torque control method (linear or square) can be chosen and torque boost can be enabled if needed. A description of the load characteristics of several common applications and guidelines for proper settings are found in chapter 6. page 31, Applications and Functions Selection. Optimization of the torque control parameter is explained in detail in section 8.7, page 55.

## 3. Mounting

This chapter describes how to mount the MSF 2.0 softstarter. Before mounting it is recommended that the installation be planned out firs:

- Be sure that the softstarter suits the mounting location.
- The mounting site must support the weight of the softstarter.
- Will the softstarter continuously withstand vibrations and/or shocks?
- Consider using a vibration damper.
- Check ambient conditions, ratings, required cooling air flow, compatibility of the motor, etc.
- Do you know how the softstarter will be lifted and transported?
Make sure that the installation is performed in accordance with the local safery regulations of the electricity supply company. And in accordance with DIN VDE 0100 for setting up heavy current plants.
Care must be taken to ensure that personnel do not come into contact with live circuit components.


WARNINGI Never operate the softstarter with the front cover removed.

### 3.1 Installation of the softstarter in a cabinet

When installing the softstarter:

- Ensure that the cabinet will be sufficiently ventilated after the installation.
- Keep the minimum free space, see the tables on page 15.
- Ensure that air can flow freely from the bottom to the top.

NOTE: When Installing the softstarter, make sure it does not come Into contact with live components. The heat generated must be dispersed vla the cooling fins to prevent damage to the thyristors (free cliculation of alr).

MSF-017 to MSF-835 are all delivered as enclosed versions with front opening. The units have bottom entry for cables etc. see Fig. 20 on page 21 and Fig. 22 on page 23. MSF1000 and MSF-1400 are delivered as open chassis.

### 3.1.1 Cooling

MSF-017 to MSF-250
Table 4 MSF-017 to MSF-250

| MSF <br> model | MInimum free space (mm): <br> above 1) |  |  |
| :--- | :--- | :--- | :--- |
| below | at side |  |  |
| $-017,-030,-045$ | 100 | 100 | 0 |
| $-060,-075,-085$ | 100 | 100 | 0 |
| $-110,-145$ | 100 | 100 | 0 |
| $-170,-210,-250$ | 100 | 100 | 0 |
| 1) Above: wall-softstarter or softstarter-softstarter |  |  |  |

MSF-310 to MSF-1400
Table 5 MSF-310 to MSF-1400.

| MSF <br> model | Minimum free space (mm): |  |  |
| :--- | :--- | :--- | :--- |
|  | above 1) | below | at side |
| $-310,-370,-450$ | 100 | 100 | 0 |
| $-570,-710,-835$ | 100 | 100 | 0 |
| $-1000,-1400$ | 100 | 100 | 100 |
| 1) Above: Wall-softstarter or softstarter-softstarter |  |  |  |

### 3.1.2 Mounting schemes

MSF-017 to MSF-250



Fig. 14 Hole pattern for screw attachment, MSF-310 to MSF-835. Hole distance (mm).

Fig. 13 Hole pattern for MSF-017 to MSF-250 (backside view).

Table 6

| $\begin{array}{c}\text { MSF } \\ \text { Model }\end{array}$ | $\begin{array}{c}\text { Hole } \\ \text { distance } \\ \text { w1 [mm] }\end{array}$ | $\begin{array}{c}\text { Hole } \\ \text { dlstance } \\ \text { H1 [mm] }\end{array}$ | $\begin{array}{c}\text { Hole } \\ \text { distance } \\ \text { E }\end{array}$ | $\begin{array}{c}\text { Hole } \\ \text { dlstance } \\ \text { F }\end{array}$ | $\begin{array}{c}\text { Dlam./ } \\ \text { screw }\end{array}$ | $\begin{array}{c}\text { Tlghtening torque for bolt [mm] } \\ \text { Cable }\end{array}$ |  | PE cable |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Supply |  |  |  |  |  |  |  |  |
| and PE |  |  |  |  |  |  |  |  |$]$

Observe that the two mounting hooks supplied (see section 1.9, page 6 and Fig. 2 on page 7) must be used for
mounting the softstarter as upper support (only MSF-310 to MSF-835).


Fig. 16 Busbar distances MSF-310 to MSF-835.
Table 7 Busbar distances

| MSF model | Dist. h1 <br> (mm) | Dlst. W1 <br> (mm) | Dist.W2 <br> (mm) | Dlst.W3 <br> (mm) |
| :--- | :--- | :--- | :--- | :--- |
| -310 to -450 | 104 | 33 | 206 | 379 |
| -570 to -835 | 129 | 35 | 239.5 | 444 |
| $-1000-1400$ |  | 55 | 322.5 | 590.5 |

Fig. 15 Hole pattern for MSF-170 to MSF-250 with upper mounting bracket instead of DIN rail.


Fig. 17 MSF-1000 to MSF-1400


Fig. 18 Hole pattern busbar MSF-1000 to MSF-1400.

## 4. Connections

The description of installation in this chapter follows the EMC standards and the Machinery Directive.
If the softstarter is temporarily stored before being connected, please check the technical data for environmental conditions. If the softstarter is moved from a cold storage room to the room where it is to be installed, condensation can form on it. Allow the softstarter to become fully accli-
matised and wait until any visible condensation has evaporated before connecting the mains voltage.

NOTE: The softstarter must be wired with shlelded control cable to fulfil EMC regulations according to section 1.6, page 6.

NOTE: For UL-approval use $75^{\circ} \mathbf{C}$ Copper wire only.

### 4.1 Connecting mains and motor cables



Fig. 19 Connection of MSF-017 to MSF-085.

## Connection of MSF-017 to MSF-085

7. Mounting of EMC gland for control cables

## Device connections

1. Protective earth, $\stackrel{\perp}{=}(\mathbf{P E})$, mains supply, motor (on the right and left inside of the cabinet)
2. Protective earth, $\stackrel{\perp}{=}$ (PE), control supply voltage
3. Control supply voltage connection $\mathbf{0 1}, 02$
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (can be mounted outside for bypass see section 8.7.5, page 67)


Fig. 20 Connection of MSF-110 to MSF-145.

## Connection of MSF-110 to MSF-145

## Device connections

1. Protective earth, $\perp(\mathrm{PE})$, mains supply, motor (on the left inside of the cabinet)
2. Protective earth $\stackrel{\perp}{=}(\mathrm{PE})$, control supply voltage
3. Control supply voltage connection $\mathbf{0 1}, 02$
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (can be mounted outside for bypass see section 8.7.5, page 67)
7. Mounting of EMC gland for control cables


Fig. 21 Connection of MSF-170 to MSF-250.

## Connection of MSF-170 to MSF-250

## Device connections

1. Protective earth, $\perp$ (PE), mains supply, motor (on the left inside of the cabinet)
2. Protective earth $\downarrow$ (PE), control supply voltage
3. Control supply voltage connection 01,02
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (can be mounted outside for bypass see section 8.7.5, page 67)
7. Mounting of EMC gland for control cables


Fig. 22 Connection of MSF-310 to MSF-1400.

## Connection of MSF-310 to MSF-1400

Device connections

1. Protective earth, $\stackrel{\perp}{\perp}$ (PE), mains supply and motor
2. Protective earth, $\perp(\mathrm{PE})$, control supply voltage
3. Control supply voltage connection $\mathbf{0 1 , 0 2}$
4. Mains supply L1, L2, L3
5. Motor power supply $\mathrm{T} 1, \mathrm{~T} 2, \mathrm{~T} 3$
6. Current transformers (possible to mount outside for bypass see section 8.7.5, page 67)
7. Mounting of EMC gland for control cables

### 4.2 Control Connection



Fig. 23 PCB (control board) connections.
Table 8 PCB Terminals

| Terminal | Function | Electrical characteristics |
| :---: | :---: | :---: |
| 01 | Control supply voltage | $100-240 \mathrm{VAC} \pm 10 \%$ alternativ |
| 02 |  | $380-500$ VAC $\pm 10 \%$ see rating plate |
| PE | Protective Earth | $\stackrel{1}{=}$ |
|  |  |  |
| 11 | Digital input 1 | $0-3 \mathrm{~V}->0 ; 8-27 \mathrm{~V}->1 .$ <br> Max. 37 V for 10 sec . Impedance to $0 \mathrm{VDC}: 2.2 \mathrm{k} \Omega$. |
| 12 | Digital input 2 |  |
| 13 | Control signal supply voltage to PCB terminal 11 and 12 , $10 \mathrm{k} \Omega$ potentiometer, etc. | +12 VDC $\pm 5 \%$. Max. current from +12 VDC: 50 mA . Short circuit-proof but not overload-roof. |
| 14 | Analogue input, 0-10 V, 2-10 V, 0-20 mA and 4-20 mA/digital input. | Impedance to terminal 15 ( 0 VDC ) voltage signal: $125 \mathrm{k} \Omega$, current signal: $100 \Omega$. |
| 15 | GND (common) | 0 VDC |
| 16 | Digital input 3 | $\begin{aligned} & 0-3 \vee \rightarrow 0 ; 8-27 \mathrm{~V}->1 \text {. } \\ & \text { Max. } 37 \mathrm{~V} \text { for } 10 \mathrm{sec} \text {. Impedance to } 0 \mathrm{VDC}: 2.2 \mathrm{k} \Omega \text {. } \end{aligned}$ |
| 17 | Digital input 4 |  |
| 18 | Control signal supply voltage to PCB terminal 16 and 17, $10 \mathrm{k} \Omega$ potentiometer, etc. | $+12 \mathrm{VDC} \pm 5 \%$. Max. current from $+12 \mathrm{VDC}=50 \mathrm{~mA}$. Short circuit-proof but not overload-proof. |
| 19 | Analogue output | Analogue output contact: <br> $0-10 \mathrm{~V}, 2-10 \mathrm{~V}$; min load impedance $700 \Omega$ <br> $0-20 \mathrm{~mA}$ and $4-20 \mathrm{~mA}$; max load impedance $750 \Omega$ |
|  |  |  |
| 21 | Programmable relay K1. Factory setting is "Operation" with indication by closing terminal 21 to 22. | 1-pole closing contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 22 |  |  |
| 23 | Programmable relay K2. Factory setting is "Full voltage" with indication by closing terminals 23 to 24 . | 1-pole closing contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 24 |  |  |
|  |  |  |
| 31 | Programmable relay K3. Factory setting is "All alarms". Indication by closing terminals 31 to 33 and opening terminals 32 to 33 . | 1-pole change-over contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 32 |  |  |
| 33 |  |  |
|  |  |  |
| 69-70 | PTC Thermistor input | Alarm level $2.4 \mathrm{k} \Omega$ Switch back level $2.2 \mathrm{k} \Omega$. |
|  |  |  |
| 71-72* | Clickson thermistor | Controlling softstarter cooling fan temperature MSF-310-MSF-1400 |
| 73-74* | NTC thermistor | Temperature measuring of softstarter cooling fin |
| 75 | Current transformér input, cable S1 (blue) | Connection of L1 or T1 phase current transformer |
| 76 | Current transformer input, cable S1 (blue) | Connection of L3, T3 phase (MSF 017 to MSF 250) or L2, T2 phase (MSF 310 to MSF 1400) |
| 77 | Current transformer input, cable S2 (brown) | Common connection for terminals 75 and 76 |
| 78* | Fan connection | 24 VDC |
| 79* | Fan connection | O VDC |

*Internal connection, no customer use.

### 4.3 Minimum wiring

The figure below shows the "minimum wiring". See section 3.1.2, page 16 , for tightening torque for bolts etc.

1. Connect Protective Earth (PE) to earth screw marked $\underset{=}{\perp}$ (PE).
2. Connect the softstarter between the 3 -phase mains supply and the motor. On the softstarter the mains side is marked L1, L2 and L3 and the motor side T1, T2 and T3.
3. Connect the control supply voltage (100-240 VAC) for the control card at terminals 01 and 02 .
4. Connect PCB terminals 12 and 13 (PCB terminals 11 and 12 must be linked) e.g. to a 2 -position switch (on/ oFF) or a PLC, etc., to obtain control of soft start/stop (for factory configuration of the digital inputs).
5. Ensure the installation complies with the appropriate local regulations.

NOTE! The softstarter should be wired with a shielded control cable to fulfil the EMC regulations outlined in section 1.6, page 6.

NOTE! If local regulations say that a mains contactor should be used, relay K1 can control It. Always use standard commercial, slow blow fuses, e.g. gl or gG types, to protect the wiring and prevent short clrcuiting. To protect the thyristors against short-circult currents, superfast semiconductor fuses can be used if preferred. The normal guarantee is valld even If superfast semiconductor fuses are not used. All signal inputs and outputs are galvanically insulated from the mains supply.

### 4.4 Wiring examples

Fig. 55 on page 79 gives an wiring example with the following functions:

- Analogue start/stop, see description on page 79.
- External control of parameter set, see section 8.9.6, page 90
- Analogue output, see "Analogue output" on page 82
- PTC input, see description of Thermal motor protection in section 8.3.1, page 46.


Fig. 24 Wiring circuit, "minimum wiring".

## 5. How to get started

This chapter briefly describes the set-up for basic soft start and soft stop using the default "Torque control" function.


WARNINGI Mounting, wiring and setting the device into operation must be carried out by properly trained personnel.

### 5.1 Checklist

- Mount the softstarter as set out in chapter 3. page 15.
- Consider the power loss at rated current when dimensioning a cabinet, max. ambient temperature is $40^{\circ} \mathrm{C}$.
- Check that the motor and supply voltage corresponds to the values on the softstarter's rating plate.
- Connect the protective earth.
- Connect the motor circuit according to Fig. 25.
- Connect the control supply to terminals 01 and 02 . The control supply voltage range is $100-240 \mathrm{VAC}$ or 380 500 VAC , see rating plate.
- Connect relay K1 (terminals 21 and 22 on the softstarter) to the contactor - the softstarter then controls the contactor (for factory configuration of K1).
- Connect terminals 12 and 13 to, e.g., a 2 -way switch (closing non-return) or a PLC and a jumper between 11 and 12 , etc., to obtain control of soft start/soft stop. (For factory configuration of digital inputs 1 and 2.)
- Ensure the installation complies with the appropriate local regulations.


### 5.2 Applications



WARNINGI Make sure that all safety measures have been taken before switching on the power supply.

Switch on the control supply voltage (normally $1 \times 230 \mathrm{~V}$ ); all segments in the display and the two LEDs will be illuminated for a few seconds. Then the display will show menu [100]. An illuminated display indicates there is control supply voltage to the softstarter unit. Check that you have mains supply voltage to the mains contactor or to the thyristors. The settings are carried out according as follows:


Fig. 25 Standard wiring.

### 5.3 Motor data

Set the data, according to the motor type plate, to obtain optimal settings for start, stop and motor protection.

NOTEI The default settings are for a standard 4-pole motor according to the nominal power of the softstarter. The softstarter will run even if no specific motor data is selected, but the performance will not be optimal.


### 5.4 Start and stop




Default "Stop method" is Coast (freewheeling).

### 5.5 Setting the start command

As default the softstarter is set up for remote operation via terminals 11,12 and 13. For easy commissioning it is possible to give start and stop signals via the control panel.

| 200 |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
| Setting |  |  |
|  |  | 2 |
| Default: | 2 (Remote control) |  |
| Range: | $1,2,3$ |  |
| 1 | Control panel. |  |
| 2 | Remote control. |  |
| 3 | Serial communication control. |  |

Menu [200] must be set to 1 to be able to operate from control panel.

NOTE! Factory default setting is remote control (2).
To start and stop from the control panel, the "START/ STOP" key is used.
To reset from the control panel, the "ENTER $\longleftarrow$ /RESET" key is used. A reset can be done both when the motor is running and when the motor is stopped. A reset by the control panel will not start or stop the motor.

### 5.6 Viewing the motor current

Set the display to menu [100]. Now the motor current can be viewed on the display.


### 5.7 Starting

Start the motor by pressing the "START/STOP" key on the control panel or through the remore control, PCB terminals 11, 12 and 13 . When the start command is given, the mains contactor will be activated by relay K 1 (softstarter terminals 21 and 22), and the motor then starts softly.


Fig. 26 Example of start current when the default torque control is used.

## 6. Applications and functions selection

This chapter is a guide to selecting the correct softstarter rating and softstarter functionality for different applications. To make the right choice the following tools are used:
The norms AC53a and AC53b
These norms help select the soffstarter rating with regard to dury cycle, starts per hour and maximum starting current.

## The Applications Rating List

With this list the softstarter rating can be selected depending on the kind of application used. The list uses two levels, see Table 9, page 33.

The Applications Function List
This table gives an overview of the most common applications and their challenges. For each application MSF 2.0 solutions are proposed and a reference to the MSF 2.0 menus, which can be used, is given. See Table 10, page 34.

### 6.1 Softstarter rating according to AC53a

The IEC 60947-4-2 standard for electronic softstarters defines $\mathrm{AC53a}$ as a norm for dimensioning of softstarters for continuous running without bypass.
The MSF 2.0 softstarter is designed to run continuously.


Fig. 27 AC53a rating example.


Fig. 28 Duty cycle, non-bypass.
The above example indicates a current rating of 210 Amps with a start current ratio of $5.0 \times$ FLC $(1050 \mathrm{~A})$ for 30 sec onds with a $50 \%$ dury cycle and 10 starts per hour.

NOTE! If more than 10 starts/hour or other duty cycles are needed, please contact your suppller.

In the Applications Rating List two commonly used levels of AC 53 a are specified. These are also given in the technical data tables (see chapter 13. on page 109).

### 6.2 Softstarter rating according to AC53b

This norm is made for bypass operation. The MSF 2.0 softstarter is designed to run continuously. In the event of high ambient temperature or for other reasons, an external bypass contactor can be used to minimize the power loss at nominal speed. In the Application Rating List, one level of AC53b is specified, normal with bypass.


Fig. 29 AC53b rating example.


Fig. 30 Duty cycle, bypassed
The above example indicates a current rating of 210 Amps with a start current ratio of $5.0 \times$ FLC $(1050 \mathrm{~A})$ for 30 seconds with a 24 -minute interval between starts.

### 6.3 The Applications Rating List

According to the norms AC53a and AC53b a softstarter can have many current ratings.
With help of the Applications Rating List the correct rating can be chosen for most applications.
The Applications Rating List uses two levels for the AC53a norm and one level for the AC53b norm:

AC53a 5.0-30:50-10 (heavy)
This level will be able to start almost all applications and follows directly the type number of the sofstarter.
Example: MSF-370 is designed for 370 A full load current (FLC) and 5 times this current for a starting time of 30 sec onds.

AC 53a 3.0-30:50-10 (normal)
This level is for lighter applications and here the MSF 2.0 can manage a higher FLC.
Example: MSF-370 can be used for an application with 450 A FLC if the starting current is not more than 3 times this current for a starting time of 30 seconds.
AC53b 3.0-30:330 (normal with bypass)
This level is for lighter applications when a bypass contactor is used. The MSF 2.0 can in this case be used for applications with an even higher nominal current.

## Example

An MSF-370 can be used for an application with a full load current of 555 A if the starting current is no more than three times this value and a bypass contactor is used.

NOTEI TO compare softstarters it is important to ensure that not only FLC (Full Load Current) is compared but also the starting performance.

## The Applications Rating List

The first column in the Applications Rating List, see Table 9 , page 33 gives various applications. If the machine or application is not in chis list, try to identify a similar machine or application. If in doubt please contact your supplier. The second and chird columns gives rypical ratings for the machine or application. The ratings are divided in Nor$\mathrm{mal} /$ Normal with by-pass and Heavy duty.

## Example

The application is a Roller Mill. From the Applications Rating List a Roller Mill is rated as a Heavy duty application due to high starting current. The proper size of MSF 2.0 has to be selected from the Heavy rating column, see Technical data.

Table 9 Applications Rating List

| Applicatlons | Normal AC53a 3.0-30:50-10 and Normal with bypass AC53b 3.0-30:300 | $\begin{gathered} \text { Heavy } \\ \text { AC 53a 5.0-30:50-10 } \end{gathered}$ |
| :---: | :---: | :---: |
| General \& Water |  |  |
| Centrifugal Pump | $x$ |  |
| Submersible Pump | $\times$ |  |
| Conveyor |  | $x$ |
| Compressor, Screw | $x$ |  |
| Compressor, Reciprocating | x |  |
| Fan | X |  |
| Blower | x |  |
| Mixer |  | $x$ |
| Agitator |  | x |
| Metals \& Mining |  |  |
| Belt Conveyor |  | $\times$ |
| Dust Collector | $x$ |  |
| Grinder | x |  |
| Hammer Mill |  | x |
| Rock Crusher |  | x |
| Roller Conveyor |  | x |
| Roller Mill |  | x |
| Tumbler |  | x |
| Wire Draw Machine |  | x |
| Food Processing |  |  |
| Bottle Washer | $\times$ |  |
| Centrifuge |  | $x$ |
| Dryer |  | x |
| Mill |  | $x$ |
| Palletiser |  | x |
| Separator |  | x |
| Slicer | $\times$ |  |
| Pulp and Paper |  |  |
| Repulper |  | x |
| Shredder |  | x |
| Trolley |  | $\times$ |
| Petrochemical |  |  |
| Ball Mill |  | x |
| Centrifuge |  | x |
| Extruder |  | $x$ |
| Screw Conveyor |  | x |
| Transport \& Machine Tool |  |  |
| Ball Mill |  | $x$ |
| Grinder |  | x |
| Material Conveyor |  | $x$ |
| Palletiser |  | $x$ |
| Press |  | x |
| Roller Mill |  | x |
| Rotary Table |  | x |
| Trolley |  | $x$ |
| Escalator |  | x |

Table 9 Applications Rating List

| Applications | Normal AC53a 3.0-30:50-10 and Normal with bypass AC53b 3.0-30:300 | $\begin{gathered} \text { Heavy } \\ \text { AC 53a 5.0-30:50-10 } \end{gathered}$ |
| :---: | :---: | :---: |
| Lumber \& Wood Products |  |  |
| Bandsaw |  | $x$ |
| Chipper |  | x |
| Circular Saw |  | $\times$ |
| Debarker |  | $x$ |
| Planer |  | $x$ |
| Sander |  | X |

### 6.4 The Application Functions List

This list gives an overview of many different applications with their challenges and a possible solution with one of the many MSF 2.0 functions.

Description and use of the table:

## Application

This column gives the various applications. If the machine or application is not on this list, try to identify a similar machine or application. If in doubt please contact your supplier.

## Challenge

This column describes possible challenges that are familiar for this kind of application.
MSF 2.0 Solution
Gives the possible solution for the challenge using one of the MSF 2.0 functions.

## Menus

Gives the menu numbers and selection for the MSF 2.0 function.
"200; $=1$ ", means: program selection 1 in menu [200].
" $323 ;=1 / 320,324$ ", means: program selection 1 in menu [323], menus [320] and [324] are related to this function.

Table 10 Application Functions List

| Application | Challenge | MSF Solution | Menus |
| :---: | :---: | :---: | :---: |
| PUMP | Too fast starts and stops | Pre-setting for pump application | 300 |
|  | Non-linear ramps | Square torque control for square loads. | $\begin{aligned} & 310 ;=2, \\ & 320 ;=2 \end{aligned}$ |
|  | Water hammer | Square torque control | 320;=2 |
|  | High current and peaks during starts | Square torque control | 310;=2 |
|  | Pump is going in wrong direction | Phase reversal alarm | 440 |
|  | Dry running | Shaft power underload | 401 |
|  | High load due to dirt in pump | Shaft power overload | 400 |
| COMPRESSOR | Mechanical shock for compressor, motor and transmissions | Linear Torque control | 310; $=1$ |
|  | Small fuses and low current available. | Linear torque control and current limit at start. | 310; $=1,314$ |
|  | Screw compressor going in wrong direction | Phase sequence alarm | 440 |
|  | Damaged compressor if liquid ammonia enters the compressor screw. | Shaft power overload | 400 |
|  | Energy consumption due to compressor running unloaded | Shaft power underload | 401 |
| BLOWER | Mechanical shock for blower, motor and transmissions. High start current requires large cables and fuses. | Torque control ensures smooth starts that minimize mechanical stress. <br> Start current is minimized by torque-controlled start. | 310; $=1$ |

Table 10 Application Functions List

| Application | Challenge | MSF Solution | Menus |
| :---: | :---: | :---: | :---: |
| CONVEYOR | Mechanical shocks for transmissions and transported goods. | Linear torque control | 310;=1 |
|  | Loading or unloading conveyors | Slow speed and accurate position control. | $\begin{array}{\|l} 330-333 \\ 500,501 \end{array}$ |
|  | Conveyor jammed | Shaft power overload | 400 |
|  | Conveyor belt or chain is off but the motor is still running | Shaft power underload | 401 |
|  | Starting after screw conveyor has stopped due to overload. | Jogging in reverse direction and then starting in forward. | 335, 500 |
|  | Conveyor blocked when starting | Locked rotor function | 228, 229 |
| FAN | High starting current in end of ramps | Square torque control for square load characteristics | 310;=2 |
|  | Slivering belts. |  |  |
|  | Fan is going in wrong direction when starting. | Catching the motor and going easy to zero speed and then starting in right direction. | 310; $=2$ |
|  | Belt or coupling broken | Shaft power underload | 401 |
|  | Blocked filter or closed damper. |  |  |
| PLANER | High inertia load with high demands on torque and current control. | Linear torque control gives linear acceleration and low starting current. | 310;=1 |
|  | Need to stop quickly both for emergency and production efficiency reasons. | Dynamic vector brake without contactor for medium loads. | $\begin{array}{l\|} \hline 320 ;=5 \\ 323 ;=1,324 \end{array}$ |
|  |  | Reverse current brake with external contactor for heavy loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=2,324 \end{aligned}$ |
|  | High speed lines | Conveyor speed set from planer shaft power analogue output. | 520-523 |
|  | Worn out tool | Shaft power overload | 400 |
|  | Broken coupling | Shaft power underload | 401 |
| ROCK CRUSHER | High inertia | Linear torque control gives linear acceleration and low starting current. | 310;=1 |
|  | Heavy load when starting with material | Torque boost | 316,317 |
|  | Low power if a diesel powered generator is used. | Current limit at start | 314 |
|  | Wrong material in crusher | Shaft power overload | 400 |
|  | Vibrations during stop | Dynamic vector brake without contactor | $\begin{aligned} & 320 ;=5 \\ & 323 ;=1,324 \end{aligned}$ |
| BANDSAW | High inertia load with high demands on torque and current control. | Linear torque ramp gives linear acceleration and low starting current. | 310;=1 |
|  | Need to stop quickly. | Dynamic vector brake without contactor for medium loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=1,324 \end{aligned}$ |
|  |  | Reverse current brake with external contactor for heavy loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=2,324 \end{aligned}$ |
|  | High speed lines | Conveyor speed set from bandsaw shaft power analogue output. | 520-523 |
|  | Worn out saw blade | Shaft power overload | 400 |
|  | Broken coupling, saw blade or belt | Shaft power underload | 401 |
| CENTRIFUGE | High inertia load | Linear torque control gives linear acceleration and low starting current. | 310;=1 |
|  | Too high load or unbalanced centrifuge | Shaft power overload | 400 |
|  | Controlled stop | Dynamic vector brake without contactor for medium loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=1,324 \end{aligned}$ |
|  |  | Reverse current brake with external contactor for heavy loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=2,324 \end{aligned}$ |
|  | Need to open centrifuge in a certain position. | Braking down to slow speed and then positioning control. | $\begin{aligned} & 330-333 \\ & 500,501 \end{aligned}$ |

Table 10 Application Functions List

| Appllcation | Challenge | MSF Solution | Menus |
| :---: | :---: | :---: | :---: |
| MIXER | Different materials | Linear torque control gives linear acceleration and low starting current. | 310; $=1$ |
|  | Need to control material viscosity | Shaft power analogue output | 520-523 |
|  | Broken or damaged blades | Shaft power overload | 400 |
|  |  | Shaft power underload | 401 |
| HAMMER MILL | Heavy load with high breakaway torque | Linear torque control gives linear acceleration and low starting current. | 310;=1 |
|  |  | Torque boost in beginning of ramp. | 316,317 |
|  | Jamming | Shaft power overload | 400 |
|  | Fast stop | Reverse current brake with reversing contactor for heavy loads. | $\begin{aligned} & 320 ;=5 \\ & 323 ;=2,324 \end{aligned}$ |
|  | Motor blocked | Locked rotor function | 228 |

## Example

Hammer Mill:

- Linear Torque control (menu 310=1) will give the best results.
- Torque boost to overcome high breakaway torque (menus [316] and [317])
- Overload alarm function for jamming protection (menu [400])
- Stop function reverse current brake (menu [323], selection 2) can be used. Menus 324 and [325] to set the brake time and strength.


### 6.5 Special conditions

### 6.5.1 Small motor or low load

The minimum load current for the MSF 2.0 softstarter is $10 \%$ of the rated current of the softstarter, except for the MSF-017 where the min. current is 2 A . Example: MSF210 , rated current $=210 \mathrm{~A}$. Min. Current 21 A . Please note that this is "minimum load current" and not minimum rated motor current.

### 6.5.2 Ambient temperature below $0^{\circ} \mathrm{C}$

For ambient temperatures below $0^{\circ} \mathrm{C}$ an electric heater or similar must be installed in the cabinet. The softstarter can also be mounted somewhere else since the distance berween the motor and the softstarter is not critical.

### 6.5.3 Phase compensation capacitor

If a phase compensation capacitor is to be used, it must be connected at the inlet of the softstarter, not berween the motor and the softstarter.

### 6.5.4 Shielded motor cable

It is not necessary to use shielded wires together with softstarters. This is due to the very low radiated emissions.

NOTEI The softstarter should be wired with a shielded control cable to fulfil the EMC regulations outifined section 1.6, page 6.

### 6.5.5 Pump control with softstarter and frequency inverter together

It is possible, e.g. in a pump station with two or more pumps, to use one frequency inverter on one pump and softstarters on each of the other pumps. The flow of the pumps can then be controlled by one common control unit.

### 6.5.6 Starting with counterclockwise rotating loads

It is possible to start a motor clockwise, even if the load and motor are rotating counterclockwise e.g. fans. Depending on the speed and the load "in the wrong direction" the current can be very high.

### 6.5.7 Running motors connected in parallel

When starting and running motors connected in parallel, the total amount of the motor current must be equal or lower than the rating of the connected softstarter. Please note that it is not possible to have individual settings for each motor or to use the internal thermal motor protection. The start ramp can only be set for an average starting ramp for all the connected motors. This means that the start time may differ from motor to motor.

For motors connected in parallel, torque control is not recommended because of the risk of oscillation between the motors. Voltage control with or without current limit is preferred instead. The use of the braking functionality is not recommended for motors connected in parallel.

### 6.5.8 Running motors linked together

When starting and running motors mechanically linked together but with one softstarter connected to each motor, there are two kinds of operation available. The first is to start the motors at the same time using voltage control with or without current limit. The second is to start one motor first with torque or voltage control and after the motor has reached full speed, the voltage to the other motors is ramped up using voltage control.

### 6.5.9 Step-up transformer for high voltage motor

A step-up transformer can be used between the MSF and the motor for controlling a motor rated at high voltage (e.g. higher than 690 V ). Torque control can be used for starting and stopping. To compensate for the step-up transformer magnetization current at start, the initial torque should be set a little higher than normal. The motor data must be recalculated for the lower voltage side of the transformer.

### 6.5.10 How to calculate heat dissipation in cabinets

See chapter 13. on page 109 "Technical Data", "Power loss ac rated motor load", "Power consumption control card" and "Power consumption fan". For further calculations please contact your local supplier of cabiners, e.g. Ritral.

### 6.5.11 Insulation test on motor

When testing the motor with high voltage e.g. insulation test, the softstarter must be disconnected from the motor. This is due to the fact that the softstarter will be seriously damaged by the high peak voltage.

### 6.5.12 Operation above 1000 m

All ratings are stared at 1000 m over sea level.
If an MSF 2.0 is placed at 3000 m for example, it must be derated.

To get information about motors and drives ar higher altitudes please contact your supplier to get technical information no 151.

## 7. Operation of the softstarter



Fig. 31 MSF sofistarter models MSF-017 to MSF-1400.

### 7.1 General description of user interface

WARNINGI Never operate the softstarter with the front cover removed.

To obtain the required operation, a number of parameters must be set in the softstarter.
Configuration is carried out either from the control panel or by a computer/control system through the serial communication interface (option). Controlling the motor i.e. start/ stop, selection of parameter set, is done either from the control panel, through the remote control inputs or through the serial communication interface (option).

## Setting



WARNINGI Make sure that all safety measures have been taken before switching on the power supply.

Switch on the control supply (normally $1^{*} 230 \mathrm{~V}$ ); all segments in the display will be illuminated for a few seconds. Then the display will show menu [100]. An illuminated display indicates that there is control supply voltage to the softstarter.

Check that you have voltage on the mains contactor or on the thyristors. Set the motor data, menus [210] to [215], to achieve correct functionality and optimized performance of the build-in functions such as torque control, motor protection, shaft power monitor etc.

### 7.2 Control panel



Fig. 32 Control panel.

The control panel is used for selection, programming and presentation. It consists of:

- 2 light emitting diodes (LEDs).
- 1 display with three 7 -segment digits showing the actual menu number.
- 1 display with four 7 -segment digits showing the actual value.
- Keyboard with eight keys.


### 7.3 LED indication

The two light emitting diodes indicate start/stop and running motor/machine.
When a start command is given either from the control panel, through the serial communication interface (option) or through the remote control inputs, the start/stop LED will be illuminated. At a stop command the start/stop LED will switch off. The start/stop LED flashes when the softstarter is in standby operation waiting for a start caused by autoreset or analogue start/stop.
When the motor is running, the running LED flashes during ramp up and down and is illuminated continuously at full motor voltage.


Fig. 33 LED indication at different operation situations.

### 7.4 The menu structure

The menus in MSF 2.0 are organized in a 1 -level structure and they are divided into the groups set out in table 8 .
For easier commissioning the menus are divided into three groups, Read-out, Setting and Multi Setting. Read-out menus are only for reading; Setting menus are for setting one parameter and Multi Setting menus are for setting several parameters which cannot be undone. The menus are selected by navigating backwards and forwards through the menu system. Sub-menus simplify setting but are not available when the corresponding main function is not activated.

Table 11 Menu structure of MSF 2.0.

| Function | Menu number |
| :--- | :--- |
| General settings | $100-101,200-202$ |
| Motor data | $210-215$ |
| Motor protection | $220-231$ |
| Parameter set handling | $240-243$ |
| Auto reset | $250-263$ |
| Serial communication | $270-273$ |
| Operation settings | $300-342$ |
| Process protection | $400-440$ |
| I/O settings | $500-534$ |
| View operation | $700-732$ |
| Alarm list | $800-814$ |
| Softstarter data | $900-902$ |

### 7.5 The keys

The function of the control panel is based on a few simple rules.

1. At power up menu [100] is shown automatically.
2. Use the "NEXT $\rightarrow$ " and "PREV $\leftarrow$ " keys to move between menus. To scroll through menu numbers, press and hold either the "NEXT $\rightarrow$ " or the "PREV $\leftarrow$ " key.
3. The " + " and " - " keys are used to increase respectively decrease the value of setting. The value is flashing during setting.
4. The "ENTER $\downarrow$ " key confirms the setting just made, and the value will go from flashing to stable.
5. The "START/STOP" key is only used to start and stop the motor/machine.
6. The $\Omega$ and $\Omega$ keys are only used for JOG from the control panel. The Jog function muse be enabled in menu [334] or [335].

Table 12 The keys

| Stary/stop motor operation. | START |
| :--- | :--- |
| Sisplay previous menu. | PREV |
| Display next menu. |  |
| Decrease value of setting. |  |
| Increase value of setting. |  |
| Confirm setting just made. |  |
| Alarm reset. |  |
| JOG Reverse |  |
| JOG Forward |  |

### 7.6 Control panel lock

The control panel can be locked to prevent parameter being set by unauthorised personnel.

- Lock control panel by simultaneously pressing both "NEXT $\rightarrow$ " and "ENTER $\leftrightarrows$ " for at least 2 sec . The message '- Loc' will be displayed for 2 seconds when locked.
- To unlock control panel, simultaneously press the same 2 keys "NEXT $\rightarrow$ " and "ENTER $\boldsymbol{~}$ " for at least 2 sec . The message 'unlo' will be displayed for 2 seconds when unlocked.

In locked mode it is possible to operate the softstarter from the control panel and to view all parameters and read-outs, but it is not possible to change any parameters.

### 7.7 Overview of softstarter

 operation and parameter set-upTable showing how parameters can be set and operation carried out.

Table 13 Control sources

| Control source | Control panel lock | Operation |  | Setting of parameters |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Start/Stop | Alarm reset |  |
| Control panel Menu [200]=1 | Unlocked control panel | Control panel | Control panel | Control panel |
|  | Locked control panel | Control panel | Control panel | - |
| Remote Menu [200]=2 | Unlocked control panel | Remote | Remote and control panel | Control panel |
|  | Locked control panel | Remote | Remote and control panel | - |
| Serial comm. Menu [200]=3 | Unlocked control panel | Serial comm. | Serial comm. and control panel | Serial comm. |
|  | Locked control panel | Serial comm. | Serial comm. and control panel | Serial comm. |

NOTE: If external control of parameter set is chosen in menu [240] no parameters except for parameter set [249] and control source [200] can be changed.

## 8. Functional description

This functional description for Softstarter MSF 2.0 describes the menus and parameters in the softstarter unit. You will find a short description of each function, their aims and settings.

The MSF 2.0 provides extensive serting possibilities via menus on the control panel, remore control or serial communication. The menus are numbered according to the menu overview in Table 10.

Table 14 Menu overview

| Function | Menu number | Description | See sectlon |
| :--- | :---: | :--- | :---: |
| General settings | $100-101$ <br> $200-202$ | General basic settings. | 8.1 |
| Motor data | $210-215$ | For insertion of technicai data for the actual motor. | 8.2 |
| Motor protection | $220-231$ | Protection associated with the motor in the application. | 8.3 |
| Parameter set <br> handling | $240-243$ | Selection and programming of parameter sets. | 8.4 |
| Auto reset | $250-263$ | Automatic reset of active alarm and restart of MSF 2.0. | 8.5 |
| Serial <br> communication | $270-273$ | Serial communication settings for the data transfer. | 8.6 |
| Operation settIngs | $300-342$ | Settings associated with the operation, for example the start- and <br> stop procedures. | 8.7 |
| Process protectlon | $400-440$ | Protection associated with the process. | 8.8 |
| I/0 settings | $500-534$ | In- and output settings for control and monitoring. | 8.9 |
| View operation | $700-732$ | For read-out of measured values. | 8.10 |
| Alarm Ilst | $800-814$ | Latest error. Available alarms. | 8.11 |
| Softstarter data | $900-902$ | Displays softstarter type, software variant and version. | 8.12 |

### 8.1 General settings

General settings for MSF 2.0 contains the following menus:
[100] Current
[101] Automatic return menu
[200] Control source
[201] Control panel locked for settings
[202] Enable US units

### 8.1.1 Current [100]

This read-out menu shows the actual current to the motor.


NOTE! This is the same read-out as menu [700].

### 8.1.2 Automatic return menu [101]

When the MSF 2.0 is powered up, menu [100] (Current read-out) is shown as default. When another menu has been selected by the user (moving through the menu list with the "NEXT" or "PREV" keys) this menu will remain active. Alternatively a specific menu can be chosen as automatic return menu. The chosen menu will be shown automatically after 60 seconds without any control panel activity.


### 8.1.3 Control source [200]

The softstarter can be controlled either via the control panel, remote control or the serial communication interface. Remote control via terminals 11,12 and 13 is the default setting.

NOTE: Depending on the setting in this menu, the softstarter may be configured via control panel or via serial communication. See Table 13, page 42 for more information.

NOTE: If control panel (1) or remote control (2) is configured, the setting can only be changed via control panel to serial communication control (3). However, If serial communication control (3) Is configured, the setting can be changed either via serial communication or via control panel.


### 8.1.4 Control panel lock [201]

The MSF 2.0 Control panel can be locked to prevent parameter being set by unauthorised personnel.

- Lock control panel by simultaneously pressing both keys "NEXT $\rightarrow$ " and "ENTER $\boxed{\text { " }}$ " for at least 2 seconds. The message "- Loc" will be displayed for 2 seconds.
- To unlock control panel, simultaneously press the same two keys "NEXT $\rightarrow$ " and "ENTER 4 " for at least 2 seconds. The message "unlo" will be displayed for 2 seconds.

In locked mode, all parameters and read-outs (menus) can be displayed, but it is forbidden to change any parameters via the control panel.
The message '-Loc' will be displayed if someone tries to set a parameter in locked mode.
The key lock status can be read out in menu [201].

NOTE: If menu [200] is configured for serial communication control, the softstarter may still be configured via serial communlcation, regardless of the control panel lock status.

| 2 0 <br> 0  |  |  | Control panel locked for settings |  |
| :---: | :---: | :---: | :---: | :---: |
|  | n | 0 |  |  |
| Default: |  | no |  |  |
| Range: |  | no, YES |  |  |
| no |  | Control panel is not locked |  |  |
| YES |  | Control panel is locked |  |  |

### 8.1.5 Enable US units [202]

By default all read-out and configuration values are given in SI units. If preferred, US customary units can be chosen instead. in chis case the following units are used:

- Powers are set and shown in HP, menus [212] and [703]
- Power consumption is shown in MHph, menu [731]
- Shaft torque is shown in Ibft, menu [705]
- Temperature is shown in degrees Fahrenheit, menu [707]

NOTE: When the setting for US units is changed, the motor data in menus [210-215] is reset to the default values for the chosen units (SI or US customary units) in all parameter sets.
[210] Nominal motor voltage - new default value ( 460 V , for US units enabled)
[211] Nominal motor current - new default value depending on softstarter size.
[212] Nominal motor power - new default value depending on soffstarter size
[213] Nominal motor speed - new default value depending on softstarter size
[215] Nominal frequency - new default value ( 60 Hz , for US units enabled)

If the setting is changed and confirmed with "ENTER", " SEt " is displayed for 2 seconds to indicate successful selection.


### 8.2 Motor data

For oprimal performance the MSF 2.0 softstarter should be configured according to the motor's rating plate:
[210] to [215] Nominal motor data

NOTE: The default factory settings are for a standard 4 pole motor according to the nominal current and power of the softstarter. The softstarter will run even If no specific motor data is selected, but the performance will not be optimal.

Nominal motor voltage.


NOTE: Make sure the softstarter's maximum voltage rating is suitable for selected motor voltage.

Nominal motor current. The current range is related to the size of the softstarter.

| 2 | 1 | 1 |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  | 1 | 7 |

Nominal motor power in kW or HP. The power range is related to the size of the softstarter.


Nominal motor speed.


Nominal motor power factor.


Nominal motor frequency


### 8.3 Motor protection

The MSF 2.0 softstarter is equipped with different motor protection functions. The following menus are available to configure these protection methods:
[220]-[223] Thermal motor protection
[224]-[227] Start limitation
[228]-[229] Locked rotor
[230] Single phase input failure
[231] Current limit start time expired
For these protection methods the following options are available (all options may not be available for all protection methods - check the description of the relevant menu for details):

Off
The protection method is disabled.

## Warning

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). However, the motor is not stopped and operation continues. The alarm message will disappear and the relay will be reset wen the fault disappears. The alarm may also be reset manually.

## Coast

The appropriate alarm message is shown in the display and relay K3 is activated (for default configuration of the relays). The motor voltage is automatically switched off. The motor freewheels until it stops.

## Stop

The appropriate alarm message is shown in the display and relay K3 is activated (for default configuration of the relays). The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

The appropriate alarm message is shown in the display and relay K3 is activated (for default configuration of the relays). The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menus [326] to [327] (braking strength and braking time).

### 8.3.1 Thermal motor protection

With MSF 2.0 an internal thermal model of the motor or an external signal from a PTC can be used for thermal motor protection. It is also possible to combine both protection methods. Slight overload for a long time and several overloads of short duration will be detected with both methods.

## Thermal motor protection [220]

Thermal motor protection is activated by choosing an alarm action in menu [220]. After that menus [221] to [223] will be available so that the type of the protection (internal and/ or PTC) can be chosen. If the operation has been interrupted due to a thermal motor protection alarm, a manual reset and a new start signal is needed to restart the motor. The reset and the start signal can be given via control panel, remote or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via the control panel.

[^11]| $2\|2\| O$ | Setting  <br>   <br> Thermal motor protection  <br> (Alarm code F2)  |
| :--- | :--- | :--- | :--- |
| Default: | 2 (Coast) |
| Range: | oFF, 1, 2, 3, 4 |
| oFF | Thermal motor protection is disabled. |
| 1 | Warning |
| 2 | Coast |
| 3 | Stop |
| 4 | Brake |

## PTC input [221]

This menu is available if thermal motor protection is enabled in menu [220]. To use the PTC functionality, connect the PTC to terminals 69 and 70 . See fig. 53. If the motor gets too warm (PTC resistance above 2.4 kOhm ), an F2 alarm will occur. The alarm will remain active until the motor has cooled down (PTC resistance below 2.2 kOhm ).


NOTE: Open terminals will give an F2 alarm immedlately. Make sure the PTC is always connected or the terminals are shorted.

## Internal protection class [222]

This menu is available if thermal motor protection is enabled in menu [220]. In this menu an internal protection class can be chosen, which enables internal thermal motor protection. With this serting a thermal curve as set out in Fig. 34 is configured. The motor's thermal capacity is calculated continuously based on the chosen curve. If the thermal capacity exceeds $100 \%$ an F 2 alarm occurs and the action chosen in menu [220] is performed. The alarm remains active until the motor model cools down to $95 \%$ of its thermal capacity. The used thermal capacity is shown in menu [223].


NOTE: Check that the motor current is configured properly in menu [211].

NOTEl If an external bypass contactor is used, check that the current transformers are placed and connected correctly.


CAUTIONI Used thermal capacity Is set to 0 If the control board loses its supply (terminal 01 and 02). This means that the internal thermal model starts with a "cold" motor, which perhaps in reality is not the case. This means that the motor can be overheated.

## Used thermal capacity [223]

This menu is available if thermal motor protection is activated in menu [220] and an internal protection class is chosen in menu [222]. The menu shows the thermal capacity of the motor according to the thermal curve chosen in menu [222].



Fig. 34 The thermal curve

### 8.3.2 Start limitation

Start limitation is used to protect the motor by limiting the numbers of starts per hour or securing a minimum time delay berween starts. Boch protection methods can be used separately or in combination.

## Start limitation [224]

Start limitation is enabled in this menu by choosing a proper alarm action. The available options are:

Off
The protection method is disabled.

## Warning

Alarm message F11 is shown in the display and relay K 3 is activated (for default configuration of the relays). However, the start will be allowed.

## Coast

Alarm message F11 is shown in the display and relay K 3 is activated (for default configuration of the relays). The start will not be allowed.

A Start limitation alarm is automatically reset when a new start signal is given. The start signal can be given via control panel, remore or via serial communication depending on the control source chosen in menu [200]. Regardless of the cho-
sen control source, it is always possible to initiate a reset via the control panel.

NOTE: A reset via the control panel will never start the motor.


## Number of starts per hour [225]

This menu is available if start limitation is enabled in menu [224]. In this menu the allowed number of starts per hour is configured. If this number is exceeded, an F11 alarm occurs and the action chosen in menu [224] is performed. The alarm is active until the hour has expired and a new start can be allowed.


## Min. time between starts [226]

This menu is available if start limitation is enabled in menu [224]. In this menua minimum time between consecutive starts can be configured. If a new start attempt is made before the configured minimum time is expired an Fil alarm will occur and the action chosen in menu [224] is performed. The alarm remains active until the chosen minimum time has expired and a new start can be allowed.


## Time to next allowed start [227]

This menu is available if start limitation is enabled in menu [224] and at least one of the protection methods described above is configured (number of starts per hour or minimum time berween starts). In this menu the remaining time to the next allowed start is shown. If both protection methods mentioned above are activated, the shown time is the total time delay to the next start, which is allowed by both methods.


### 8.3.3 Locked rotor

This alarm is used to avoid high motor current due to a mechanically locked rotor. If the operation has been interrupted due to a locked rotor alarm, a manual reset and a new start signal is needed to restart the motor. The reset and the start signal can be given via control panel, remote or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reser via the control panel.

NOTE: A reset via the control panel will never start the motor.

## Locked rotor [228]

Locked rotor alarm is activated in this menu by choosing a proper alarm action.


## Locked rotor time [229]

This menu is available if Locked rotor alarm is enabled in menu [228]. In this menu the time delay for detection of a locked rotor is configured. If a high motor current (4.8 times the nominal motor current) is floating for a time exceeding the chosen value, an FS alarm will occur and the action chosen in menu [228] will be performed.


NOTE: Check that the motor current is configured properly in menu [211].

### 8.3.4 Phase input failure

All phase input failures shorter than 100 ms are ignored.

## Multiple phase input failure

If the failure duration time is above 100 ms , operation is temporary stopped and a new soft start is made if the failure disappears within 2 s . If the failure duration time is longer than 2 s an Fl alarm occurs and the voltage to the motor remains off. During deceleration, regardless of the failure duration time, the motor voltage is automatically switched off and the motor freewheels until it stops.

## Single phase input failure

During acceleration and deceleration the behaviour is the same as described above for multiple phase inpur failure. When running with full voltage, the softstarter can be configured for different actions in the event of a single phase input failure (menu [230]).

A phase inpur failure alarm is automatically reset when a new start signal is given. The start signal can be given via control panel, remote or via serial communication depending on the control source chosen in menu 200. Regardless of the chosen control source, it is always possible to initiate a reset via the control panel.

NOTE: A reset via the control panel will never start the motor.

## Single phase input failure [230]

The softstarter's action on a single phase input failure occurring during full voltage running can be configured in this menu. In the event of a single phase input failure, alarm Fl is activated after 2 s (see description above) and the chosen action is performed. The alarm remains active until the failure disappears.


### 8.3.5 Current limit start time expired

If current limit at start is activated in menu [314], an F4 alarm can be activated if the operation is still at current limit when the configured start time has expired. A curtent limit start time expired alarm is automatically reset when a new start signal is given. The start signal can be given via control panel, remote or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset via the control panel will never start the motor.

## Current limit start time expired [231]

In this menu the alarm for current limit start time expired can be enabled and a proper action can be selected.

| 2 | 3 | 1 |  |
| :--- | :--- | :--- | :--- |
|  |  |  | Setting |
|  | Current Ilmit start time expired <br> (alarm code F4) |  |  |
| Default: | 2 |  |  |
| Range: | oFF, 1, 2, 3, 4 |  |  |
| ofF | Current limit start time expired protection is <br> disabled. |  |  |
| 1 | Warning |  |  |
| 2 | Coast |  |  |
| 3 | Stop |  |  |
| 4 | Brake |  |  |

NOTE: If the action for current limit start time expired is configured as Warning or the protection is not activated at all, the softstarter will ramp up to full voltage with a ramp time of 6 s if the start time has expired in current limit mode. The current is then no longer controlled.

### 8.4 Parameter set handling

The use of different parameter sets can be helpful when using one softstarter to start different motors or when working under various load conditions. There are four parameter sets available in MSF 2.0. Parameter set handling is controlled by the following menus:
[240] Select parameter set
[241] Actual parameter set
[242] Copy parameter set
[243] Reset to factory setting

### 8.4.1 Select parameter set [240]



Fig. 35 Parameter overview

## Select parameter set [240]

In this menu one of the parameter sets $1-4$ can be selected directly or external control of parameter sets via digital inputs can be chosen. If external control of parameter sets is chosen, the digital inputs have to be configured properly (see description of menus [510] to [513]). By default digital inputs 3 and 4 (terminals 16 and 17) are configured for external control of parameter sets.

| 2 4 0 <br> 0   |  | Setting |
| :---: | :---: | :---: |
|  | 1 Select parameter set |  |
| Default: | 1 |  |
| Range: | 0, 1, 2, 3, 4 |  |
| 0 | External control of parameter sets. |  |
| 1, 2, 3, 4 | Selection of parameter sets 1-4. |  |

## Actual parameter set [241]

This menu is available when external control of parameter sets is chosen in menu [240]. This menu shows which parameter set is actually selected via the digital inputs.


### 8.4.2 Copy parameter set [242]

When programming a new parameter set, this function will simplify the procedure. It is possible to copy an already programmed parameter set into another set as follows:

- Select a copy alternative in this menu, for example P1-2. Press Enter. "CoPY" is displayed for 2 seconds to indicate successful copy process. After that, "no" is displayed.
- Go to menu [240] and select parameter set 2.
- Make the required new settings in corresponding menus for parameter set 2.


NOTE: Copying parameter sets is only allowed when the softstarter is not running.

### 8.4.3 Reset to factory setting [243]

This menu enables all parameters to be reset to the default values. This includes all four parameter sets and the common parameters except for parameter [202] (enable US units). As Enable US units is not reset to default, the values loaded for the normal motor data in menus [210] to [215] correspond to the chosen units (SI or US customary), see description of menu [202] on page 45 for more information. The alarm list, the power consumption and the operation time will not be affected by resetting the parameters. When the reset of all parameters to the factory default values has been executed successfully, menu [100] is shown on the display.


NOTEI Reset to factory settings is not allowed when the softstarter is running.

### 8.5 Autoreset

For several non-critical application-related failure conditions, it is possible to automatically generate a reset and initiate a restart to overcome the fault condition. Autoreset functionality is configured using the following menus:
[250] Autoreset attempts.
[251] to [263] Autoreset items.
In menu [250] the maximum number of automatically generated restarts allowed can be set. When this number is exceeded and a new fault occurs, the softstarter will stay in fault condition because external assistance is required. In menus [251] to [263], autoreset is enabled for the different protection cypes by choosing a delay time. If a fault occurs for which autoreset is enabled, the motor is stopped according to the action chosen for the relevant protection method (see menus [220] to [231] and [400] to [440] for description of protection methods and configuration of actions on failures). When the fault has disappeared, and the configured delay time has elapsed, the motor is restarted.

## Example:

The motor is protected by internal thermal protection. When a thermal protection alarm occurs, the sofsstarter should wait until the motor is cooled down enough before resuming normal operation. When this problem occurs several times in a short period of time, external assistance is required.

The following settings should be applied:

- Activate thermal motor protection, e.g. set menu [220] to 2 (Coast).
- Activate internal thermal motor protection, e.g. set menu [222] to 10 (thermal curve for 10 s ).
- Insert maximum number of restarts: e.g. set menu [250] to 3.
- Activate thermal motor protection to be automatically reset: e.g. set menu [251] to 100 .
- Configure one of the relays to give an alarm when external assistance is required: e.g. set menu [532] to 19 (all alarms which need manual reset).
The autoreset functionality is not available if control panel is chosen as control source in menu [220].


WARNING: A flashing start/stop LED indicates standby mode e.g. walting for autoreset. The motor may be started automatically at a moment's notice.

NOTE: The autoreset cycle will be interrupted when a stop signal is given (remote or via serial communication) or If the control source is changed to control panel in menu [200].

### 8.5.1 Autoreset attempts [250]

In this menu the maximum allowed number of automatically generated restart attempts is set. If any number of autoreset attempts is selected in this menu the Autoreset functionality is activated and menus [251] to [263], will become available. If an alarm occurs for which autoreser is enabled (in menus [251] to [263]), the motor will automatically be restarted when the fault has disappeared and the delay time has expired. For each automatically generated restart, the internal autoreset counter (not visible) will go up one place. If no alarm occurs for more than 10 minutes, the autoreset counter will be decreased by one. When the maximum number of autoreset attempts is reached, no further restart will be allowed and the softstarter will remain in fault condition. In this case a manual reset (either via control panel, remote or serial communication, see description on page 39) is needed.
Example:

- Autoreser attempts (menu [250]=5)
- Within 10 minutes 6 alarms occur.
- At the 6th trip there is no autoreser, because the autoreset counter contains already 5 autoreset attempts.
- To reset, apply a normal reser. This will also reser the autoreset counter.

NOTE: The Internal autoreset counter is reset to zero if a stop signal is given. After each new start signal (via remote or serlal communication) the maximum number of restart attempts will be allowed as configured in menu [250].


### 8.5.2 Autoreset items [251]-[263]

Menus [251] to [263] are available if autoreset is enabled in menu [250]. With these menus the delay time for autoreset is configured. The delay time starts counting when the fault is gone. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

NOTE: Enabling autoreset for an alarm has no effect if the alarm action for the respective alarm is set to oFF or Warning (1).

## Thermal motor protection autoreset [251]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for thermal motor protection autoreset is configured. The delay time starts counting when the fault is gone. This means the internal thermal motor model has to cool down to a thermal capacity of $95 \%$ (if internal thermal motor protection is enabled) and the PTC resistance has to go down to 2.2 kOhm (if PTC is enabled), which indicates that the motor has cooled down. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.


## Start limitation autoreset [252]

This menu is available if autoreser is activared in menu [250]. In this menu the delay time for an autoreset after a start limitation alarm (alarm code F11) is configured. The delay time starts counting when the fault is gone. This means the minimum time between starts has to be expired (if Minimum time between starts protection is enabled) and a start has to be allowed for the actual hour (if starts per hour protection is enabled). When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Locked rotor alarm autoreset [253]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after a locked rotor alarm (alarm code F5) is configured. As a locked rotor cannot be detected in stopped state, the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Current limit start time expired autoreset [254]

This menu is available if autoreset is activared in menu [250]. In this menu the delay time for an autoreset after a current limit start time expired alarm (alarm code F4) is configured. As a current limit start time expired fault condition cannot be detected in stopped state, the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Max power alarm autoreset [255]

This menu is available if autoreset is activared in menu [250]. In this menu the delay time for an autoreset after a max power alarm (alarm code F6) is configured. As a max power fault condition cannot be detected in stopped state, the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Min power alarm autoreset [256]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after a min power alarm (alarm code F7) is configured. As a min power fault condition cannot be detected in stopped state, the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## External alarm autoreset [257]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after a external alarm (alarm code F17) is configured. The delay time starts counting when the fault is gone. This means the external alarm signal inpur has to be closed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Phase input failure autoreset [258]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreser after a phase input failure (alarm code F1) is configured. As a phase input failure cannot be detected in stopped state, the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Voltage unbalance alarm autoreset [259]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after a voltage unbalance alarm (alarm code F8) is configured. The delay time starts counting when the fault is gone. Usually, the mains voltage will not be available to the softstarter in stopped state as the mains contactor is deactivated. In this case a voltage unbalance failure cannor be derected in stopped state and the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Over voltage alarm autoreset [260]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after an over voltage alarm (alarm code F9) is configured. The delay time starts counting when the fault is gone. Usually, the mains voltage will not be available to the softstarter in stopped state as the mains contactor is deactivated. In this case an over voltage failure cannor be detected in stopped state and the delay time starts counting immediately after the alarm action has been executed. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Under voltage alarm autoreset [261]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for an autoreset after an under voltage alarm (alarm code F10) is configured. The delay time starts counting when the fault is gone. Usually, the mains voltage will not be available to the softstarter in stopped state as the mains contactor is deactivated. In this case an under voltage failure cannor be derected in stopped state and the delay time starts counting immediately after the alarm action has been executed. When the delay time
has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Serial communication autoreset [262]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for autoreser after a serial communication broken alarm (alarm code F15) is configured. The delay time starts counting when the fault is gone. This means serial communication has to be re-established. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

## Softstarter overheated autoreset [263]

This menu is available if autoreset is activated in menu [250]. In this menu the delay time for autoreset after a softstarter overheated alarm (alarm code F3) is configured. The delay time starts counting when the fault is gone. This means the softstarter has to be cooled down. When the delay time has elapsed, the alarm will be reset and a restart attempt will automatically be made.

### 8.6 Serial communication

There are several serial communication options available for MSF 2.0 (see page 107 for more information). The softstarter can be configured and controlled via serial communication if this is configured in menu [200] (see page 44). The following parameters are available to configure serial communication:
[270] Serial comm. unit address
[271] Serial comm. baudrate
[272] Serial comm. parity
[273] Serial comm. contact broken

NOTE: The communication parameters [270] to [272] must be set up via the control panel. To enable configuration via the control panel, menu [200] must be set to 1 (control panel) or 2 (remote control).

Serial comm. unit address [270]
Serial communication unit address.

| 2 | 7 | 0 | Setting  <br>   |
| :--- | :--- | :--- | :--- |
|  |  |  | 1 |

Serial comm. baudrate [271]
Serial communication baudrate.


Serial comm. parity [272]
Serial communication parity.

| 2 | 7 | 2 |  |
| :--- | :--- | :--- | :--- |
|  |  | Setting   <br>    |  |
| Default: | 0 |  |  |
| Range: | 0,1 |  |  |
| 0 | No parity |  |  |
| 1 | Even parity. |  |  |

## Serial comm. contact broken [273]

If the softstarter is configured for control via serial communications (menu [200] = 3) and the serial communication contact is broken during operation, an F15 alarm can be configured to occur. In this menu the alarm can be enabled and an accion to be performed can be chosen. The following options are available:

## Off

Serial communication contact broken alarm is disabled.

## Warning

Alarm message F15 is shown in the display and relay K 3 is acrivated (for defaule configuration of the relays). However, the moror is not sropped and operation continues. The alarm message will disappear and the relay will be reser when the fault disappears. The alarm may also be reset manually from the control panel.

## Coast

Alarm message F 15 is shown in the display and relay K 3 is activated (for defaulic configuration of the relays). The motor voltage is automatically swirched off. The motor freewheels until it stops.

## Stop

Alarm message F 15 is shown in the display and relay K 3 is activated (for defaule configuration of the relays). The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

Alarm message F15 is shown in the display and relay K 3 is activated (for defaulc configuration of the relays). The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake sertings in menus [326] to [327] (braking strength and braking time).
A serial communication broken alarm is auromatically reset when a new start signal is given. The start signal can be given via control panel, remorely or via serial communication depending on the control source chosen in menu 200. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset via control panel will never start the motor.


### 8.7 Operation settings

Operation settings include paramerers for configuration of starting and stopping, some of these can be pre-configuted for pump applications. Furthermore, some special sertings for stop behaviour at alarm, parameters for slow speed and jog and additional settings such as bypass operation, power factor control and control of the internal fan are included in this section.
[300] Preset pump control parameters
[310]-[317] Start
[320]-[327] Srop including stop at alarm
[330]-[335] Slow speed/JOG
[340]-[342] Additional settings
The MSF Softstarter controls all three phases supplied to the motor. In contrast to a simple softstarter controlling only one or two phases, the three-phase control enables different starting methods, voltage, current and torque concrol. A current limit can even be used in combination with either voltage or torque control.

With voltage control the output voltage to the motor is linearly increased to full line voltage during the set start time. The softstarter gives a smooth start but does not get any feedback on current or torque. The typical sertings to optimize a voltage controlled start are the initial voltage and the start time.
With current control the output voltage to the motor is regulated so the set current limit is not exceeded during the start. Even with this starting method the starter does not get any feedback on the motor torque. However, current control can be combined with both voltage and torque control. The typical settings to optimize a current controlled start are the current limit and the maximum starting time.
Torque control is the most sophisticated way of starting motors. The softstarter continually monitors the motor torque and controls the output voltage to the motor so the torque follows the set ramp. Both linear- and square torque ramps can be chosen according to the application requirments. In this way constant acceleration can be accomplished during start which is very important in many applications. Torque control can also be used for stopping with constant deceleration. For pumps constant deceleration is important for avoiding water hammer.

### 8.7.1 Preset pump control [300]

With this multi-setting parameter the MSF 2.0 softstarter can easily be configured for pump applications. The following parameters are set if preset pump control parameters are chosen.
[310] Start method is set to square torque control (2)
[312] Initial torque at statt is set to $10 \%$
[313] End torque at start is set to $125 \%$
[315] Start time is set to 10 seconds
[314] and [316] Current limit at statt and torque boost are deactivated.
[320] Stop method is set to square torque control (2)
[321] End torque at stop is set to $10 \%$
[325] Stop time is set to 15 seconds.
These settings will lead to a smooth start with linear acceleration and a linear stop without water hammer for most pump applications. However, if the pre-set parameters need to be adapred for a specific application, the values in the relevant menus can be adapted.
The following figure shows typical current characteristics at start and speed curve at stop.


Fig. 36 Pump control. Current at start and speed at stop.
When the pre-setting of the parameters for pump control has been executed successfully, " SEt " is shown in the display for two seconds. After that "no" will be shown again.

Note: Pre-setting of parameters for pump control Is not allowed when the softstarter is running.


### 8.7.2 Start

With MSF 2.0, torque control, voltage control and direct on-line are available as start methods. Torque control is available both for loads with a linear torque characteristic like conveyors and planers and with square torque characteristics for pumps and fans. In general torque control is recommended as a starting method; voltage control may be used when for some special reasons a linear voltage ramp is desired. With Direct on-line (DOL) as a start method, neither the current nor the voltage will be controlled; full voltage is applied to the motor immediately. DOL can be used to start the motor if the softstarter has been damaged and the thyristors are short-circuited.
All start methods can be combined with a current limit. However, only a properly configured torque-controlled start will lead to constant acceleration. For this reason it is not recommended to set a current limit for pump applications. With a proper set-up of the torque control parameters, the starting current will be very low. For applications with variable load characteristics from start to start, the current limit functionality may be useful to avoid overloading the mains fuses. However, as the motor torque is proportional to the square of the current, setting a low current limit will limit the motor torque considerably. If the current limit is set too low in relation to the application's requirements, the motor will not be able to accelerate the load.

## Start method [310]

In this menu the start method is chosen. The menus necessary for configuration of the start will be available depending on the chosen start method.

| 3 1 0 <br> 0   |  | Start method | Setting |
| :---: | :---: | :---: | :---: |
|  | 1 |  |  |
| Default: | 1 |  |  |
| Range: | 1, 2, 3, 4 |  |  |
| 1 | Linear torque control |  |  |
| 2 | Square torque control |  |  |
| 3 | Voltage control |  |  |
| 4 | Dire | n-line, DOL |  |

## Torque control

The default settings for initial torque at start is $10 \%$ and for end torque at start it is $150 \%$. In Fig. 37 the resulting torque curve is shown versus time for linear and square torque characteristics.


Fig. 37 Torque control at start
A Properly configured torque-controlled start will lead to a linear speed increase and low starting current without current peaks.


Fig. 38 Current and speed in torque control

To optimize the start, use the setting for initial torque at start, menu [311] and end torque at start, menu (312].

When the start command is given, the motor should immediately start to rotate to avoid unnecessary heat development in the motor. If required, increase the initial torque at start.

The end torque at start should be adjusted so that the time for the motor to come up to nominal speed approximately matches the start time set in menu [315]. If the actual start time is much shorter than the set start time in menu [315], the End torque at stop can be decreased. If the motor does not reach full speed before the start time set in menu [315] has expired, the end torque at stop has to be increased to avoid current peaks and jerking at the end of the ramp. This may be needed for high inertia loads such as planers, saws and centrifuges.

The read-out of shaft torque in percentage of $\mathrm{T}_{\mathrm{n}}$ in menu [706] may be useful for fine-tuning the start ramp.

## Initial torque at start [311]

This menu is availahle if torque control is selected in menu [310]. In this menu the initial torque at start is set.


## End torque at start [312]

This menu is available if torque control is selected in menu [310]. In this menu the end torque at start is set.


## Voltage control

Voltage control can be used when a linear voltage ramp is desired. The voltage to the motor will be ramped up linearly, from initial voltage up to full mains voltage.


Fig. 39 Menu numbers for initial voltage and start time.

## Initial voltage at start [313]

This menu is available if voltage control is chosen as start method in menu [310]. In this menu the initial voltage at start is set.

| 3 | 1 | 3 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  | 3 | 0 |
|  |  |  |  |
|  |  |  |  |
| Default: | $30 \%$ |  |  |
| Range: | $25-90 \% \mathrm{U}$ |  |  |
| $25-90$ | Sets initial voltage at start |  |  |

## Direct on-line, DOL

If this alternative is selected in menu [310], the motor can be accelerated as if it was connected directly to the mains.

For this cype of operation:
Check whether the motor can accelerate the required load (DOL start). This function can be used evern with shorted thyristors.


Fig. 40 DOL-start.

## Current limit

Current limit at start can be used together with all start methods to limit the current to a defined max level when starting ( $150-500 \%$ of In). However, only a properly configured torque-controlled start will lead to linear acceleration. For this reason it is not recommended to set a current limit for pump applications. Moreover, as the motor torque is proportional to the square of the current, setting a low current limit will limit the motor torque considerably. If the current limit is set too low in relation to the application's requirements, the motor will not be able to accelerate the load.

The combination DOL start and current limit at start gives a start ramp with constant current. The softstarter will control the current up to the set current limit immediately at start, and keep it there until the start is completed or the set start-up time expires.


Fig. 41 Direct on-line start in combination with current limit at start.

Current limit at start [314]
In this menu the current limit at start is set.


NOTE: Even though the current limit can be set as low as $150 \%$ of the nominal motor current value, this minimum value cannot be used generally. If the current limit is set too low in relation to the application's requirements, the motor will not be able to accelerate the load.

NOTE: Check that the nominal motor current is configured properly in menu [211] if the current limit functlonality is used.

If the starting time is exceeded and the softstarter is still operating at current limit, an alarm will be activated according to "Current limit start time expired" settings for motor protection, menu [231]. Operation may be stopped or continued with a pre-defined voltage ramp. Note that the current will rise unchecked if the operation continues.

## Start time [315]

In this menu the desired start time is set. This menu is not available if DOL is chosen as a start method and no current limit is configured.


## Torque boost

In specific applications torque boost is required for the start. The torque boost parameter enables a high torque to be obtained by providing a high current for $0.1-2$ seconds at start. This enables a soft start of the motor even if the break away torque is high at start. For example in crushing mills applications etc.
When the torque boost function has finished, starting continues according to the selected start method.


Fig. 42 The principle of the torque boost when starting the motor.

## Torque boost current limit [316]

In this menu torque boost is enabled and the current limit for torque boost is configured.


## Torque boost active time [317]

This menu is available if torque boost is enabled in menu [316]. In this menu the time for the torque boost to be active is selected.


NOTEI Check whether the motor can accelerate the load with "Torque boost" without any harmful mechanical stress.

NOTE: Check that the nominal motor current is configured properly in menu [221].

### 8.7.3 Stop

With MSF 2.0, four stop methods are available: torque control, voltage control, coast and braking. Torque control is available for loads with linear or square torque characteristic. A torque or voltage-controlled stop is used for applications where the motor stopping suddenly could harm the application, e.g. water hammer in pump applications. In general a torque-controlled stop is recommended for these applications. The voltage-controlled stop can be used if a linear voltage ramp is desired. When coast is selected as a stop method, the voltage to the motor will be switched off and the motor will be left freewheeling. Braking may be used in applications where the motor needs to be stopped quickly, e.g for planers and bandsaws.

Any start method except for direct on-line (DOL) can be combined with any stop method, e.g. torque control can be used at start and brake for stop. The DOL start method can only be combined with coast or brake stop methods.

## Stop method [320]

In this menu the stop method is chosen. The menus necessary for configuring the stop will be available depending on the chosen stop method.

| 320 |  | Setting |
| :---: | :---: | :---: |
| 4 Stop method |  |  |
| Default: | 4 |  |
| Range: | 1, 2, |  |
| 1 | Linea |  |
| 2 | Square |  |
| 3 | Voltag |  |
| 4 | Coast |  |
| 5 | Brake |  |

## Torque control

With torque control at stop, the torque to the motor will be controlled from the nominal torque down to the chosen end torque at stop (menu [321]). Examples for the torque ramps for linear and square torque control are shown in Fig. 43.
The default value for end torque at stop is 0 ; this value may be increased if the motor is standing still before the stop is finished to avoid unnecessary heat development in the motor. With the end torque at stop set properly, the motor speed will decrease linearly down to standstill.


Fig. 43 Torque control at stop

## End torque at stop [321]

This menu will be available if torque control is chosen as stop method in menu [320] (alternative 1 or 2 ). In this menu the end torque at stop is configured.

| 3 | 2 | 1 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |

## Voltage control

With voltage control at stop, the voltage to the motor will be decreased to the chosen step down voltage at stop immediately after a stop signal. Then the voltage to the motor will follow a linear ramp down to the minimum voltage of $25 \%$ of the nominal voltage. An example of this voltage ramp is shown in Fig. 44.


Fig. 44 Menu numbers for step down voltage at stop and stop time.

## Step down voltage at stop [322]

This menu is available if voltage control is chosen as stop method in menu [320] (alternative 3). In this menu the step down voltage at stop is chosen in percentage of the nominal motor voltage.


## Braking

Braking can be used in applications where there is a need for a quick stop.
There are two built-in braking methods: dynamic vector brake for normal loads and reverse current brake for heavy loads with high inertia. In both braking methods the MSF 2.0 continuously detects the motor speed. At low speed the DC brake mode is activated until the motor is standing still. The MSF 2.0 will automatically turn off the output voltage when the moror has stopped or when the stop time has expired. Oprionally an external rotation senaor can be connected via digital input, see description for menu [500] on page 77 for more information.

## Dynamic vector brake

With dynamic vector brake, the braking torque applied to the motor will increase with decreasing speed. Dynamic vector brake can be used for all loads which are not rotating too close to synchronous speed when the motor voltage is switched off. This is valid for most applications as the load speed usually decreases because of frictional losses in gears or belt drives as soon as the motor voltage is switched off. However, loads with very high inertia may remain at high speed even though the motor is not supplying any torque. For these applications the reverse current brake can be used instead.
When the dynamic vector brake is used, no additional connections or contactors are needed.

## Reverse current brake

With reverse current brake, a very high braking torque can be applied to the motor even close to synchronous speed. All kind of loads can be stopped quickly using reverse current brake, including loads with very high inertia. If high braking torques are needed, it should be checked carefully whether the motor, the gear or belt drive and the load can withstand the high mechanical forces. To avoid harmful vibrations, it is generally recommended to select as low a braking torque as possible which also fulfils the demands for a short braking time.
For reverse current brake, two mains contactors are needed. The connection is shown in Fig. 45. The contactors have to be controlled by the MSF's relay outputs. During start and fuil voltage operation contactor K 1 will be closed, for braking K 1 will be opened and after a time delay K 2 will be closed to change the phase sequence.

NOTE: For several start/stops it is recommend that the motor temperature be monitored using the PTC input.

WARNING: When reverse current brake is selected, the relays K1 and K2 are automatically programmed for reverse current brake functionallty. The relay setting remains even if reverse current brake is deactivated. Therefore It may be necessary to adapt the relay functions manually.


Fig. 45 Reverse current brake wiring example.

## Braking method [323]

This menu is available if brake is selected as stop method in menu [320] (alternative 5) or if alarm brake is activated in menu [326] (see description of menus [326] to [327] for more information). In this menu the brake method is selected.


## Braking strength [324]

This menu is available if brake is selected as stop method in menu [320] (alternative 5). In this menu the braking strength is selected. To avoid unnecessary heat development in the motor and high mechanical stress it is generally recommended to select as low a braking strength as possible which still fulfils the dermands for a short braking time.


## Stop time [325]

This menu is available if any stop method except coast is selected in menu [320] (alternative 1, 2, 3 or 5 ). In this method the desired stop time is selected.


## Alarm braking

For most alarms it is possible to configure them so that when they are triggered either operation continues or the motor stops (see chapter 9. page 95 for more information). Brake is one of the actions available. If this option is chosen, the braking functionality is activated according to the brake method selected in menu [323] (see descriprion of the braking functionality above for more information). While the braking strength and stop time chosen in menus [324] and [325] are used for braking on a stop signal, different braking strengths and times can be configured in menus [326] and [327] if braking is activated by an alarm. This function may mainly be used in combination with an external alarm (see description on page 73), where an external signal is used to initiate a quick stop with a higher braking strength and a shorter braking time compared to normal operation.
If alarm braking is disabled in menu [326] and brake is chosen as an alarm action, the volcage to the motor will be switched off and the motor will freewheel if the specific alarm occurrs.

## Alarm braking strength [326]

In this menu braking as an alarm action is enabled and the alarm braking strength is selected. If alarm braking is not activated, the motor will be left freewheeling if an alarm occurs for which brake is configured as alarm action.


## Alarm braking time [327]

This menu is available if alarm brake is enabled in menu 327. In this menu the braking time to be used in the event of braking as an alarm action is configured.

| 3 | 2 | 7 |
| :--- | :--- | :--- | |  | $\quad$ Slarm braking time |  |
| :--- | :--- | :--- |
|  |  | 1 |

### 8.7.4 Slow speed and JOG functions

MSF 2.0 is able to run the motor at a fixed slow speed for a limited period of cime. The slow speed will be about $14 \%$ of the full speed in the forward direction and $9 \%$ in the reverse direction.

NOTE: As the motor torque during slow speed is limited to about 30\% of the nominal torque, slow speed can not be used in applications which need a high brake-away torque to start rotating.

The following funcrions are possible:

## Slow speed during a selected time period

Slow speed will be active for a selected time period before a start is initiated or after a stop is performed.

## Slow speed controlled by an external signal

The time period during which slow speed is active before a start is initiated or after a stop is performed is controlled by an external signal via the analogue/digital input. Slow speed will be active until a selected number of pulses has been detected on the input.

## Slow speed using the JOG commands

Slow speed can be activated independently from a start or stop via the control panel using the jog keys, via remote control using the analogue/digital input or via serial communication depending on che control source chosen in menu [200].


Fig. 46 Slow speed controlled by an external signal.

## Slow speed for a selected time

Slow speed in forward direction can be activated before a start and/or after a stop. The resulting speed curve is shown in Fig. 47 overleaf. Slow speed will be active for the time period selected in menus [331] and [332]. Slow speed can be combined with any statt and stop method. However, when slow speed at stop is used, it should be ensecured that the motor speed is decreased to a low value when slow speed is activated. If necessary, brake can be activated as stop method in menu [320].
The slow speed strength can be adapted to the application's requirements in menu [330]. Maximum available slow speed strength corresponds to about $30 \%$ of nominal motor torque.
If so desired, the DC brake can be activated after slow speed at stop. If activated, the DC brake will be active for the time period chosen in menu [333].
Slow speed during a selected time is configured using the following menus:
[330] Slow speed strength
[331] Slow speed time at start
[332] Slow speed time at stop
[333] DC-brake at slow speed
[324] Braking strength

## Slow speed controlled by an external signal

Slow speed controlled by an external signal is basically the same functionality as slow speed during a selected time described above. An external signal connected to the analogue/digital input is also used to deactivate slow speed before the set time period has expired.
When slow speed at start is configured and the analogue/ digital input (menu [500]) is configured for slow speed, the motor will start rotating at slow speed in a forward direction after a statt signal. When the number of edges set in menu [501] is detected on the analogue/digital input, slow speed is deactivated and a start is performed according to the start settings (menu [310] Off).
When slow speed at stop is configured and the analogue/digital input (menu [500]) is configured for slow speed, the motor will start rotating with slow speed in forward direction after a stop has performed. When the number of pulses set in menu [501] is detected on the analogue/digital input, slow speed is deactivated and the DC brake is activated if configured in menu [333].

Slow speed controlled by an external signal is configured using the following menus:
[500] Digital/analogue input
[501] Digital input pulses
[330] Slow speed strength
[331] Slow speed time at start
[332] Slow speed time at stop
[333] DC-brake at slow speed
[324] Braking strength

## Slow speed strength [330]

In this menu the slow speed strength is selected. The chosen setting applies for both slow speed during a selected time period, slow speed controlled by an external signal and slow speed using the JOG commands. The maximum setting (100) for the slow speed strength corresponds to about $30 \%$ of the nominal motor torque.

## Slow speed time at start [331]

In this menu slow speed at start is activated and the time is set for which slow speed is active before a start. If slow speed at start is controlled by an external signal via the analogue/ digital input, the set time becomes the maximum time for which slow speed is activated before a start is performed - if the number of edges set in menu [501] is not detected during the slow speed period.




Fig. 47 Slow speed at start/stop during a selected time period.

## Slow speed time at stop [332]

In this menu slow speed at stop is activated and the time is set for which slow speed is active after a stop. If slow speed at stop is controlled by an external signal via the analogue/digital input, the set time becomes the maximum time for which slow speed is activated after a stop - if the number of edges is set in menu [501] is not detected during the slow speed period.


## DC brake at slow speed [333]

In this menu the DC brake can be activated after slow speed at stop. This may be useful for loads with high interia or if an exact stop position is desired. The DC brake will be active during the time set in this menu.

NOTE: The brake strength used for DC brake after slow speed corresponds to the brake strength used for braking as stop method. The braking strength can be adjusted in menu [324].

| 3 | 3 | 3 | 0 |
| :--- | :--- | :--- | :--- |
|  | Setting   <br>  0 $F$ | DC Brake at slow speed |  |
| Default: | oFF |  |  |
| Range: | oFF, 1-60 s |  |  |
| oFF | DC brake at slow speed disabled. |  |  |
| 1-60 | DC brake duration time at slow speed. |  |  |



Fig. 48 Jog keys
If remore control is chosen (menu [200]=2) and the JOG commands are enabled in menus [334] and [335], the JOG commands can be given via analogue/digital input. The analogue/digital input can be configured either for jog forward or jog reverse (see description of menu [500] on page 77 for more information). Slow speed will be active as long as the signal on the analogue/digital input is active.

If serial communication control is chosen (menu [200]=3) and the JOG commands are enabled in menus [334] and [335], the JOG commands can be given via serial communication. (See separate instruction manual for serial communications options.)

## JOG forward enable [334]

In chis menu the command for JOG in forward direction is enabled. Depending on the control source chosen in menu [200], the JOG forward command may be accepted from the control panel, via remote control or serial communication.

NOTEI The enable functions are for all control sources.


## Slow speed using the JOG commands

Slow speed in forward or reverse direction can be activated using the JOG commands. To use the JOG commands these have to be independently enabled for slow speed in forward or reverse direction in menus [334] and [335]. Depending on the control source chosen in menu [200], the JOG commands are accepted via control panel, remotely via analogue/ digital input or via serial communications.
If the control panel is chosen as control source (menu [200]=1) and the JOG commands are enabled in menus [334] and [335], the JOG keys on the control panel can be used. Slow speed in forward or reverse direction will be active as long as the relevant button is pushed.

## JOG reverse enable [335]

In this menu the command for JOG in reverse direction is enabled. Depending on the control source chosen in menu [200,], the JOG reverse command may be accepted from the control panel, via remote control or serial communication.


### 8.7.5 Additional settings [340]-[342]

In this section the bypass functionality, power factor control and the control of the internal fan are described.

## Bypass [340]

As the MSF 2.0 is designed for continuous running, a bypass contactor is not normally needed. However, where there is high ambient temperature or other special conditions, the use of a bypass contactor can be advantageous. In this case the by-pass contactor can be controlled by one of the relays. By default, relay K 2 is configured to control a bypass contactor (for full voltage functionality, see description of menus [530]-[532] on page 85 for more information).
The use of a bypass contactor can be combined with any start and stop method without any connection changes being necessary. However, to use the motor protection functions, the load monitor and the viewing functions in bypassed state, the current cransformers have to be moved outside the softstarter. For this purpose an optional extension cable is available, see chapter 12. page 107 (Options) for more information. Figures 49-51 below show a connection example.
If a bypass contactor is used, bypass operation musc be enabled in menu [340] for the softstarter to work properly.


## CAUTION: If the current transformers are not moved outside the softstarter, several alarm functions will not work properly.



Fig. 49 Bypass wiring example MSF 310-1400.


Fig. 50 Current transformer position for Bypass on MSF-017 to MSF-250.


Fig. 51 Current transformer position for Bypass on MSF-310 to MSF-I 400 .

## Power Factor Control PFC [341]

During operation, the softstarter continuously monitors the load of the motor. Particularly when idling or when only partially loaded, it is sometimes desirable to improve the power factor. If Power Factor Control (PFC) is selected, the softstarter reduces the motor voltage when the load is lower. Power consumption is reduced and the degree of efficiency improved.


> CAUTION: If Power Factor Control Is used, the EMC Directive will not be complled with. External measures will be necessary to meet the requirements of the EMC Directive.

## Fan continuously on [342]

This menu enables the internal fan to be switched on continuously. the default setting is for the fan only to run when the softstarter heatsink is too warm. The lifetime of the fan is increased by only running it when needed.


### 8.8 Process protection

The MSF 2.0 softstarter is equipped with different functions for process protection:
[400]-[413] Load monitor
[420] External alarm
[430]-[440] Mains protection

### 8.8.1 Load monitor

The MSF 2.0 has a built-in load monitor, which continuously supervises the motor shaft power. This means, the process can easily be protected both from overload and underload conditions. The load monitor functionality includes both alarms and pre-alarms for overload (max power) and underload (min power). While the max. and min power alarms can be configured to affect operation (OFF, Warning, Coast, Stop, Brake), the respective prealarms only give an indication that an over- or underload situation may be close. The pre-alarm status is available on one of the programmable relays K1 to K3 if so configured (see description of the relays, menus [530] to [532] on page 85 for more information)

All load monitor alarms and pre-alarms are configured using a delay time and an alarm margin. The alarm margin is chosen as a percentage of nominal motor load. A max power alarm will occur when the actual power exceeds the normal load plus the max power alarm margin and a min power alarm will occur when the actual load is lower than the normal load minus the min power margin. Normal load is the shaft power needed under normal operation conditions. The default normal load is considered to be $100 \%$ of the nominal motor power. Depending on the dimensioning of the motor with respect to the application, this value may need to be adapted. Normal load can easily be adapted by using the Autoset function in menu [411]. When an Autoset is performed the actual motor shaft power will be measured and stored to the Normal load.

A start delay can be configured to avoid faulty alarms due to initial over- or underload situations at start.
Fig. 52 illustrates the load monitor functionality with an example of a load curve.
If the operation has been interrupted due to a max or min power alarm, a manual reset and a new start signal is needed to continue operation. The reset and the start signal can be given via control panel, remotely or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset via control panel will never start the motor.

NOTEI The load monitor alarms are disabled durling deceleration.

NOTE: When using the load monitor, check that the nominal motor power is set properly in menu [212].


Fig. 52 Load monitor alarm functions

For max and min power alarms the following alarm actions are available:

## Off

The protection method is deactivated.

## Warning

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). However, the motor is not stopped and operation continues. The alarm message will disappear and the relay will be reset when the fault disappears. The alarm may also be reset manually.

## Coast

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The motor voltage is automatically switched off. The motor freewheels until it stops.

## Stop

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

The appropriare alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menus [326] to [327] (braking strength and braking time).
If the operation has been interrupted due to a max or min power alarm, a reset signal and a new start signal are needed to restart the motor. The reset and the start signal can be given via control panel, remorely or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset vla control panel will never start the motor.

## Max power alarm [400]

In this menu max power alarm is enabled and a proper alarm action is selected. The pre-alarm functionality for max power is automatically enabled together with the max power alarm.


## Min power alarm [401]

In this menu min power alarm is enabled and a proper alarm action is selected. The pre-alarm functionality for min power is automatically enabled together with the min power alarm.


## Start delay power alarms [402]

This menu is available if max or min power alarm is enabled in menu [400] or [401]. In this menu the start delay for the power alarms and pre-alarms is selected. A start delay is useful for avoiding faulty alarms due to initial over- or underload situations. The start delay begins when a start of the motor is initiared.


## Max power alarm margin [403]

This menu is available if Max power alarm is enabled in menu [400]. In this menu the max power alarm margin is configured. The margin is selected as percentage of nominal motor power. A max power alarm will occur if che actual motor shaft power exceeds the normal load (menu [412]) plus the chosen max power alarm margin for a longer time period than the max power alarm response delay set in menu [404].


## Max power alarm response delay [404]

This menu is available if max power alarm is enabled in menu [400]. In this menu the response delay for the max power alarm is configured. A max power alarm will occur if the actual motor shaft power exceeds the normal load (menu [412]) plus the max power alarm margin set in menu [403] for a longer time period than the chosen max power alarm response delay.

| 4 | 0 |  |  |
| :--- | :--- | :--- | :--- |
|  |  | 0. | SettingMax power alarm response <br> delay |
| Default: | 0.5 s |  |  |
| Range: | $0.1-90.0 \mathrm{~s}$ |  |  |
| $0.1-90.0$ | Response delay for max power alarm. |  |  |

## Max power pre-alarm margin [405]

This menu is available if max power alarm is enabled in menu [400]. In this menu the max power pre-alarm margin is configured. The margin is selected in percent of nominal motor power. A max power pre-alarm will occur if the actual motor shaft power exceeds the normal load (menu [412]) plus the chosen max power pre-alarm margin for a longer time period than the max power pre-alarm response delay set in menu [406]. The max power pre-alarm status is available on one of the programmable relays $\mathrm{K} 1-\mathrm{K} 3$ if so configured (see description of the relays, menus [530] to [532] for more information).

| 40 |  |  |  |
| :--- | :--- | :--- | :--- |
|  |  | Setting  <br>   |  |

## Max power pre-alarm response delay [406]

This menu is available if max power alarm is enabled in menu [400]. In this menu the response delay for max power pre-alarm is configured. A max power pre-alarm will occur if the actual motor shaft power exceeds the normal load (menu [412]) plus the max power pre-alarm margin set in menu [405] for a longer time period than the chosen max power pre-alarm response delay.


## Min power pre-alarm margin [407]

This menu is available if min power alarm is enabled in menu [401]. In this menu the min power pre-alarm margin is configured. The margin is selected as a percentage of nominal motor power. A min power pre-alarm will occur if the actual motor load is below the nominal load (menu [412]) minus the chosen min power pre-alarm margin for a longer time period than the min power pre-alarm response delay set in menu [408]. The min power pre-alarm status is available on one of the programmable relays $\mathrm{K} 2-\mathrm{K} 3$ if so configured (see description of the relays, menus [530] to [532] for more information.


## Min power pre-alarm response delay [408]

This menu is available if min power alarm is enabled in menu [401]. In this menu the response delay for min power pre-alarm is configured. A min power pre-alarm will occur if the actual motor shaft power is below the normal load (menu [412]) minus the min power pre-alarm margin set in menu [407] for a longer time period than the chosen min power pre-alarm response delay.


## Min power alarm margin [409]

This menu is available if min power alarm is enabled in menu [401]. In this menu the min power alarm margin is configured. The margin is selected as a percentage of nominal motor power. A min power alarm will occur if the actual motor shaft power is below the normal load (menu [412]) minus the chosen min power alarm margin for a longer time period than the min power alarm response delay set in menu [410].

| $4090^{\circ}$ |  |  | Min power alarm margin |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 6 |  |  |
| Default: |  | 16\% |  |  |
| Range: |  | 0-100\% of $\mathrm{P}_{\mathrm{n}}$ |  |  |
| 0.100 |  | Min power alarm margin. |  |  |

## Min power alarm response delay [410]

This menu is available if min power alarm is enabled in menu [401]. In this menu the response delay for min power alarm is configured. A min power alarm will occur if the actual motor shaft power is below the normal load (menu [412]) minus the min power alarm margin set in menu [409] for a longer time period than the chosen min power alarm response delay.


## Autoset [411]

This menu is available if max or min power alarm is enabled in menu [400] or [401]. The Autoset command performs a measurement of the actual motor load and automatically sets the normal load in menu [412].

To perform an Auroset, select YES, and press Enter during normal operation. If Autoset has been executed successfully, " SEt " is shown in the display for two seconds. After that "no" is shown again. An Autoset can also be initiated via the analogue/digital input, see description of menu [500] for more information.

NOTE: Autoset is only allowed during full voltage running.

| 4 | 1 | 1 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  | $n$ | 0 |

## Normal load [412]

This menu is available if Max or Min power alarm is enabled in menu [400] or [401]. Normal load is the shaft power needed under normal operation conditions. By default, Normal load is considered to be $100 \%$ of the nominal motor power. Depending on the dimensioning of the motor with respect to the application, this value may need to be adapted. Normal load can easily be adapted by using the Autoset function in menu [411]. Normal load is set as apercentage of nominal motor power.

NOTE: When using the load monitor, check that the nominal motor power is set properly in menu [212].

| 4 | 1 | 2 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |
|  | 1 | 0 | 0 |
| Netting |  |  |  |
|  |  |  |  |
| Default: | $100 \%$ |  |  |
| Range: | 0-200\% of $P_{n}$ |  |  |
| $0-200$ | Normal load |  |  |

## Output shaft power [413]

This menu is available if max or min power alarm is enabled in menu [400] or [401]. The menu provides a read-out of the actual shaft power. It can be used as input information when the normal load is set manually.


### 8.8.2 External alarm [420]

The MSF 2.0 can generate an alarm according to the status of an external signal. For a detailed description of the external alarm functionality see section 8.9.5, page 89.
The following alternatives are available for external alarm:
Off
External alarm is deactivated.

## Warning

Alarm message F17 is shown in the display and relay K 3 is activated (for default configuration of the relays) if the external alarm input is opened. However, the motor is not stopped and operation continues. The alarm message will disappear and the relay will be reset when the external alarm input is closed again. The alarm may also be reset manually.

## Coast

Alarm message F17 is shown in the display and relay K 3 is activated (for default configuration of the relays) if the external alarm input is opened. The motor voltage is automatically switched off. The motor freewheels until it stops.

## Stop

Alarm message F 17 is shown in the display and relay K 3 is activated (for default configuration of the relays) if the external alarm input is opened. The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

Alarm message F 17 is shown in the display and relay K 3 is activated (for default configuration of the relays) if the external alarm input is opened. The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menus [326] to [327] (braking strength and braking time).

## Spinbrake

The functionality for the spinbrake alternative is the same as described above for the brake alternative. However, if spinbrake is chosen, braking can even be initiated from an inactive state by opening the external alarm input. This means the softstarter can catch a freewheeling motor and brake it down to standstill. The spinbrake alternative is only available for external alarm.

If the operation has been interrupted due to an external alarm, a reset signal and a new start signal are needed to restart the motor. The reset and the start signal can be given via control panel, remotely or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel..

NOTE: A reset via control panel will never start the motor.


### 8.8.3 Mains protection

The MSF 2.0 continuously monitors the mains voltage.
This means the motor can easily be protected from over- and undervoltages as well as from voltage unbalance conditions. A phase reversal alarm is also available.

For mains protection the following alternatives are available:
Off
The protection method is deactivated.

## Warning

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). However, the motor is not stopped and operation continues.

The alarm message will disappear and the relay will be reset when the fault disappears. The alarm may also be reset manually.

## Coast

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The motor voltage is automatically switched off. The motor freewheels until it stops.

## Stop

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays). The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menus [326] to [327] (braking strength and braking time).

An overvoltage, undervoltage or voltage unbalance alarm is automatically reset when a new start signal is given. If the operation has been interrupted due to a phase reversal alarm, a reset signal and a new start signal are needed to restart the motor. The reset and the start signal can be given via control panel, remotely or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset via control panel will never start the motor.

## Voltage unbalance alarm [430]

In this menu voltage unbalance alarm is enabled and a proper action is selected.


## Unbalance voltage level [431]

This menu is available if voltage unbalance alarm is enabled in menu [430]. In this menu the maximurn allowed voltage unbalance level is selected. If the difference between any two line voltages exceeds the chosen level for the response delay time set in menu [432], a voltage unbalance alarm will occur and the action selected in menu [430] will be executed.


## Response delay voltage level unbalance alarm [432]

This menu is available if voltage unbalance alarm is enabled in menu [430]. In this menu the response delay for voltage unbalance alarm is selected. If the difference between any two line voltages exceeds the level set in menu [431] for the chosen response delay time, a voltage unbalance alarm will occur and the action selected in menu [430] will be executed.


## Overvoltage alarm [433]

In this menu overvoltage alarm is enabled and a proper action is selected.


## Overvoltage level [434]

This menu is available if overvoltage alarm is enabled in menu [433]. In this menu the voltage level for an overvoltage alarm is selected. If any line voltage exceeds the chosen level for the response delay time set in menu [435], an overvoltage alarm will occur and the action selected in menu [433] will be execured.


## Response delay overvoltage alarm [435]

This menu is available if overvoltage alarm is enabled in menu [433]. In this menu the response delay for overvoltage alarm is selected. If any line voltage exceeds the level set in menu [434] for the chosen response delay time, an overvoltage alarm will occur and the action selected in menu [433] will be execured.

| $43 \mid 5{ }^{0}$ |  | Setting <br> Response delay overvoltage alarm |
| :---: | :---: | :---: |
|  | 1 |  |
| Default: | 1 s |  |
| Range: | 1-90 |  |
| 1-90 | Respo | e delay for overvoltage alarm. |

Undervoltage alarm [436]
In this menu undervoltage alarm is enabled and a proper action is selected.


## Undervoltage level [437]

This menu is available if undervoltage alarm is enabled in menu [436]. In this menu the voltage level for an undervoltage alarm is selected. If any line voltage is below the chosen level for the response delay time set in menu [438], an undervoltage alarm will occur and the action selected in menu [436] will be executed.

| 4 | 3 | 7 | 0 |
| :--- | :--- | :--- | :--- | :--- |
|  |  | Setting   <br>   8 |  |
| Default: | $85 \%$ |  |  |
| Range: | $75-100 \%$ of $U_{n}$ |  |  |
| $75-100$ | Undervoltage level |  |  |

## Response delay undervoltage alarm [438]

This menu is available if undervoltage alarm is enabled in menu [436]. In this menu the response delay for undervoltage alarm is selected. If any line voltage is below the level set in menu [437] for the chosen response delay time, an undervoltage alarm will occur and the action selected in menu [436] will be executed.


Phase sequence [439]
In this menu the actual phase sequence is shown.
NOTEI The actual phase sequence can only be shown with a motor connected.

| 4390 |  |  |  | Read-out |
| :---: | :---: | :---: | :---: | :---: |
| $L^{-}-_{-}{ }_{-}$ |  |  |  |  |
| Range: |  | L123, L321 |  |  |
| L123 |  | Phase sequence L1, L2, L3 |  |  |
| L321 |  | Phase sequence L3, L2, L1 |  |  |
| L- - |  | Phase sequence can not be detected |  |  |

## Phase reversal alarm [440]

In this menu phase reversal alarm is enabled and a proper action can be chosen. The softstarter will detect the phase sequence prior to each start attempt. If the actual phase sequence does not match the phase sequence stored during activation of phase reversal alarm, the action chosen in this menu will be executed. If alternative 2 (Coast) is chosen, no start will be performed if the wrong phase sequence is detected.
To activate phase reversal alarm, a motor has to be connected and the mains voltage has to be switched on. This means activation of phase reversal alarm can either be done in stopped state with the mains contactor switched on manually or during full voltage running.


NOTEI The actual phase sequence can be viewed in menu [439].

### 8.9 I/O settings

In this section the programmable inputs and outputs are described.
[500]-[513] Input signals
[520]-[534] Output signals
A connection example using most of the available in- and outputs is shown in Fig. 53.
This section includes also detailed descriptions of the following functions:

- Start/stop/reset command functionality
- Start right/left funcrionality
- External alarm functionality
- External control of parameter set


### 8.9.1 Input signals

The MSF 2.0 has one programmable analogue/digital input and four programmable digital inputs for remore control.

## Analogue/digital input [500]

The analogue/digital input can either be programmed for analog or digital functionality. The following alternatives are available when using the input for digital signals:

## Rotation sensor

An external rotation sensor can be used for the braking functions. If the analogue/digital input is configured for rotation sensor functionality in menu [500], braking will be deactivated if the number of edges chosen in menu [501] is detected on the input.

## Slow speed

This alternative is used for slow speed controlled by an external signal (see the description of slow speed and jog functions in section 8.7.4, page 63 for more information). If the number of edges set in menu [501] is detected on the input, slow speed at start or stop will be finished.

## Jog Forward

With this alternative, slow speed in forward direction can be activated via the analogue/digital input. Slow speed will be active as long as the input signal is high. See the description of slow speed and jog funcrions in section 8.7.4, page 63 for more information. Note that "JOG" forward has to be enabled in menu [334] to use this function.

## Jog reverse

With this alternative, slow speed in reverse direction can be activated via the analogue/digital input. Slow speed will be active as long as the input signal is high. See the description of slow speed and jog functions in section 8.7.4, page 63 for more information. Note that "JOG" reverse has to be enabled in menu [335] to use this function.

## Autoset

When the analogue/digital input is configured for Autoset, a rising edge on the input will initiate an Autoset. Note that an Auroset only can be performed during full voltage running. See description of load monitor functionality in section 8.8.1, page 69 for more information

The following alternatives are available when using the input for analogue signals:

Analogue start/stop: 0-10 V/0-20 mA or 2-10 V/4-20 mA:
The analogue/digital input is used for the reference signal which controls analogue start stop. Two signal ranges ( $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ or $2-10 \mathrm{~V} / 4-20 \mathrm{~mA}$ ) can be chosen. Analogue start/stop is activated if alternative 6 or 7 is chosen in menu [500]. See the description of Analogue start/stop on page 79 for more information.



Fig. 53 Connection example when using the digital and analogue inputs and outputs

## Digital input

The analogue/digital input is used as a digital input if one of alternatives $1-5$ in menu [500] is selected. Jumper J1 has to be set for voltage control, which is the default setting.

The input signal is interpreted as 1 (high) when the input voltage exceeds 5 V . When the input voltage is below 5 V the input signal is interpreted as 0 (low). The input signal can be generated using the internal control supply voltage by connecting a switch between terminal 14 (analogue/digital input) and 18 (supply voltage to terminals 14,16 and 17).


## Digital input pulses [501]

This menu is available if the analogue/digital input is programmed for digital input signals for rotation sensor (alternative 1 ) or for slow speed (alternative 2 ) in menu [500]. In this menu the number of edges is chosen to deactivate the braking function or the slow speed function respectively. .

NOTE: All edges, both positive and negative transitions, will be counted.


Fig. 54 Wiring for digital input signal.

## Analogue input

The analogue/digital input is used as an analogue input if one of alternatives 6-7 in menu [500] is selected. In this case, the input can be configured for voltage or current signal using jumper Jl (see Fig. 55). By default jumper Jl is set to voltage signal. According to the chosen alternative in menu [500], the signal will be interpreted as $0-10 \mathrm{~V} /$ $0-20 \mathrm{~mA}$ or $2-10 \mathrm{~V} / 4-20 \mathrm{~mA}$ (see Fig. 56).


Fig. 55 Wiring for analogueldigital input and setting of JI for analogue current or voltage control.


Fig. 56 Analogue input

## Analogue start/stop

Starts and stops can be performed according to a process signal on the analogue/digital input. This means that e.g. the operation of a pump may be controlled according to a flow signal.
Analogue start/stop is available if remote control or serial communication control is chosen in menu [200] (alternatives 2 or 3 ).

NOTE: Analogue start/stop is not avaliable if control panel is chosen as control source in menu [200] (alternatlve 1).

If a start signal is given via remote or serial communication (according to the setting in menu [200]), the softstarter will check the reference signal on the analogue/digital signal. A start will be performed if the level of the reference signal is below the analogue start/stop on-value chosen in menu
[502] for a longer time than the analogue start/stop delay time set in menu [504]. A stop will be performed if the reference signal exceeds the analogue start/stop off-value chosen in menu [503] for a longer time than the analogue start/ stop delay time set in menu [504].

NOTE: If the selected analogue start/stop on-value is blgger than or equal to the off-value, a level above the on-value at the analogue input will cause a start. A value below the off-value will In this case cause a stop.

The start/stop LED on the front of the MSF will be flashing if the softstarter is in standby mode waiting for an analogue start.

Warning: A flashing start/stop LED is Indicating standby mode - e.g. waiting for an analogue start. The motor may be started automatically at a moment's notice

## Analogue start/stop on-value [502]

This menu is available if analogue start/stop is activated in menu [500] (alternative 6 or 7). If the reference signal on the analogue/digital input is below the chosen on-level for a longer time than the analogue start/srop delay time chosen in menu [504], a start will be performed..

NOTE: If the selected analogue start/stop on-value is blgger than or equal to the off-value, a level above the on-value at the analogue/digital input will cause a start.

NOTE: An analogue start will only be performed if the softstarter has been set to standby mode by a valld start signal via remote control or serial communication.

The analogue start/srop on-value is chosen as a percentage of the input signal range. This means, if the analogue/digital input is configured for $0-10 \mathrm{VDC} / 0-20 \mathrm{~mA}$ (alternative 6 in menu [500]), $25 \%$ corresponds to 2.5 V or 5 mA . If the analogue/digital input is configured for $2-10 \mathrm{VDC} / 4-20 \mathrm{~mA}$ (alternative 7 in menu [500]), $25 \%$ corresponds to 4 V or 8 mA .


## Analogue start/stop off-value [503]

This menu is available if analogue start/stop is activated in menu [500] (alternatives 6 or 7). If the refetence signal on the analogue/digital input exceeds the chosen off-level for a longer time than the analogue start/stop delay time chosen in menu [504], a stop will be performed.

NOTE: If the selected analogue start/stop off-value is less than or equal to the on-value, a level below the offvalue at the analogue/digital input will cause a stop.

NOTE: A stop will also be performed If the softstarter receives a stop signal via remote control or serial communication.

The analogue start/stop off-value is chosen as a percentage of the input signal range. This means if the analogue/digital input is configured for $0.10 \mathrm{~V} / 0-20 \mathrm{~mA}$ (alternative 6 in menu [500]), $25 \%$ corresponds to 2.5 V or 5 mA . If the analogue/digital input is configured for $2-10 \mathrm{~V} / 4-20 \mathrm{~mA}$ (alternative 7 in menu [500]), $25 \%$ corresponds to 4 V or 8 mA .


## Analogue start/stop delay time [504]

This menu is available if analogue start/stop is activated in menu [500] (alternatives 6 or 7). In this menu the delay time for starts and stops caused by the analogue reference signal is set.


## Digital inputs

The MSF 2.0 has four programmable digital inputs. The four inputs and their corresponding control supply terminals are shown overleaf in Fig. 57.


Fig. 57 Wiring for digital inputs 1-4.
The four digital inputs are electrically identical. The digital inputs can be used for remote control of start, stop and reset, for choice of parameter set and for external alarm.

## Stop signal

If remote control is chosen in menu [200] (alternative 2), one digital input has to be programmed as stop signal.

NOTE: No starts will be allowed if the input set for stop signal is open or if no input is configured for stop signal.

If the motor is running a stop will be performed according to the stop settings in menus [320] to [325] as soon as the input configured for stop signal is opened. If more than one input is configured for stop signal, opening one of these will lead to a stop. Accordingly no starts will be allowed if any of these inputs is open.

## Start and reset signal

The digital inputs can be configured for several different start signals (start, start R or start L signal). Closing any input, which is configured for start, will start the motor. Moreover, a rising edge on any input configured for start is interpreted as a reset signal.

NOTE: If more than one digital input is configured for any of the start slgnals (start, start R or start L), closing more than one of these inputs at the same time will lead to a stop. However, if several digltal inputs are configured for the same start functionality, e.g. start R, closing any of these inputs will lead to a start.

Naturally the softstarter has no way of controlling the motor's running direction internally. However, if two mains contactors - one for each phase sequence - are used, these can be controlled by the softstarter using the programmable relays. The settings for the programmable relays in menus [530] to [532] correspond to the different start signals, which can be chosen for the digital inputs. In this way different running directions for the motor can be chosen.

## Example

1. If only one running direction is used, digital input 1 can be configured for start signal and digital input 2 for stop signal (default setting). In this case relay K1 may be configured for operation (default setting) and can control the mains relay. When digital inputs 1 and 2 are closed, the mains contactor will be acrivated and the motor will start. When digital inpur 2 is opened the motor will stop. The mains contactor will be deactivated after the scop has been finished.
2. If two running directions are desired, digital input 1 can be configured for start R , digital input 2 for stop and digital input 3 for start L. Relay K1 controls the mains contactor for running in right direction and may be configured for Operation R. Relay K2 controls the mains contactor with the opposite phase sequence for running in left direction and may be configured for Operation L. In this case closing digital inpurs 1 and 2 (stare right command) will lead to activation of the mains contactor for running in right direction and the motor will start in right direction. Opening digital input 2 will lead to a stop; the mains contactor for running right will be deactivated after the stop has been finished. Closing digital inputs 2 and 3 (while digital input 1 is open) will lead to activation of the mains contactor for running in left direction and the motor will start in left direction.
For more information see the description of the start right/ left functionality in section 8.9.4, page 87.

## External alarm

The digital inputs can be configured as external alarm inputs. If an input configured for external alarm is opened, the action chosen in menu [420] for external alarm is performed. See description of the external alarm functionality in section 8.9.5, page 89 for more information.

NOTE: If more than one digital input is configured for external alarm, opening any of these will lead to an external alarm.

## Parameter set

This configuration enables choice of parameter set by an external signal. See description of external control of parameter set in section 8.9.6, page 90 for more information.

## Digital input 1 function [510]

In this menu the function for digital input 1 (terminal 11) is selecred.

| 0 <br> 0 |  | Setting <br> on |
| :---: | :---: | :---: |
|  | $1$ |  |
| Default: | 1 |  |
| Range: | oFF, |  |
| ofF | Digit |  |
| 1 | Start |  |
| 2 | Stop |  |
| 3 | Para |  |
| 4 | Para |  |
| 5 | Exter |  |
| 6 | Start |  |
| 7 | Start |  |

Digital input 2 function [511]
In this menu the function for digital input 2 (terminal 12) is selected.

| 5 | 1 | 1 |
| :--- | :--- | :--- |
|  |  | Setting  <br>   |
| Default: | 2 |  |
| Range: | Off, 1, 2, 3, 4, 5, 6, 7 |  |
| ofF | Digital input 2 2 is disabled. |  |
| 1 | Start signal |  |
| 2 | Stop signal |  |
| 3 | Parameter set, input 1 |  |
| 4 | Parameter set, input 2 |  |
| 5 | Starnal alarm signal |  |
| 6 | Start L signal |  |
| 7 |  |  |

## Digital input 3 function [512]

In this menu the function for digital input 3 (terminal 16) is selected.


## Digital input 4 function [513]

In this menu the function for digital input 4 (terminal 17) is selected.

| 0 <br> 0 |  | Setting |
| :---: | :---: | :---: |
|  | 4 |  |
| Default: | 4 |  |
| Range: | off, |  |
| OFF | Digit |  |
| 1 | Start |  |
| 2 | Stop |  |
| 3 | Para |  |
| 4 | Para |  |
| 5 | Exte |  |
| 6 | Star |  |
| 7 | Star |  |

### 8.9.2 Output signals

The MSF 2.0 has one programmable analogue output and three programmable relays.

## Analogue output

The analogue output can present current, voltage, shaft power and torque for connection to a recording instrument, PLC etc. The external device is connected to terminals 19 $(+)$ and $15(-)$ according to Fig. 58 below. The analogue output can be configured for voltage or current signal. The
selection is made by jumper J 2 on the control board. The default setting for J 2 is voltage signal according to Fig. 58.


Fig. 58 Wiring for analogue output and setting of J2 for analogue current or voltage signal.

## Analogue output [520]

In this menu the analogue output can be set to provide either one of the signal ranges shown in Fig. 59.


Fig. 59 Analogue output


## Analogue output function [521]

This menu is available if the analogue output is enabled in menu [520] (alternatives 1-4). In this menu the desired output function is chosen.


The scaling of the analogue output is reser to the default values ( $0-100 \%$ ) if a new output value is chosen in menu [521].

## Analogue output scaling

By default the scaling of the analogue output corresponds to Fig. 60. In this case the signal range of the analogue output chosen in menu [520] corresponds to 0 to $100 \%$ of the nominal motor current $\mathrm{I}_{n}$, the nominal motor voltage $\mathrm{U}_{\mathrm{n}}$, the nominal motor power $\mathrm{P}_{\mathrm{n}}$ or the nominal motor torque $\mathrm{T}_{\mathrm{n}}$ respectively.

## Example

If $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ is chosen in menu [ 520 ] (alternative 1) and RMS current is chosen as output value in menu [521] (alternative 1), a current of $100 \%$ of the nominal motor current gives 10 V or 20 mA at the analogue outpur. A current of $25 \%$ of the nominal motor current gives 2.5 V or 5 mA at the analogue output.
The scaling of the analogue output may be adapted for higher resolution or if values above the nominal values are to be monitored. The scaling is done by choosing a minimum scaling value in menu [522] and a maximum value in menu [523]. An example for a different scaling is shown in Fig. 60.


Fig. 60 Scaling of analogue output
Wich the scaling for wide range (menu [522]=50 and menu $[523]=500$ ) according to the example in Fig. 60 the following will apply.
If $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ is chosen in menu [ 520 ] (alternative 1) and RMS current is chosen as output value in menu [ 521 ] (alternative 1), a current of $100 \%$ of the nominal motor current gives approximately 1.1 V or 2.2 mA at the analogue output.

## Scaling analogue output, min [522]

This menu is available if the analogue output is enabled in menu [520]. In this menu the minimum value to be shown at the analogue output is chosen. The value is chosen in percent of $I_{n}, U_{n}, P_{n}$ or $T_{n}$ according to the output value chosen in menu [521].


NOTE: The minimum value for scaling the analogue output is reset to the default value $0 \%$ If a new output value is chosen in menu [521].

## Scaling analogue output, max [523]

This menu is available if the analogue output is enabled in menu [520]. In this menu the maximum value to be shown at the analogue output is chosen. The value is chosen as a percentage of $\mathrm{I}_{\mathrm{n}}, \mathrm{U}_{\mathrm{n}}, \mathrm{P}_{\mathrm{n}}$ or $\mathrm{T}_{\mathrm{n}}$ according to the output value chosen in menu [521].


NOTE: The maximum value for scaling the analogue output is reset to the default value $100 \%$ if a new output value is chosen in menu [521].

## Programmable relay outputs

The softstarter has three built-in relays, K1, K2 and K3. All three relays are programmable.
For relay K1 (terminals 21 and 22) and K2 (terminals 23 and 24) the contact function can be programmed in menus [533] and [534] respectively to be normally open (NO) or normally closed (NC). Relay K3 is a change-over relay with three terminals (31-33), the NO functionality is available between terminals 31 and 32 , NC functionality between terminals 32 and 33 .
The relays can be used to control mains contactors or a bypass contactor or to indicate alarm conditions. As illustrated in Fig. 61 overleaf, the Operation setting (alternative 1) should be chosen to activate the mains contactor both during start, full voltage operation and stop. If a by-pass contactor is used, this can be controlled by a relay with the setting Full voltage (2). The settings Run (5) and Brake (4) are used when reverse current brake is chosen as stop method. In this case one relay has to be configured for Run and will control the mains contactor during the start and during full voltage operation. Another relay has to be configured for Brake and will control the contactor with reversed phase sequence during braking. For security reasons the relay configured for Brake will nor be activated until after a time delay of 500 ms after deactivation of the relay configured for Run.

The settings Run R, Run L, Operation R and Operation L are used for the start right/left functionality. Consult section 8.9.4, page 87 for more information.

Different alarms can also be indicated on the relay outputs. With the setting Power pre-alarms (alrernative 3), both a Max power pre-alarm or a Min power pre-alarm occurring will activate the relay. When Power alarms (10) is chosen as a setting, both a Max power alarm or a Min power alarm will activate the relay. If so desired, the relays can instead be pro-
grammed to react only to one specific power alarm or prealarm (11-14).
With setting All alarms (15) the relay will be activated for any alarm. As the power pre-alarms are not considered to be real alarms, the relay will not react to those. With alternative 16 chosen, even the power alarms are excluded. When External alarm (17) is chosen, only an External alarm will activate the relay. With setting 18 , Autoreser expired, the relay will be activated when an additional fault occurs after the maximum allowed number of autoreset attempts have been executed. This may indicate that external help is needed to rectify a re-occurring fault (see description of Autoreset in section 8.5, page 52 for detailed information). With alternative 19 the relay will indicate all alarms which need a manual reset. This includes all alarms which are not solved with an automatic Autoreset, e.g. all alarms for which Autoreset is not enabled and each alarm occurring after the maximum allowed number of autoreset attempts has been executed.


Fig. 61 The relay functions for operation, run and full voltage.

Relay K1 [530]
In this menu the function for relay K1 (terminals 21 and 22) is chosen.

| $\begin{array}{l\|l\|l\|} \hline 5 & 0 \\ 0 \end{array}$ |  |
| :---: | :---: |
| Relay K1 |  |
| Default: | 1 |
| Range: | oFF, 1-19 |
| oFF | Relay inactive |
| 1 | Operation |
| 2 | Full voltage |
| 3 | Power pre-alarms |
| 4 | Brake |
| 5 | Run |
| 6 | Run R |
| 7 | Run L |
| 8 | Operation R |
| 9 | Operation L |
| 10 | Power alarms |
| 11 | Max power alarm |
| 12 | Max power pre-alarm |
| 13 | Min power alarm |
| 14 | Min power pre-alarm |
| 15 | All alarms (except power pre-alarms) |
| 16 | All alarms (except power alarms and prealarms) |
| 17 | External alarm |
| 18 | Autoreset expired |
| 19 | All alarms which need manual reset |

NOTE: If relay K1 is chosen to be inactive (oFF), the relay state is determined by the contact function in menu [533].


WARNING: When reverse current brake is activated by changing the settings in menu [320] (stop method), [323] (brakIng method) or [326] (alarm brake strength), relay K1 is automatically set for Run (5). If a different setting is desired for the specific application, the relay setting has to be changed afterwards.

Relay K2 [531]
In this menu the function for relay K2 (terminals 23 and 24) is chosen.


NOTE: If relay $K 2$ Is chosen to be inactive ( $O F F$ ), the relay state is determined by the contact function in menu [534].


WARNING: When reverse current brake is activated by changing the settings in menu [320] (stop method), [323] (braking method) or [326] (alarm brake strength), relay $K 2$ is automatically set for Brake (4). If a different setting is desired for the specific application, the relay setting has to be changed afterwards.

Relay K3 [532]
In this menu the function for relay K 3 (terminals 31-33) is chosen.

| 5 3 2 | Setting |  | 1 |
| :--- | :--- | :--- | :--- |

## K1 contact function [533]

In this menu the contact function for relay K 1 can be chosen. The available alternatives are Normally open ( $1=$ Closing on relay activation) and Normally closed ( $2=$ Opening on relay activation).

| 5 | 3 |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

## K2 contact function [534]

In this menu the contact function for relay K2 can be chosen. The available alternatives are Normally open ( $1=$ Closing on relay activation) and Normally closed ( $2=$ Opening on relay activation).

| 5 3 4 <br> 0   |  | Setting |
| :---: | :---: | :---: |
| K2 contact function |  |  |
| Default: | 1 |  |
| Range: | 1, 2 |  |
| 1 | Norm |  |
| 2 | Norm |  |

### 8.9.3 Start/stop/reset command functionality

Starting/stopping of the motor and alarm reset is done either from the control panel, through the remote control inputs or through the serial communication interface depending on the control source chosen in menu [200].

## Control panel

To start and stop from the control panel, the "START/ STOP" key is used.

To reset from the control panel, the "ENTER $\leftarrow$ /RESET" key is used.

Regardless of the chosen control source, it is always possible to initiate a reset via the control panel.

NOTEI A reset via the control panel will never start the motor.

## Serial communication

For description of the start, stop and reset commands via serial communication see the operation instruction supplied with this option.

## Remote control

When remote control is chosen in menu [200], the digital inputs are used to start and stop the motor and to reset upcoming alarms. In the following sections different possibilities for connecting the digital inputs are described. For the following explanations the following settings are assumed:

| Menu | Description | Setting |
| :--- | :--- | :--- |
| 510 | Digital input 1 (terminal 11) | Start signal (1) |
| 511 | Digital input 2 (terminal 12) | Stop signal (2) |

## 2-wire start/stop with automatic reset at start



Fig. 62 2-wire connection of terminals for start/stoplautomatic reset at start

An external switch is connected between terminals 12 and 13 and a jumper is connected between terminals 11 and 12 .

## Start

Closing terminal 12 to terminal 13 will give a start command. If terminal 12 is closed to terminal 13 at power up, a start command is given immediately (automatic start at power up).

Stop
Opening terminal 12 will give a stop command.
Reset
When a start command is given there will automatically be a reset.

## 2-wire start/stop with separate reset



Fig. 63 2-wire connection of terminals for start/stop/separate reset

One external switch is connected between terminals 11 and 13 and a second switch is connected berween terminals 12 and 13.

## Start

Closing terminals 11 and 12 to terminal 13 will give a start command. If terminals 11 and 12 are closed at power up, a start command is given immediately (automatic start at power up).

Stop
Opening terminal 12 will give a stop command.

## Reset

When terminal 11 is opened and closed again a reset is given. A reset can be given both when the motor is running and when it is stopped.

## 3-wire start/stop with automatic reset at start

 and 13 .

Fig. 64 Connection of terminals for start/stop/reset
An external switch is connected between terminals 11 and 13 and a second switch is connected between terminals 12

The connection between terminal 11 and 13 is normally open and the connection between terminal 12 and 13 is normally closed.

## Start

Closing terminal 11 momentarily to terminal 13 , will give a start command. There will not be an automatic start at power up as long as terminal 11 is open.

## Stop

To stop, cerminal 12 is momentarily opened.

## Reset

When a start command is given there will automatically be a reser.

### 8.9.4 Start right/left functionality

The digital inpurs can be configured to enable starting a motor in two different directions in combination with the programmable relays K 1 and K 2 . A connection example is shown in Fig. 65. For the following description of the start right/left functionality, the following settings for the digital inputs are assumed.

| Menu | Description | Setting |
| :--- | :--- | :--- |
| 510 | Digital input 1 (terminal 11) | Start R signal (6) |
| 511 | Digital input 2 (terminal 12) | Stop signal (2) |
| 512 | Digital input 3 (terminal 16) | Start L signal (7) |



Fig. 65 Connection for start rightleft

The configuration of the relays depends on the application's requirements. For applicarions which do not use the reverse current brake functionalicy, the following sertings may be used.

| Menu | Description | Setting |
| :--- | :---: | :---: |
| 530 | Relay K1 (terminals 21 and 22) | Operation R (8) |
| 531 | Relay K2 (terminals 23 and 24) | Operation L (9) |

With these setrings the funcrionality is as follows:
If terminals 1 land 12 are closed to terminal 13 while terminal. 16 is open, the mains contactor for running in right direction will be activared by relay K1 and the motor will start in right direction. If eerminal 12 is opened, a stop according to the stop settings in menus [320] to [325] will be performed. When the stop is finished, the mains contactor for running right will be deacrivated by relay K 1 .
If terminal 12 is closed to terminal 13 and terminal 16 is closed to terminal 18 while terminal 11 is open, the mains contactor for running in left direction will be activated by relay K 2 and the motor will start in left direction. If terminal 12 is opened, a stop according to the stop settings in menus [320] to [325] will be performed. When the stop is finished, the mains contactor for running left will be deactivated by relay K 2 .

If both start terminals (11 and 16) are closed to their respective supply voltage at the same time, a stop is performed in the same way as described above. In this case no start will be allowed.
A motor can be reversed from right to left direction as follows: When the motor is running in right direction, terminal 11 is opened. Terminal 16 is then closed to terminal 18. In this case the voltage to the moror is switched off and the mains contactor for running right is deactivated by relay K1. After a time delay of 500 ms the mains contactor for running left will be activated by relay K 2 and a start in left direction will be performed. The motor can be reversed from running left to running right in the same way by opening terminal 16 while running left and then closing terminal 11.


CAUTION: Very high currents can arise when the motor is reversed from running at full speed in one direction to running at full speed in the opposite direction.


WARNING: If configured according to the description above, relays K1 and K2 will never be activated at the same time. There is a time delay of 500 ms for the change-over between the relays. However, if the relays are not conflgured properly, they may be activated at the same time.

For applications which use the reverse current brake functionality, the following settings for the relays may be used.

| Menu | Descriptlon | Setting |
| :--- | :--- | :--- |
| 530 | Relay K1 (terminals 21 and 22) | Run R (6) |
| 531 | Relay K2 (terminals 23 and 24) | Run L (7) |

With these settings the functionality is as follows:
If terminals 1 land 12 are closed to terminal 13 while terminal 16 is open, the mains contactor for running in right direction will be activated by relay K 1 and the motor will start in right direction. If terminal 12 is opened the voltage to the motor is switched off and the mains contactor for running right is deactivated by relay KI. After a time delay of 500 ms the mains contactor for running left will be activated by relay K 2 and the reverse current brake will brake the motor to standstill. When the stop is finished, the mains contactor for running left will be deactivared by relay K 2 .

If terminal 12 is closed to terminal 13 and terminal 16 is closed to terminal 18 while terminal 11 is open, the mains contactor for running in left direction will be activated by relay K 2 and the motor will start in left direction. If terminal 12 is opened the voltage to the motor is switched off and the mains contactor for running left is deactivated by relay K 2 . After a time delay of 500 ms the mains contactor for running right will be activated by relay KI and the reverse current brake will brake the motor to standstill. When the stop is finished, the mains contactor for running right will be deactivared by relay K1.

If both start terminals (11 and 16) are closed to their respective supply voltage at the same time, a stop is performed in the same way as described above. In this case no start will be allowed.

A motor can be reversed in the same way as described above for applications which do not use the reverse current brake functionality.

WARNING: If configured according to the description above, relays K1 and K2 wIII never be activated at the same time. There is a time delay of 500 ms for the change-over between the relays. However, if the relays are not configured properly, they may be activated at the same tlme.

NOTE: When reverse current brake is actlvated by changing the settings in menu [320] (stop method), [323] (braking method) or [326] (alarm brake strength), relay K 1 is automatically set for Run (5) and relay K 2 is automatically set for Brake (4). To use the start right/ left functionality in combination with reverse brake, the relay settings have to be adapted as described above once reverse current brake has been enabled.

### 8.9.5 External alarm functionality

The external alarm functionality is used to generate an alarm depending on the state of an external alarm signal. Each of the digital inputs can be configured for external alarm signal. Fig. 66 shows a connection example with digital input 3 (terminal 16) configured for external alarm signal.


Fig. 66 Connection of terminals for external alarm

If any digital input is configured for external alarm signal, opening this input will cause an external alarm to occur if external alarm is enabled in menu [420].

NOTE: If more than one digital input is conflgured for external alarm signal, opening any of these inputs will generate an external alarm if external alarm is enabled in menu [420].

The following alarm actions are available for external alarm:

## Off

External alarm is disabled.

## Warning

An F17 alarm message is shown in the display and relay K3 is activated (for default configuration of the relays) if the external alarm input is opened. However, the motor is not stopped and operation continues. The alarm message will disappear and the relay will be reser when the external alarm input is closed again. The alarm may also be reset manually.

## Coast

An F17 alarm message is shown in the display and relay K3 is activated (for default configuration of the relays) if the external alarm input is opened. The motor voltage is automatically switched off. The motor freewheels until it stops.

## Stop

The appropriate alarm message is shown in the display and relay K 3 is activated (for default configuration of the relays) if the external alarm input is opened. The motor is stopped according to the stop settings in menus [320] to [325].

## Brake

The appropriate alarm message is shown in the display and relay K 3 is activared (for default configuration of the relays) if the external alarm inpur is opened. The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menu [326] - [327] (Braking strength and braking time).

## Spinbrake

The functionality for the spinbrake alternative is che same as described above for the brake alternative. However, if spinbrake is chosen, braking can even be initiated from an inactive state by opening the external alarm input. This means the softstarter can catch a freewheeling motor and brake it down to standstill. The Spinbrake alternative is only available for external alarm.
External alarm can be used together with any setting for the control source chosen in menu [200].

If the operation has been interrupted due to an external alarm, a reset signal and a new start signal are needed to restart the motor. The reset and the start signal can be given via control panel, remote or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control source, it is always possible to initiate a reset via control panel.

NOTE: A reset via control panel will never start the motor.

### 8.9.6 External control of parameter set

The parameter set can be chosen via the digital inputs if external control of paramerer set is chosen in menu [240] (alternative 0 ). For this purpose any of the digital inputs can be configured for parameter set input 1 (PS1, alternative 3 in menus [510] to [513]) or parameter set input 2 (PS2, alternative 4 in menus [510] to [513]). Fig. 67 shows a connection example for external control of paramerer ser, in this example digital inpurs 3 and 4 are configured for PS1 and PS2.


Fig. 67 Connection of external control inputs.
Table 15 How parameter set inputs are evaluated

| Parameter Set | PS1 (16-18) | PS2 (17-18) |
| :--- | :--- | :--- |
| 1 | Open | Open |
| 2 | Closed | Open |
| 3 | Open | Closed |
| 4 | Closed | Closed |

It is possible to use just one digital input to change between two parameter sets. According to the example above, digital input 3 is configured for PS1. If no digital input is configured for PS2, PS2 is considered to be open. In this case digital input 3 can be used to change between parameter set 1 and 2.
Changing the parameter set via external signal is only execured in stopped mode and at full voltage operation. If the input signals for PS1 and PS2 are changed during acceleration or deceleration, only the new parameters for the control source (menu [200]), the analogue/digital input (menu [500]), the digital input pulses (menu [501]), the analogue start/stop on- and off-value (menus [502] and [503]) and the analogue start/stop delay (menu [504]) are loaded immediately. All other parameters will not change until the softstarter is in stopped mode or at full voltage running. In this way a change of the control source will take effect immediately, which can be useful for changing from remote to manual operation for maintenance.

NOTE: No parameters, except for the control source in menu [200] and the parameter set in menu [240], may be changed if external control of parameter set is activated In menu [240] (alternative 0).

### 8.10 View operation

MSF 2.0 includes numerous viewing functions which eliminate the need for additional transducers and meters for monitoring the operation.
[700] to [716] Operation (current, voltage, power etc.)
[720] to [725] Status (softstart status, input/output status) [730] to [732] Stored values (operation time etc.)

### 8.10.1 Operation

RMS current


NOTEI This is the same read-out as menu [100].

## Line main voltage



Power factor


## Output shaftpower

The output shaft power is shown in kW or in HP depending on the setting for Enable US units in menu [202].

| $70 \mid 3$ | Read-out |  |
| :--- | :--- | :--- |
|  |  |  |
|  |  | 0.0 |
|  |  |  |

Output shaftpower in percentage unit


NOTE: This is the same read-out as menu [413].

## Shaft torque

The shaft torque is shown in Nm or in lbft depending on the setting for Enable US units in menu [202].


Shaft torque in percentage unit


## Softstarter temperature

The softstart temperature is shown in degrees Celsius or in degrees Fahrenheit depending on the setting for Enable US units in menu [202].


Current phase I1


Current phase L2


## Current phase L3



Line main voltage L1-L2

| 7 | 1 | 1 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

Line main voltage L1-L3


Line main voltage L2-L3


Phase sequence


Used thermal capacity


Time to next allowed start


### 8.10.2 Status

## Softstarter status



## Digital Input Status

Status of the digital inputs $1-4$ from left to right. L or H are displayed for input status low (open) or high (closed).


## Analogue/digital Input status

Status of the analogue/digital input when it is used as digital input. L and H are displayed for input status low (open) and high (closed).


## Analogue/digital input value

Value on the analogue/digital input as a percentage of the input range. This read-out depends on the configuration of the analogue/digital input in menu [500], e.g. if the analogue/digital input is configured for analogue start/stop $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ (alternative 6), an input signal of 4 V or 8 mA will be shown as $40 \%$. However, if the analogue/digital inpur is configured for analogue start/stop $2.10 \mathrm{~V} / 4-20$ mA (alternative 7), an input signal of 4 V or 8 mA will be shown as $25 \%$.


## Relay status

Status of the relays K1 to K3 from the left to the right. L or H are displayed for relay status low (opened) or high (closed). The status described for relay K3 corresponds to the status of terminal 3.


## Analogue Output value

Value on the analogue output as a percentage of the output range. This read-out depends on the configuration of the analogue output in menu (520], e.g. if the analogue/digital input is configured for $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ (alternative 1) or for $10-0 \mathrm{~V} / 20-0 \mathrm{~mA}$ (alternative 3), an output signal of 4 V or 8 mA will be shown as $40 \%$. However, if the analogue output is configured for $2-10 \mathrm{~V} / 4-20 \mathrm{~mA}$ (alternative 2 ) or $10-2 \mathrm{~V} / 20-4 \mathrm{~mA}$ (alternative 4), an output signal of 4 V or 8 mA will be shown as $25 \%$.


### 8.10.3 Stored values

Operation time. The operation time is the time during which the motor connected to the sofrstarter is running, not the time during which the supply power is on.
If the actual value for the operation time exceeds 9999 hours the display will alternate between the four lower digits and the higher digits.

## Example

If the actual operation time is 12467 , 1 will be shown for 1 s , then 2467 will be shown for 5 s and so on.


## Energy consumption



## Reset energy consumption

In this menu the stored power consumption (menu [713]) can be reset to 0 .


### 8.11 Alarm list

The alarm list is generated automatically. It shows the latest 15 alarms (F1-F17). The alarm list can be useful for tracking failures in the softstarter or its control circuit. In the alarm list both the alarm message and the operation time is saved for each alarms that occurs. In menu [800] the latest alarm message and the corresponding operation time are shown alternately, in the same way, older alarms are shown in menus [801] to [814].

## Example

- If the latest alarm was a phase input failure ( F 1 ), which occurred at operation time 524 . F1 is shown for 4 s then 524 is shown for $2 s$ and so on.
- If the latest alarm was a thermal motor protection alarm (F2), which occurred at operation time 17852. F2 is shown for 3 s , after that 1 is shown for 1 s , then 7852 is shown for 2 s and so on.

Alarm list, latest error


Alarm list, error


| Menu | Function |
| :--- | :--- |
| 802 | Alarm list, error 13 |
| 803 | Alarm list, error 12 |
| 804 | Alarm list, error 11 |
| 805 | Alarm list, error 10 |
| 806 | Alarm list, error 9 |
| 807 | Alarm list, error 8 |
| 808 | Alarm list, error 7 |
| 809 | Alarm list, error 6 |
| 810 | Alarm list, error 5 |
| 811 | Alarm list, error 4 |
| 812 | Alarm list, error 2 |
| 813 | Alarm list, error 1 |
| 814 |  |

### 8.12 Softstarter data

In menus [900] to [902] the softstarter type is shown and the softstarter's software version is specified.

## Softstarter type



## Software variant

| 9 0101 |  |  |  | Sead-out |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Range: |  |  | Sam | label |  |

Software version


## 9. Protection and alarm

MSF 2.0 is equipped with functions for motor protection, process protection and protection of the softstarter itself.

### 9.1 Alarm codes

Different alarm codes are used for the different errors, see Table 16 for a description of the alarni codes used. When an alarm occurs, this is indicated with the appropriate alarm message flashing in the display. If more than one alarm is active at the same time, the alarm code for the last alarm is presented on the display. The alarm code for each occurring alarm is also saved in the alarm list in menus [800] to [814].

### 9.2 Alarm actions

For most protection methods a proper action can be chosen to be performed if the relevant alarm occurs. The following alternatives are available as alarm actions (all alternatives may not be available for all protection methods - check Table 16):

## Off

The alarm is deactivated.

## Warning

The appropriate alarm code is flashing in the display and relay K 3 is activated (for default configuration of the relays) if an the alarm occurs. However, the motor is not stopped ans operation continues. The alarm message in the display will disappear and the relay will be reset when the alarm has disappeared. The alarm may also be reset manually. This setting alternative may be useful if it is desired to control operation in alarm state by an external control unit.

## Coast

The appropriate alarm code is flashing in the display and relay K3 is activated (for default configuration of the relays) if an the alarm occurs. The motor voltage is automatically switched off. The motor is freewheels until it stops.
This setting alternative is useful if continuous running or active stopping could harm the process or the motor. This may be appplicable for applications with very high inertia that use braking as the normal stop method. In this case it may be a good idea to choose Coast as alarm action on thermal motor protection alarm, because continuous running or braking could harm the motor seriously when this alarm has occurred.

## Stop

The appropriate alarm code is flashing in the display and relay K 3 is activated (for default configuration of the relays) if an alarm occurs. The motor is stopped according to the stop settings in menus [320] to [325].
This setting is useful for applications where a correct stop is important. This may apply to most pump applications, as Coast as an alarm action could cause water hammer.

## Brake

The appropriate alarm code is flashing in the display and relay K3 is activated (for default configuration of the relays) if an alarm occurs. The brake function is activated according to the braking method chosen in menu [323] and the motor is stopped according to the alarm brake settings in menus [326] to [327] (braking strength and braking time). If alarm braking is deactivated in menu [326] and Brake is chosen as an alarm action, the action will be the same as described above for Coast.
Brake as an alarm action may mainly be used in combination with External alarm, where an external signal is used to initiate a quick stop with a higher braking strength and a shorter braking time compared to normal operation.

## Spinbrake

The functionality for the Spinbrake alcernative is the same as described above for the Brake alternative. However, if Spinbrake is chosen, braking can even be initiated from an inactive state. This means the softstarter can catch a freewheeling motor and brake it down to standstill.
The Spinbrake alternative is only available for External alarm. It may be useful e.g. for test running of planers and bandsaws after tool exchange. It may be desirable to accelerate the tool up to a specific speed and then leave it coasting to check if there is any unbalance. In this case it is possible to activate braking immediately by opening the external input.
In Table 16 below the alarm actions available for each alarm rype are specified in detail.

### 9.3 Reset

For the following explanations it is important to distinguish between Reset and Restart. Reset means that the alarm message on the display disappears and the alarm relay K3 (for default configuration of the relays) is deactivated. If the operation has been interrupted due to an alarm the softstarter is prepared for a Restart. However, giving a Reset signal without giving a new start signal will never lead to a start.
The Reset signal can be given via control panel, remotely or via serial communication depending on the control source chosen in menu [200]. Regardless of the chosen control method, it is always possible to give a Reset signal via control panel.
If an alarm occurs whose alarm action is configured for Warning (see description of alarm actions above), the alarm will automatically be reset as soon as the failure disappears. The alarm may also be reset manually by giving a Reset signal as described above.

If operation has been interrupted due to an alarm, a Reser signal and a new start signal may be needed to Restart the motor. However, some alarms are automatically reset when a new start signal is given. Table 16 covers all alarm types and
whether they need a Reset signal (manual reset) or if they are reset automatically when a new start signal is given.
An alarm can always be reset by giving a Reset signal, even if the failure that caused the alarm has not disappeared yet. Giving a Reset will cause the alarm message on the display to disappear and the alarm relay K 3 to be deactivated (for default configuration of the relays). However, if operation has been interrupted due to an alarm, a Restart will not be
possible until the failure has disappeared. If a new start signal is given while the failure still is active, the alarm message will appear flashing in the display and the alarm relay K3 will be activated again (for default configuration of the relays).

MSF 2.0 is also provided with an Autoreset function. This functionality is described in detail in section 8.5 , page 52 .

### 9.4 Alarm overview

Table 16 Alarm overview

| Alarm <br> code | Alarm descriptlon | Alarm action | Protection system | Reset |
| :--- | :--- | :--- | :--- | :--- |
| F1 | Phase input failure. | Warning <br> Coast | Motor protection <br> (menu [230]) | Automatic Reset when new start signal is <br> given. |
| F2 | Thermal motor protec- <br> tion <br> F4 | Warning <br> Coast <br> Stop <br> Brake | Motor protection <br> (menu [220]) | Separate Reset signal needed. |

Table 16 Alarm overview

| Alarm <br> code | Alarm description | Alarm action | Protection system | Reset |
| :--- | :--- | :--- | :--- | :--- |
| F11 | Start limitation. | Off <br> Warning <br> Coast | Motor protection <br> (menu [224]) | Automatic Reset when new start signal is <br> given. |
| F12 | Shorted thyristor. | Coast |  | Separate Reset signal needed. |
| F13 | Open thyristor. | Coast |  | Separate Reset signal needed. |
| F14 | Motor terminal open. | Coast |  | Separate Reset signal needed. |
| F15 | Serial communication <br> contact broken. | Off <br> Warning <br> Coast <br> Stop <br> Brake | Control source pro- <br> tection (menu <br> [273]) | Automatic Reset when new start signal is <br> given. |
| F16 | Phase reversal alarm. | Off <br> Warning <br> Coast | Process protection <br> (menu [440]) | Separate Reset signal needed. |
| F17 | External alarm. | Off <br> Warning <br> Coast <br> Stop <br> Brake <br> Spinbrake | Process protection |  |
| (menu [420]) | Separate Reset signal needed. |  |  |  |

## 10. Troubleshooting

### 10.1 Fault, cause and solution

| Observation | Fault Indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The display is not illuminated. | None | No control supply voltage. | Switch on the control supply voltage. |
| The motor does not run. | F1 (Phase input failure) | Fuse defective. | Renew the fuse. |
|  |  | No mains supply. | Switch on the mains supply. |
|  | F2 <br> (Thermal motor protection) | PTC connection could be open. Incorrect nominal motor current could be entered in menu [211]. | Check the PTC input if PTC protection is used. <br> If internal thermal motor protection is used, perhaps an other internal thermal protection class could be used (menu [222]). <br> Cool down the motor and restart. |
|  | F3 (Softstarter overheated) | Ambient temperature too high. Softstarter duty cycle exceeded. Could be fan failure. | Check ventilation of cabinet. Check the size of the cabinet. Clean the cooling fins. If the fan(s) is (are) not working correctly, contact your local MSF sales outlet. |
|  | F4 (Current limit start time expired) | Current limit parameters are perhaps not matched to the load and motor. | Increase the start time (menu [315]) and/or the current limit at start (menu [314]). |
|  | F5 (Locked rotor) | Something stuck in the machine or perhaps motor bearing failure. | Check the machine and motor bearings. Perhaps the Locked rotor time can be set longer (menu [229]). |
|  | F6 <br> (Max power alarm) | Overload | Check the machine. Perhaps the Max power alarm response delay can be set longer menu [404]. |
|  | $\begin{aligned} & \text { F7 } \\ & \text { (Mn power alarm) } \end{aligned}$ | Underload | Check the machine. Perhaps the Min power alarm response delay can be set longer menu [410]. |
|  | F8 (Voltage unbalance) | Mains supply voltage unbalance. | Check mains supply. |
|  | F9 (Overvoltage) | Mains supply overvoltage. | Check mains supply. |
|  | $\begin{array}{\|l} \text { F10 } \\ \text { (Undervoltage) } \end{array}$ | Mains supply undervoltage. | Check mains supply. |
|  | F11 <br> (Start limitation) | Number of starts per hour exceeded, min time between starts not kept. | Wait and start again. Perhaps the number of starts per hour could be increased in menu [225] or the min time between starts could be decreased (menu [226]). |
|  | F13 <br> (Open thyristor) | Perhaps a damaged thyristor. | Initiate a reset and a restart. If the same alarm appears immediately, contact your local MSF sales outlet |
|  | F14 <br> (Motor terminal open) | Open motor contact, cable or motor winding. | If the fault is not found, reset the alarm and inspect the alarm list. If alarm F12 is found, a thyristor is probably shorted. <br> Initiate a restart. If alarm F14 appears immediately, contact your local MSF sales outlet. |


| Observation | Fault Indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The motor does not run. | F15 <br> (Serial communication contact broken) | Serial communication contact broken. | Initiate a reset and try to establish contact. Check contacts, cables and option board. <br> Verify <br> - Serial communication unit address [270]. <br> - Baudrate menu [271]. <br> - Parity menu [272]. <br> If the fault is not found, run the motor from the control panel if urgent set menu [200] to 1 . See also manual for serial communication. |
|  | F16 <br> (Phase reversal) | Incorrect phase sequence on main supply. | Switch L2 and L3 input phases. |
|  | F17 (External alarm) | External alarm signal input open | Check the digital input configured for External alarm. Check the configuration of the digital inputs (menus [510] to [513]). |
|  | -.-- | Start command comes perhaps from incorrect control source. (I.e. start from control panel when remote control is selected). | Give start command from correct control source menu [200]. |
| The motor is running but an alarm is given. | F1 <br> (Phase input failure) | Failure in one phase. Perhaps fuse is defective. | Check fuses and mains supply. Select a different alarm action for Single phase input failure in menu [230] if stop is desired at single phase loss. |
|  | F4 <br> (Current limit start time expired) | Current limit parameters are perhaps not matched to the load and motor. | Increase the start time (menu [315]) and/or the current limit at start (menu [314]). Select a different action for Current limit start time expired alarm in menu [231], if stop is desired at current limit time-out. |
|  | F12 <br> (Shorted thyristor) | Perhaps a damaged thyristor. | When stop command is given, a freewheel stop is made. Initiate a reset and a restart. If alarm F14 appears immediately, contact your local MSF sales outlet. If the motor must be started urgently, the softstarter can start the motor direct on-line (DOL). Set the start method to DOL in this case (menu $[310]=4$ ). |
|  |  | Bypass contactor is used but menu [340] 'Bypass' is not set to "on". | Set menu [340] Bypass to on. |
|  | F15 <br> (Serial communication contact broken) | Serial communication contact broken. | Initiate a reset and try to establish contact. Check contacts, cables and option board. <br> Verify <br> - Serial communication unit address [270]. <br> - Baudrate menu [271]. <br> - Parity menu [272]. <br> If the fault is not found, run the motor from the control panel if urgent, see also manual for serial communication. |


| Observation | Fault Indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The motor jerks etc. | When starting, motor reaches full speed but it jerks or vibrates. | If "Torque control" or "Pump control" is selected, it is necessary to input motor data into the system. | Input nominal motor data in menus [210]-[215]. Select the proper torque control alternative in menu [310] (linear or square) according to the load characteristic. <br> Select a correct initial- and end torque at start in menus [311] and [312]. If 'Bypass' is selected, check that the current transformers are correctly connected. |
|  |  | Start time too short. | Increase start time [315]. |
|  |  | If voltage control is used as start method, the initial voltage at start may be too low. Starting voltage incorrectly set. | Adjust initial voltage at start [311]. |
|  |  | Motor too small in relation to rated current of softstarter. | Use a smaller model of the softstarter. |
|  |  | Motor too large in relation to load of softstarter. | Use larger model of softstarter. |
|  |  | Starting voltage not set correctly. | Readjust the start ramp. |
|  |  |  | Select the current limit function. |
|  | Starting or stopping time too long. | Ramp times not set correctly. | Readjust the start and/or stop ramp time. |
|  |  | Motor too large or too small in relation to load. | Change to another motor size. |
| The monitor function does not work. | No alarm or pre-alarm | It is necessary to input nominal motor data for this function. Incorrect alarm margins or normal load. | Input nominal motor data in menus [210]-[215]. Adjust alarm margins and normal load in menus [402] [412]. Use Autoset [411] if needed. If a Bypass contactor is used, check that the current transformers are correctly connected. |
| Unexplainable alarm. | F5, F6, F7, F8, F9, F10 | Alarm delay time is too short. | Adjust the response delay times for the alarms in menus [229], [404], [410], [432], [435] and [438]. |
| The system seems locked in an alarm. | F2 <br> (Thermal motor protection) | PTC input terminal could be open. Motor could still be too warm. If internal motor protection is used, the cooling in the internal model may take some time. | PTC input terminal should be short circuit if not used. Wait until motor PTC gives an OK (not overheated) signal. Wait until the internal cooling is done. Try to restart after a while. |
|  | F3 <br> (Softstarter overheated) | Ambient temperature to high. Perhaps fan failure. | Check that cables from power part are connected in terminals 71 to 74. MSF-017 to MSF-250 should have a jumper between terminals 71 and 72. Check also that the fan(s) is(are) rotating. |


| Observation | Fault Indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| Parameter will not be accepted. |  | If menu 240, "Parameter set" is set to " 0 ", the system is configured for external control of parameter set. Most parameters are not allowed to be changed in this mode. | Set the menu 240, "Parameter set" to a value between " 1 " - " 4 " and then any parameter can be changed. |
|  |  | During start, stop and slow speed changing parameters is not permitted. | Set parameters during standstill or full voltage running. |
|  |  | If control source is serial comm., it is impossible to change parameters from keyboard and vice versa | Change parameters from the actual control source. |
|  |  | Some menus include only readout values and not parameters. | Read-out values cannot be altered. In Table 14, read-out menus have '-' in the factory setting column. |
|  | -Loc | Control panel is locked for settings. | Unlock control panel by pressing the keys "NEXT" and "ENTER'"for at least 3 sec . |

## 11. Maintenance

In general the softstarter is maintenance-free. There are however some things which should be checked regularly. In particular, if the surroundings are dusty the unit should be cleaned regularly.

## WARNING! Do not touch parts inside the enclosure of the unit when the control supply voltage or the mains supply voltage is

 switched on.
### 11.1 Regular maintenance

- Check that nothing in the softstarter has been damaged by vibration (loose screws or connections).
- Check external wiring, connections and control signals. Tighten terminal screws and busbar bolts if necessary.
- Check that printed circuit boards, thyristors and cooling fins are free from dust. Clean with compressed air if necessary. Make sure the printed circuit boards and the thyristors are undamaged.
- Check for signs of overheating (changes in colour on printed circuit boards, oxidation of solder points etc.). Check that the temperature is within permissible limits.
- Check that the cooling fan(s) permit free air flow. Clean any external air filters if necessary.


## 12. Options

The following options are available. Please contact your supplier for more detailed information.

### 12.1 Serial communication

For serial communication the MODBUS RTU (RS232/ RS485) option board is available, order part number: 01-1733-00.


Fig. 68 Option RS232/485

### 12.2 Fieldbus systems

Various option boards are available for the following bus systems:

- PROFIBUS DP order part number: 01-1734-01
- Device NET, order part number: 01-1736-01

Each system has its own board. The option is delivered with an instruction manual containing all the details for the installation and set-up of the board and the protocol for programming.


Fig. 69 Profibus Option

### 12.3 External control panel

The external control panel option is used to move the control panel from the softstarter to the front of a panel door or control cabinet.

The maximum distance between the softstarter and the external control panel is 3 m .
The part number to order for the external control panel is $01-2138-00$. A separate data sheet for this option is available.


Fig. 70 Use of the external control panel.

### 12.3.1 Cable kit for external current transformers

This kit is used for the bypass function, to connect the current transformers externally. order part number: 01-202000.


Fig. 71 Cable kit

### 12.4 Terminal clamp

Data: Single cables, Cu or Al

| Cables | $95-300 \mathrm{~mm}^{2}$ |
| :--- | :--- |
| MSF type Cu Cable | 310 |
| Bolt for connection to busbar | M10 |
| Dimensions in mm | $33 \times 84 \times 47 \mathrm{~mm}$ |
| Part no. single | 9350 |
| Data: Parallel cables, Cu or Al |  |
| Cables | $2 \times 95-300 \mathrm{~mm}^{2}$ |
| MSF type and Cu Cable | 310 to 835 |
| Bolt for connection to busbar | M10 |
| Dimensions in mm | $35 \times 87 \times 65$ |
| Part no. parallel | 9351 |



Fig. 72 The terminal clamp.

## 13. Technical data

### 13.1 Electrical specifications

Table 17 Typical motor power at mains voltage 400 V

| MSF model | $\begin{gathered} \text { Heavy } \\ \text { AC-53a } 5.0-30: 50-10 \end{gathered}$ |  | $\begin{gathered} \text { Normal } \\ \text { AC-53a 3.0-30:50-10 } \end{gathered}$ |  | Normal with bypass AC-53b 3.0-30:300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power @400V [kW] | Rated current [A] | Power @400V [kW] | Rated current [A] | Power @400V [kW] | Rated current [A] |
| MSF-017 | 7.5 | 17 | 11 | 22 | 11 | 25 |
| -030 | 15 | 30 | 18.5 | 37 | 22 | 45 |
| -045 | 22 | 45 | 30 | 60 | 37 | 67 |
| -060 | 30 | 60 | 37 | 72 | 45 | 85 |
| -075 | 37 | 75 | 45 | 85 | 55 | 103 |
| -085 | 45 | 85 | 45 | 96 | 55 | 120 |
| -110 | 55 | 110 | 75 | 134 | 90 | 165 |
| -145 | 75 | 145 | 75 | 156 | 110 | 210 |
| -170 | 90 | 170 | 110 | 210 | 132 | 255 |
| -210 | 110 | 210 | 132 | 250 | 160 | 300 |
| -250 | 132 | 250 | 132 | 262 | 200 | 360 |
| -310 | 160 | 310 | 200 | 370 | 250 | 450 |
| -370 | 200 | 370 | 250 | 450 | 315 | 555 |
| -450 | 250 | 450 | 315 | 549 | 355 | 675 |
| -570 | 315 | 570 | 400 | 710 | 450 | 820 |
| -710 | 400 | 710 | 450 | 835 | 500 | 945 |
| -835 | 450 | 835 | 500 | 960 | 630 | 1125 |
| -1000 | 560 | 1000 | 630 | 1125 | 800 | 1400 |
| -1400 | 800 | 1400 | 900 | 1650 | 1000 | 1800 |

Table 18 Typical motor power at mains voltage 460 V

| MSF model | $\begin{gathered} \text { Heavy } \\ \text { AC-53a 5.0-30:50-10 } \end{gathered}$ |  | $\begin{gathered} \text { Normal } \\ \text { AC-53a 3.0-30:50-10 } \end{gathered}$ |  | Normal with bypass AC-53b 3.0-30:300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power @460V [hp] | Rated current [A] | Power @460V [hp] | Rated current [A] | Power @460V [hp] | Rated current [A] |
| MSF-017 | 10 | 17 | 15 | 22 | 20 | 25 |
| . 030 | 20 | 30 | 25 | 37 | 30 | 45 |
| -045 | 30 | 45 | 40 | 60 | 50 | 68 |
| -060 | 40 | 60 | 50 | 72 | 60 | 85 |
| -075 | 60 | 75 | 60 | 85 | 75 | 103 |
| -085 | 60 | 85 | 75 | 96 | 100 | 120 |
| -110 | 75 | 110 | 100 | 134 | 125 | 165 |
| -145 | 100 | 145 | 125 | 156 | 150 | 210 |
| $-170$ | 125 | 170 | 150 | 210 | 200 | 255 |
| -210 | 150 | 210 | 200 | 250 | 250 | 300 |
| -250 | 200 | 250 | 200 | 262 | 300 | 360 |
| -310 | 250 | 310 | 300 | 370 | 350 | 450 |
| -370 | 300 | 370 | 350 | 450 | 450 | 555 |
| -450 | 350 | 450 | 450 | 549 | 500 | 675 |
| -570 | 500 | 570 | 600 | 710 | 650 | 820 |
| -710 | 600 | 710 | 700 | 835 | 800 | 945 |
| -835 | 700 | 835 | 800 | 960 | 900 | 1125 |
| -1000 | 800 | 1000 | 900 | 1125 | 1000 | 1400 |
| -1400 | 1000 | 1400 | 1250 | 1650 | 1500 | 1800 |

Table 19 Typical motor power at mains voltage 525 V

| MSF model | $\begin{gathered} \text { Heavy } \\ \text { AC-53a 5.0-30:50-10 } \end{gathered}$ |  | $\begin{gathered} \text { Normal } \\ \text { AC-53a 3.0-30:50-10 } \end{gathered}$ |  | Normal with bypass AC-53b 3.0-30:300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power @525V [kW] | Rated current <br> [A] | Power @ 525V [kW] | Rated current <br> [A] | Power @525V [ kW ] | Rated current <br> [A] |
| MSF-017 | 11 | 17 | 15 | 22 | 15 | 25 |
| -030 | 18,5 | 30 | 22 | 37 | 30 | 45 |
| -045 | 30 | 45 | 37 | 60 | 45 | 68 |
| -060 | 37 | 60 | 45 | 72 | 55 | 85 |
| -075 | 45 | 75 | 55 | 85 | 75 | 103 |
| -085 | 55 | 85 | 55 | 96 | 75 | 120 |
| -110 | 75 | 110 | 90 | 134 | 110 | 165 |
| -145 | 90 | 145 | 110 | 156 | 132 | 210 |
| -170 | 110 | 170 | 132 | 210 | 160 | 255 |
| -210 | 132 | 210 | 160 | 250 | 200 | 300 |
| -250 | 160 | 250 | 160 | 262 | 250 | 360 |
| -310 | 200 | 310 | 250 | 370 | 315 | 450 |
| -370 | 250 | 370 | 315 | 450 | 355 | 555 |
| -450 | 315 | 450 | 400 | 549 | 450 | 675 |
| -570 | 400 | 570 | 500 | 710 | 560 | 820 |
| . 710 | 500 | 710 | 560 | 835 | 630 | 945 |
| -835 | 560 | 835 | 710 | 960 | 800 | 1125 |
| -1000 | 710 | 1000 | 800 | 1125 | 1000 | 1400 |
| -1400 | 1000 | 1400 | 1250 | 1650 | 1400 | 1800 |

Table 20 Typical motor power at mains voltage 575 V

| MSF model | $\begin{gathered} \text { Heavy } \\ \text { AC-53a 5.0-30:50-10 } \end{gathered}$ |  | NormalAC-53a 3.0-30:50-10 |  | Normal with bypass AC-53b 3.0-30:300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power @575V [hp] | Rated current [A] | Power @575V [hp] | Rated current [A] | Power @575V [hp] | Rated current [A] |
| MSF-017 | 15 | 17 | 20 | 22 | 25 | 25 |
| -030 | 25 | 30 | 30 | 37 | 40 | 45 |
| -045 | 40 | 45 | 50 | 60 | 60 | 68 |
| -060 | 50 | 60 | 60 | 72 | 75 | 85 |
| -075 | 75 | 75 | 75 | 85 | 100 | 103 |
| -085 | 75 | 85 | 75 | 90 | 125 | 120 |
| -110 | 100 | 110 | 125 | 134 | 150 | 165 |
| -145 | 150 | 145 | 150 | 156 | 200 | 210 |
| -170 | 150 | 170 | 200 | 210 | 250 | 255 |
| -210 | 200 | 210 | 250 | 250 | 300 | 300 |
| -250 | 250 | 250 | 250 | 262 | 350 | 360 |
| -310 | 300 | 310 | 400 | 370 | 450 | 450 |
| -370 | 400 | 370 | 500 | 450 | 600 | 555 |
| -450 | 500 | 450 | 600 | 549 | 700 | 675 |
| -570 | 600 | 570 | 700 | 640 | 800 | 820 |
| -710 | 700 | 710 | 800 | 835 | 1000 | 945 |
| -835 | 800 | 835 | 900 | 880 | 1250 | 1125 |
| -1000 | 1000 | 1000 | 1250 | 1125 | 1500 | 1400 |
| -1400 | 1500 | 1400 | 1500 | 1524 | 2000 | 1800 |

Table 21 Typical motor power at mains voltage 690 V

| MSF model | $\begin{gathered} \text { Heavy } \\ \text { AC-53a 5.0-30:50-10 } \end{gathered}$ |  | $\begin{gathered} \text { Normal } \\ \text { AC-53a 3.0-30:50-10 } \end{gathered}$ |  | Normal with bypass AC-53b 3.0-30:300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power ©690V [kW] | Rated current <br> [A] | Power ©690V [kW] | Rated current <br> [A] | Power ©690V [kW] | Rated current [A] |
| MSF-017 | 15 | 17 | 18,5 | 22 | 22 | 25 |
| -030 | 22 | 30 | 30 | 37 | 37 | 45 |
| -045 | 37 | 45 | 55 | 60 | 55 | 68 |
| -060 | 55 | 60 | 55 | 72 | 75 | 85 |
| -075 | 55 | 75 | 75 | 85 | 90 | 103 |
| -085 | 75 | 85 | 90 | 90 | 110 | 120 |
| -110 | 90 | 110 | 110 | 134 | 160 | 165 |
| -145 | 132 | 145 | 132 | 156 | 200 | 210 |
| -170 | 160 | 170 | 200 | 210 | 250 | 255 |
| -210 | 200 | 210 | 250 | 250 | 250 | 300 |
| -250 | 250 | 250 | 250 | 262 | 355 | 360 |
| -310 | 315 | 310 | 355 | 370 | 400 | 450 |
| -370 | 355 | 370 | 400 | 450 | 500 | 555 |
| -450 | 400 | 450 | 560 | 549 | 630 | 675 |
| -570 | 560 | 570 | 630 | 640 | 800 | 820 |
| -710 | 710 | 710 | 800 | 835 | 900 | 945 |
| -835 | 800 | 835 | 900 | 880 | 1120 | 1125 |
| -1000 | 1000 | 1000 | 1120 | 1125 | 1400 | 1400 |
| -1400 | 1400 | 1400 | 1600 | 1524 | 1800 | 1800 |

### 13.2 General electrical specifications

## Table 22 General electrical specifications

| $\|$Parameter Description <br> General  <br> Mains supply voltage $200-525 \mathrm{~V} \pm 10 \%$ <br> $200-690 \mathrm{~V}+5 \%,-10 \%$ <br> Control supply voltage $100-240 \mathrm{~V} \pm 10 \%$ <br> $380-500 \mathrm{~V} \pm 10 \%$ <br> Mains and Control supply frequency $50 / 60 \mathrm{~Hz} \pm 10 \%$ <br> Number of fully controlled phases 3 <br> Recommended fuse for control supply Max 10 A |
| :--- |

Control signal inputs

| Digital input voltage | $0-3 \mathrm{~V} \rightarrow 0,8-27 \mathrm{~V} \rightarrow 1$. Max 37 V for 10 sec. |
| :--- | :--- |
| Digital input impedance to GND (0 VDC) | $2.2 \mathrm{k} \Omega$ |
| Analoueg input voitage/current | $0-10 \mathrm{~V}, 2-10 \mathrm{~V}, 0-20 \mathrm{~mA}, 4-20 \mathrm{~mA}$ |
| Analoueg input impedance to GND (0 VDC) | Voltage signal $125 \mathrm{k} \Omega$, current signal $100 \Omega$ |

Control signal outputs

| Output relays contact | $8 \mathrm{~A}, 250 \mathrm{VAC}$ or 24 VDC resistive load; $3 \mathrm{~A}, 250 \mathrm{VAC}$ inductive load (PF 0.4) |
| :--- | :--- |
| Analogue output voltage/current | $0-10 \mathrm{~V}, 2-10 \mathrm{~V}, 0-20 \mathrm{~mA}, 4-20 \mathrm{~mA}$ |
| Analogue output load impedance | Voltage signal min load $700 \Omega$, current signal max load $750 \Omega$ |
| Control signal supply |  |
| +12 VDC | $+12 \mathrm{VDC} \pm 5 \%$. Max current 50 mA. Short circuit proof. |

### 13.3 Fuses and power losses

Table 23 Fuses, power losses

| Model | Recommended wiring fuses [A] First column Ramp start/second column Direct-on-line start |  | Power loss at rated motor load [W] No losses with bypass |  | Power consumption control card [VA] |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Heavy | Normal | Heavy | Normal |  |
| MSF-017 | 25/50 | 32 | 50 | 70 | 20 |
| -030 | 35/80 | 50 | 90 | 120 | 20 |
| -045 | 50/125 | 80 | 140 | 180 | 25 |
| -060 | 63/160 | 100 | 180 | 215 | 25 |
| -075 | 80/200 | 100 | 230 | 260 | 25 |
| -085 | 100/250 | 125 | 260 | 290 | 25 |
| -110 | 125/315 | 180 | 330 | 400 | 25 |
| -145 | 160/400 | 200 | 440 | 470 | 25 |
| -170 | 200/400 | 200 | 510 | 630 | 35 |
| -210 | 250/400 | 315 | 630 | 750 | 35 |
| -250 | 250/500 | 315 | 750 | 750 | 35 |
| -310 | $315 / 630$ | 400 | 930 | 1100 | 35 |
| -370 | 400/800 | 500 | 1100 | 1535 | 35 |
| -450 | 500/1000 | 630 | 1400 | 1730 | 35 |
| -570 | 630/1000 | 800 | 1700 | 2100 | 35 |
| -710 | 800/1000 | 1000 | 2100 | 2500 | 35 |
| -835 | 1000/1200 | 1000 | 2500 | 2875 | 35 |
| -1000 | 1000/1400 | 1200 | 3000 | 3375 | 35 |
| -1400 | 1400/1800 | 1800 | 4200 | 4950 | 35 |

### 13.4 Mechanical specifications including mechanical drawings

| MSF <br> Model | Dimensions $\mathrm{H}^{*} \mathrm{~W} * \mathbf{D}$ [mm] | Mounting position [Vertical/ Horizontal] | Weight [kg] | Connection busbars [mm] | $\begin{gathered} \text { PE } \\ \text { screw } \end{gathered}$ | Cooling system | Protection class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -017, . 030 | 320 * 126 * 260 | Vertical | 6.7 | 15*4, Cu (M6) | M6 | Convection | IP20 |
| $\begin{aligned} & -045,-060,-075 \\ & -085 \end{aligned}$ | 320*126*260 | Vert. or Horiz. | 6.9 | 15*4, Cu (M6) | M6 | Fan | IP20 |
| -110, -145 | 400*176*260 | Vert. or Horiz. | 12 | $20 * 4, \mathrm{Cu}(\mathrm{M} 10)$ | M8 | Fan | IP20 |
| -170, -210, -250 | 500*260*260 | Vert. or Horiz. | 20 | $30 * 4, \mathrm{Cu}(\mathrm{M} 10)$ | M8 | Fan | IP20 |
| -310, -370, -450 | 532*547*278 | Vert. or Horiz | 46 | 40*8, Al (M12) | M8 | Fan | 1920 |
| -570, -710, -835 | 687*640*302 | Vert. or Horiz | 80 | $40 \times 10, \mathrm{Al}$ (M12) | M8 | Fan | 1920 |
| -1000, -1400 | 900*875*336 | Vert. or Horiz | 175 | 75*10, AI (M12) |  | Fan | IPOO |



Fig. 73 MSF -310 to MSF -835 .

### 13.5 Derating at higher temperature

By derating the current to $80 \%$ of nominal current, the MSF can be operated at an ambient temperature of up to $50^{\circ} \mathrm{C}$. E.g. a MSF-045 can operate a heavy load of 36 A ( 45 $\mathrm{A}^{*} 0.8$ ).

### 13.6 Environmental conditions

| Normal operation |  |
| :--- | :--- |
| Temperature | $0-40^{\circ} \mathrm{C}$ |
| Relative humidity | $95 \%$, non-condensing |
| Max altitude without derating | 1000 m |
| Storage |  |
| Temperature | $-25-+70^{\circ} \mathrm{C}$ |
| Relative humidity | $95 \%$, non-condensing |

### 13.7 Standards

| Market | Standard | Descrlption |
| :--- | :--- | :--- |
| All | IEC 60947-1 | Low-voltage switch gear and control gear. General part. |
|  | IEC 60947-4-2 | AC semiconductors motor controller and starters |
|  | EN 60204-1 | Safety of machinery - Electrical equipment of machines |
| European | Machinery Directive | $89 / 392 / \mathrm{ECC}$, Amendment 98/37/ECC |
|  | EMC Directive | $89 / 336 / \mathrm{ECC}$, Amendment 91/263/ECC, 93/68/ECC |
|  | Low Voltage Directive | $73 / 23 / E C C$, Amendment 93/68/ECC |
| Russian | GOST R | Russia certificate of conformity |
| American | UL 508 | Outline of investigation for power conversion equipment. <br> Only models MSF-017 to MSF-250 up to 600 vAC |

### 13.8 Power- and signal connectors.

Table 24 PCB Terminals

| Terminal | Function | Electrical characteristics |
| :---: | :---: | :---: |
| 01 | Control supply voltage | $100-240 \mathrm{VAC} \pm 10 \%$ alternative |
| 02 |  | $380-500 \mathrm{VAC} \pm 10 \%$ see rating plate |
| PE | Protective Earth | $\stackrel{1}{\square}$ |
| 11 | Digital input 1 | $0-3 \mathrm{~V} \rightarrow 0 ; 8-27 \mathrm{~V} \rightarrow 1 .$ <br> Max. 37 V for 10 sec . Impedance to $0 \mathrm{VDC}: 2.2 \mathrm{k} \Omega$. |
| 12 | Digital input 2 |  |
| 13 | Control signal supply voltage to PCB terminal 11 and 12 , $10 \mathrm{k} \Omega$ potentiometer, etc. | +12 VDC $\pm 5 \%$. Max. current from $+12 \mathrm{VDC}: 50 \mathrm{~mA}$. Short circuit-proof but not overload-roof. |
| 14 | Analogue input, $0-10 \mathrm{~V}, 2-10 \mathrm{~V}, 0-20 \mathrm{~mA}$ and $4-20 \mathrm{~mA} /$ digital input. | Impedance to terminal 15 ( 0 VDC) voltage signal: $125 \mathrm{k} \Omega$, current signal: $100 \Omega$. |
| 15 | GND (common) | 0 VDC |
| 16 | Digital input 3 | $0-3 \mathrm{~V} \rightarrow>0 ; 8-27 \mathrm{~V} \rightarrow 1$. |
| 17 | Digital input 4 | Max. 37 V for 10 sec . Impedance to 0 VDC : $2.2 \mathrm{k} \Omega$. |
| 18 | Control signal supply voltage to PCB terminal 16 and 17 , $10 \mathrm{k} \Omega$ potentiometer, etc. | +12 VDC $\pm 5 \%$. Max. current from $+12 \mathrm{VDC}=50 \mathrm{~mA}$. Short circuit-proof but not overload-proof. |
| 19 | Analogue output | Analogue output contact: <br> 0-10 V, 2-10 V; min load impedance $700 \Omega$ <br> $0-20 \mathrm{~mA}$ and $4-20 \mathrm{~mA}$; max load impedance $750 \Omega$ |
| 21 | Programmable relay K1. Factory setting is "Operation" with indication by closing terminal 21 to 22. | 1-pole closing contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3$ A inductive. |
| 22 |  |  |
| 23 | Programmable relay K 2 . Factory setting is "Full voltage" with indication by closing terminals 23 to 24 . | 1 -pole closing contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 24 |  |  |
| 31 | Programmable relay K3. Factory setting is "All alarms". Indication by closing terminals 31 to 33 and opening terminals 32 to 33 . | 1-pole change-over contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 32 |  |  |
| 33 |  |  |
| 69-70 | PTC Thermistor input | Alarm level $2.4 \mathrm{k} \Omega$ Switch back level $2.2 \mathrm{k} \Omega$. |
| 71-72* | Clickson thermistor | Controlling softstarter cooling fan temperature MSF-310 - MSF-1400 |
|  |  |  |
| 73-74* | NTC thermistor | Temperature measuring of softstarter cooling fin |
| 75 | Current transformer input, cable S1 (blue) | Connection of L1 or T1 phase current transformer |
| 76 | Current transformer input, cable S1 (blue) | Connection of L3, T3 phase (MSF 017 to MSF 250) or L2, T2 phase (MSF 310 to MSF 1400) |
| 77 | Current transformer input, cable S2 (brown) | Common connection for terminals 75 and 76 |
| 78* | Fan connection | 24 VDC |
| 79* | Fan connection | 0 VDC |

*Internal connection, no customer use.

### 13.9 Semi-conductor fuses

Always use standard commercial fuses to protect the wiring and prevent short circuiting. To protect the thyristors against short-circuit currents, superfast semiconductor fuses can be used if preferred (e.g. Bussmann type FWP or similar, see table below).
The normal guarantee is valid even if superfast semiconductor fuses are not used.

| Type | FWP Bussmann fuse |  |
| :--- | :--- | :--- |
|  | A |  |
| $\mathbf{I}^{\mathbf{2} t} \mathbf{t}$ (fuse) $\times \mathbf{1 0 0 0}$ |  |  |
| MSF-017 | 80 | 2.4 |
| MSF-030 | 125 | 7.3 |
| MSF-045 | 150 | 11.7 |
| MSF-060 | 200 | 22 |
| MSF-075 | 250 | 42.5 |
| MSF-085 | 300 | 71.2 |
| MSF-110 | 350 | 95.6 |
| MSF-145 | 450 | 137 |
| MSF-170 | 700 | 300 |
| MSF-210 | 700 | 300 |
| MSF-250 | 800 | 450 |

NOTE: Short circuit withstand MSF017-MSF060 5000 rms A when used with K5 or RK5 fuses.

NOTE: Short circuit withstand MSF075-MSF145 10000 rms A when used with K5 or RK5 fuses.

NOTE! Short circuit withstand MSF170-250 18000 rms A when used with K5 or RK5 fuses.

## 14. Set-up menu list

| Menu | Function/Parameter | Range | Parameter alt. <br> Alarm codes | Param. <br> set | Factory <br> setting | Value | Page |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | General settings |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 100 | Current | $0.0-9999 \mathrm{~A}$ |  | - | - |  | page 44 |
| 101 | Automatic return menu | oFF, 1-999 |  | - | oFF |  | page 44 |
|  |  |  |  |  |  |  |  |
| 200 | Control source | $1,2,3$ | 1. Control panel <br> 2. Remote control <br> 3. Serial comm. | $1-4$ | 2 |  | page 44 |
| 201 | Control panel locked for settings | no, YES |  | - | - |  | page 44 |
| 202 | Enable US units | oFF, on |  | --- | oFF |  | page 45 |


|  | Motor data |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 210 | Nominal motor voltage | $200-700 \mathrm{~V}$ |  | $1-4$ | 400 |  | page 45 |
| 211 | Nominal motor current | $25-200 \%$ of $\mathrm{I}_{\text {nsoft }}$ in A |  | $1-4$ | $\mathrm{I}_{\text {nooft }}$ |  | page 45 |
| 212 | Nominal motor power | $25-400 \%$ of $\mathrm{P}_{\text {nsoft }}$ in <br> kW resp. hp |  | $1-4$ | $\mathrm{P}_{\text {nsoft }}$ |  | page 45 |
| 213 | Nominal speed | $500-3600 \mathrm{rpm}$ |  | $1-4$ | $\mathrm{~N}_{\text {nsoft }}$ |  | page 45 |
| 214 | Nominal power factor | $0.50-1.00$ |  | $1-4$ | 0.86 |  | page 45 |
| 215 | Nominal frequency | $50,60 \mathrm{~Hz}$ |  | - | 50 | page 45 |  |


|  | Motor protection |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | THERMAL MOTOR PROTECTION |  |  |  |  |  |
| 220 | Thermal motor protection | oFF, 1, 2, 3, 4 | OFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | 2 | page 46 |
| 221 | PTC input | oFF, on |  | 1-4 | oFF | page 47 |
| 222 | Internal protection class | off, 2-40 s |  | 1-4 | 10 | page 47 |
| 223 | Used thermal capacity | 0-150\% |  | - | - | page 47 |
|  | Start limitation |  |  |  |  |  |
| 224 | Start limitation | oFF, 1, 2 | oFF <br> 1. Warning <br> 2. Coast | 1-4 | oFF | page 48 |
| 225 | Number of starts per hour | OFF, 1-99 |  | 1-4 | oFF | page 49 |
| 226 | Min time between starts | oFF, 1-60 min |  | 1-4 | ofF | page 49 |
| 227 | Time to next allowed start | $0-60 \mathrm{~min}$ |  | - | - | page 49 |
|  | LOCKED ROTOR |  |  |  |  |  |
| 228 | Locked rotor alarm | oFF, 1, 2 | OFF <br> 1. Warning <br> 2. Coast | 1-4 | ofF | page 49 |
| 229 | Locked rotor time | 1,0-10,0 s |  | 1-4 | 5,0 s | page 49 |
|  | SINGLE PHASE INPUT FAILURE |  |  |  |  |  |
| 230 | Single phase input failure | 1,2 ${ }^{\text {" }}$ | 1. Warning <br> 2. Coast | 1-4 | 2 | page 50 |
|  | CURRENT LIMIT START TIME EXPIRED |  |  |  |  |  |


| Menu | Function/Parameter | Range | Parameter alt. <br> Alarm codes | Param. <br> set | Factory <br> setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 231 | Current limit start time expired | ofF, 1, 2,3,4 | OFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | $1-4$ | 2 |  | page 50 |


|  | Parameter set handling |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 240 | Select parameter set | $0,1,2,3,4$ | 0 - External control of <br> parameter set <br> $1-4-$ - Parameter set 1-4 | - | 1 | page 51 |  |
| 241 | Actual parameter set | $1,2,3,4$ |  | -- | - |  | page 51 |
| 242 | Copy parameter set | no, P1-2, P1-3, P1-4, <br> P2-1, P2-3, P2-4, P3- <br> 1, no-no action <br> P1-2 - Copy parameter <br> P4-2, P4-3, P4-1, | set 1 to parameter set 2 <br> etc. | - | no | page 51 |  |
| 243 | Reset to factory settings | no, YES |  | - | no | page 52 |  |


|  | Autoreset |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 250 | Autoreset attempts | OFF, 0-10 |  | 1-4 | oFF | page 52 |
| 251 | Thermal motor protection autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |
| 252 | Start limitation autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |
| 253 | Locked rotor alarm autoreset | oFF, 0-3600 s |  | $1-4$ | OFF | page 53 |
| 254 | Current limit start time expired autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |
| 255 | Max power alarm autoreset | oFF, 0-3600 s |  | $1-4$ | OFF | page 53 |
| 256 | Min power alarm autoreset | OFF, 0-3600 s |  | 1-4 | OFF | page 53 |
| 257 | External alarm autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |
| 258 | Phase input failure autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |
| 259 | Voltage unbalance alarm autoreset | OFF, 0.3600 s |  | 1-4 | OFF | page 53 |
| 260 | Overvoltage alarm autoreset | OFF, O-3600 s |  | 1-4 | OFF | page 53 |
| 261 | Undervoltage alarm autoreset | oFF, 0-3600 s |  | 1-4 | ofF | page 53 |
| 262 | Serial communication autoreset | OFF, 0-3600 s |  | $1-4$ | ofF | page 53 |
| 263 | Softstarter overheated autoreset | oFF, 0-3600 s |  | 1-4 | oFF | page 53 |


|  | Serlal communication |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 270 | Serial comm. unit address | $1-247$ | $2.4-38.4$ kBaud |  | - | 1 |
| 271 | Serial comm. baudrate | 0,1 | O. No parity <br> 1. Even parity | - | 9.6 |  |
| 272 | Serial comm. parity | oFF, 1, 2, 3,4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | page 55 |  |  |
| 273. | Serial comm. contact broken |  | - | 0 |  | page 55 |


|  | Operation settIngs |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | PRE-SETTING |  |  |  |  |  |
| 300 | Preset pump control parameters | no, yes |  |  |  |  |
|  | START |  |  |  | no |  |


| Menu | Function/Parameter | Range | Parameter alt. Alarm codes | Param. set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 310 | Start method | 1, 2, 3, 4 | 1. Linear torque control <br> 2. Square torque control <br> 3. Voltage control <br> 4. DOL | 1-4 | 1 |  | page 57 |
| 311 | Initial torque at start | 0-250\% of $\mathrm{T}_{n}$ |  | 1-4 | 10 |  | page 58 |
| 312 | End torque at start | 25-250\% of $\mathrm{T}_{\mathrm{n}}$ |  | 1-4 | 150 |  | page 58 |
| 313 | Initial voltage at start | 25-80\% of U |  | 1-4 | 30 |  | page 58 |
| 314 | Current limit at start | off, $150-500 \%$ of $\mathrm{I}_{\mathrm{n}}$ |  | 1-4 | oFF |  | page 59 |


| 315 | Start time | 1-60 s |  | 1-4 | 10 | page 59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 316 | Torque boost current limit | off, $300-700 \%$ of $\mathrm{I}_{\mathrm{n}}$ |  | 1-4 | OFF | page 60 |
| 317 | Torque boost active time | 0.1-2.0 s |  | 1-4 | 1.0 | page 60 |
|  | STOP |  |  |  |  |  |
| 320 | Stop method | 1, 2, 3, 4, 5 | 1. Linear torque control <br> 2. Square torque control <br> 3. Voltage control <br> 4. Coast <br> 5. Brake | 1-4 | 4 | page 60 |
| 321 | End torque at stop | 0-100\% of $\mathrm{T}_{\mathrm{n}}$ |  | 1-4 | 0 | page 61 |
| 322 | Step down voltage at stop | 100-40\% of U |  | 1-4 | 100 | page 61 |
| 323 | Braking method | 1, 2 | 1. Dynamic vector brake <br> 2. Reverse current brake | - | 1 | page 62 |
| 324 | Braking strength | 150-500\% |  | 1-4 | 150 | page 62 |
| 325 | Stop time | 1-120 s |  | 1.4 | 10 | page 63 |
| 326 | Alarm braking strength | oFF, 150-500\% |  | 1-4 | OFF | page 63 |
| 327 | Alarm braking time | $1-120 \mathrm{~s}$ |  | 1-4 | 10 | page 63 |
|  | SLOW SPEED / JOG |  |  |  |  |  |
| 330 | Slow speed strength | 10-100 |  | 1.4 | 10 | page 65 |
| 331 | Slow speed time at start | oFF, 1.60 s |  | 1-4 | oFF | page 65 |
| 332 | Slow speed time at stop | oFF, 1-60 s |  | 1.4 | OFF | page 66 |
| 333 | DC brake at slow speed | oFF, 1-60 s |  | 1-4 | OFF | page 66 |
| 334 | Jog forward enable | oFF, on |  | 1-4 | OFF | page 66 |
| 335 | Jog reverse enable | oFF, on |  | 1-4 | oFF | page 66 |
|  | ADDITIONAL SETTINGS |  |  |  |  |  |
| 340 | Bypass | oFF, on |  | 1.4 | OFF | page 67 |
| 341 | Power Factor Control (PFC) | oFF, on |  | 1-4 | OFF | page 69 |
| 342 | Fan continuously on | oFF, on |  | 1-4 | OFF | page 69 |


|  | Process protection |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOAD MONITOR |  |  |  |  |  |
| 400 | Max power alarm | oFF, 1, 2, 3, 4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | OFF | page 71 |
| 401 | Min power alarm | oFF, 1, 2, 3, 4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | oFF | page 71 |
| 402 | Start delay power alarms | 1-999 s |  | 1-4 | 10 | page 71 |


| Menu | Functlon/Parameter | Range | Parameter alt. <br> Alarm codes | Param. <br> set | Factory <br> settIng | Value | Page |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| 403 | Max power alarm margin | $0-100 \%$ of $P_{n}$ |  | $1-4$ | 16 |  | page 71 |
| 404 | Max power alarm response delay | $0.1-90.0 \mathrm{~s}$ |  | $1-4$ | 0.5 |  | page 71 |
| 405 | Max power pre-alarm margin | $0-100 \%$ of $P_{n}$ |  | $1-4$ | 8 |  | page 72 |
| 406 | Max power pre-alarm response <br> delay | $0.1-90.0 \mathrm{~s}$ |  | $1-4$ | 0.5 |  | page 72 |
| 407 | Min power pre-alarm margin | $0-100 \%$ of $P_{n}$ |  | $1-4$ | 8 |  | page 72 |
| 408 | Min power pre-alarm response delay | $0.1-90.0 \mathrm{~s}$ |  | $1-4$ | 0.5 |  | page 72 |
| 409 | Min power alarm margin | $0-100 \%$ of $P_{\mathrm{n}}$ |  | $1-4$ | 16 |  | page 72 |
| 410 | Min power alarm response delay | $0.1-90.0 \mathrm{~s}$ |  | $1-4$ | 0.5 |  | page 73 |


| 411 | Autoset power limits | no, YES |  | - | no | page 73 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 412 | Normal load | 0-200\% of $\mathrm{P}_{\mathrm{n}}$ |  | 1-4 | 100 | page 73 |
| 413 | Output shaft power | 0.0-200.0\% of $\mathrm{P}_{\mathrm{n}}$ |  | - | - | page 73 |
|  | EXTERNAL ALARM |  |  |  |  |  |
| 420 | External alarm | OFF, 1, 2, 3, 4, 5 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake <br> 5. Spinbrake | $1-4$ | oFF | page 73 |
|  | MAINS PROTECTION |  |  |  |  |  |
| 430 | Voltage unbalance alarm | oFF, 1, 2, 3, 4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | oFF | page 74 |
| 431 | Voltage unbalance level | 2-25\% of $U_{n}$ |  | 1-4 | 10 | page 75 |
| 432 | Response delay voltage unbalance alarm | $1-905$ |  | 1-4 | 1 | page 75 |
| 433 | Overvoltage alarm | oFF, 1, 2, 3, 4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | oFF | page 75 |
| 434 | Overvoltage level | 100-150\% of $U_{n}$ |  | 1-4 | 115 | page 75 |
| 435 | Response delay overvoltage alarm | $1-90 \mathrm{~s}$ |  | 1-4 | 1 | page 75 |
| 436 | Undervoltage alarm | oFF, 1, 2, 3, 4 | oFF <br> 1. Warning <br> 2. Coast <br> 3. Stop <br> 4. Brake | 1-4 | oFF | page 75 |
| 437 | Undervoltage level | 75-100\% of $\mathrm{U}_{\mathrm{n}}$ |  | 1-4 | 85 | page 76 |
| 438 | Response delay undervoltage alarm | 1-90 s |  | 1-4 | 1 | page 76 |
| 439 | Phase sequence | L123, L321 |  | --- | - | page 76 |
| 440 | Phase reversal alarm | OFF, 1, 2 | oFF <br> 1. Warning <br> 2. Coast | - | oFF | page 76 |


|  | I/0 settIngs |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | INPUT SIGNALS |  |  |  |  |  |  |


| Menu | Function/Parameter | Range | Parameter alt. Alarm codes | Param. set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | Digital/analogue input | oFF, 1, 2, 3, 4, 5, 6, 7 | ofF <br> 1. Digital, Rotation sensor <br> 2. Digital, Slow speed <br> 3. Digital, Jog fwd <br> 4. Digital, Jog rev <br> 5. Digital, Autoset <br> 6. Analogue start-stop, $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ <br> 7. Analogue start-stop, 2-10V/4-20 mA | 1-4 | oFF |  | page 77 |
| 501 | Digital input pulses | 1-100 |  | 1.4 | 1 |  | page 78 |
| 502 | Analogue start-stop on-value | 0-100\% of signal range |  | 1-4 | 25 |  | page 79 |
| 503 | Analogue start-stop off-value | $0-100 \%$ of signal range |  | 1-4 | 75 |  | page 80 |
| 504 | Analogue start-stop delay time | $1-999 \mathrm{~s}$ |  | 1-4 | 1 |  | page 80 |


| 510 | Digital input 1 function | oFF, 1, 2, 3, 4, 5, 6, 7 | oFF <br> 1. Start signal <br> 2. Stop signal <br> 3. Parameter set input 1 <br> 4. Parameter set input 2 <br> 5. External alarm signal <br> 6. Start R signal <br> 7. Start L signal | - | 1 | page 81 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 511 | Digital input 2 function | oFF, 1, 2, 3, 4, 5, 6, 7 | See 510 | - | 2 | page 81 |
| 512 | Digital input 3 function | ofF, 1, 2, 3, 4, 5, 6, 7 | See 510 | - | 3 | page 82 |
| 513 | Digital input 4 function | ofF, 1, 2, 3, 4, 5, 6, 7 | See 510 | - | 4 | page 82 |
|  | OUTPUT SIGNALS |  |  |  |  |  |
| 520 | Analogue output | OFF, 1, 2, 3, 4 | OFF <br> 1. $0-10 \mathrm{~V} / 0-20 \mathrm{~mA}$ <br> 2. 2-10V/4-20mA <br> 3. $10-0 \mathrm{~V} / 20-0 \mathrm{~mA}$ <br> 4. $10-2 \mathrm{~V} / 20-4 \mathrm{~mA}$ | 1.4 | ofF | page 82 |
| 521 | Analogue output function | 1,2,3,4 | 1. RMS current <br> 2. Line voltage <br> 3. Shaft power <br> 4. Torque | 1-4 | 1 | page 82 |
| 522 | Scaling analogue output, min | $0-500 \%$ of value range |  | 1-4 | 0 | page 83 |
| 523 | Scaling analogue output, max | $0.500 \%$ of value range |  | 1-4 | 100 | page 84 |
|  |  |  |  |  |  |  |


| Menu | Function/Parameter | Range | Parameter alt. Alarm codes | Param. set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 530 | Relay K1 | off, 1-19 | oFF <br> 1. Operation <br> 2. Full voltage <br> 3. Power pre-alarms <br> 4. Brake <br> 5. Run <br> 6. Run R <br> 7. Run L <br> 8. Operation R <br> 9. Operation $L$ <br> 10. Power alarms <br> 11. Max power alarm <br> 12. Max power pre-alarm <br> 13. Min power alarm <br> 14. Min power pre-alarm <br> 15. All alarms (except power pre-alarms) <br> 16. All alarms (except power alarm and prealarms) <br> 17. External alarm <br> 18. Autoreset expired <br> 19. All alarms which <br> need manual reset | - | 1 |  | page 85 |
| 531 | Relay K2 | off, 1-19 | Same as 530 | -- | 2 |  | page 85 |


| 532 | Relay K3 | off, 1-19 | Same as 530 | - | 15 | page 85 |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 533 | K1 contact function | 1,2 | 1. N.O. <br> 2. N.C. | - | 1 | page 85 |
| 534 | K2 contact function | 1. N.O. <br> 2. N.C. | - | 1 | page 86 |  |


|  | View operation |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | OPERATION |  |  |  |  |  |
| 700 | Current | 0.0-9999 A |  | - | -- | page 91 |
| 701 | Line main voltage | 0.720 V |  | - | - | page 91 |
| 702 | Power factor | 0.00-1.00 |  | - | - | page 91 |
| 703 | Output shaft power | -999-9999 kW |  | - | - | page 91 |
| 704 | Output shaft power in percentage units | 0-200\% of $P_{\text {n }}$ |  | - | - | page 91 |
| 705 | Shaft torque | -999-9999 Nm |  | -- | - | page 91 |
| 706 | Shaft torque in percentage units | 0-250\% of $\mathrm{T}_{n}$ |  | - | - | page 91 |
| 707 | Softstarter temperature | $\begin{aligned} & \text { low, } 30-96^{\circ} \mathrm{C} \\ & \text { low, } 85-204^{\circ} \mathrm{F} \end{aligned}$ |  | - | - | page 92 |
| 708 | Current phase L1 | 0.0-9999 A |  | - | - | page 92 |
| 709 | Current phase L2 | 0.0-9999 A |  | - | - | page 92 |
| 710 | Current phase L3 | 0.0-9999 A |  | -- | - | page 92 |
| 711 | Line main voltage L1-L2 | $0-720 \mathrm{~V}$ |  | - | - | page 92 |
| 712 | Line main voltage L1-L3 | $0-720 \mathrm{~V}$ |  | - | -- | page 92 |
| 713 | Line main voltage L2-L3 | 0.720 V |  | - | - | page 92 |
| 714 | Phase sequence | L-, L123, L321 |  | - | - | page 92 |
| 715 | Used thermal capacity | 0-150\% |  | -- | - | page 92 |
| 716 | Time to next allowed start | 0-60 min |  | - | - | page 92 |


| Menu | Function/Parameter | Range | Parameter alt. <br> Alarm codes | Param. <br> set | Factory <br> setting | Value |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | Page


|  | STORED VALUES |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 730 | Operation time | $0-9999999 \mathrm{~h}$ |  | - | - |  | page 94 |
| 731 | Energy consumption | $0.000-2000 \mathrm{MWh}$ |  | - | - |  | page 94 |
| 732 | Reset energy consumption | no, YES |  | - | no |  | page 94 |


|  | Alarm list |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 800 | Alarm list, latest error | F1-F17, h |  | - | - | page 94 |
| 801 | Alarm list, error 14 | F1-F17, h |  | - | - | page 94 |
| 802 | Alarm list, error 13 | F1-F17, h |  | - | - | page 94 |
| 803 | Alarm list, error 12 | F1-F17, h |  | -- | - | page 94 |
| 804 | Alarm list, error 11 | F1-F17, h |  | - | - | page 94 |
| 805 | Alarm list, error 10 | F1-F17, h |  | - | - | page 94 |
| 806 | Alarm list, error 9 | F1-F17, h |  | - | - | page 94 |
| 807 | Alarm list, error 8 | F1-F17, h |  | - | - | page 94 |
| 808 | Alarm list, error 7 | F1-F17, h |  | - | -- | page 94 |
| 809 | Alarm list, error 6 | F1-F17, h |  | - | - | page 94 |
| 810 | Alarm list, error 5 | F1-F17, h |  | - | - | page 94 |
| 811 | Alarm list, error 4 | F1-F17, h |  | - | - | page 94 |
| 812 | Alarm list, error 3 | F1-F17, h |  | - | - | page 94 |
| 813 | Alarm list, error 2 | F1-F17, h |  | - | - | page 94 |
| 814 | Alarm list, error 1 | F1-F17, h |  | - | - | page 94 |


|  | Softstarter data |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| 900 | Softstarter type | $17-1400 \mathrm{~A}$ |  | - | 17 |  | page 95 |
| 901 | Software variant text | Same as label |  | - | V220 |  | page 95 |
| 902 | Software version text | Same as label |  | - | R15 |  | page 95 |

Explanation of units:

| $U$ | Input line voltage |
| :--- | :--- |
| $U_{n}$ | Nominal motor voltage. |
| $I_{n}$ | Nominal motor current. |
| $P_{n}$ | Nominal motor power. |
| $N_{n}$ | Nominal motor speed. |
| $T_{n}$ | Nominal shaft torque. |
| $I_{\text {nsoft }}$ | Nominal current softstarter. |
| $\mathrm{P}_{\text {nsoft }}$ | Nominal power softstarter. |
| $\mathrm{N}_{\text {nsoft }}$ | Nominal speed sofstarter, |
| Calculation shaft torque |  |

$$
T_{n}=\frac{P_{n}}{\left(\frac{N_{n}}{60} \times 2 \pi\right)}
$$

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DEDICATED DRIVE

## Endorsements

These are the details you are about to submit. Please print a copy for your records. If any of these details are not correct return to the relevant section to make changes.

## Endorsements

ELECTRICAL MECHANIC Yes

## Current Details

| Title | Mr |
| :--- | :--- |
| First Name: | BRETT |
| Other Name | DAVID |
| (s): |  |
| Family Name: | ARMSTRONG |
| Date of Birth: | 9 of Oct 1976 |

Residential Address

| Shop No: | Building: |
| :--- | :--- | :--- |
| Street 6 | Street <br> Name: |
| No: WATTLEBIRD |  |

Postal Address

| Use residential No address? |  |  |  |
| :---: | :---: | :---: | :---: |
| PO Box: |  |  |  |
| Shop No: |  | Building: |  |
| Street No: | 6 | Street Name: | $\text { WATTLEBIRD } \begin{aligned} & \text { Street } \\ & \text { Type: } \end{aligned}$ |
| Suburb: | LANDSBOROUGH | Post Code: | 4550 |
| State: | QLD | Country: | AUSTRALIA |
| Phone, Fax \& Email |  |  |  |
| Telephone no: | 0754951423 | Fax no: |  |
| Mobile no: | 0418557278 | Email: | bretta@sjelectric.com.au |

## Resuscitation Certificate (CPR)

Yes I am competent to carry out resuscitation

Issue date of qualification/certificate/training: 23 of Nov 2009
No I am competent to carry out pole-top rescue (Electrical Linesperson Only)
Issue date of qualification/certificate/training:

## Skills Maintenance

Yes I have met the Skills Maintenance requirements needed for the renewal/reinstatement/recognition of my licence.
You must provide documentary evidence, if you have completed any or all parts of the skills maintenance requirements through a Registered Training Organisation (RTO). Refer to guidelines for details located at
http://www.deir.qld.gov.au/publications/type/forms/index.htm\#f
Back Cancel Print Next

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Queensland Government

Current version 2.0.38 (8 July 2009 11:48)

# TECHNICAL DATA SHEET 

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type: Automatic Transfer Switch
Location: Generator Section
Model Numbers: ..... 62W3FD240VAC
Manufacturer: AICHI
Supplier:
NHP Pty Ltd
25 Turbo Drive
Coorparoo QLD ..... 4151
Ph: 0738916008Fx: 0738916139


## Operating Instructions VEGABAR 74 <br> 4 ... 20 mA/HART




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## Supplementary documentation

## i

## Information:

Depending on the ordered version, supplementary documentation belongs to the scope of delivery. You find this documentation in chapter "Product description".

## Instructions manuals for accessories and replacement parts

## 1

Tip:
To ensure reliable setup and operation of your VEGABAR 74, we offer accessories and replacement parts. The associated documents are:

- Supplementary instructions manual 32036 "Welded socket and seals"
- Operating instructions manual 32798 "Breather housing VEGABOX 02"
- Operating instructions manual 20591 "External indicating and adjustment unit VEGADIS 12"


## 1 About this document

## 1．1 Function

This operating instructions manual provides all the information you need for mounting，connection and setup as well as important instructions for maintenance and fault rectification． Please read this information before putting the instrument into operation and keep this manual accessible in the immediate vicinity of the device．

## 1．2 Target group

This operating instructions manual is directed to trained personnel．The contents of this manual should be made available to these personnel and put into practice by them．

## 1．3 Symbolism used

－Information，tip，note
1 This symbol indicates helpful additional information．
Caution：If this warning is ignored，faults or malfunc－ tions can result．
Warning：If this warning is ignored，injury to persons and／or serious damage to the instrument can result．
Danger：If this warning is ignored，serious injury to persons and／or destruction of the instrument can result．

## Ex applications

This symbol indicates special instructions for Ex applications．
－List
The dot set in front indicates a list with no implied sequence．

## $\rightarrow$ Action

This arrow indicates a single action．

## 1 Sequence

Numbers set in front indicate successive steps in a procedure．

## 2 For your safety

### 2.1 Authorised personnel

All operations described in this operating instructions manual must be carried out only by trained specialist personnel authorised by the operator.

During work on and with the device the required personal protection equipment must always be worn.

### 2.2 Appropriate use

VEGABAR 74 is a pressure transmitter for measurement of gauge pressure, absolute pressure and vacuum.

You can find detailed information on the application range in chapter "Product description".

Operational reliability is ensured only if the instrument is properly used according to the specifications in the operating instructions manual as well as possible supplementary instructions.

Due to safety and warranty reasons, any invasive work on the device beyond that described in the operating instructions manual may be carried out only by personnel authorised by the manufacturer. Arbitrary conversions or modifications are explicitly forbidden.

### 2.3 Warning about misuse

Inappropriate or incorrect use of the instrument can give rise to application-specific hazards, e.g. vessel overfill or damage to system components through incorrect mounting or adjustment.

### 2.4 General safety instructions

This is a high-tech instrument requiring the strict observance of standard regulations and guidelines. The user must take note of the safety instructions in this operating instructions manual, the country-specific installation standards as well as all prevailing safety regulations and accident prevention rules.

The instrument must only be operated in a technically flawless and reliable condition. The operator is responsible for troublefree operation of the instrument.

During the entire duration of use，the user is obliged to determine the compliance of the required occupational safety measures with the current valid rules and regulations and also take note of new regulations．

## 2．5 Safety approval markings and safety tips

The safety approval markings and safety tips on the device must be observed．

## 2．6 CE conformity

VEGABAR 74 is in CE conformity with EMC（89／336／EWG）， fulfils NAMUR recommendation NE 21 and is in CE conformity with LVD（73／23／EWG）．

Conformity has been judged according to the following standards：
－EMC：
－Emission EN 61326： 2004 （class B）
－Susceptibility EN 61326： 2004 including supplement A
－LVD：EN 61010－1： 2001
VEGABAR 74 is not subject to the pressure device guideline．${ }^{11}$

## 2．7 Fulfilling NAMUR recommendations

VEGABAR 74 fulfills the following NAMUR recommendations：
－NE 21 （interference resistane and emitted interference）
－NE 43 （signal level for failure information）
－NE 53 （compatibility sensor and indicating／adjustment components）
VEGA instruments are generally upward and downward compatible：
－Sensor software to DTM VEGABAR 74 HART
－DTM VEGABAR 74 for adjustment software PACTware ${ }^{\text {TM }}$ The parameter adjustment of the basic sensor functions is independent of the software version．The range of available functions depends on the respective software version of the individual components．

The software version of VEGABAR 74 HART can be read out via PACTware ${ }^{\text {TM }}$ ．

[^12]You can view all software histories on our website www.vega. com. Make use of this advantage and get registered for update information via e-mail.

### 2.8 Safety instructions for Ex areas

Please note the Ex-specific safety information for installation and operation in Ex areas. These safety instructions are part of the operating instructions manual and come with the Exapproved instruments.

### 2.9 Environmental instructions

Protection of the environment is one of our most important duties. That is why we have introduced an environment management system with the goal of continuously improving company environmental protection. The environment management system is certified according to DIN EN ISO 14001.

Please help us fulfil this obligation by observing the environmental instructions in this manual:

- Chapter "Packaging, transport and storage"
- Chapter "Disposal"


## 3 Product description

### 3.1 Configuration

## Scope of delivery

## Components

The scope of delivery encompasses:

- VEGABAR 74 pressure transmitter
- Documentation
- this operating instructions manual
- Test certificate for pressure transmitters
- Ex-specific "Safety instructions" (with Ex-versions)
- if necessary, further certificates

VEGABAR 74 consists of the following components:

- Process fitting with measuring cell
- Housing with electronics
- Connection cable (direct cable outlet)

The components are available in different versions.


Fig. 1: Example of a VEGABAR 74 with process fitting G112 A
1 Connection cable
2 Housing with electronics
3 Process fitting with measuring cell

Area of application

Functional principle

Supply

### 3.2 Principle of operation

VEGABAR 74 is a pressure transmitter for use in the paper, food processing and pharmaceutical industry. Thanks to the high protection class IP 68/IP 69K it is particularly suitable for use in humid environment. Depending on the version, it is used for level, gauge pressure, absolute pressure or vacuum measurements. Measured products are gases, vapours and liquids, also with abrasive contents.

The sensor element is the CERTEC ${ }^{\circledR}$ measuring cell with flush, abrasion resistant ceramic diaphragm. The hydrostatic pressure of the medium or the process pressure causes a capacitance change in the measuring cell via the diaphragm. This change is converted into an appropriate output signal and outputted as measured value.
The CERTEC ${ }^{\circledR}$ measuring cell is also equipped with a temperature sensor. The temperature value can be processed via the signal output.

Two-wire electronics $4 \ldots 20 \mathrm{~mA} / \mathrm{HART}$ for power supply and measured value transmission over the same cable.

The supply voltage range can differ depending on the instrument version.

The data for power supply are stated in chapter "Technical data" in the "Supplement".

### 3.3 Operation

VEGABAR $744 \ldots 20 \mathrm{~mA} / \mathrm{HART}$ can be adjusted with different adjustment media:

- with external adjustment/indication VEGADIS 12
- an adjustment software according to FDT/DTM standard, e.g. PACTware ${ }^{\text {TM }}$ and PC
- with a HART handheld

The kind of adjustment and the adjustment options depend on the selected adjustment component. The entered parameters are generally saved in the respecitive sensor, when adjusting with PACTware ${ }^{\text {TM }}$ and PC optionally also in the PC.
\(\left.$$
\begin{array}{ll} & \begin{array}{l}3.4 \text { Packaging, transport and storage } \\
\text { Packaging } \\
\\
\text { Your instrument was protected by packaging during transport. } \\
\text { Its capacity to handle normal loads during transport is assured } \\
\text { by a test according to DIN EN } 24180 .\end{array} \\
& \begin{array}{l}\text { The packaging of standard instruments consists of environ- } \\
\text { ment-friendly, recyclable cardboard. For special versions, PE } \\
\text { foam or PE foil is also used. Dispose of the packaging material }\end{array}
$$ <br>

\& via specialised recycling companies.\end{array}\right\}\)| Transport must be carried out under consideration of the notes |
| :--- |
| on the transport packaging. Nonobservance of these instruc- |
| tions can cause damage to the device. |

## 4 Mounting

### 4.1 General instructions

Make sure that the wetted parts of VEGABAR 74, especially the seal and process fitting, are suitable for the existing process conditions such as pressure, temperature etc. as well as the chemical properties of the medium.

You can find the specifications in chapter "Technical data" in the "Supplement".

Higher process temperatures often mean also higher ambient temperatures. Make sure that the upper temperature limits stated in chapter "Technical data" for the environment of the electronics housing and connection cable are not exceeded.


Fig. 2: Temperature ranges
1 Process temperature
2 Ambient temperature

## Connection

- The connection cable has a capillary for atmospheric pressure compensation
$\rightarrow$ Lead the cable end into a dry space or into a suitable terminal housing.


## Information:

VEGA recommends the breather housing VEGABOX 02 or the indication/adjustment VEGADIS 12. Both contain terminals and a ventilation filter for pressure compensation. For mounting outdoors, a suitable protective cover is available.

## 4．2 Mounting steps

Sealing／Screwing in threaded versions

## Sealing／Screwing in flange versions

Sealing／Screwing in hygienic fittings

Seal the thread with teflon，hemp or a similar resistant seal material on the process fitting thread $11 / 2$ NPT．
$\rightarrow$ Screw VEGABAR 74 into the welded socket．Tighten the hexagon on the process fitting with a suitable wrench． Wrench size，see chapter＂Dimensions＂．

Seal the flange connections according to DIN／ANSI with a suitable，resistant seal and mount VEGABAR 74 with suitable screws．

Use the seal suitable for the respective process fitting．You can find the components in the line of VEGA accessories in the supplementary instructions manual＂Welded socket and seals＂．

## 5 Connecting to power supply

### 5.1 Preparing the connection

Note safety instructions

Take note of safety instructions for Ex applications


Select power supply

Selecting connection cable

Always keep in mind the following safety instructions:

- Connect only in the complete absence of line voltage
- If overvoltage surges are expected, versions with integrated overvoltage arresters should be used or external overvoltage arresters should be installed


## Tip:

We recommend the version of VEGABAR 74 with integrated overvoltage arrester or VEGA type ÜSB62-36G.X as external overvoltage arreaster.

In hazardous areas you should take note of the appropriate regulations, conformity and type approval certificates of the sensors and power supply units.

Power supply and current signal are carried on the same twowire cable. The voltage supply range can differ depending on the instrument version.

The data for power supply are stated in chapter "Technical data" in the "Supplement".

Provide a reliable separation of the supply circuit from the mains circuits according to DIN VDE 0106 part 101.

VEGA power supply units VEGATRENN 149AEx, VEGASTAB 690, VEGADIS 371 as well as all VEGAMETs meet this requirement. When using one of these instruments, protection class III is ensured for VEGABAR 74.

Bear in mind the following factors regarding supply voltage:

- Output voltage of the power supply unit can be lower under nominal load (with a sensor current of 20.5 mA or 22 mA in case of fault message)
- Influence of additional instruments in the circuit (see load values in chapter "Technical data")

VEGABAR 74 is connected with standard two-wire cable without screen. An outer cable diameter of $5 \ldots 9 \mathrm{~mm}$ ensures the seal effect of the cable gland when connecting via VEGABOX 02 or VEGADIS 12. If electromagnetic interference is expected which is above the test values of EN 61326 for
industrial areas，screened cable should be used．For HART multidrop operation we recommend as standard practice the use of screened cable．


Fig．3：Connection of VEGABAR 74
1 Direct connection
2 Connection via VEGABOX 02 or VEGADIS 12

Cable screening and ground－ ing

## Select connection cable for Ex applica－ tions



If screened cable is necessary，connect the cable screen on both ends to ground potential．In the VEGABOX 02 or VEGADIS 12，the screen must be connected directly to the internal ground terminal．The ground terminal on the outside of the housing must be connected to the potential equalisation （low impedance）．
If potential equalisation currents are expected，the connection on the processing side must be made via a ceramic capacitor （e．g． $1 \mathrm{nF}, 1500 \mathrm{~V}$ ）．The low frequency potential equalisation currents are thus suppressed，but the protective effect against high frequency interference signals remains．

Take note of the corresponding installation regulations for Ex applications．In particular，make sure that no potential equal－ isation currents flow over the cable screen．In case of grounding on both sides this can be achieved by the use of a capacitor or a separate potential equalisation．

### 5.2 Connection procedure

## Direct connection

Proceed as follows:
1 Wire the connection cable up to the connection compartment. The bending radius must be at least $25 \mathrm{~mm} .{ }^{2}$ )
2 Connect the wire ends to the screw terminals according to the wiring plan

Via VEGABOX 01 or VEGADIS Proceed as follows:
12
1 Snap connection housing onto the carrier rail or screw it to the mounting plate
2 Loosen the cover screws and remove the cover
3 Insert the cable through the cable entry into the connection housing housing
4 Loosen the screws with a screwdriver
5 Insert the wire ends into the open terminals according to the wiring plan
6 Tighten the screws with a screwdriver
7 Check the hold of the wires in the terminals by lightly pulling on them
8 Tighten the compression nut of the cable entry. The seal ring must completely encircle the cable
9 Connect the supply cable according to steps 3 to 8
10 Screw the housing cover back on
The electrical connection is finished.
${ }^{2)}$ The connection cable is already preconfectioned. After shortening the cable, fasten the type plate with support again to the cable.

## 5．3 Wiring plan

## Direct connection



Fig．4：Wire assignment，connection cable
1 brown（＋）：to power supply or to the processing system
2 blue（ - ）：to power supply or to the processing system
3 yellow：is only required with VEGADIS 12，otherwise connect to minus or with VEGABOX 01 to terminal $3^{3)}$
4 Screen
5 Breather capillaries with filter element

Fig．5：Terminal assignment VEGABAR 74
1 To power supply or the processing system
2 Screen4）

| Wire number | Wire colour／Polarity | VEGABAR 74 terminal |
| :--- | :--- | :--- |
| 1 | brown $(+)$ | 1 |
| 2 | blue $(-)$ | 2 |
| 3 | Yellow | 2 |
|  | Screen | Ground |

## Connection via VEGADIS 12



Fig. 6: Terminal assignment, VEGADIS 12
1 To power supply or the processing system
2 Control instrument (4 ... 20 mA measurement)
3 Screens)
4 Breather capillaries
5 Suspension cable

| Wire number | Wire colour/Polarity | Terminal VEGADIS <br> $\mathbf{1 2}$ |
| :--- | :--- | :--- |
| 1 | brown $(+)$ | 1 |
| 2 | blue $(-)$ | 2 |
| 3 | Yellow | 3 |

5) Connect screen to ground terminal. Connect ground terminal on the outside of the housing as prescribed. The two terminals are galvanically connected.

## 6 Set up

## 6．1 Setup steps without VEGADIS 12

After mounting and electrical connection，VEGABAR 74 is ready for operation．
$\rightarrow$ Switch on voltage
The electronics now carries out a self－check for approx． 2 seconds．Then VEGABAR 74 delivers a current of $4 \ldots 20 \mathrm{~mA}$ according to the actual level．

## 6．2 Setup steps with VEGADIS 12

－zero－measuring range begin
－span－measuring range end
－ti－Integration time
Adjustment system


Fig．7：Adjustment elements of VEGADIS 12
1 Rotary switch：choose the requested function
2 ［ + ］key，change value（rising）
3 ［－］key，change value（falling）
－With the rotary switch the requested function is selected
－With the［＋］and［－］keys，the signal current or the integration time are adjusted
－Finally the rotary switch is set to position＂OPERATE＂
The set values are transmitted to the EEPROM memory and remain there even in case of voltage loss．

Adjustment steps，adjustment
Proceed as follows for adjustment with VEGADIS 12：
1 Open housing cover
2 Connect hand multimeter to terminals 10 and 12
3 Meas．range begin：Set rotary switch to＂zero＂

Set up

4 Empty the vessel or reduce process pressure
5 Set a current of 4 mA with the [ +$]$ and [-] keys
6 Meas. range end: Set rotary switch to "span"
7 Fill the vessel or increase process pressure
8 Set a current of 20 mA with the [+] and [-] keys
9 Operation: Set rotary switch to "OPERATE"
10 Close housing cover
The adjustment data are effective, the output current $4 \ldots 20 \mathrm{~mA}$ corresponds to the actual level.

Adjustment steps, integration time

Proceed as follows for the adjustment of the integration time with VEGADIS 12:

1 Open housing cover
2 Set rotary switch to "ti"
3 By pushing the [-] key 10 -times, make sure that the integration time is set to 0 sec .
4 For every 1 sec . requested integration time, push the [+] key once.
5 The integration time is the time required by the output current signal to reach $90 \%$ of the actual height after a sudden level change.
6 Set rotary switch to "OPERATE"
7 Close housing cover
Adjustment steps, scaling The display outputs the current $4 \ldots 20 \mathrm{~mA}$ as bar graph and digital value.

With 4 mA no segment of the bar graph appears, with 20 mA all segments appear. This assignment is fix.

You can scale the digital value to any value between -9999... +9999 via the adjustment module.

Proceed as follows for scaling the indication of VEGADIS 12:
1 Open housing cover
2 Initial value: Set rotary switch to "zero"
3 Set the requested value, e.g. 0 with the [ +$]$ and $[-]$ keys
4 Final value: Set the rotary switch to "span"
5 Set the requested value, e.g. 1000 with the [+] and [-] keys
6 Decimal point: Set the rotary switch to "point"
7 With the [+] and [-] keys you can adjust the requested value, e.g. 8888 (no decimal point)

## 8 Set rotary switch to＂OPERATE＂ <br> 9 Close housing cover <br> The adjustment data are effective，the output current $4 \ldots 20 \mathrm{~mA}$ corresponds to the actual level．

## 7 Setup with PACTware ${ }^{\text {TM }}$

### 7.1 Connect the PC with VEGACONNECT 3

Connecting the PC to the signal cable


Fig. 8: Connecting the PC to the signal cable
1 RS232 connection (with VEGACONNECT 3) or USB connection (with VEGACONNECT 4)
2 VEGABAR 74
3 HART adapter cable
4 HART resistance 250 Ohm (optional depending on the processing)

Necessary components:

- VEGABAR 74
- PC with PACTware ${ }^{\text {TM }}$ and suitable VEGA DTM
- VEGACONNECT 3 or 4 with HART adapter cable (art. no. 2.25397)
- HART resistance approx. 250 Ohm
- Power supply unit


## Note:

With power supply units with integrated HART resistance (internal resistance approx. 250 Ohm ), an additional external resistance is not necessary (e.g. VEGATRENN 149A, VEGADIS 371, VEGAMET 381/624/625, VEGASCAN 693). In such cases, VEGACONNECT 3 can be connected parallel to the 4 ... 20 mA cable.

### 7.2 Connect the PC with VEGACONNECT 4

## Connection via HART



Fig. 9: Connecting the PC via HART to the signal cable 1 VEGABAR 74
2 HART resistance 250 Ohm (optional depending on the processing) 3 Connection cable with 2 mm pins and terminals
4 Processing system/PLCNoltage supply

Necessary components:

- VEGABAR 74
- PC with PACTware ${ }^{T M}$ and suitable VEGA DTM
- VEGACONNECT 4
- HART resistance 250 Ohm (optional depending on the processing)
- Power supply unit or processing system


## Note:

With power supply units with integrated HART resistance (internal resistance approx. 250 Ohm), an additional external resistance is not necessary. This applies, e.g. to the VEGA instruments VEGATRENN 149A, VEGADIS 371, VEGAMET 381). Also usual Ex separators are most of the time equipped with a sufficient current limitation resistor. In such cases, VEGACONNECT 4 can be connected parallel to the $4 \ldots 20 \mathrm{~mA}$ cable.

### 7.3 Parameter adjustment with PACTware ${ }^{\text {TM }}$

Further setup steps are described in the operating instructions manual "DTM Collection/PACTware ${ }^{\text {TM" }}$ attached to each CD and which can also be downloaded from our homepage. A detailed description is available in the online help of PACTware ${ }^{\mathrm{TM}}$ and the VEGA DTMs.

## i

Note:
Keep in mind that for setup of VEGABAR 74, DTM-Collection in the actual version must be used.

All currently available VEGA DTMs are provided in the DTM Collection on CD and can be obtained from the responsible VEGA agency for a token fee. This CD includes also the up-todate PACTware ${ }^{\text {TM }}$ version. The basic version of this DTM Collection incl. PACTware ${ }^{\text {TM }}$ is also available as a free-ofcharge download from the Internet.

Go via www.vega.com and "Downloads" to the item "Software".

### 7.4 Parameter adjustment with AMS $^{\text {TM }}$ and PDM

For VEGA sensors, instrument descriptions for the adjustment programs AMS ${ }^{\text {M }}$ and PDM are available as DD or EDD. The instrument descriptions are already implemented in the current versions of AMS $^{\text {TM }}$ and PDM. For older versions of AMS ${ }^{\text {TM }}$ and PDM, a free-of-charge download is available via Internet.

Go via www.vega.com and "Downloads" to the item "Software".

### 7.5 Saving the parameter adjustment data

It is recommended to document or save the parameter adjustment data. They are hence available for multiple use or service purposes.

The VEGA DTM Collection and PACTware ${ }^{\text {TM }}$ in the licensed, professional version provide suitable tools for systematic project documentation and storage.

## 8 Maintenance and fault rectification

## 8．1 Maintenance

When used as directed in normal operation，VEGABAR 74 is completely maintenance free．

## 8．2 Fault clearance

The operator of the system is responsible for taken suitable measures to remove interferences．

## Causes of malfunction

Fault rectification

24 hour service hotline
However，if these measures are not successful，call the VEGA service hotline in urgent cases under the phone no．＋49 1805 858550.

The hotline is available to you 7 days a week round－the－clock． Since we offer this service world－wide，the support is only available in the English language．The service is free of charge，only the standard telephone costs will be charged．

## Checking the 4 ．．． 20 mA sig－ nal

Connect a handheld multimeter in the suitable measuring range according to the wiring plan．
？ $4 \ldots 20 \mathrm{~mA}$ signal not stable
－Level fluctuations
$\rightarrow$ Adjust integration time via PACTware ${ }^{\text {TM }}$
－no atmospheric pressure compensation
$\rightarrow$ Check the capillaries and cut them clean
$\rightarrow$ Check the pressure compensation in the housing and clean the filter element, if necessary
? $4 \ldots 20 \mathrm{~mA}$ signal missing

- Wrong connection to power supply
$\rightarrow$ Check connection according to chapter "Connection steps" and if necessary, correct according to chapter "Wiring plan"
- No voltage supply
$\rightarrow$ Check cables for breaks; repair if necessary
- supply voltage too low or load resistance too high
$\rightarrow$ Check, adapt if necessary
? Current signal 3.6 mA ; 22 mA
- electronics module or measuring cell defective
$\rightarrow$ Exchange instrument or return instrument for repair

Reaction after fault rectification

In Ex applications, the regulations for the wiring of intrinsically safe circuits must be observed.

Depending on the failure reason and measures taken, the steps described in chapter "Set up" must be carried out again, if necessary.

### 8.3 Instrument repair

If a repair is necessary, please proceed as follows:
You can download a return form ( 23 KB ) from the Internet on our homepage www.vega.com under: "Downloads - Forms and certificates-Repair form".

By doing this you help us carry out the repair quickly and without having to call back for needed information.

- Print and fill out one form per instrument
- Clean the instrument and pack it damage-proof
- Attach the completed form and, if need be, also a safety data sheet outside on the packaging
- Please ask the agency serving you for the address of your return shipment. You can find the respective agency on our website www.vega.com under: "Company - VEGA worldwide"


## 9 Dismounting

## 9．1 Dismounting steps

## Warning：

Before dismounting，be aware of dangerous process con－ ditions such as e．g．pressure in the vessel，high temperatures， corrosive or toxic products etc．

Take note of chapters＂Mounting＂and＂Connecting to power supply＂and carry out the listed steps in reverse order．

## 9．2 Disposal

The instrument consists of materials which can be recycled by specialised recycling companies．We use recyclable materials and have designed the electronics to be easily separable．

## WEEE directive 2002／96／EG

This instrument is not subject to the WEEE directive 2002／96／ EG and the respective national laws（in Germany，e．g． ElektroG）．Pass the instrument directly on to a specialised recycling company and do not use the municipal collecting points．These may be used only for privately used products according to the WEEE directive．

Correct disposal avoids negative effects to persons and environment and ensures recycling of useful raw materials．

Materials：see chapter＂Technical data＂
If you cannot dispose of the instrument properly，please contact us about disposal methods or return．

## 10 Supplement

### 10.1 Technical data

General data

Manufacturer
Type name
Parameter, pressure
Measuring principle
Communication interface

VEGA Grieshaber KG, D-77761 Schiltach
VEGABAR 74
Gauge pressure, absolute pressure, vacuum
Ceramic-capacitive, dry measuring cell
None

## Materials and weights

Material 316L corresponds to 1.4404 or 1.4435
Materials, wetted parts

- Process fitting 316L
- Diaphragm sapphire ceramic ${ }^{\circledR}$ ( $99.9 \%$ oxide ceramic)
- Seal
- Seal process fitting thread $G 1 / 2 A$, G11⁄2 A

Materials, non-wetted parts

- Housing 316L
- Ground terminal 316Ti/316L
- Connection cable
- type label support on cable

Weight
PUR, FEP, PE
PE-HART
$0.8 \ldots 8 \mathrm{~kg}(1.8 \ldots 17.6 \mathrm{lbs})$, depending on process fitting

## Output variable

Output signal
Failure signal
Max. output current
Damping (63 \% of the input variable)
Step response or adjustment time
Fulfilled NAMUR recommendations
$4 \ldots 20 \mathrm{~mA} / \mathrm{HART}$
22 mA ( 3.6 mA ), adjustable
22.5 mA
$0 \ldots 10 \mathrm{~s}$, adjustable
70 ms (ti: $0 \mathrm{~s}, 0 \ldots 63 \%$ )
NE 43

## Additional output parameter - temperature



Range
Resolution
$-50 \ldots+150^{\circ} \mathrm{C}\left(-58 \ldots+302^{\circ} \mathrm{F}\right)$

Accuracy

- in the range of $0 \ldots+100^{\circ} \mathrm{C}$ $\pm 3 \mathrm{~K}$
$\left(+32 \ldots+212^{\circ} \mathrm{F}\right)$
- in the range of $-50 \ldots 0^{\circ} \mathrm{C}$ typ. $\pm 4 \mathrm{~K}$
$\left(-58 \ldots+32^{\circ} \mathrm{F}\right)$ and $+100 \ldots+150^{\circ} \mathrm{C}$ $\left(+212 \ldots+302{ }^{\circ} \mathrm{F}\right)$


## Input variable

Adjustment

| Zero adjustable | $-20 \ldots+95 \%$ of the nominal measuring range |
| :--- | :--- |
| Span adjustable | $3.3 \ldots+120 \%$ of the nominal measuring range |
| Recommended max. turn down | $10: 1$ |

Nominal measuring ranges and overload resistance

| Nominal range |  |  |
| :--- | :--- | :--- |
| Gauge pressure | Overload, max. pressure $\left.{ }^{6}\right)$ | Overload, min. pressure |
| $0 \ldots 0.1 \mathrm{bar} / 0 \ldots 10 \mathrm{kPa}$ | $15 \mathrm{bar} / 1500 \mathrm{kPa}$ | $-0.2 \mathrm{bar} /-20 \mathrm{kPa}$ |
| $0 \ldots 0.2 \mathrm{bar} / 0 \ldots 20 \mathrm{kPa}$ | $20 \mathrm{bar} / 2000 \mathrm{kPa}$ | $-0.4 \mathrm{bar} /-40 \mathrm{kPa}$ |
| $0 \ldots 0.4 \mathrm{bar} / 0 \ldots 40 \mathrm{kPa}$ | $30 \mathrm{bar} / 3000 \mathrm{kPa}$ | $-0.8 \mathrm{bar} /-80 \mathrm{kPa}$ |
| $0 \ldots 1 \mathrm{bar} / 0 \ldots 100 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $0 \ldots 2.5 \mathrm{bar} / 0 \ldots 250 \mathrm{kPa}$ | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $0 \ldots 5 \mathrm{bar} / 0 \ldots 500 \mathrm{kPa}$ | $65 \mathrm{bar} / 6500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $0 \ldots 10 \mathrm{bar} / 0 \ldots 1000 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $0 \ldots 25 \mathrm{bar} / 0 \ldots 2500 \mathrm{kPa}$ | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $0 \ldots 60 \mathrm{bar} / 0 \ldots 6000 \mathrm{kPa}$ | $200 \mathrm{bar} / 20000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 0 \mathrm{bar} /-100 \ldots 0 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 1.5 \mathrm{bar} /-100 \ldots 150 \mathrm{kPa}$ | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 5 \mathrm{bar} /-100 \ldots 500 \mathrm{kPa}$ | $65 \mathrm{bar} / 6500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 10 \mathrm{bar} /-100 \ldots 1000 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 25 \mathrm{bar} /-100 \ldots 2500 \mathrm{kPa}$ | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-1 \ldots 60 \mathrm{bar} /-100 \ldots 6000 \mathrm{kPa}$ | $300 \mathrm{bar} / 30000 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| $-0.05 \ldots 0.05 \mathrm{bar} /-5 \ldots 5 \mathrm{kPa}$ | $15 \mathrm{bar} / 1500 \mathrm{kPa}$ | $-0.2 \mathrm{bar} /-20 \mathrm{kPa}$ |
| $-0.1 \ldots 0.1 \mathrm{bar} /-10 \ldots 10 \mathrm{kPa}$ | $20 \mathrm{bar} / 2000 \mathrm{kPa}$ | $-0.4 \mathrm{bar} /-40 \mathrm{kPa}$ |

[^13]| Nominal range | Overload, max. pres- <br> sure6) | Overload, min. pressure |
| :--- | :--- | :--- |
| $-0.2 \ldots 0.2 \mathrm{bar} /-20 \ldots 20 \mathrm{kPa}$ | $30 \mathrm{bar} / 3000 \mathrm{kPa}$ | $-0.8 \mathrm{bar} /-80 \mathrm{kPa}$ |
| $-0.5 \ldots 0.5 \mathrm{bar} /-50 \ldots 50 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| Absolute pressure | $15 \mathrm{bar} / 1500 \mathrm{kPa}$ |  |
| $0 \ldots 0.1 \mathrm{bar} / 0 \ldots 10 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ |  |
| $0 \ldots 1 \mathrm{bar} / 0 \ldots 100 \mathrm{kPa}$ | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ |  |
| $0 \ldots 2.5 \mathrm{bar} / 0 \ldots 250 \mathrm{kPa}$ | $65 \mathrm{bar} / 6500 \mathrm{kPa}$ |  |
| $0 \ldots 5 \mathrm{bar} / 0 \ldots 500 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ |  |
| $0 \ldots 10 \mathrm{bar} / 0 \ldots 1000 \mathrm{kPa}$ | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ |  |
| $0 \ldots 25 \mathrm{bar} / 0 \ldots 2500 \mathrm{kPa}$ | $200 \mathrm{bar} / 20000 \mathrm{kPa}$ |  |
| $0 \ldots 60 \mathrm{bar} / 0 \ldots 6000 \mathrm{kPa}$ |  |  |

## Reference conditions and influencing variables (similar to DIN EN 60770-1)

Reference conditions according to DIN EN 61298-1

- Temperature
- Relative humidity
- Air pressure

Determination of characteristics

Characteristics
Reference installation position
Influence of the installation position
$+15 \ldots+25^{\circ} \mathrm{C}\left(+59 \ldots+77^{\circ} \mathrm{F}\right)$
45 ... 75 \%
860 ... 1060 mbar/86 ... 106 kPa (12.5 ... 15.4 psi )

Limit point adjustment according to IEC 61298-2
linear
upright, diaphragm points downward $<0.2 \mathrm{mbar} / 20 \mathrm{~Pa}(0.003 \mathrm{psi})$

Deviation determined according to the limit point method according to IEC 607707)
Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$.
Specifications refer to the set span. Turn down (TD) = nominal measuring range/set span.

## Deviation

- Turn down 1:1 up to 5:1
$<0.075$ \%
- Turn down up to 10:1
<0.015 \% x TD
Deviation with absolutely flush process fittings EV, FT
- Turn down 1:1 up to 5:1
- Turn down up to 10:1
<0.05 \%
$<0.01 \% \times$ TD

[^14]Deviation with absolute pressure measuring range 0.1 bar
－Turn down 1：1 up to $5: 1$
$<0.25 \% \times$ TD
－Turn down up to 10：1

$$
<0.05 \% \times \text { TD }
$$

## Influence of the product or ambient temperature

Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$ ．
Specifications refer to the set span．Turn down（TD）＝nominal measuring range／set span．

## Average temperature coefficient of the zero signal

In the compensated temperature range of $0 \ldots+100^{\circ} \mathrm{C}\left(+212^{\circ} \mathrm{F}\right)$ ，reference temperature $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$ ：
Average temperature coefficient of the zero signal
－Turn down 1：1

$$
<0.05 \% / 10 \mathrm{~K}
$$

－Turn down 1：1 up to 5：1
$<0.1 \% / 10 \mathrm{~K}$
－Turn down up to 10：1
$<0.15 \% / 10 \mathrm{~K}$
Outside the compensated temperature range：
Average temperature coefficient of the zero signal
－Turn down 1：1

$$
\text { typ. }<0.05 \% / 10 \mathrm{~K}
$$

## Thermal change of the current output

Applies also to the analogue $4 \ldots 20 \mathrm{~mA}$ current output and refers to the set span．
Thermal change，current output $<0.15 \%$ at $-40 \ldots+80^{\circ} \mathrm{C}\left(-40 \ldots+176{ }^{\circ} \mathrm{F}\right)$

## Long－term stability（similar to DIN 16086，DINV 19259－1 and IEC 60770－1）

Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$ ．
Specifications refer to the set span．Turn down（TD）＝nominal measuring range／set span．
Long－term drift of the zero signal $<(0.1 \% \times$ TD）／1 year

## Total deviation（similar to DIN 16086）

The total deviation（max．practical deviation）is the sum of basic accuracy and long－term stability：
$F_{\text {total }}=F_{\text {perf }}+F_{\text {stab }}$
$F_{\text {perf }}=\sqrt{ }\left(\left(F_{T}\right)^{2}+\left(F_{K I}\right)^{2}\right)$
With
－$F_{\text {total：}}$ Total deviation
－$F_{\text {pert：}}$ Basic accuracy
－$F_{\text {stab：}}$ Long－term drift

- $\mathrm{F}_{\mathrm{T}}$ : Temperature coefficient (influence of medium or ambient temperature)
- $\mathrm{F}_{\text {KI }}$ Deviation


## Ambient conditions

Ambient, storage and transport temperature

- Connection cable PE
$-40 \ldots+60^{\circ} \mathrm{C}\left(-40 \ldots+140^{\circ} \mathrm{F}\right)$
- Connection cable PUR, FEP $-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$


## Process conditions

The specifications of the pressure stage are used as an overview. The specifications on the type plate are applicable.

Pressure stage, process fitting

- Thread 316L

PN 60

- Thread Alu

PN 25

- Hygienic fittings 316L

PN 10, PN 16, PN 25, PN 40

- Flange 316L, flange with extension 316L

PN 40 or $150 \mathrm{lbs}, 300 \mathrm{lbs}$

Product temperature depending on the measuring cell seal

- FKM (e.g. Viton)
- EPDM
- Kalrez 6375 (FFKM)
- Chemraz 535

Vibration resistance
Shock resistance
$-20 \ldots+100^{\circ} \mathrm{C}\left(-4 \ldots+212^{\circ} \mathrm{F}\right)$
$-40 \ldots+100^{\circ} \mathrm{C}\left(-40 \ldots+212^{\circ} \mathrm{F}\right), 1 \mathrm{~h}: 140^{\circ} \mathrm{C} /$
$284{ }^{\circ} \mathrm{F}$ cleaning temperature
$-10 \ldots+100^{\circ} \mathrm{C}\left(+14 \ldots+212^{\circ} \mathrm{F}\right)$
$-30 \ldots+100^{\circ} \mathrm{C}\left(-22 \ldots+212^{\circ} \mathrm{F}\right)$
mechanical vibrations with 4 g and $5 \ldots 100 \mathrm{~Hz}^{8)}$
Acceleration $100 \mathrm{~g} / 6 \mathrm{~ms}^{9}$ )

## Electromechanical data

Connection cable

- Configuration
- Wire cross-section
- wire resistance
- Standard length
- max. length with VEGADIS 12
four wires, one suspension cable, one breather capillary, screen braiding, metal foil, mantle
$0.5 \mathrm{~mm}^{2}$ (AWG no. 20)
$<0.036 \mathrm{Ohm} / \mathrm{m}(0.011 \mathrm{Ohm} / \mathrm{ft})$
6 m (19.685 ft)
$200 \mathrm{~m}(656.168 \mathrm{ft})$

8) Tested according to the regulations of German Lloyd, GL directive 2.
9) Tested according to EN 60068-2-27.

- Min. bending radius at $25^{\circ} \mathrm{C} / 77^{\circ} \mathrm{F}$
- Diameter
- Colour - standard PE
- Colour - standard PUR
- Colour - Ex-version

25 mm ( 0.985 in )
approx. 8 mm ( 0.315 in )
Black
Blue
Blue

## Voltage supply

Supply voltage

- Non-Ex instrument

12 ... 36 V DC

- EEx ia instrument

12 ... 29 V DC
Permissible residual ripple

- $<100 \mathrm{~Hz}$
$\mathrm{U}_{\mathrm{ss}}<1 \mathrm{~V}$
- 100 Hz ... 10 kHz
$\mathrm{U}_{\mathrm{ss}}<10 \mathrm{mV}$
Load
see diagram


Fig. 10: Voltage diagram VEGABAR 74
1 HART load
2 Voltage limit Ex instrument
3 Voltage limit non-Ex instrument
4 Voltage supply
see diagram


Fig. 11: Voltage diagram VEGABAR 74 with VEGADIS 12
1 HART load
2 Voltage limit Ex instrument
3 Voltage limit non-Ex instrument
4 Voltage supply

## Integrated overvoltage protection

Nominal leakage current $(8 / 20 \mu \mathrm{~s}) \quad 10 \mathrm{kA}$

Min. response time
$<25 \mathrm{~ns}$

## Electrical protective measures

Protection
Overvoltage category
Protection class

## Approvals ${ }^{10)}$

ATEX ia

Ship approvals
Others

ATEX II 1G EEx ia IIC T6; ATEX II 2G
EEx ia IIC T6
GL, LRS, ABS, CCS, RINA, DNV
WHG

IP 68 (25 bar)/IP 69K
III
III
10.2 Dimensions

VEGABAR 74 - threaded fitting


Fig. 12: VEGABAR 74 threaded fiting: $G V=G 1 / 2$ A manometer connection $E N 837, G /=G 1 / 2 A$ inner $G 1 / 4 A, G G=G 11 / 2 A$, $G N=11 / 2 N P T, G M=G 11 / 2 A 70 \mathrm{~mm}, G R=1 / 2$ NPT inner $1 / 4 \mathrm{NPT}$

VEGABAR 74 - hygienic fitting 1


Fig. 13: VEGABAR 74 hygienic fitting: $C C=$ Tri-Clamp 11/2", CA =Tri-Clamp 2", $L A=$ hygienic fitting with compression nut F40, TA = Tuchenhagen Varivent DN 32, TB = Tuchenhagen Varivent DN 25, RA/RB = bolting DN 40/DN 50 according to DIN 11851

## VEGABAR 74 - hygienic fitting 2



Fig. 14: VEGABAR 74 KA/KH = cone DN 40, AA = DRD, SD/SE = Anderson 3" long/short fitting

VEGABAR 74 - flange connection


EA, FB, FE, FQ, FH, FI


TV, TS

| (1) | DN | PN | D | b | $k$ | d2 | d4 | 1 | PL | d5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EA | 40 | 40 | 529/32" | 45/64" | $421 / 64^{\prime \prime}$ | 4x645/64" | $315 / 32^{\prime \prime}$ | $1 / 8^{\prime \prime}$ | - |  |
| FB | 50 | 40 | $61 / 2^{\prime \prime}$ | 25/32" | $459 / 64^{\prime \prime}$ | $4 \times 045 / 64{ }^{4}$ | 41/64* | $1 / 8^{\circ}$ |  |  |
| FE | 80 | 40 | 77/8" | 15/18* | $6^{19 / 64 *}$ | $8 \times 045 / 644$ | 57/16" | $1 / 8{ }^{\prime \prime}$ |  | - |


| (2) |  | Ibs | D | b | $k$ | d2 | d4 | 1 | RL | d5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FQ | 11/2" | 150 | $5{ }^{\text {a }}$ | 11/16" | $314 / 16^{\prime \prime}$ | 4x0 5/8" | $27 / 8^{\prime \prime}$ | 1/8" | - | - |
| FH | $2^{\prime \prime}$ | 150 | $6 "$ | $3 / 4{ }^{\prime \prime}$ | 43/4" | $4 \times 05 / 8{ }^{\prime \prime}$ | 35/8 ${ }^{\text {" }}$ | $1 / 8{ }^{\prime \prime}$ | - | - |
| Fl | $3^{\prime \prime}$ | 150 | $71 / 2^{\prime \prime}$ | $3 / 4^{\prime \prime}$ | 6 | $4 \times 05 / 8{ }^{\prime \prime}$ | 6 | 1/8" | - | - |


| (3) | DN | PN | D | b | $k$ | d2 | d4 | 1 | RL | d5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TV | 50 | 40 | $61 / 2^{\prime \prime}$ | 25/32 | $459 / 64$ " | 4×ø 45/64* | $41 / 64{ }^{4}$ | $1 / 8{ }^{\prime \prime}$ | (4) | $11 / 2^{\prime \prime}$ |
| TS | 80 | 40 | 7 $7 / 8^{\prime \prime}$ | 15/16" | $619 / 64{ }^{\text {\| }}$ | 8×0 45/64 ${ }^{4}$ | $57 / 16^{\circ}$ | $1 / 8^{\circ}$ |  | $11 / 2^{\prime \prime}$ |

Fig. 15: VEGABAR 74 - flange connection
1 Flange connection according to DIN 2501
2 Flange fitting according to ANSI B16.5
3 Flange with extension
4 Order-specific

## VEGABAR 74 －threaded fitting for paper industry



BA／BB

Fig．16：VEGABAR 74 －connection for paper industry：$B A / B B=M 44 \times 1.25$

VEGABAR 74 - extension fitting for paper industry


Fig. 17: VEGABAR 74 - extension fitting for paper industry: EV/FT = absolutely flush for pulper (EV 2-times flattened), EG = extension for ball valve fitting ( $L=$ order-specific)

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# TECHNICAL DATA SHEET 

## For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

Equipment Type: Delivery Pressure Transmitter
Location: Common Control
Model Numbers: BR74XXGG1FHA2X
(SP119 50m Range \& SP175 100m Range)
Manufacturer: Vega
Supplier:
Vega398 The Boulevard
KirraweeNSW2232

Refer catalogue MTS

MAC DT transfer switches are basically a solenoid operated changeover contactor. Simplicity of operation is obtained via a unique single coil, thereby keeping control requirements to a minimum.

Transfer switches
With "OFF" position

| Current <br> rating (A) | Number of poles | Cat. No. |
| :---: | :---: | :---: |
| 100 | 3 | 61WN3FD240VAC ${ }^{\text { }}$ ) |
| 100 | 4 | 61WN4FD240VAC ) |
| 200 | 3 | 62WN3FD240VAC ${ }^{\text {' }}$ ) |
| 200 | 4 | 62WN4FD240VAC ${ }^{\text { }}$ ) |
| 400 | 3 | 64WN3FD240VAC ) |
| 400 | 4 | 64WN4FD240VAC ${ }^{\text {) }}$ |
| 600 | 3 | 66WN3FD240VAC ${ }^{\text {\% }}$ ) |
| 600 | 4 | 66WN4FD240VAC 7) |
| 800 | 3 | 68WNA3FD240VAC ${ }^{\text {? }}$ ) |
| 800 | 4 | 68WNA4FD240VAC ${ }^{\text { }}$ ) |
| 1000 | 3 | 610 WN3FD240VAC ${ }^{\text { }}$ ) |
| 1000 | 4 | 610WN4FD240VAC \%) |
| 1200 | 3 | 612WNA3FD240VAC ) |
| 1200 | 4 | 612WNA4FD240VAC ) |
| 1600 | 3 | 616WN3FD240VAC ${ }^{\text { }}$ ) |
| 1600 | 4 | 616WN4FD240VAC *) |
| 2000 | 3 | $620 \mathrm{WN3BD240VAC}{ }^{\text { }}$ ) |
| $\underline{2000}$ | 4 | 620WN4BD240VAC ) |
| 3000 | 3 | $630 \mathrm{WN} 3 \mathrm{BD} 240 \mathrm{VAC}{ }^{\text { }}$ ) |
| 3000 | 4 | 630WN4BD240VAC ${ }^{\text { }}$ ) |
| 4000 | 3 | 640WN3BD240VAC ${ }^{\text { }}$ ) |
| 5000 | 3 | 850WN3BD240VAC ${ }^{\text {) }}$ |

Without "OFF" position

| Current <br> rating (A) | Number of poles | Cat. No. ') |
| :---: | :---: | :---: |
| 100 | 3 | 61W3FD240VAC ! |
| 100 | 4 | 61W4FD240VAC ') |
| 200 | 3 | 62W3FD240VAC ') |
| 200 | 4 | 62W4FD240VAC ') |
| 400 | 3 | 64W3FD240VAC ) |
| 400 | 4 | 64W4FD240VAC ${ }^{\text { }}$ ) |

- $2 \mathrm{C} / \mathrm{O}$ Auxillaries fitted as standard
- Additional auxillary contacts available
- Easy manual operation if control voltage fails
- Logic panels available - for automatic sensing \& switching


Cat. No 61W-4FD


Cat. No 61WN-4FD


Cat. No 66WN-4FD

Standard voltage: 240 V AC (for availability of $24,48,110 \mathrm{~V}$ DC and 110 V AC contact NHP.)
For an additional $2 \times \mathrm{C} / \mathrm{O}$ auxillary contacts, add to " $2 \mathrm{C}^{\prime}$ to above Cat. No. (Part prefix WWN2C)
Auxiliaries are a factory fit. Each changeover (C/O) contact is $1 \mathrm{~N} / \mathrm{O}+1 \mathrm{~N} / \mathrm{C}$ with a common terminal: SPDT
Notes: ${ }^{1}$ Prices are for front connected units, rear connected units.
${ }^{2}$ ) Prices are for front connected units, rear connected units available from 600A.
") Prices are for rear connected units, front connected units are not available.

## Technical data

| Transfer switch | Rated short time <br> current (1 sec.) kA | Short circuit peak <br> value kA |
| :--- | :---: | :---: |
| $61 \mathrm{~W} / 61 \mathrm{WN}$ | 5 | 12.5 |
| $62 \mathrm{~W} / 62 \mathrm{WN}$ | 10 | 25 |
| $64 \mathrm{~W} / 64 \mathrm{WN}$ | 12 | 30 |
| $66 \mathrm{WN} / 68 \mathrm{WNA}$ | 15 | 37.5 |
| $610 \mathrm{WN} / 612 \mathrm{WNA}$ | 22 | 50 |
| 616 WN | 25 | 55 |
| 620 WN | 35 | 60 |
| 630 WN | 50 | 80 |
| 640 WN | 50 | 100 |
| 650 WN | 50 | 120 |



Dimensions and weights

| Transfer switch | $\begin{aligned} & \text { Dim "A" } \\ & 3 \text { pole } \end{aligned}$ | $\begin{aligned} & \text { Dim "A" } \\ & 4 \text { pole } \end{aligned}$ | "B" | "C" | "D" | "E" | "F" | Weigh 3P | $4 P$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61W/61WN ${ }^{1}$ ) | 239 | 269 | 193 | 112 | 15 | 60 | 230 | 6 | 8 |
| 62W/62WN ${ }^{1}$ ) | 289 | 329 | 220 | 112 | 30 | 60 | 230 | 8 | 10 |
| 64W/64WN ') | 340 | 400 | 290 | 132 | 40 | 60 | 234 | 14 | 18 |
| 66WN ') | 465 | 530 | 520 | 220 | 30 | 90 | 343 | 33 | 42 |
| 68WNA ${ }^{1}$ ) | 465 | 530 | 520 | 220 | 30 | 90 | 343 | 33 | 42 |
| 610WN ${ }^{1}$ ) | 510 | 590 | 600 | 220 | 50 | 90 | 343 | 39 | 49 |
| 612WNA ${ }^{1}$ ) | 510 | 590 | 600 | 220 | 50 | 90 | 343 | 40 | 51 |
| 616WN ') | 570 | 670 | 610 | 220 | 75 | 90 | 343 | 47 | 59 |
| 620WN ${ }^{2}$ ) | 675 | 810 | 580 | 340 | 100 | 100 | 405 | 115 | 135 |
| 630WN ${ }^{2}$ ) | 825 | 1010 | 580 | 370 | 125 | 100 | 405 | 150 | 190 |
| $640 \mathrm{WN}^{2}$ ) | 1040 | - | 610 | 380 | 190 | 100 | 520 | 207 |  |
| $650 \mathrm{WN}^{2}$ ) | 1190 | - | 610 | 380 | 240 | 100 | 520 | 265 |  |

Dimension " D " = Busbar width.
Dimension " E " = Distance required behind panel for insulation purposes.
Dimension "F" = Distance required for handle operation.

Notes: ') Dimensions and weights for front connected units.
${ }^{2}$ ) Dimensions and weights for rear connected units. All dimensions are in millimetres ( mm ) and weights in kilograms ( kg ).

Refer catalogue MTS

## Technical data <br> Circuit diagrams

"W" range - without OFF


## Internal control circuitry

| Xa1 $\cdot \mathbf{X a 2 :}$ | Control switch |
| :--- | :--- |
| $\mathbf{X b 1} \cdot \mathbf{X b 2 :}$ |  |
| $\mathbf{C C}:$ | Closing coil |
| Si: | Silicon rectifier |

## Operating circuit terminal

A1-A2: A power source side (ON)
B1-B2: B-power source side (ON)
AUX: Auxiliary switch
External connections
"WN" range - with OFF


| CC: | Closing coil | AX•BX: | Control switch |
| :--- | :--- | :--- | :--- |
| Si: | Silicon rectifier | SC: | Selective coil |
| LS: | Selective switch | TC: | Trip coil |
| ATS1•ATS2: | Control switch | AUX: | Auxiliary switch |
| BTS1•BTS2: |  |  |  |

Note: The above control and power circuitry is contained within the switch.

Note: All Aichi transfer switches are supplied with a set of varistors, which can be fitted as an option. The purpose of the varistors is to protect the control circuitry of the transfer switch against any external voltage surges. The varistors are connected across the coil terminals A1-A2, B1-B2, AT1-AT2, BT1-BT2.

## TECHNICAL DATA SHEET

For

## SEWAGE PUMP STATION SP218 <br> Westlake Drv

| Equipment Type: | Wet Well Level Transmitte |
| :--- | :--- |
| Location: | Common Control |
|  |  |
| Model Numbers: | FM167-A2BMD1A3 |
|  |  |
| Manufacturer: | Endress \& Hauser |
|  |  |
| Supplier: | Unit 8/277 Lane Cove Rd |
|  | North Ryde |
|  | NSW |
|  | 2113 |
|  | Tel: 0288777000 |
|  | Fax: 0288777099 |



Technical Information

## Waterpilot FMX167

Hydrostatic Level Measurement Reliable and rugged level probe with ceramic measuring cell Compact device for level measurement in fresh water, wastewater and saltwater


## Applications

The Waterpilot FMX167 is a pressure sensor for hydrostatic level measurement. Three versions of FMX167 are available at Endress+Hauser:

- $\operatorname{FMX1} 167$ with an outer diameter $=22 \mathrm{~mm}$ ( 0.87 inch): Version very suitable for drinking water applications and for use in probe tubes with small diameters
- FMX167 with an outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch): Heavy version and very easy to clean thanks to the flush-mounted diaphragm. Very suitable for wastewater and sewage treatment plants
- $\mathrm{FMX1} 167$ with an outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch): Resistant version for use in saltwater and very suitable for applications on ships (e.g. ballast water tanks)


## Your benefits

- High mechanical resistance to overload and aggressive media
- High-precision and long-term stability ceramic measuring cell
- Resistant to climatic changes thanks to potted electronics and 2 -filter pressure compensation system
- $4 \ldots 20 \mathrm{~mA}$ output signal with integrated overvoltage protection
- Simultaneous level and temperature measurement by optional integrated temperature sensor Pt 100
- Drinking water approval: KTW, NSF, ACS
- Certified to ATEX, FM and CSA
- Marine approval: GL, ABS
- Complete measuring point solutions through comprehensive accessories


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Function and system design
Device selection

| Waterpilot FMX167 |  |  |  |
| :---: | :---: | :---: | :---: |
| Field of application | Hydrostatic level measurement in deep wells e.g. drinking water | Hydrostatic level measurement in wastewater | Hydrostatic level measurement in saltwater |
| Process connection | - Suspension clamp <br> - Extension cable mounting screw with | G1 1/2 A or $11 / 2 \mathrm{NPT}$ thread |  |
| Outer diameter $\mathrm{d}_{0}$ | 22 mm (0.87 inch) | 42 mm (1.66 inch) | Max. 29 mm (1.15 inch) |
| Seals | - FKM Viton <br> - EPDM ${ }^{11}$ | - FKM Viton | - FKM Viton <br> - EPDM |
| Measuring ranges | - Nine fixed pressure measuring ranges from $0 . . .0 .1$ bar to $0 . . .20$ bar ( $0 . . .1 \mathrm{~m}$ $0 . . .1 .5$ psi to $0 . . .300 \mathrm{psi} / 0 . . .3 \mathrm{ftH}_{2} \mathrm{O}$ <br> - Customer-specific measuring ranges; | $\begin{aligned} & \text { in bar, } \mathrm{mH}_{2} \mathrm{O} \text {, psi and } \mathrm{ft} \mathrm{H}_{2} \mathrm{O} \text {, } \\ & \mathrm{H}_{2} \mathrm{O} \text { to } 0 \ldots 200 \mathrm{mH}_{2} \mathrm{O} / \\ & \text { to } \left.0 \ldots 600 \mathrm{ftH}_{2} \mathrm{O}\right) \\ & \text { factory-calibrated } \end{aligned}$ | - Seven fixed pressure measuring ranges in bar, $\mathrm{mH}_{2} \mathrm{O}$, psi and $\mathrm{ftH}_{2} \mathrm{O}$, from $0 . . .0 .1$ bar to $0 . . .4$ bar ( $0 . . .1 \mathrm{mH}_{2} \mathrm{O}$ to $0 . . .40 \mathrm{mH}_{2} \mathrm{O}$ / <br> $0 . . .1 .5$ psi to $0 . . .60 \mathrm{psi} /$ <br> $0 . .3 \mathrm{ft}_{2} \mathrm{O}$ to $0 \ldots 150 \mathrm{ftH}_{2} \mathrm{O}$ ) <br> - Customer-specific measuring ranges; factory-calibrated |
| Overload | Up to 40 bar ( 580 psi ) |  | Up to 25 bar (362 psi) |
| Process temperature | $-10 \ldots+70^{\circ} \mathrm{C}\left(-14 \ldots+158^{\circ} \mathrm{F}\right)$ |  | $0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$ |
| Ambient temperature range | $-10 \ldots+70^{\circ} \mathrm{C}\left(-14 \ldots+158^{\circ} \mathrm{F}\right)$ |  | $0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$ |
| Maximum measured error | $\pm 0.2 \%$ of upper range value (URV) |  |  |
| Supply voltage | $10 . .30 \mathrm{~V}$ DC |  |  |
| Output | $4 . .20 \mathrm{~mA}$ |  |  |
| Options | - Drinking water approval <br> - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT1 81 ( $4 \ldots 20 \mathrm{~mA}$ ) <br> - Marine approval | - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT181 (4... 20 mA ) <br> - Marine approval | - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT181 (4... 20 mA ) <br> - Marine approval |
| Specialties | - Integrated overvoltage protection <br> - Large selection of approvals, includin <br> - High-precision, long-term stable and | ATEX II 2 G, FM and CSA ugged ceramic measuring cell |  |

[^15]
## Measuring principle

The ceramic measuring cell is dry, i.e. pressure acts directly on the rugged ceramic diaphragm of Waterpilot FMX167 and causes it to move by max. 0.005 mm .
The effects of air pressure on the liquid surface are transferred via a pressure compensation tube through the extension cable to the rear of the ceramic diaphragm and compensated. Pressure-dependent changes in capacitance caused by diaphragm movement are measured at the electrodes of the ceramic carrier. The electronics convert the movement into a pressure-proportional signal which is linear to the medium level.


## FMXI 67 measuring principle

1 Ceramic measuring cell
2 Pressure compensation tube
$h$ Level height
p Total pressure $=$ hydrostatic pressure + atmospheric pressure
$\rho \quad$ Medium density
g Gravitational acceleration
$p_{\text {hydr. }}$ Hydrostatic pressure
$p_{\text {atm }}$ Atmospheric pressure

## Temperature measurement with optional Pt 100

Endress+Hauser offers an optional 4-wire Pt 100 resistance thermometer for Waterpilot FMX167 to measure level and temperature simultaneously. The Pt 100 belongs to Accuracy Class B to DIN EN 60751.

## Temperature measurement with optional Pt 100 and temperature transmitter TMT181

To convert the Pt 100 signal to a $4 \ldots 20 \mathrm{~mA}$ signal, Endress + Hauser also offers the TMT181 temperature transmitter.

## Measuring system

The complete standard measuring system consists of Waterpilot FMX167 and a transmitter power supply unit with supply voltage of $10 \ldots 30 \mathrm{~V}$ DC.

Example for other measuring point solutions with transmitter and possible evaluation units from Endress+Hauser:


Application examples with FMX167
OP Overvoltage protection e.g. HAW from Endress+Hauser

1. Simple cost-effective measuring point solution: Power supply of Waterpilot in hazardous and nonhazardous areas using RN221N active barrier.
Power supply and additional control of two consumers, e.g. pumps, via limit switch RTA421 with onsite display.
2. Power supply, onsite display, two switch outputs and a signal adaptation (turn down) are integrated in evaluation devices RMA421 (for mounting on hat rails) and RIA250 (for panel mounting). The evaluation unit RMA421 also has a trend recognition function, e.g. optimizing pump control in stormwater overflow basins. This function detects and evaluates changes in a measurable value within a specific time period.
3. If several pumps are used, pump life can be prolonged by alternate switching. With alternating pump control, the pump which was out of service for the longest period of time is switched on. The evaluation units RIA452 (for panel mounting) and RMA422 (for mounting on hat rails) offer this function as well as several others.
4. State-of-the-art recording technology with monitor recorders from Endress+Hauser, e.g. Ecograph, Memograph or hardcopy recorders such as Alphalog for documenting, monitoring, visualizing and archiving.


Application examples with FMXI 07 with Pt 100
OP Overvoltage protection e.g. HAW from Endress+Hauser
5. If you want to measure, display and evaluate temperature as well as level, e.g. to monitor temperature in fresh water to detect temperature limits for germ formation, you have the following options: The optional temperature transmitter can convert the Pt 100 signal into a $4 \ldots 20 \mathrm{~mA}$ signal and transfer it to any customary evaluation unit. Evaluation devices RMA421, RIA250 and RIA452 also offer a direct input for the Pt 100 signal.
6. If you want to detect and evaluate level and temperature with one device, choose the evaluation unit RMA422 with two inputs. It even includes the mathematical operation for linking the input signals.

## Input

| Measured variable | FMX167 + Pt 100 (optional) <br> - Hydrostatic pressure of a liquid <br> - Pt 100: Temperature of a liquid | Temperature transmitter (optional) <br> - Temperature |
| :---: | :---: | :---: |
| Measuring range | - Nine fixed pressure measuring ranges in bar, $\mathrm{mH}_{2} \mathrm{O}$, psi and $\mathrm{ftH}_{2} \mathrm{O}$; <br> $\rightarrow$ Page 18, "Ordering information" Section <br> - Customer-specific measuring ranges; factory-calibrated <br> - Temperature measurement from $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$ (optional with Pt 100 ) |  |
| Input signal | FMX $167+$ Pt 100 (optional) <br> - Change in capacitance <br> - Pt 100: Change in resistance | Temperature transmitter (optional) <br> - Pt 100 resistance signal, 4 -wire |

## Output

| Output signal | FMX167 + Pt 100 (optional) <br> - FMX167: 4 ... 20 mA for hydrostatic pressure measured value, two-wire <br> - Pt 100: Temperature-dependent resistance of Pt 100 | Temperature transmitter (optional) <br> $4 . .20 \mathrm{~mA}$ for temperature measured value, twowire |
| :---: | :---: | :---: |
| Load | FMX 167 + Pt 100 (optional) $R_{t 01} \leqslant \frac{U_{b}-10 \mathrm{~V}}{0.0225 \mathrm{~A}}-2 \cdot 0.09 \frac{\Omega}{\mathrm{~m}} \cdot 1-R_{\mathrm{add}}$ <br> P01-FMX $10711-16-15-21-12-000$ | Temperature transmitter (optional) |
|  |  | $R_{\mathrm{tot}} \leq \frac{\mathrm{U}_{\mathrm{b}}-8 \mathrm{~V}}{0.025 \mathrm{~A}}-R_{\mathrm{add}}$ <br>  |
|  | $\begin{aligned} R_{t o t}= & \text { Max. load resistance } / \Omega / \\ R_{\text {add }}= & \text { Additional resistances such as resistance of evall } \\ & \text { line resistance } / \Omega / \\ U_{b}= & \text { Supply voltage } M \\ l= & \text { Simple length of extension cable } / \mathrm{m} / \text { (cable resis } \end{aligned}$ | device and/or display instrument, per wire $\leq 0.09 / \Omega m$ ) |
|  |  |  |
|  | Load chart FMXI67 for estimating load resistance. Subtract the additional resistances, e.g. resistance of extension cable, from the calculated value as shown in the equation. | Load chart temperature transmitter for estimating load resistance. Subtract the additional resistances from the calculated value as shown in the equation. |

## Power supply

## Electrical connection

Note!

- When using the measuring device in hazardous areas, national standards and regulations as well as the Safety Instructions (XAs) or Installation or Control Drawings (ZDs) have to be observed. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections.
- Reverse polarity protection is integrated in the Waterpilot FMX167 and in the temperature transmitter TMT181. Changing the polarities bas no impact on operation.
- The cable must end in a dry room or in a proper terminal box. For installation outside, use the terminal box (IP 66/IP 67) with a CORE-TEX ${ }^{\otimes}$ filter from Endress+Hauser. The terminal box can be ordered using the order code of FMX167 $\rightarrow$ see Page 18, "Ordering information" Section) or an accessory (order number: 52006252).


## Waterpilot FMX167, standard



FMX107 electrical connection, versions "7" or "3" for
Feature 70 "Additional options" in the order code $\rightarrow$ see Page 18).

## Waterpilot FMX167 with Pt 100



FMX107 electrical connection with Pt 100, versions " 1 " or " 4 " for Feature 70 "Additional options" in the order code $\rightarrow$ see Page 18).

Waterpilot FMX167 with Pt 100 and TMT181 temperature transmitter ( $4 \ldots 20 \mathrm{~mA}$ )


FMXI 67 with Pt 100 and TMT181 temperature transmitter ( $4 . .20 \mathrm{~mA}$ ),
version " 5 " for Feature 70 in the order code $(\rightarrow$ see Page 18).
I Not for FMXI 67 with outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch)
Wire colors: $\mathrm{RD}=$ red, $\mathrm{BK}=$ black, $\mathrm{WH}=$ white, $\mathrm{YE}=$ yellow, $\mathrm{BU}=$ blue, $\mathrm{BR}=$ brown


## Performance characteristics

| Reference operating conditions | FMX167 + Pt 100 (optional) <br> DIN EN $60770 \mathrm{~T}_{\mathrm{U}}=25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$ | Temperature transmitter (optional) <br> Calibration temperature $23^{\circ} \mathrm{C} \pm 5 \mathrm{~K}\left(73^{\circ} \mathrm{F} \pm 5 \mathrm{~K}\right)$ |
| :---: | :---: | :---: |
| Maximum measured error | FMX167 + Pt 100 (optional) <br> - Non-linearity including hysteresis and nonrepeatability as per DIN EN 60770: $\pm 0.2 \%$ of upper range value (URV) <br> - Pt 100: Max. $\pm 0.7 \mathrm{~K}$ (Class B to DIN EN 60751) | Temperature transmitter (optional) <br> - $\pm 0.2 \mathrm{~K}$ <br> - With Pt 100: Max. $\pm 0.9 \mathrm{~K}$ |
| Long-term stability | FMX167 + Pt 100 (optional) <br> $\pm 0.1 \%$ of upper range value (URL) per year | Temperature transmitter (optional) $\leq 0.1 \mathrm{~K}$ per year |
| Influence of medium temperature on the hydrostatic level measurement of FMX167 | - Thermal change in zero signal and output span for typical application temperature range 0 . $\pm 0.4 \%( \pm 0.5 \%)^{*}$ of the upper range limit (URL) <br> - Thermal change in zero signal and output spa for the entire medium temperature range $\pm 1.0 \%( \pm 1.5 \%)^{*}$ of the upper range limit (U <br> a Temperature coefficient ( $\mathrm{T}_{\mathrm{k}}$ ) of zero signal $0.15 \% / 10 \mathrm{~K}(0.3 \% / 10 \mathrm{~K})^{*}$ of the upper ran <br> * Specifications for sensors $0.1 \mathrm{bar}\left(1 \mathrm{mH}_{2} \mathrm{O}\right.$, | $\left(+32 \ldots+86^{\circ} \mathrm{F}\right):$ $0^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right):$ <br> ut span: <br> (URL) <br> $3 \mathrm{ftH}_{2} \mathrm{O}$ ) and 0.6 bar ( $6 \mathrm{mH}_{2} \mathrm{O}, 10 \mathrm{psi}, 20 \mathrm{ftH}_{2} \mathrm{O}$ ) |
| Warm-up period | FMX167 + Pt 100 (optional) <br> 20 ms | Temperature transmitter (optional) $4 \mathrm{~s}$ |
| Rise time | FMX167 + Pt 100 (optional) <br> - FMX167: 80 ms <br> - Pt 100: 160 s |  |
| Settling time | FMX1 $67+$ Pt 100 (optional) <br> - FMX167: 150 ms <br> - Pt 100: 300 s |  |

## Installation

## Installation instructions



Installation examples, here shown with FMX 107 with an outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$
1 Extension cable mounting screw can be ordered via order code or as an accessory, $\rightarrow$ see Page 14 and 19
2 Terminal housing can be ordered via order code or as an accessory, $\rightarrow$ see Page 15 and 19
3 Extension cable bending radius $>120 \mathrm{~mm}$ ( 4.72 inch)
4 Suspension clamp can be ordered via order code or as an accessory, $\rightarrow$ see Page 14 and 19
5 Extension cable up to $300 \mathrm{~m}(384 \mathrm{ft})$, for max. length $\rightarrow$ see Page 10 , "Extension cable" Section
$0 \quad$ Guide tube for FMXI 67 with outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$ internal diameter $>23 \mathrm{~mm}$ ( 0.91 inch )
7 Additional weight can be ordered as an accessory for FMXIO 7 with outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$ and 29 mm ( 1.15 inch ) $\rightarrow$ see Page 19
8 Protection cap

Note!

- A sideways movement of the level probe can lead to measuring errors. Therefore install the probe at a point free from flow and turbulence, or use a guide tube. The internal diameter of the guide tube should be at least $1 \mathrm{~mm}(0.04$ inch $)$ bigger than the outer diameter of the selected FMX167.
- The cable must end in a dry room or in a proper terminal box. The terminal box from Endress + Hauser provides optimum humidity and climatic protection and is suitable for outdoor installation.
- Protective cap: to avoid mechanical damage to the measuring cell, the device is provided with a protective cap, which should not be removed during transport and installation.
- After shortening of the cable, the filter must be re-fitted on the pressure compensation hose.


## Environment

| Ambient temperature range | FMX167 + Pt 100 (optional) <br> - FMX167 with outer diameter $=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and 42 mm ( 1.66 inch ): $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$ ( $=$ medium temperature) <br> - FMX 167 with outer diameter $\begin{aligned} & =29 \mathrm{~mm}(1.15 \mathrm{inch}): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right) \\ & (=\text { medium temperature }) \end{aligned}$ | Temperature transmitter (optional) $-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$ |
| :---: | :---: | :---: |
| Storage temperature | FMX167 + Pt 100 (optional) $-40 \ldots+80^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$ | Temperature transmitter (optional) $-40 \ldots+100^{\circ} \mathrm{C}\left(-40 \ldots+212^{\circ} \mathrm{F}\right)$ |
| gree of protection | FMX 167 + Pt 100 (optional) <br> - IP 08 , permanently hermetically sealed <br> - Optional terminal box: IP $66 /$ IP 67 | Temperature transmitter (optional) <br> - IP 00, moisture condensation permissible <br> - When mounted in the optional terminal boxes: IP 66/IP67 |

Electromagnetic
compatibility (EMC)

FMX $167+\mathrm{Pt} 100$ (optional)

- Interference emission to EN 61326 Class B equipment, interference immunity to EN 61326 Appendix A (Industrial)
- Maximum deviation: $<0.5 \%$ of span


## Temperature transmitter (optional)

- Interference emission to EN 61326 Class B equipment, interference immunity to EN 61326 Appendix A (Industrial)

Overvoltage protection

## FMX167 + Pt 100 (optional)

Integrated overvoltage protection to EN 61000-4-5 $\leq 1.2 \mathrm{kV}$
Install overvoltage protection $\geq 1.2 \mathrm{kV}$, external if necessary

## Temperature transmitter (optional)

Install overvoltage protection, external if necessary.

## Process

Medium temperature range
FMX167 + Pt 100 (optional)

- FMX167 with outer diameter $=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and 42 mm ( 1.66 inch$)$ :
$-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$
- FMX 167 with outer diameter $=29 \mathrm{~mm}(1.15 \mathrm{inch}): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$

Temperature transmitter (optional)
$-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{C}\right)$ (= ambient temperature), install temperature transmitter outside medium.

Medium temperature limits $\quad$ FMX167 + Pt 100 (optional)

- FMX167 with outer diameter
$=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and 42 mm ( 1.66 inch$)$ :
$-20 \ldots+70^{\circ} \mathrm{C}\left(-4 \ldots+158^{\circ} \mathrm{F}\right)$
- FMX 167 with outer diameter
$=29 \mathrm{~mm}(1.15 \mathrm{inch}): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$
(You may operate the FMX167 in this temperature range. The specification can then be exceeded, e.g. measuring accuracy).

Mechanical construction

## Dimensions of level probe



## Versions of FMX167

1 FMX107, version "A" or "D" for Feature 30 "Probe tube" in the order code $(\rightarrow$ see Page 18)
2 FMX167, version "B" for Feature 30 "Probe tube" in the order code $(\rightarrow$ see Page 18)
3 FMX107, version " $C$ " for Feature 30 "Probe tube" in the order code $(\rightarrow$ see Page 18)
4 Pressure compensation tube
5 Extension cable
o Protection cap

Dimensions of suspension clamp


Suspension clamp, version 2 for Feature 20 "Connection" in the order code $(\rightarrow$ see Page 18)

Dimensions of extension cable mounting screws


Extension cable mounting screws
1 Extension cable mounting screw G $1 / / 2$ A, version " 3 " for Feature $20^{\circ}$ "Connection" in the order code $\rightarrow \rightarrow$ see Page 18)
2 Extension cable mounting screw / 1/2 NPT, version "4" for Feature $20^{\circ}$ "Connection" in the order code $\rightarrow$ see Page 18)

## Dimensions of the terminal

 box IP 66/IP 67 with filter

Terminal box
Version "3", "4" or "5" for Feature 70 "Additional options" in the order code $\rightarrow$ see Page 18)
1 Dummy plug M 20xI. 5
2 GORE-TEX ${ }^{\oplus}$ fitter
3 Terminals for $0.08 . .2 .5 \mathrm{~mm}^{2}$

Dimensions of temperature transmitter TMT181


Temperature transmitter TMTI 81 ( $4 \ldots 20 \mathrm{~mA}$ )
Version "5" for Feature 70 "Additional options" in the order code $\rightarrow$ see Page 18). The temperature transmitter can be used in non hazardous areas and for $E E X \cap A$.

## Weight

- Level probe, outer diameter $=22 \mathrm{~mm}(0.87$ inch $): 290 \mathrm{~g}$
- Level probe, outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch): 1150 g
- Level probe, outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch): 340 g
- Extension cable PE: $52 \mathrm{~g} / \mathrm{m}$
- Extension cable FEP: $108 \mathrm{~g} / \mathrm{m}$
- Suspension clamp: 170 g
- Extension cable mounting screw G $11 / 2 \mathrm{~A}: 770 \mathrm{~g}$
- Extension cable mounting screw $1 / 1 / 2$ NPT: 724 g
- Terminal box: 235 g
- Temperature transmitter: 40 g
- Additional weight: 300 g

| Material | Level probe <br> - Level probe, outer diameter $=22 \mathrm{~mm}$ ( 0.87 inch): 1.4435 (AISI 316L) <br> - Level probe, outer diameter $=42 \mathrm{~mm}$ ( 1.60 inch): 1.4435 (AISI 316L) <br> - Level probe, outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch): <br> - Level probe: 1.4435 (AISI 316L) <br> - Sensor sleeve: PPS (polyphenylene sulfide) <br> - Heat-shrink sleeve/cover: Polyolefin <br> Metal does not come into contact with the medium. <br> - Process ceramic: $\mathrm{Al}_{2} \mathrm{O}_{3}$ aluminium oxide ceramic <br> - Seal (internal): EPDM or Viton <br> - Protective cap: <br> - PE-HD (high-density polyethylene) for FMX167 with outer diameter $=22 \mathrm{~mm}$ and $29 \mathrm{~mm}(0.87$ inch and $1.15 \mathrm{inch})$. <br> - PFA (perfluoralkoxy) for FMX167 with outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch ). <br> - Extension cable insulation: Either PE-LD (low density polyethylene) or FEP (fluorinated ethylene propylene). For more information, see the next Section - "Extension cable" <br> - Suspension clamp: 1.4404 (AISI 316L) and glass fiber reinforced PA (polyamide) <br> - Extension cable mounting screw G $11 / 2 \mathrm{~A}: 1.4301$ (AISI 304) <br> - Extension cable mounting screw 1 1/2 NPT: 1.4301 (AISI 304) <br> - Terminal box: PC (polycarbonate) <br> - Temperature transmitter: Housing PC (polycarbonate) |
| :---: | :---: |
| Extension cable | PE extension cable <br> - Slip-resistant extension cable with strain-relief members made of Dynemo; shielded using aluminium-coated film; insulated with polyethylene (PE), black; copper wires, twisted <br> - Pressure compensation tube with Teflon filter |
|  | FEP extension cable <br> - Slip-resistant extension cable; shielded using galvanized steel wire netting; insulated with fluorinated ethylene propylene (FEP), black; copper wires, twisted <br> - Pressure compensation tube with Teflon filter <br> Cross-section of PE and FEP extension cable <br> - Total outer diameter: $8.0 \mathrm{~mm} \pm 0.25 \mathrm{~mm}(0.315$ inch $\pm 0.0098$ inch) <br> - FMX167: $3 \times 0.227 \mathrm{~mm}^{2}+$ pressure compensation tube with Teflon filter <br> - FMX167 with Pt 100 (optional): $7 \times 0.227 \mathrm{~mm}^{2}+$ pressure compensation tube with Teflon filter <br> - Pressure compensation tube with Teflon filter: <br> Outer diameter $=2.5 \mathrm{~mm}$ ( 0.098 inch ), internal diameter $=1.5 \mathrm{~mm}$ ( 0.059 inch ) |
|  | Cable resistance of PE and FEP extension cable <br> - Cable resistance per wire: $\leq 0.09 \Omega / \mathrm{m}$ |
|  | Cable length of PE and FEP extension cable <br> - Please also refer to Page 7, "Load" Section. <br> - When using the measuring device in hazardous areas, national standards and regulations as well as the safety instructions (XAs) or Installation or Control Drawings (ZDs) have to be observed. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections. |
|  | Further technical data of PE and FEP extension cable <br> - Minimum bending radius: 120 mm ( 4.72 inch) <br> - Tensile strength: max. 950 N <br> - Cable extraction force: $\geq 450 \mathrm{~N}$ <br> (The extension cable could be extracted from the level probe at a tensile force of $\geq 450 \mathrm{~N}$.) <br> - Resistance to UV light <br> - PE: approved for use with drinking water |
| Terminals | - 3 standard terminals in terminal box <br> - 4-terminal strip can be ordered as accessory, Order No. 52008938 Wire cross-section $0.08 \ldots 2.5 \mathrm{~mm}^{2}$ |

## Certificates and approvals

| CE approval | By attaching the CE symbol, Endress+Hauser confirms that the instrument fulfills all the requirements of the relevant $E C$ directives. |
| :---: | :---: |
| Ex approval, type of protection | - ATEXII 2 G EExia IIC To <br> - ATEXII 3 G EExnA IITo <br> - FM: IS, Class I, Division 1, Groups A-D ${ }^{1}$ <br> - CSA: IS, Class I, Division 1, Groups A-D' |
|  | 1 Only for Waterpilot FMX167 without Pt 100 |
|  | Waterpilot FMX167 with outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$ is only suitable for use in hazardous areas with the FKM Viton seal. |
|  | All explosion protection data are contained in separate explosion protection documentation which you can also request. Explosion protection documents are supplied as standard for all devices approved for use in explosion bazardous areas. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections. |
| Drinking water approval (for FMX167 with $\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}(0.87 \mathrm{inch})$ ) | - XTW certificate <br> - NSF 01 approval <br> - ACS approval |
| Marine approval | - GL approval <br> - ABS approval |
| External standards and guidelines | DIN EN 60770 (IEC 60770): <br> Transmitters for use in industrial-control systems <br> Part 1: Methods for performance evaluation |
|  | DIN 10080: <br> Electrical pressure measuring instruments, pressure sensors, pressure transmitters, pressure measuring instruments, concepts, specifications on data sheets |
|  | EN 61320 (IEC $01326-1$ ): <br> Electrical equipment for measurement, control and laboratory use - EMC requirements |
| Registered trademarks | GORE-TEX ${ }^{\text {® }}$ <br> Registered trademark of W.L. Gore \& Associates, Inc., USA |

## Ordering information

FMX167

| 10 Approval  <br> A Version for non-hazardous area  <br> B ATEX II. 2 G EEx ia IIC T6 <br> C ATEX II 3 G EEx nA II T6 <br> S FM IS, Class I, Division I, Groups A - D <br> E CSA IS, Class I, Division 1, Groups A - D <br> F CSA General Purpose |
| :--- |
| 20 |


| 30 | Probe tube: |  |
| :---: | :---: | :---: |
|  | A | Outer diameter $d=22 \mathrm{~mm}(0.87 \mathrm{inch})$, AlSI 316 <br> Outer diameter $d=42 \mathrm{~mm}$ ( 1.66 inch ), flush mount, AIS1 316 L <br> Outer diameter $d=29 \mathrm{~mm}$ ( 1.15 inch), ASSI 316 L with heat-shrink sleeve PPS/polyolefin for saltwater applications <br> Outer diameter $\mathrm{d}=22 \mathrm{~mm}(0.87 \mathrm{inch})$, AiSI $316 \mathrm{~L}+$ drinking water approval KTW/NSF/ACS (can only be selected in conjunction with EPDM seal and PE probe cable) |


$\rightarrow$ Ordering information for FMX167 continued on next page.


## Accessories

| Suspension clamp | - Endress + Hauser offers a suspension clamp for simple FMX167 mounting. $\rightarrow$ See also Page 14. <br> - Material: 1.4404 (AISI 316L) and glass fiber reinforced PA (polyamide) <br> - Order number: 52006151 |
| :---: | :---: |
| Terminal box | - Terminal box IP $66 / \mathrm{IP} 67$ with GORE-TEX ${ }^{\text {® }}$ filter incl. 3 mounted terminals. <br> The terminal box is also suitable for installing a temperature transmitter (Order No. 52008794) or for four additional terminals (Order No. 52008938). $\rightarrow$ See also Page 15. <br> - Order number: 52006152 |
| Additional weight <br> (for FMX 167 with $\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and $\mathrm{d}_{\mathrm{O}}=29 \mathrm{~mm}(1.15 \mathrm{inch})$ ) | - To prevent sideways movement leading to measuring errors or to ensure that the device lowers into a guide tube, Endress+Hauser provides additional weights. <br> You can screw several weights together. The weights are then attached directly to the FMX167. For FMX 167 with outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch ), a maximum of 5 weights may be screwed on to FMX167. <br> - Material: 1.4435 (AISI 316L) <br> - Weight: 300 g <br> - Order number: 52006153 |


| Temperature transmitter | - Temperature transmitter, 2 -wire, preset for measuring range from $-20 \ldots+80^{\circ} \mathrm{C}\left(-4 \ldots+176^{\circ} \mathrm{F}\right)$. This setting offers an easily displayable temperature range of 100 K . Note that the Pt 100 resistance thermometer is designed for a temperature range of $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right) . \rightarrow$ See also Page 15 . <br> - Order number: 52008794 |
| :---: | :---: |
| Extension cable mounting screw | - Endress+Hauser offers extension cable mounting screws to simplify the installation of the FMX167 and to close the measuring open. $\rightarrow$ See also Page 14. <br> - Material: 1.4301 (AISI 304) <br> - Order number for extension cable mounting screw with G 11/2 A thread: 52008264 <br> - Order number for extension cable mounting screw with I 1/2 NPT thread: 52009311 |
| Terminals | - Four terminals in strip for FMX167 terminal box, suitable for wire cross-section of $0.08 \ldots 2.5 \mathrm{~mm}^{2}$ <br> - Order number: 52008938 |

Test adapter
(for FMX167 with
$\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and $\left.\mathrm{d}_{\mathrm{O}}=29 \mathrm{~mm}(1.15 \mathrm{inch})\right)$


Test adapter
A Connection suitable for level probe FMXI07
B Connection compressed air hose, internal diameter, quick hose gland $4 \mathrm{~mm}(0.157 \mathrm{inch})$

- Endress+Hauser offers a test adapter to simplify the function test of level probes.
- Note the maximum pressure for the compressed air hose and the maximum level probe overload. $\rightarrow$ See also Page 18.
- The maximum pressure for the supplied quick hose gland is 10 bar (145 psi).
- Adapter material: I: 4301 (AISI 304)
- Quick hose gland material: Anodized aluminium
- Adapter weight: 39 g
- Order number: 52011808


## Documentation

| Field of Activities | - Pressure Measurement: FA004P/00/en <br> - Recording Technology: FA014R/09/de <br> - System Components: FA016K/09/en |
| :---: | :---: |
| Technical Information | - Temperature Head Transmitter iTEMP PCP TMT181: TI070R/09/en |
| Operating Instructions | - Waterpilot FMX107: BA231P/00/en |
| Safety Instructions | - ATEX II 2 G EEx ia IIC To: XA131P/00/a3 <br> - ATEX II 3 G EExnA IIT T6: XA132P/00/a3 |
| Installation/ Control Drawings | - FM IS Class I, Div. 1, Groups A - D: ZD063P/00/en <br> - CSA IS Class I, Div. 1, Groups A - D: ZD064P/00/en |
| Drinking water approval | - SD126P/00/a3 |

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People for Process Automation


[^0]:    Electrical Contactor's Supervisor
    Name:... ㄴ․…........... Signature:
    

    BW Commissioning Manager
    Name:
    Date:

    Signature:

    | Doc ld: | 006142 | Active Dat:: |
    | :--- | :--- | :---: |
    | Printed: | $10 / 12 / 2008$ | Owner: 10 Dec 2008 |
    | Alex With on |  |  |

    Note: $\quad$ Printed copies of this document should be verified for currency against the published electronic copy.

[^1]:    Note: Printed copies of this document should be verified for currency against the published electronic copy.

[^2]:    XH250NJ

[^3]:    Note: Settings; 3-poles can be adjusted simultaneously with one adjustment dial.

[^4]:    Note: A special generator $T_{1}$ setting adjustment of $1-5 \sec$ (at $l_{1} \times 600 \%$ ), is also

[^5]:    Note: PowerCad is a product of PowerCad Software Pty Ltd. Purchases of this software can be obtained from
    PowerCad. www.powercad.com.au

[^6]:    Sprecher + Schuh US Division Headquarters
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    Publication No: F-CA7-R1 10/02

[^7]:    * Please contact your distributor or agent before returning any product for repair or warranty claim.

[^8]:    1 * SLIP ® $\circledR^{\text {TM }}$ KISS $®^{\text {TM }}$

[^9]:    2 "Data and Computer Communications" William Stallings
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    Page 68

[^10]:    *Cable Length $10 \mathrm{~m} / 33 \mathrm{ft}$ or $30 \mathrm{~m} / 100 \mathrm{ft}$

    | Probe Length <br> (meters) | Sensor <br> Points | Cable Length <br> (meters) |
    | :---: | :---: | :---: |
    | 2.5 | 10 | 10 |

[^11]:    NOTE: A reset via the control panel will never start the motor.

[^12]:    1）Due to the flush diaphragm，no own pressure compartment is formed．

[^13]:    ${ }^{8)}$ Limited to 200 bar according to the pressure device directive.

[^14]:    7 Incl. non-inearity, hysteresis and non-repeatability.

[^15]:    1) Recommended for drinking water applications, not suitable for use in hazardous areas
