



Queensland Urban Utilities

PRV154

Cordelia Street

Contract:

BW 70103-060

Job Number:

43400306

ELECTRICAL INSTALLATION

OPERATIONS and MAINTENANCE MANUAL

VOLUME 1

INSTALLATION BY:

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1. General

1.1 General Workplace Health and Safety

- The Workplace Health and Safety Act (1995) sets out the laws about Workplace Health and Safety for all workplaces, workplace activities and specified high risk plant. The Electrical Safety Act (2002) sets out the laws covering electrical safety. Nothing in this document is designed, in any way, to undermine the authority of the Acts.
- All reasonable care must always be taken to ensure the plant is without risk to the health and safety of personnel operating and maintaining plant and equipment.
- Employers have an obligation to ensure the workplace health and safety of all personnel at work.
- It is employer responsibility to ensure that all persons entering or working on the premises use appropriate personal protective equipment.
- Personal protective equipment includes gloves, safety glasses, hard hats, ear protection, safe foot ware and, where necessary, specialist protective clothing for hazardous areas.
- Any item of equipment should always be isolated before maintenance or repairs commence to ensure that inadvertent operation of the item does not result in risk to the health and safety of any person.
- Where the item is isolated, any total or partial shutdown should not allow a hazardous situation to be created.
- Where the item cannot be isolated, another person should be stationed at the
 controls of the item and an effective means of direct communication should
 exist between the persons carrying out the maintenance and the person at the
 controls.

General Operating Principles

- All persons working the premises must be qualified Electrical Engineers or electrical trades persons capable of performing the required tasks competently. All personnel must also be familiar with plant and equipment.
- Adequate information, instruction, training and supervision must be provided to enable personnel to perform work without risk to health and safety.
- Work in an orderly way.
- Plan work in advance to avoid hazardous situations.
- Warn others of any hazards.
- Make inquiries before starting work, particularly on any unfamiliar installation or equipment.
- Before any work begins ensure that any instructions received or given are fully understood.
- Concentrate on the task on hand.
- Do not distract others or allow yourself to be distracted by foolish actions.
- Work from a safe and convenient position that provides a maximum working space that you do not have to over reach, you cannot slip, trip or stumble and so endanger yourself and others.
- Keep the working area tidy and free of unwanted materials and equipment.
- Use insulated tools where possible.
- Inspect tools and equipment regularly and ensure that any necessary maintenance is carried out.
- Keep yourself in good health.
- Do not work if ill or over tired, to the extent that your concentration, movement or alertness is affected. Illness or fatigue can endanger yourself and others.

15/05/12

1.2 Project Overview

Contract BW70103-060 was for the manufacture and testing of One (1) new solar powered switchboard to supply power to a QUU free issued PRV switchboard located at Cordelia St South Brisbane.

Equipment provided by SJ Electric ensures safe and efficient operation of the switchboard. Equipment supplied and installed by SJ Electric includes: -

- Switchboards
- Instrumentation
- Civil Works
- Pole mounted Solar Panel

The switchboard incorporates the latest technology in power monitoring, and instrumentation. It is important engineers, technicians and operators are familiar with the equipment installed before attempting any adjustments, modifications or maintenance.

The following Sections of this manual contain a comprehensive description of all equipment supplied, by SJ Electric. It is recommended that this manual be referred to before carrying out any work on any equipment.

1.3 Plant Maintenance

To ensure proper operation of the plant the following should be observed: -

- The plant should be kept clean and tidy at all times. Not only is this of aesthetic value, it extends equipment life.
- Check that all plant and equipment is operating correctly. Correctly operating equipment promotes overall plant efficiency.
- All items and areas of equipment should be hosed down and cleaned regularly.

WARNING

- Avoid directly hosing <u>any</u> drive motor or electrical item.
- All maintenance, service, modifications and significant deviations from Normal operating conditions should be recorded in the Plant Service Log
- After a month of operation, check the tension of all bolts associated with the
 plant and thereafter periodically. Bolted connections on painted surfaces can
 loosen due to thinning of the paint underneath the bolt head-bearing surface.
 Motor mounting bolts and other bolted connections subjected to vibration
 should be periodically checked for loosening.

WARNING

- Before starting work on any item ensure that the power supply is isolated, tagged off, and the item cannot be started.
- The importance of preventative maintenance cannot be over-emphasized.
 Regular maintenance and suitable care of the equipment will ensure a long and reliable service life of the equipment.
- Many stoppages can be avoided by following the recommended maintenance procedures. Do not wait until you hear the grinding of equipment that has broken down. If you see any item wearing down, replace it, before it causes damage to other associated items.

15/05/12

Preventive Maintenance

Maintenance procedures recommended to extend switchboard life are outlined as follows: -

- Switchboard exterior should be regularly wiped down with a solvent base cleaner such as "Spray & Wipe". This will ensure longevity of the powder-coated surface.
- Accessible areas like distribution boards and motor starter panels should be cleaned with a vacuum cleaner to remove dust and foreign matter.
- PLC panels should be maintained as dust free as possible. Dusting with a dry rag is recommended - taking care not allows dust inside the I/O modules or processor.
- When removing or installing PLC modules care should be taken to ensure that power is turned off to the rack before modules are removed or installed.
- Connections and efficient operation of circuit breakers, contactors and isolators should be checked every 12 months - especially where connected to busbars.
- Busbar connections should be checked every 12 months.
- Globes for indicator lights should be checked on a weekly basis with any faulty lamps replaced.
- Cubicle Fans Filter should be inspected and cleaned frequently.

1.4 Electrical Control System

General Description

The switchboards are manufactured from 3mm aluminium and are suitable for location outdoors; the switchboards have been designed by Brisbane Water and contain several separate sections including:

- Incoming Section.
- Distribution Section.
- RTU Section.

1.5 Control and Monitoring System.

The control and monitoring of the system is performed by the Brisbane Water telemetry system and was not included in this contract.

15/05/12

2. Manufacturer's Technical Data

2.1. Terasaki Circuit Breakers

MINIATURE CIRCUIT BREAKERS



TD3 M06 6kA MCBs Functions: protection against overloads and short circuits, switching and isolation. Application: in commercial and industrial electrical distribution systems.

Breaking capacity: Icn = 6kA to EN 60898.

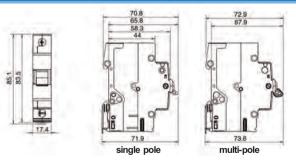
Certified by KEMA Voltage: Un: 230 -240V AC phase-to-neutral, 400-415V AC phase-to-phase Pollution degree: 3 Rigid conductor: 25mm2 maximum lexible conductor: 16mm2 maximum

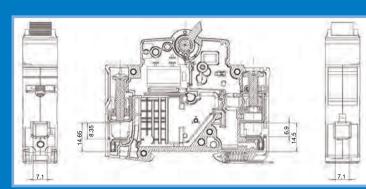
Dual bottom terminal allows simultaneous connection of

busbar and cable

In (A) at 30°C C Type 6-63 6-63 6-63 6-63 6-63 6-63 6-63 6-63 6-63 6-63









Functions: protection against overloads and short circuits, switching and isolation. Application: in commercial and industrial electrical distribution systems.

Breaking capacity: Icn = 10kA to EN60898, Certified by KEMA Icu = 15kA to EN 60947-2 Voltage: Un: 230 -240V AC phase-to-neutral, 400-415V AC phase-to-phase Rigid conductor: 35mm2 maximum Flexible conductor: 25mm2 maximum Dual bottom terminal allows simultaneous connection of busbar and cable

16-63

6-63

6-63

6-63

DIMENSIONS

In (A) at 30°C

2-63

6-63

2-63

2-63

2-63 2-63 1-63

1-63

1-63

1-63



TD31P1M 1 pole + N in 1 module Functions: protection against overloads and short circuits, switching and isolation. Application: single phase circuits where neutral must be

Breaking capacity: Icn = 6kA to EN 60898 Voltage: Un: 240V AC Pollution degree: 2 Rigid conductor: 16mm2 maximum Flexible conductor: 10mm2 maximum

DIN Modules

In (A) at 30°C

B Type

6-40

switched.



TD3 XA MCRs < 125A Functions: protection against overloads and short circuits, switching and isolation. Application: to feed large loads or downstream distribution boards

> Breaking capacity: Icn = 10kA to EN 60898 Breaking capacity: Icu = 10kA to EN 60947-2 Voltage: Un, 240V AC phase-to-neutral, 415V AC phase-to-phase Rigid conductor: 50mm2 maximum Flexible conductor: 35mm2 maximum

> > In (A) at 30°C

C Type

80, 100, 125 80, 100, 125

80, 100, 125 80, 100, 125

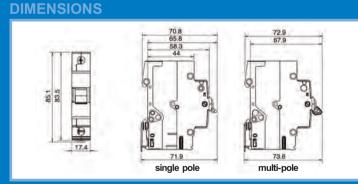
80, 100, 125 80, 100, 125

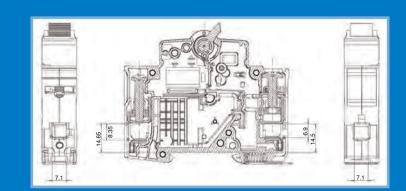


MINIATURE CIRCUIT BREAKERS FOR UTILITY SUPPLIES Function: protection against overloads and short-circuits. Switching and isolation. Application: restriction of maximum current supplied to user by electricity utility company

> Standard: UNE EN 20317 Breaking Capacity: 6kA Voltage: Un, 230 -240V AC phase-to-neutral, 400-415V AC phase-to-phase Rigid conductor: 25mm2 maximum Flexible conductor: 16mm2 maximum Dual bottom terminal allows simultaneous connection of busbar and cable

	In (A)		
Poles	DIN Modules	B Type	
1P	1	5-63	
1P+N	2	5-63	
2P	2	5-63	
3P	3	5-63	
4P	4	5-63	







RESIDUAL CURRENT CIRCUIT BREAKERS

Function: detection and interruption of earth leakage current, overloads and short-circuits. Application: commercial premises. Neutral conductor is switched on 2-module versions and unswitched on 1-module versions

Breaking capacity Icn: 6kA (2P), 10kA (1P) to EN 61009-1 /oltage: Un: 240V AC r: 16mm2 maximum (1P), 25mm2 maximum (2P) Flexible conductor: 10mm2 maximum (1P), 16mm2 (2P)

at 30°C

300mA

25-100 types

AC, A, AC-S

In (A) at 30°C				In (A)
Modules	30mA	300mA	DIN Modules	30mA
2	25-63 types AC, A	25-63, type AC	1	6-40, types B,C
4	25-100 types AC, A	25-100 types AC, A AC-S	2	25-100 types AC, A, AC-S





Application: control systems, distribution systems Standard: EN 60947-3

Class: AC 22 Voltage: Un, 240V AC phase-to-neutral, 415V AC phase-to-phase
Rigid conductor: 16mm2 maximum (32A), 25mm2 maximum (63A), 50mm2 maximum (100A, 125A) Flexible conductor: 10mm2 maximum (32A), 16mm2 maximum (63A), 35mm2 maximum (100A, 125A)

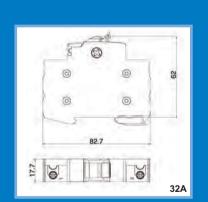
Function: switching and isolation of circuits

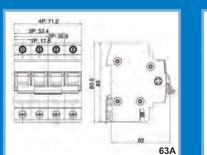
MODULAR SWITCHES

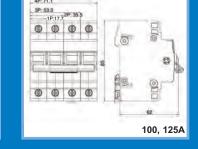
Poles	In (A)
1P	32, 63, 125
2P	63, 125
3P	63, 100*, 125*
4P	63, 100*, 125

*Available with red toggle

DIMENSIONS

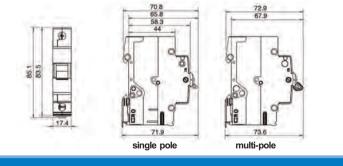


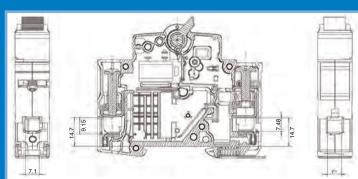




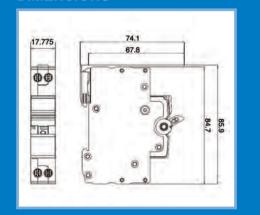
C Type

6-40

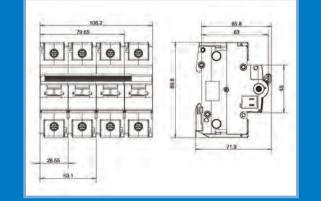




DIMENSIONS



DIMENSIONS









n: detection and interruption of earth leakage

current

Application: protection from electric shock. Must be

combined with an upstream device providing appropriate

overload and short-circuit protection for the circuit.

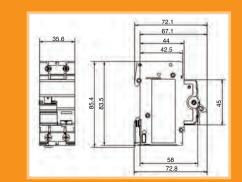
Standard: EN 61008-1 Voltage: Un: 240V AC phase-to-neutral,

415V AC phase-to-phase

Residual current breaking capacity: Im = 1500A

Rigid conductor: 25mm2 maximum

Flexible conductor: 16mm2 maximum



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ACCESSORIES



- Auxiliary contact, 1NO, 1NC, 6A, 230V AC, Not suitable for TD3RCCB
- Alarm contact, 1NO, 1NC, 6A, 230V AC. Not suitable for TD3RCCB
- RCCB switch. Combined auxiliary contact (1NO, 1NC, 6A, 230V AC) + Alarm contact (1NO, 1NC, 6A, 230V AC)
- Shunt trip. RCCB switch (C) must be fitted before fitting the shunt trip to the TD3RCCB
- Undervoltage trip. RCCB switch (C) must be fitted before fitting the undervoltage trip to the TD3RCCB
- Overvoltage trip. Rated voltage, Un, 230V AC. Opens the circuit breaker if supply voltage exceeds 280V AC. RCCB switch (C) must be fitted before fitting the overvoltage trip to the TD3RCCB

TD3 M06, TD3 M10, TD3 XA: auxiliary contact + alarm contact + (shunt trip or undervoltage trip or overvoltage trip) TD3RCCB: RCCB switch + (shunt trip or undervoltage trip or overvoltage trip)

Residual Current Block for TD3 M06. TD3 M10

detection and interruption of earth leakage current Mechanically coupled to miniature circuit breaker

In = 63A maximum			
DIN Modules	30mA	300mA	1000mA
2	2 Types AC, A	Types AC, A	
4	4 Types AC, A	Types AC, A	Types AC A, S





Suitable for locking TD3 M06, TD3 M10, TD3 XA miniature circuit breakers in the open or closed positions. Suitable for locking TD31P1M miniature circuit breakers in the open position only. Accepts two padlocks with hasp diameter up to 4.75mm, or three packlocks with hasp diameter up to 3mm. The miniature circuit breaker may be mounted, or removed from the DIN rail with the

Rotary handle clips onto TD3 ICP miniature circuit breakers, and operates the device from outside the door



Safety and protection are the prime purposes of Terasaki products. Our range of DIN Modular Protection products covers ratings from 0.5A to 125A and includes:

- -Circuit breakers for overload and shortcircuit protection
- -Residual current devices for the prevention of electric shock and fires -Circuit breakers combining overload, short-circuit and residual current protection

With more than 500 items in the range, there is a solution for most applications.



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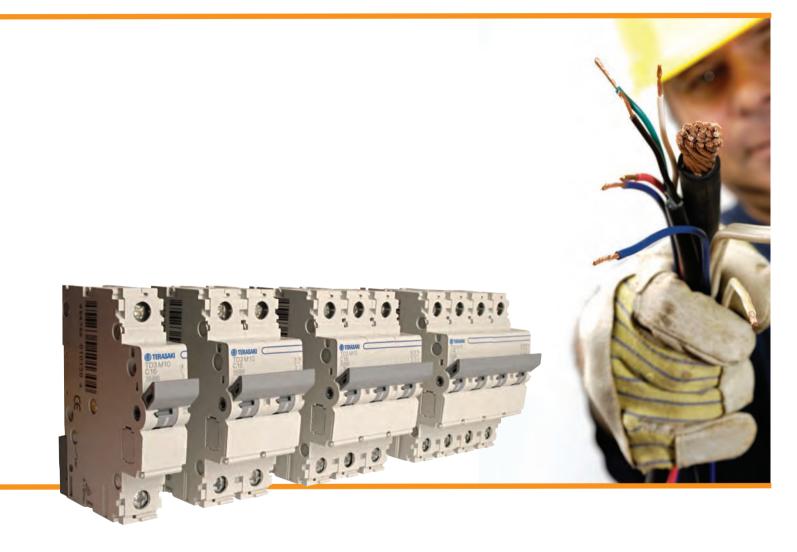
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Ratings and specifications are subject to change without notice.





DIN Modular Protection

For Final Circuits in Industrial and Commercial Buildings

15/10/2012

2.2. Sprecher and Schuh CA-7Contactors

sprecher+ schuh

Contact Block

Performance & Selection



Contact Block	Contact Material			
Considerations	Contact Construction			
	Contact Size/Volume — Stationary vs. Movable			
	Contact Reliability5			
	Contact Resistance			
Switch Design	Single Break vs. Double Break			
Considerations	Contact Motion6			
	Spring Force			
	Overtravel			
	Contact Underlap vs. Contact Overlap			
	Direct Drive			
	Contact Action8			
	Mechanically Linked Contacts			
	Time Delay9			
	Stacking9			
	Wiring Termination			
	Finger-Safe 12			
Special	Environmental Considerations			
Considerations	Environmentally Sealed Devices			
	Standards and Approvals			
	Switch Life			
	Shock and Vibration			
	Dielectric Strength			
	Contact Block Ratings 17			

A combination of many factors affect the dependability, life expectancy, and suitability of a contact block in any given application. Understanding the most important of those factors can help you select the best switch for your needs. In the pages that follow you'll gain a basic understanding of switch materials and properties, and how they affect switch performance.

Contact Material

The contact material forms the surfaces that come in contact with each other to establish an electrical circuit. Typical contact materials include fine silver, nickel-silver, and silver alloys. Fine silver provides low electrical resistance between the movable and stationary contact interface. Silver alloys form harder surfaces to reduce wear and help prevent contact welding.

In low voltage applications (below 48V DC and 0.1 A, or below 24V AC and 0.4 A) where excess oil or dust is present, the use of more noble alloys (such as palladium, gold, and their alloys) in the contact material is recommended. These alloys are highly reliable in this type of environment.

Silver alloys are susceptible to chemical attack which can affect reliability at low voltages. Noble metals resist chemical attack, but are susceptible to frictional polymer formation, which can affect reliability. Combining gold and palladium will resist frictional polymer formation.

Contact Construction

The perimeter of the contact is often shaped like a circle or rectangle and may have little effect on contact performance. The shape of the faces where the fixed and movable contacts meet is more important. This interface should not have two flat surfaces meeting. If one of the contacts has a flat surface, the other contact should be a rounded surface to provide a more defined and controlled touch point.

Figure 1. Bifurcated Spanner Example



The bifurcated style of construction provides a higher degree of reliability than the butt spanner because it divides each movable contact into two sections at the tip of the spanner. This minimizes the chance of foreign materials accumulating on contact surfaces and preventing the completion of the circuit. Even if foreign material accumulates on one of the contact tips, the second tip will most likely touch a clean spot establishing the circuit. Typically, the bifurcated spanner is designed for use in full voltage applications, where the arc between the spanner and stationary contacts will burn off small amounts of contamination in most cases. To aid contact cleaning the contact spanner is designed to flex, which wipes the stationary surface and allows each finger to act independently.

Figure 2. Pentafurcated and Quadfurcated Spanner Examples





In low voltage applications (below 48V DC and 0.1 A or below 24V AC and 0.4 A) pentafurcated/quadfurcated styles of construction provide the highest degree of reliability because they divide each movable spanner contact side into separate flexible fingers. Every part in the system is corrosion-resistant and the flexible spanner is designed to wipe the stationary contacts clean every time the circuit is opened or closed. This is important since the absence of an arc in low voltage environments means that contaminants will not be burned off, but will be eliminated by the wiping action. Therefore, the pentafurcated or quadfurcated are the most reliable styles of spanners available.

Some manufacturers use protrusions such as bars or nibs raised on the face of either the movable or stationary contact to help establish the circuit under low power conditions. These raised surfaces will tend to penetrate non-conducting films that may be present on contact surfaces. They may also lessen the chance of foreign matter preventing completion of the circuit. Such protrusions may, however, quickly burn away under arcing or higher current conditions.

Base materials to which the contact material is attached include copper alloys and steel. Copper alloy is preferable because of its thermal conductivity, electrical conductivity, and corrosion properties.

Contact Size/ Volume — Stationary vs. Movable Contact size refers to the size of the face of the contact or the areas that meet to form the interface between the movable and stationary contacts. Volume is the total amount of contact material.

It is desirable to make one of the contacts smaller than the other so it stays within the perimeter of the other contact when switch action takes place. This arrangement provides greater assurance that alignment of contacts is maintained under repeated operation and resulting wear. Misalignment can cause severe contact wear and shorten switch life.

In the contact set, the movable contact is most often the smaller contact in both size and volume, so that its mass and resulting inertia can be minimized. Partly because of its low volume, the movable contact operates at a higher temperature than the stationary contact. Consequently, the stationary contact will also contribute to a greater rate of wear on the movable contact. The stationary contact is generally attached to a more massive base structure that provides a better heat sink than the movable contact structure.

In alternating current applications, the higher temperature of the movable contact can cause material to be expelled from the surface of the contact. The higher temperature can cause transfer of material to the cooler surface of the stationary contact as well. In direct current applications, the relative polarity of the contacts has a major effect on how the contact material is transferred from one surface to the other.

Contact Reliability

Contact reliability pertains to the ability of contacts to establish a circuit across the interface between the stationary and movable contact set(s) each time the switch is operated. This reliability can be most often adversely affected by two conditions:

- Mechanical debris within the switch
- Non-conducting films that form on the contact surfaces

Mechanical debris or dirt can be introduced into the switch during assembly. Dirt and debris can also be interjected during installation or can be a product of switch action. The wear produced by internal switch components sliding past one another during operation can generate dirt. Care must be taken in the design of moving mechanisms to keep this wear to a minimum.

Non-conducting film and oxides can be formed from gaseous contaminants that enter the switch from an external environment as well as being formed from internally generated reactants. Sealing methods have been developed to isolate the switch interior from the external environment. An understanding of the relationship of all the material used in the construction of a switch is required to eliminate the internally generated reactants. This requires knowledge of the post curing outgassing of any plastics, elastomers, paint, and other components used in the construction of the system. Some gases will react in the presence of an electric arc to form non-conducting films that will cause reliability problems if deposited on the contact face. The tendency of many thermoset plastics to continue to outgas for a period of time after curing has led to the use of thermoplastic materials in switch interiors.

Contact Resistance

Contact resistance pertains to resistance across the interface between a pair of movable and stationary contacts. The higher the value of this resistance, the more difficult it is to establish a circuit when the contacts close. This is especially true in low power circuits. Higher resistance also contributes to contact heating.

The initial contact resistance of both fine silver contacts and noble contact materials (gold, palladium, and their alloys) is 10...15 milliohms. However, the resistance of noble contact materials will remain relatively constant during their lifetime compared to silver contacts, which typically increase over time. These resistance values could vary with the ambient conditions in the vicinity of the contacts themselves

Sealed switches have slightly higher initial contact resistances compared to silver contacts (80...150 milliohms, depending on type), but they remain stable over the life of the device.

In addition to the physical characteristics of the materials used in manufacturing, design considerations also affect the performance of a switching mechanism. In this section you'll gain an overview of those switch design fundamentals and how they affect switch performance.

Single Break vs. Double Break

Figure 3. Single Break Design



Figure 4. Double Break Design



Single break and double break refer to the number of contact pairs that are used to make or break the electrical circuit. Single break means the electrical circuit is controlled by one set of contacts. Double break means the electrical circuit is controlled by two sets of contacts in series.

In a single break design, the contact pair tends to repeatedly make and break the circuit on the same spot on the contact faces. This helps to keep the contact touch point clean, enhancing the contact reliability.

The double break design provides twice the length of air gap in the electrical circuit using the same stroke of the actuating member as with the single break design. The result is the electrical arc that is created by the opening of the circuit will be extinguished sooner and with less actuator movement as compared to a single break design.

Also, since the energy in the arc created upon contact opening is distributed across two air gaps, there is less tendency for the contacts to weld in the double break design.

On the other hand, because of the nature of the double break design, the contact points of the spanner may vary slightly with each actuation. This variation may, over time, affect switch reliability.

Contact Motion

Contact motion refers to the relative motion of the contact faces as they begin to touch one another. Various design techniques are utilized to increase the reliability of the contacts establishing the circuit as they meet.

A wiping or sliding action will help clear surfaces of dirt and oxides and break any nonconducting film that may have formed on contact surfaces. This type of action must be carefully controlled, especially with precious metal contacts, to avoid excessive mechanical wear of the contacts.

Contact tips on the end of the spanner must be capable of flexing and twisting to establish a seat on the surfaces of bifurcated/quadfurcated/pentafurcated stationary contacts. A sliding action of one contact against the other could cause continuity interruptions if the moving contact slides up over a piece of debris.

Spring Force

The spring force discussed in the following paragraphs is the force provided within the contact block that returns the contact structure to its normal or unoperated state when the external force applied to the device operator is removed. This force holds the contact structure in its normal state until an external force is again applied to the device operator.

The amount of spring force is determined by the force required to insure contact reliability under the conditions in a variety of applications. Sufficient force is required to break through contaminants that may be present on the contact faces on the normally closed (N.C.) contacts. The force should insure that contacts stay stable under possible shock and vibration. Light welds created by contact arcing on the normally open (N.O.) contacts should be able to be broken by spring force. The spring force required to maintain circuit reliability is dependant on the contact material hardness. Greater force is required for harder materials.

Spring force directly affects the external force required to operate and to some extent contribute to internal switch friction. Consideration must be given to these factors when determining the spring force used.

Overtravel

Overtravel in a switch pertains to the amount of travel occurring in a switch beyond what is required to operate. Overtravel allows for wear within the switch mechanism. It helps to insure the switch will continue to function as the contacts wear or erode. Overtravel also provides contact stabilization under conditions of shock and vibration.

Contact Underlap vs. Contact Overlap

Contact underlap and overlap refer to the relative action of the N.O. and N.C. contacts when the switch is actuated.

Underlap is the more common type of switch action. As the device operator is moved from its rest position to initiate switch action, the following events take place in order:

- 1. The N.C. contact opens.
- 2. There is a duration where no electrical continuity is present.
- 3. The N.O. contact closes.

In overlap type switch action, the N.O. contact makes its circuit before the N.C. contact breaks its circuit. There is never a period of time when electrical continuity is absent:

- 1. The N.O. contact closes.
- 2. There is a duration where both circuits are active.

7

3. The N.C. contact opens.

The type of switch action selected is dependant on the requirements of the specific user circuit application.

Switch Design Considerations

Direct Drive

NFPA 79 and EN 418 both require that emergency stops must be a direct drive design. A direct drive design switch will have continuous mechanical linkage from the external operating member to the contact carrier. It will not employ the use of any resilient members or springs in the mechanical actuating path to open the N.C. contacts.

A special case of direct drive design is a switch that complies with IEC 60947-5-1. It is designed so that contact separation will take place even though the contacts may have been welded or "sticking" during fault circuit conditions. A direct drive switch is designed to allow contact separation even if the contacts have been lightly welded during fault circuit conditions. The manufacturer provides the fusing level requirements needed to protect these contacts from welding. The actuator movement and actuator force required affecting contact separation are specified by the switch manufacturer.

This type of switch construction is used to help ensure that contact action takes place when the external operating member is actuated. By avoiding the use of any springs in the actuating path, a solid connection is provided directly from the external mushroom operator to the contacts.

Contact opening should always take place at the same point in the actuating stroke and with the same operating force. By their nature, these types of switches fall into the slow break/slow make category of devices although some special designs have been developed that provide positive opening in snap action devices. With increased awareness of safety concerns and the movement toward designing devices that are used globally, greater emphasis has been placed on the direct drive feature.

Contact Action

Contact action refers to how contacts make and/or break the electrical circuit they intend to control. There are two basic types of contact action: slow make/slow break and snap action.

In slow make/slow break action, the contact carrier and contacts move at the same rate of travel as the actuating mechanism. This action is most often obtained with direct drive switch designs. Since the rate of movement of the contacts is solely dependant on the speed of the external actuator, it can result in slow separation of contacts and create a condition called "teasing".

In the teasing condition, the air gap created to break the electrical circuit opens so slowly that arcing occurs between the faces of the stationary and moveable contacts. This arcing is detrimental to the contacts because of accelerated contact wear and material transfer and can cause the contacts to weld rather than separate. The arcing can also cause circuit problems by introducing noise.

Snap action design incorporates a resilient member or springs between the actuator and contact carrier. The springs cause the contacts to move independently of the actuating mechanism. The mechanism is designed so that when actuator movement takes place, not only does the contact carrier movement take place, but energy is also built up in the spring system. Prior to the point in the travel of the actuator where contact separation takes place, the contact carrier and spring system are designed to go into an overcenter mode.

Switch Design Considerations

At the overcenter point, sufficient energy is available in the spring system allowing the carrier to move independently of any further actuator motion and the contacts snap open. This rapid opening prevents teasing and minimizes contact welding. Some snap action devices also incorporate direct opening action. The direct opening action occurs slightly later in the travel than the normal snapover point if the contacts were slightly welded.

Mechanically Linked Contacts

This construction has also been known as "positively guided contacts". It combines a N.C. and N.O. contact combination to prevent N.C. and N.O. contacts from closing at the same time. This nomenclature is generally applied to control relays, but is also applicable to push buttons, pressure and temperature switches, and other control circuit devices. It is generally used for checking control circuit functions.

Time Delay

Time delay of a switching device is the interval between the time when the external operator of the switching device is actuated and the time when the contact action actually occurs.

In a switching device where time delay is provided, contact action takes place at a predetermined time interval after physical action has taken place to displace the external operator in a sufficient manner to operate the device. This time delay is fixed in some devices and adjustable in others to meet circuit requirements. Pneumatic timers are commonly used to perform this function.

Stacking

A switching device that has been designed for stacking has provisions for attaching multiple contact elements to the operator.

Stacking provides a means for multiple circuits to be actuated from a single external operator. A switching device with this capability can perform multiple functions or combinations of functions depending on the type of external operator. A selector switch type operator with several positions in combination with multiple contact elements is one example of this type of device.

Wiring Termination

The following are examples of some of the more common methods of termination used.

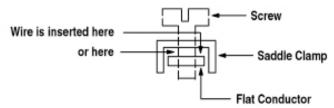
Binding Head Screw

This screw has a larger than normal head. The underside of the screw head has a groove where the wire seats and is secured when the screw is tightened. It is most effective when used with solid wire. A cup washer can be added to accommodate stranded wire, but care must be exercised to ensure that all strands are secured

Saddle Clamp

This is a U-shaped clamp with a screw in the center. The screw threads into a flat conductor on the switching device and the legs of the U slide over the edges of the flat conductor in order to trap the wire.

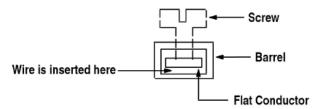
Figure 5.



The saddle clamp should be designed so it tilts to securely clamp a single wire on one side or a different wire size on each side of the clamp.

Barrel Type — This is similar to the saddle clamp design, but instead of a U-shaped clamp, the clamp is rectangular.

Figure 6.



The screw is not threaded into the flat conductor but rather bears against its top surface. This causes the barrel to be drawn upward clamping the wire between the undersurface of the flat conductor and the lower portion of the barrel. A major advantage is the wire is easy to insert into the clamping area.

Pressure Plate

A pressure plate is essentially a flat piece of material with a screw in the center. As with the saddle clamp, the screw threads into the flat conductor on the switching device. Even though the pressure plate is flat, it is designed to force the individual strands of wire to the center of the face plate that comes in contact with the conductor on the switching device where they are restrained. In addition, features are often designed into the body of the switching device that prevent any wire strands from escaping the pressure plate clamping action.

Stab Type

This type of termination is often termed quick-connect, push-on, fast-on, etc. The connection between the switching device and the wire is made with special complementary connection parts. The male part is normally built into the switching device and the female part is mechanically attached to the wire end. Termination is accomplished by mating the connector parts. This method provides a quick way to attach wires to the switching device and it is easy to remove the wires for service.

PC Pin

These are switching devices that can be soldered directly to a printed circuit board or plugged with pin connectors into receptacles mounted on the board.

Lugs and Ferrules

These devices are mechanically secured to the wire end. They make it easier to attach the wire to the switch terminal. They are normally used with stranded wire.

- Lugs provide a flat projection that is usually shaped like a fork or ring. The projection can be inserted under the head of the screw, inserted into saddle clamps, or slipped under pressure plates.
- Ferrules provide a pin type projection well suited for use with saddle clamps, pressure plates, and barrel type terminals.

Solder

Solder can be applied to the end of stranded wire to prevent the individual strands of wire from separating. The end of the wire becomes solid when soldered and can be used with saddle clamps, pressure plates, and barrel type terminals. It should be noted that the solder end will be quite hard and will resist the crushing effect of clamping means. Because of the irregular shape obtained through soldering, only partial contact between the wire and the terminal could result.

Spring-Clamp

This termination style is designed to minimize wiring time. The optimized spring-clamp is designed to reduce stress relaxation while maintaining contact force. An opening force is applied by a lever. The wire is then inserted and the opening force is removed. Upon force removal, the spring-clamp closes on the wire. This design is good for vibration environments.

Because of the large variety of termination options and the importance of establishing and maintaining a reliable connection between the switching device and the circuit, standards have been developed to address this area. The Underwriters Laboratories Pullout and Secureness test is used to insure that termination methods have sufficient strength to retain the wire under conditions of use. This test also determines if the wire strands have been damaged during the wiring process or are susceptible to breakage under conditions of use.

Switch Design Considerations

Finger-Safe

A finger-safe device provides a degree of protection from accidental, casual contact of live electrical parts by personnel. Only those components meeting or exceeding the requirements of IEC standard IP2X (listed under IEC 529) can be considered finger-safe.

Those standards describe a model test finger, along with guidelines for the manner in which the test finger is to be manipulated in the vicinity of the wiring terminals to determine if the switching device provides the required degree of protection.

Some switching devices achieve the finger-safe condition by basic device design while others require an external attachment.

The finger-safe feature is becoming more prevalent as safety issues take on added importance. Higher voltage levels pose a greater risk of injury and liability. A concern of finger-safe design is it may provide a false sense of security to personnel who have access to the area where electrical terminations are made.

Every switch serves as just one element in a complete system. Where and how that system operates plays a significant role in which switch will deliver the most cost-effective performance over time. In the section that follows, you'll gain a better understanding of some of the extraordinary issues involved in switch specification.

Environmental Considerations

Careful consideration of the environment to which the switching device is subjected will help ensure proper operation and acceptable service life. Consideration of external environmental conditions of the operators includes temperature and humidity, shock and vibration, and exposure to washdown, cutting fluids, etc., encountered during operation.

In installations where an unfriendly external environment exists, the switching device should be housed in an enclosure designed to isolate it from the environment. Various enclosure ratings have been developed for use in specific environments and these ratings are regulated by industry standards. The external environment of the switching device can have a profound effect on the operation of the device and on its service life.

Conditions generated within enclosures can also have a negative effect on switch operation and life. Condensation, internally generated chemicals, or trapped dirt are some of the more common problems. In addition, since each switching device is made of a variety of materials, each produces its own internal environment. Caution must be taken during the design of the switching device to ensure the materials selected are proper for this kind of device and are compatible with one another.

The following information points out some key internal and external conditions affecting switching devices, as well as their effects.

Temperature

All electrical devices have a maximum operating temperature rating and this rating is generally understood by the user. The maximum storage temperature and the effects of low temperature are not as well-understood.

Exceeding the high temperature limits can cause degradation of materials within the switch. This degradation can weaken switch parts or release gases from plastics and elastomers. A change in physical dimensions may occur, affecting operational travel and force. A very low temperature environment can cause sticking of the actuator and compromise the return action provided by the internal springs within the switching devices. Great care should be taken to exclude freezing liquids from the vicinity of the external operator or the switch may be inoperative under available levels of operating force.

Large fluctuations in temperature can lead to condensation of water or other liquids, and result in the problems relating to humidity, chemicals, and gases listed below (in those cases it is generally helpful to ventilate the enclosure).

Humidity

Moisture can cause the formation of rust and corrosion on metallic parts as well as contribute to electrical problems such as arc tracking.

Chemicals and Gases

This class of contaminants can cause degradation of material used in the product in a

variety of ways. Corrosion of metallic parts and the degradation of physical properties of plastics and elastomers are among the most common effects. The formation of conductive films on the surface of the insulation can cause arc tracking.

Dirt and Debris

Whether originating internally from wear or damage, or externally, this material can cause friction between moving parts, increase wear, and reduce switch life. Dirt on contacts increases resistance and contributes to contact reliability problems.

Shock and Vibration

Consideration must be given to the shock and vibration to which the switching device is subjected. Severe shocks can cause unintended momentary contact operation that could result in circuit malfunction. Long term exposure to vibration can cause premature wear of the switch elements and generation of internal dirt. Even a poorly designed panel door can repeatedly subject a switching device to damaging shock and vibration.

It's also important to handle a switch with care during installation to avoid damaging shock.

Physical Abuse

Improper handling of the switching device during shipping or installation can cause damage to device components that could affect operation.

Environmentally Sealed Devices

An environmentally sealed device isolates the contact area from the environment.

The most common type of construction has the contacts hermetically sealed within a glass envelope. Prior to sealing, the interior of the glass envelope is filled with an inert gas that keeps the environment around the contacts stable. This construction keeps out explosive gases or contaminants that could affect contact reliability. Since the contacts are not accessible for actuation by mechanical means, they are operated by means of magnetic flux.

A special version of the sealed switch known as a logic reed is used in logic circuits. The logic reed is characterized by very short contact bounce, typically less than 0.5 milliseconds.

Contact isolation can also be accomplished by mechanical means such as a flexible diaphragm. These methods do not, however, provide a true hermetic seal, and are more susceptible to wear and degradation.

Switch Design Considerations

Standards and Approvals

Standards have been developed by industry groups and governmental units to help ensure that switching devices meet certain requirements with regard to installation criteria, safe operation, load carrying ability, minimum mechanical and electrical life, etc.

Once a particular design has met the requirements of a specific standard, a marking may be affixed to devices constructed according to that design indicating that the standards of that particular agency have been met.

Users need to be aware of which standards pertain to the products used in their locations and which approvals are required. Requirements vary depending on the application and the governmental unit having jurisdiction. Some of the standards that apply to switching devices are listed below:

- UL 508
- NEMA ICS 5 part 1
- IEC 60947-5-1
- CSA 22.2 No. 14

Switch Life

Switch life can be defined in a variety of ways. It can be defined as the time when the switch physically fails and can no longer provide contact action. It can also be defined as the point when the operating characteristics change to such a degree that switch action is no longer reliable or the parameters fall outside those required for that application. Examples of the latter would be an increase in operating force or excessive travel to obtain contact action.

A switching device may wear out due to mechanical considerations. Repeated operations cause physical wear of parts due to friction, shock, and stress, and can lead to eventual component failure. Dirt and debris generated by the moving mechanism can cause binding and can be a source of contact contamination.

The electrical life of a switch is not necessarily related to its mechanical life. The electrical life of a switch is primarily load dependant, because the electrical load is the main source of heating in — and damage to — current carrying components. High current loads can also contribute to arcing at the contacts during contact action. This arcing action results in contact erosion and deformation and can lead to welding of the contacts. As a result, it is good practice to evaluate both mechanical and electrical life ratings before selecting a switching device.

The switch environment can cause corrosion. This may lead to friction, physical failure of components, and dirt or corrosion in the contact areas.

Low level switching and infrequent use may allow buildup of film on contact faces, affecting contact reliability. Logic reed switches or switches with precious metal contacts are ideal in these applications.

Shock and Vibration

Shock and vibration refer to the physical conditions that are present in the environment where the switch operates. These conditions often introduce undesirable motion into the device mechanism.

Sources of shock can be the normal motion of the equipment where the device is mounted or the expected movement of the entire control system. Such motion may be repetitive in nature or may occur only periodically under specific situations such as startup, etc. The user may try to anticipate random, abnormal conditions which could result in a high shock situation. One-time mishandling during shipping and installation can cause damage that will affect operation.

Another source of high shock is the slamming of control panel doors where the switching devices are mounted. In order to minimize the effect of known vibration, the axis of actuation of the switching device should not lie on the same plane as that of the direction of normal equipment vibration.

Contact reliability can be affected by shock and vibration. Continual vibration causes mechanical wear and under load conditions, arcing can lead to welding of contacts. A severe shock can cause unintended, momentary contact operation that could result in circuit malfunction.

The mechanical wear caused by long term exposure to vibration can result in the generation of dirt and debris which affects contact reliability and causes added friction in the sliding portions of the mechanism.

Dielectric Strength

Dielectric strength is a measure of the ability of the insulation used in the switching device to withstand the application of a voltage across its surface or through its mass. This will determine the maximum electrical rating of the device.

Degradation of the dielectric strength of insulation can lead to failure of the device. Unintended electrical continuity may be established between circuit elements and ground. In either case, the result is a failure of the switch to perform its intended function.

The most common type of failure is due to arc tracking across the surface of the insulation. The combination of a particular insulation and environmental conditions such as moisture and/or certain gases in the presence of an electrical arc can result in the buildup of a conducting path.

Special Considerations

Contact Block Ratings

The contact block rating of a switching device is the electrical load that the device is capable of switching. This rating is expressed in voltage and current and typically refers to the maximum values that can be switched in a specified number of operations. Although contact blocks are usually rated for maximum conditions, there is a practical low load limit that the contacts will switch in a reliable manner.

Exceeding the high loads can cause burning and pitting of the contacts leading to welding and contributing to arc tracking. If the load to be switched is of a very low energy level, any contaminants or non-conducting films on the contacts may prevent a circuit from being established when the contacts are operated. If loads below 48V DC and 0.1 A, or below 24V AC and 0.4 A, are to be switched, the user must be cautious when selecting the contact materials. If the switching is within a typical Type 4/4X/13 environment, the quadfurcated/pentafurcated blocks should be used for ultimate reliability. If the switching is within Class 1 and 2 Division 2 environment, without a sealing well or a conduit seal off, logic reed, sealed switch, or stackable sealed switch contact blocks should be used. If this type of switch is used at the high end of the rating, then caution should be exercised if these contacts are used for switching low energy loads. The feature built in for establishment of low energy loads may have been burned away during high load switching operations.

Due to the growing popularity of solid-state devices being used in control circuits, the trend in industry is toward lower energy loads.

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2.3. Critec DSF-6A-275 Surge Protection



INSTALLATION INSTRUCTIONS



MODEL NUMBER
 DSF-6A-30V
 DSF-6A-75V
 DSF-6A-150V
 DSF-6A-275V
 DSF-10A-150V
 DSF-20A-150V
 DSF-10A-275V

1. PREPARATION



DANGER: Electrical shock or burn hazard. Installation of this DINLINE Surge Filter should only be made by qualified personnel. Failure

to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections to the electrical panel be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.



CAUTION NOTES:

- Check to make sure line voltage does not exceed Surge Filter voltage requirement.
- 2. Prior to installation ensure that the DSF is of the correct voltage, current, and frequency rating for your application.
- 3. The earth terminal must be connected to a low impedance earth (< 10 ohms) for correct operation.
- Do not perform a "Flash Test" or use a Mega-Ohm Meter (Megger) to test circuits that are protected with DSF modules. Damage may occur to the DSF modules.
- 5. Follow all instructions to ensure correct and safe operation.
- 6. Do not attempt to open or tamper with the DSF units in any way as this may compromise performance and will void warranty.

2. INTRODUCTION

Dinline Surge Filters (DSF) are packaged in "DIN 43 880" profile enclosures for simple installation onto 35mm DIN rails. They can be selected for use on distribution systems with maximum RMS voltages of 30V, 75V, 150V or 275V at frequencies of 50/60Hz. For applications were the voltage regulation on site is poor, refer to the Transient Discriminating Filter (TDF) product range.

3. QUICK INSTALLATION OVERVIEW

Install in the following manner:

- 1. Ensure that power is removed from the area and the circuits that will be connected.
- 2. Snap lock the DSF module to the DIN rail.
- 3. Install the appropriate upstream overcurrent protection (refer to Section 8)
- 4. Connect wiring to the indicated input and output terminals.
- Apply power and observe correct operation of the Status Indication LED.

4. PROTECTION CONCEPTS

To optimise effectiveness of the DSF protection, the unprotected and protected wiring should be separated. Wiring from the exposed transient source to the DSF should be considered unprotected and kept approximately 300mm from all other wiring wherever possible. Wiring on the equipment side of the DSF should be considered protected.

The separation of protected and unprotected wiring is recommended to minimize the risk that transients conducted on unprotected wiring may cross couple onto protected circuits, and diminish the level of protection available from the DSF module.

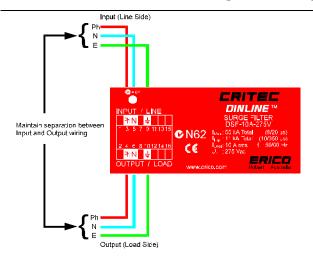
The terminals on the DSF module are labeled "INPUT/LINE" (unprotected side) and "OUTPUT/LOAD" (protected side) assuming that the source of the transients is on the input side of the DSF module.

For applications where the transient source is on the load side of the DSF module, the DSF should be reverse connected with the INPUT/LINE terminals connected to the load side, toward the source of the transients.

NOTE: The terminals on the DSF-6A modules are labeled "L1", "L2" (unprotected side) and "E1", "E2" (protected side). For DC systems the polarity of L1/E1 connections may be either positive or negative with respect to L2/E2. For single phase AC systems with neutral it is recommended to use L1/E1 for the "hot"/phase/line conductors and L2/E2 terminals for the neutral conductors.

DINLINE SURGE FILTER

INSTALLATION INSTRUCTIONS



5. MOUNTING

DSF's are designed to clip to 35mm DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the DSF module spring clips to the bottom and the label text the correct way up.

NOTE: DSF's must be installed in an enclosure or panel that:

- prevents the DSF unit temperature from exceeding 60°C
- provides adequate electrical and safety protection
- · prevents the ingress of moisture and water
- · allows DSF status indicators to be inspected

6. RESIDUAL CURRENT DEVICES

Where RCD's/ELCB's protectors are used, it is preferable that the DSF modules be installed prior to these devices (i.e. upstream). If this is not done, nuisance tripping of the RCD's/ELCB's may occur during transient activity.

7. CONDUCTOR TERMINATION

Each DSF terminal is designed to accept wire sizes from 1.5mm² to 6mm² solid or stranded conductor. The wire insulation should be stripped back 8mm before terminating into the tunnel terminal.

NOTE: Do not use greater than 1Nm of torque when tightening the terminals. Where two wires may need to be terminated into one terminal, the permissible wire size is 4mm² each.

8. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of every DSF to provide protection to the unit itself, the load and the wiring in case of fault situations. The current rating of the breaker or fuse used should be determined according to below. However, the current rating should be less than the rating of the wiring. For example, if a 20A DSF were installed in a circuit with wiring that can carry 16A, then a 16A overcurrent device must be installed upstream to protect both the DSF and wiring from overload.

MAX FUSE SIZES:	DSF RATING	FUSE RATING
	6A	6A
	10A	10A
	20A	20A

9. STATUS INDICATION

DSF modules have a single Status Indicator LED on the front panel. When power is applied and full surge capacity is available, the Status Indicator will be illuminated. Should power be applied and the indicator fail to illuminate, the DSF should be replaced, as optimum protection is no longer provided.

10. MAINTENANCE & TESTING

Before removing a DSF module from service, ensure that the power has been removed from the module. Replacement of a DSF module should only be undertaken by qualified personnel.

NOTE: DSF units should be inspected periodically, and also following any periods of lightning or transient voltage activity. Check the Status Indicator and replace the module if it is not illuminated as detailed in Section 9 STATUS INDICATION.

11. EXTENDED WARRANTY

This product has a limited warranty to be free from defects in materials and workmanship for a period of five (5) years from the date of dispatch from the Manufacturer. The Purchaser acknowledges that lightning is a natural event with statistical variation in behaviour and energy levels which may exceed the product ratings, and 100 % protection is not offered and cannot be provided for. Therefore the Manufacturer's liability is limited to the repair or replacement of the product (at the Manufacturer's sole option) which in its judgement has not been abused, misused, interfered with by any person not authorised by the Manufacturer, or exposed to energy or transient levels exceeding the Manufacturer's specification for the product. The product must be installed and earthed (where applicable) in strict accordance with the Manufacturer's specification and all relevant Electricity and Safety Standards. The Manufacturer and Purchaser mutually acknowledge that the product, by its nature, may be subject to degradation as a consequence of the number and severity of surges and transients that it experiences in normal use, and that this warranty excludes such gradual or sudden degradation. This warranty does not indemnify the Purchaser of the product for consequential claim for the damages or loss of operations or service or profits. Customers should contact their nearest ERICO Lightning Technologies agent to obtain a Product Repair Authorisation Number prior to making any claim under this warranty. This is only a summary of the warranty given by the Manufacturer. The full text of the warranty is set out in the Manufacturer's Conditions of Quotation and Sale. The above limited warranty additional to the rights which arise in respect of the sale of industrial and technical products and services to knowledgeable buyers under the Australian Trade Practices Act 1974 as amended.

2.4. Critec TDS Surge Diverters



CRITEC® Transient Discriminating Surge Diverters





Surge Protection And Surge Ratings

The stress, which an SPD will experience under surge conditions, is a function of many complex and interrelated parameters. These include:

- Location of the SPD(s) within the structure are they located at the main distribution board or within the facility at secondary board, or even in front of the end-user equipment?
- Method of coupling the lightning strike to the facility for example, is this via a direct strike to the structures LPS, or via induction onto building wiring due to a nearby strike?
- Distribution of lightning currents within the structure –
 for example, what portion of the lightning current enters
 the earthing system and what remaining portion seeks
 a path to remote grounds via the power distribution
 system and equipotential bonding SPDs?
- Type of power distribution system the distribution of lightning current on a power distribution system is strongly influenced by the grounding practice for the neutral conductor. For example, in the TN-C system with its multiple earthed neutral, a more direct and lower impedance path to ground is provided for lightning currents than in a TT system.
- Additional conductive services connected to the facility
 these will carry a portion of the direct lightning current and therefore reduce the portion which flows through the power distribution system via the lightning equipotential bonding SPD.
- Type of waveshape it is not possible to simply consider the peak current which the SPD will have to conduct, one also has to consider the waveshape of this surge. It is also not possible to simply equate the areas under the current-time curves (also referred to as the action integral) for SPDs under different waveshapes.

Many attempts have been made to quantify the electrical environment and "threat level" which an SPD will experience at different locations within a facility. The new IEC™ standard on lightning protection, IEC 62305-4 "Protection against lightning - Part 4: Electrical and electronic systems within structures" has sought to address this issue by considering the highest surge magnitude which may be presented to an SPD based on the lightning protection level (LPL) being considered. For example, this standard postulates that under a LPL I the magnitude of a direct strike to the structure's LPS may be as high as 200kA 10/350. While this level is possible, its statistical probability of occurrence is approximately 1%. In other words, 99% of discharges will be less than this postulated 200 kA peak current level.

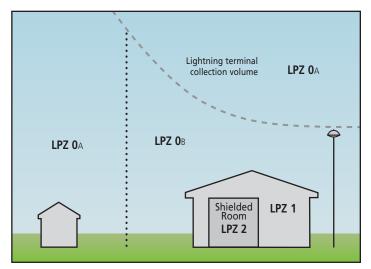
An assumption is made that 50% of this current is conducted via the building's earthing system, and 50% returns via the equipotential bonding SPDs connected to

a three wire plus neutral power distribution system. It is also assumed that no additional conductive service exists. This implies that the portion of the initial 200 kA discharge experienced by each SPD is 25 kA.

Simplified assumptions of current dispersion are useful in considering the possible threat level, which the SPD(s) may experience, but it is important to keep in context the assumptions being made. In the example above, a lightning discharge of 200kA has been considered. It follows that the threat level to the equipotential bonding SPDs will be less than 25kA for 99% of the time. In addition, it has been assumed that the waveshape of this current component through the SPD(s) will be of the same waveshape as the initial discharge, namely 10/350, while in reality the waveshape have been altered by the impedance of building wiring, etc.

Many standards have sought to base their considerations on field experience collected overtime. For example, the IEEE® guide to the environment C62.41.1 and the recommended practice C62.41.2 present two scenarios of lightning discharge and different exposure levels under each of these depending on the location where the SPD is installed. In this standard, Scenario II depicts a direct strike to the structure, while Scenario I depicts a nearby strike and the subsequent conducted current into a structure via power and data lines. The highest surge exposure considered feasible to an SPD installed at the service entrance to a facility under Scenario I is 10kA 8/20, while under Scenario II it is considered to be 10kA 10/350 (exposure Level 3).

From the above, it is apparent that the selection of the appropriate surge rating for an SPD depends on many complex and interconnected parameters. When addressing such complexities, one needs to keep in mind that one of the more important parameters in selecting an SPD is its limiting voltage performance during the expected surge event, and not the energy withstand which it can handle.



Protection zones defined by specific product application.

Advanced Technologies – The ERICO® Advantage

Transient Discriminating Technology

To meet the fundamental requirements of performance, longer service life and greater safety under real world conditions, ERICO has developed Transient Discriminating (TD) Technology.

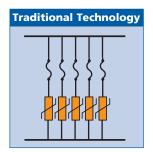
This quantum leap in technology adds a level of "intelligence" to the Surge Protection Device enabling it to discriminate between sustained abnormal over-voltage conditions and true transient or surge events. Not only does this help ensure safe operation under practical application, but it also prolongs the life of the protector since permanent disconnects are not required as a means of achieving internal over-voltage protection.

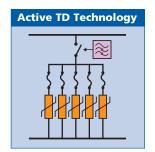
Traditional Technologies

Conventional SPD technologies utilize metal oxide varistors and/ or silicon avalanche diodes to clamp or limit transient events. However, these devices are susceptible to sustained 50/60Hz mains over-voltage conditions which often occur during faults to the utility system. Such occurrences present a significant safety hazard when the suppression device attempts to clamp the peak of each half cycle on the mains over-voltage. This condition can cause the device to rapidly accumulate heat and in turn fail with the possibility of inducing a fire hazard.

The Core of TD Technology

The secret to ERICO's Transient Discriminating Technology is its active frequency discrimination circuit. This patented device can discriminate between a temporary over-voltage (TOV) condition



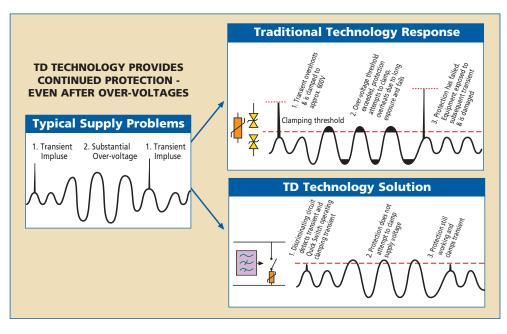


and a very fast transient, which is associated with lightning or switching-induced surges. When the transient frequencies are detected, the patented Quick-Switch within TD activates to allow the robust protection to limit the incoming transient. The frequency discriminating circuit that controls the Quick-Switch helps ensure that the SPD device is immune to the effects of a sustained 50 or 60Hz TOV. This allows the device to keep operating, in order to help provide safe and reliable transient protection, even after an abnormal over-voltage condition has occurred.

Meeting & Exceeding UL® Standards

The CRITEC® range of surge protection devices from ERICO® employing TD Technology has been specifically designed to meet and exceed the new safety requirements of UL 1449 Edition 3. To meet the abnormal over-voltage testing of UL 1449 Edition 3, many manufacturers of SPD devices have incorporated fuse or thermal disconnect devices which permanently disconnect all protection from the circuit during an over-voltage event. Transient Discriminating Technology on the other hand will allow the SPD device to experience an abnormal overvoltage up to twice its nominal operating voltage and still remain operational even after this event! This allows the device to help provide safe, reliable and continuous protection to your sensitive electronic equipment. TD Technology is especially recommended for any site where sustained over-voltages are known to occur, and where failure of traditional SPD technologies cannot be tolerated.

The UL 1449 testing standard addresses the safety of an SPD device under temporary and abnormal overvoltage conditions, but does not specifically mandate a design that will give a reliable, long length of service in the real world. Specifically, UL 1449 tests that the SPD remains operational at 10% above nominal supply voltage, allowing SPD manufacturers to design products that permanently disconnect just above that. Most reputable manufacturer's designs allow for up to a 25% overvoltage, while ERICO's TD Technology gives even greater overhead.



Features

- CRITEC TD
 Technology with
 thermal disconnect
 protection
- Compact package, modular DIN rail mounting for limited space requirements
- Three modes of protection: L-N, L-PE & N-PE
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 15kA 8/20µs surge rating per mode
- CE, UL® 1449 Edition 3 Listed

CRITEC® TDS Surge Diverter - TDS130 Series

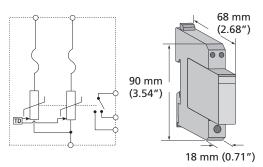
Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.

The TDS130 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. The TDS130 is specifically designed for the protection of single phase power supplies within instrumentation and control applications. They are conveniently packaged for easy installation on 35 mm DIN rail within control panels.

CRITEC® TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of life. A visual indicator flag provides user-feedback in the event of such operation. The TDS130 provides a set of optional voltage-free contacts for remote signaling that maintenance is required.

The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.





Model	TDS1301TR150	TDS1301TR240	
Item Number for Europe	702421	702422	
Nominal Voltage, U _n	120-150 VAC	220-240 VAC	
Max Cont. Operating Voltage, Uc	170VAC	275VAC	
Stand-off Voltage	230VAC	440VAC	
Frequency	0-100Hz		
Nominal Discharge Current, In	8kA 8/20µs per mode		
Max Discharge Current, I _{max}	15kA 8/20µs L-N		
	15kA 8/20µs L-PE		
Protection Modes	L-G, L-N, N-G		
Technology	TD Technology with thermal disconnect		
Short Circuit Current Rating, Isc	200kAIC		
Back-up Overcurrent Protection	63AgL, if supply > 63A		
Voltage Protection Level, Up	500V @ 3kA (L+N-G)	800V @ 3kA (L+N-G)	
	800V @ 3kA (L-N)	1500V @ 3kA (L-N)	
Status	N/O, N/C Change-over contact, 250V~/0.5A,	max 1.5 mm ² (#14AWG) terminals	
	Mechanical flag / remote contacts (R model	l only)	
Module Width	1 M		
Dimensions H x D x W: mm (in)	90 x 68 x 18 (3.54 x 2.68 x 0.71)		
Weight: kg (lbs)	0.12 (0.26)		
Enclosure	DIN 43 880, UL94V-0 thermoplastic, IP 20 (N	IEMA-1)	
Connection	1 mm ² to 6 mm ² (#18AWG to #10AWG)		
	Line and Neutral Terminals		
	≤25 mm² (#4AWG) stranded		
	≤35 mm² (#2AWG) solid		
	PE Terminal		
Mounting	35 mm top hat DIN rail		
Temperature	-40°C to 80°C (-40°F to 176°F)		
Humidity	0% to 90%		
Approvals	CE, IEC® 61643-1, UL® 1449 Ed 3 Recognized	Component Type 2	
Surge Rated to Meet	ANSI®/IEEE® C62.41.2 Cat A, Cat B		
_	IEC 61643-1 Class II		
	UL® 1449 Ed3 In 3kA mode		
Replacement Module	TDS130M150 TDS130M240		
Replacement Module (Europe)	702432 702424		

Features

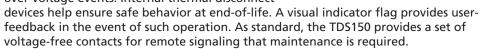
- CRITEC® TD
 Technology with
 thermal disconnect
 protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount – DIN 43 880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 50kA 8/20µs maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL[®] 1449
 Edition 3 Listed

CRITEC® TDS Surge Diverter - TDS150 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.

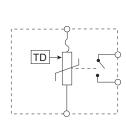
The TDS150 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.

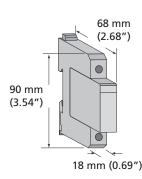
CRITEC® TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect



The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.







Model	TDS1501SR150	TDS1501SR240	TDS1501SR277	TDS1501SR560
Item Number for Europe	702404	702406	702407	702408
Nominal Voltage, Un	120-150 VAC	220-240 VAC	240-277 VAC	480-560 VAC
Max Cont. Operating Voltage, Uc	170VAC	275VAC	320VAC	610VAC
Stand-off Voltage	240VAC	440VAC	480VAC	700VAC
Frequency	0-100Hz			
Short Circuit Current Rating, Isc	200kAIC			
Back-up Overcurrent Protection	125AgL, if supply	' > 100A		
Technology	TD with thermal	disconnect		
Max Discharge Current, I _{max}	50kA 8/20µs			
Nominal Discharge Current, In	25kA 8/20µs	20kA 8/20		
Protection Modes	Single mode (L-G	, L-N or N-G)		
Voltage Protection Level Up	400V @ 3kA	700V @ 3kA	800V @ 3kA	1.8kV @ 3kA
	1.0kV @ In	1.2kV @ In	1.6kV @ In	2.4kV @ In
Status	N/O, N/C Change-over contact, 250V~/0.5A, max 1.5 mm ² (#14AWG)			
	terminals			
	Mechanical flag /	remote contacts ((R model only)	
Dimensions H x D x W: mm (in)	90 x 68 x 18 (3.54 x 2.68 x 0.69)			
Module Width	1 M	,		
Weight: kg (lbs)	0.12 (0.26)			
Enclosure	DIN 43 880, UL94	V-0 thermoplastic	, IP 20 (NEMA-1)	
Connection	≤25 mm² (#4AW0	3) stranded		
	≤35 mm² (#2AW0	G) solid		
Mounting	35 mm top hat D	ÍN rail		
Temperature	-40°C to 80°C (-40)°F to 176°F)		
Humidity	0% to 90%	•		
Approvals	CE, IEC® 61643-1,	UL® 1449 Ed 3 Red	cognized Compon	ent Type 2
Surge Rated to Meet	ANSI®/IEEE® C62.41.2 Cat A, Cat B, Cat C			
			posure 2, 50kA 8/2	20µs
	IEC 61643-1 Class II			
	UL® 1449 Ed3 In 20kA mode			
Replacement Module	TDS150M150	TDS150M240	TDS150M277	TDS150M560
replacement Module	טכו ואוטכו כטון	I DO I DOIVIZAO	I D J I J U I V I Z I I	טטכואוטכו כסון

TDS1100

Features

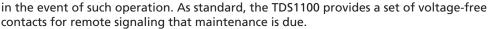
- CRITEC® TD
 Technology with thermal disconnect protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount – DIN 43 880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 100kA 8/20µs maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL[®] 1449
 Edition 3 Listed

CRITEC® TDS Surge Diverter - TDS1100 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.

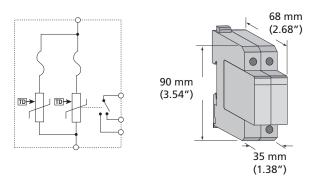
The TDS1100 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.

CRITEC® TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A visual indicator flag provides user-feedback



The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.





Model	TDS11002SR150	TDS11002SR240	TDS11002SR277	TDS11002SR560
Item Number for Europe	702409	702411	702412	702413
Nominal Voltage, Un	120-150 VAC	220-240 VAC	240-277 VAC	480-560 VAC
Max Cont. Operating Voltage, Uc	170VAC	275VAC	320VAC	610VAC
Stand-off Voltage	240VAC	440VAC	480VAC	700VAC
Frequency	0-100Hz			
Short Circuit Current Rating, Isc	200kAIC			
Back-up Overcurrent Protection	125AgL, if supply >			
Technology	TD with thermal di	sconnect		
Max Discharge Current, I _{max}	100kA 8/20µs			
Impulse Current, I _{imp}	12.5kA 10/350µs			
Nominal Discharge Current, In	50kA 8/20µs	40kA 8/20µs		
Protection Modes	Single mode (L-G, I			
Voltage Protection Level, Up	400V @ 3kA	700V @ 3kA	800V @ 3kA	1.8kV @ 3kA
	1.0kV @ 20kA	1.2kV @ 20kA	1.6kV @ 20kA	2.4kV @ 20kA
Status	N/O, N/C Change-over contact, 250V~/0.5A, max 1.5 mm² (#14AWG) terminals			
	Mechanical flag / remote contacts (R model only)			
Dimensions H x D x W: mm (in)	90 x 68 x 35 (3.54 x	2.68 x 1.38)		
Module Width	2 M			
Weight: kg (lbs)	0.24 (0.53)			
Enclosure		-0 thermoplastic, IP :	20 (NEMA-1)	
Connection	≤25 mm² (#4AWG)	stranded		
	≤35 mm² (#2AWG)	solid		
Mounting	35 mm top hat DIN			
Temperature	-40°C to 80°C (-40°	F to 176°F)		
Humidity	0% to 90%			
Approvals		IL® 1449 Ed 3 Recogi		ype 2
Surge Rated to Meet	ANSI®/IEEE® C62.41.2 Cat A, Cat B, Cat C			
	ANSI®/IEEE® C62.41	.2 Scenario II, Expos	ure 3, 100kA 8/20µs	, 10kA 10/350µs
	IEC 61643-1 Class I and Class II			
	UL® 1449 Ed3 In 20kA mode			
Replacement MOV Module	TDS150M150	TDS150M240	TDS150M277	TDS150M560

Features

- CRITEC® TD
 Technology with
 thermal disconnect
 protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount – DIN 43 880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 50kA 8/20µs maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL® 1449 Edition 3 Listed

CRITEC® TDS Surge Diverter - TDS350 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.

CRITEC® TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A visual indicator flag provides user-feedback in the

event of such operation. As standard, the TDS provides a set of voltage-free contacts for remote signaling that maintenance is due.

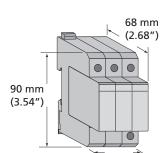
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.



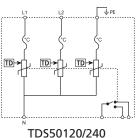
90 mm

(3.54")





70 mm (2.76")



₽				
TDS350TNC				

10330120/240		אווטככנטו	•	53	3 mm (2.07")
Model	TDS350TNC150	TDS50120240	TDS350TNC277	TDS350TT150	TDS350TT277
Item Number for Europe	702414	702419	702417	702416	702418
Nominal Voltage, U _n	120-150 VAC		240-277 VAC	120-150 VAC	240-277 VAC
Max Cont. Operating Voltage, Uc	170/295VAC	240/480VAC	320/536VAC	170/295VAC	320/536VAC
Stand-off Voltage	240/415VAC	240/480VAC	480/813VAC	240/415VAC	480/813VAC
Frequency	0-100Hz				
Short Circuit Current Rating, Isc	200kAIC				
Back-up Overcurrent Protection	125AgL, if supply	y > 100A			
Technology	TD with thermal	disconnect			
Max Discharge Current, I _{max}	50kA 8/20µs			12.5kA 10/350	µs N-PE
				50kA 8/20µs	
Nominal Discharge Current, In	25kA 8/20µs		20kA 8/20	25kA 8/20µs	20kA 8/20
Protection Modes	L-N	L-N, N-PE	L-N	L-N, N-PE	
Voltage Protection Level, Up	400V @ 3kA		800V @ 3kA	400V @ 3kA	800V @ 3kA
	1.0kV @ In		1.6kV @ In	1.0kV @ In	1.6kV @ In
Status			.50V~/0.5A, max 1	.5 mm² (#14AW	/G) terminals
	Mechanical flag	/ remote contac	ts		
Dimensions H x D x W: mm (in)	90 x 68 x 53 (3.54 x 2.68 x 2.07)			90 x 68 x 70 (3.54 x 2.68 x 2.76)	
Module Width	3 M			4 M	
Weight: kg (lbs)	0.36 (0.79)			0.5 (1.10)	
Enclosure			stic, IP 20 (NEMA-	1)	
Connection	≤25 mm² (#4AW	.,			
	≤35 mm² (#2AW				
Mounting	35 mm top hat D				
Temperature	-40°C to 80°C (-4	0°F to 176°F)			
Humidity	0% to 90%				
Approvals			Recognized Comp	oonent Type 2	
Surge Rated to Meet	ANSI®/IEEE® C62.				
	ANSI®/IEEE® C62.41.2 Scenario II, Exposure 2, 50kA 8/20µs				
	IEC 61643-1 Class II				
	UL® 1449 Ed3 In	20kA mode			
Replacement MOV Module	TDS150M150		TDS150M277	TDS150M150	TDS150M277
Replacement GDT Module	- SGD112M				
Replacement GDT Module (Europe)	702403				







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WARNING

ERICO products shall be installed and used only as indicated in ERICO's product instruction sheets and training materials. Instruction sheets are available at www.erico.com and from your ERICO customer service representative. Improper installation, misuse, misapplication or other failure to completely follow ERICO's instructions and warnings may cause product malfunction, property damage, serious bodily injury and death.

2.5. Critec DAR-275V Alarm Relay



INSTALLATION INSTRUCTIONS



MODEL NUMBER DAR 275V

1. PREPARATION

Installation of this device should only be made by qualified personnel. Failure to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.



CAUTION NOTES:

- The installation of this device should follow all applicable electrical codes, such as the National Electrical Code.
- 2. Check to make sure line voltage does not exceed DAR275V voltage ratings.
- 3. Follow all instructions to ensure correct and safe operation.
- Do not attempt to open or tamper with the DAR in any way as this may compromise performance and will void warranty. No user serviceable parts are contained.

2. INTRODUCTION

Selected DSD, TDS & TDF DINLINE Surge Protection Devices include status monitoring circuits which provide visual status display of device capacity. They may also provide a low voltage opto-coupler alarm output circuit that can be connect to the DAR to provide potential free (Form C) change-over contacts. The DAR alarm contacts may be used to provide output to external alarm systems or remote monitoring circuits.

One DAR can be used per DSD/TDS/TDF opto-coupler alarm or up to 16 DSD opto-coupler alarms can be connected in series to the one DAR to provide a common output. It is recommended that the DAR be powered from the same power circuit that feeds the device(s) being monitored, however the DAR can be powered from other circuits. This allows for example, one DAR unit to be connected to separate SPDs that are protecting a three phase circuit.

Note. Depending upon the usage of the DAR output contacts, failure of power to the DAR may be interpreted as a failure of one or more of the SPDs being monitored. Visual inspection of the DAR and SPDs status displays would determine this.

3. MOUNTING

The DAR is designed to clip to 35mm (top hat) DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the DAR module spring clips to the bottom and the label text the correct way up.

NOTE: The DAR must be installed in an enclosure or panel that:

- prevents the DAR temperature from exceeding 131°F (55°C)
- provides adequate electrical and safety protection
- · prevents the ingress of moisture and water
- allows DAR status indicators to be inspected

4. ELECTRICAL CONNECTION

The interconnecting wiring should:

- be of size #10 to #14 AWG (2.5mm² to 6mm²) solid or stranded conductor.
- The wire insulation should be stripped back 5/16" (8mm).
- NOTE: Do not use greater than 9inlbs (1Nm) of torque when tightening the terminals.

CONNECTION TO TELECOMMUNICATIONS NETWORKS

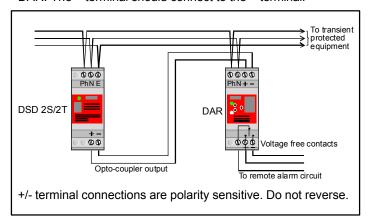
The DAR is approved for use in Australia where the alarm contacts may be connected to private lines or building cabling associated with the telecommunications network. NO direct connection to the public switched network should be made.



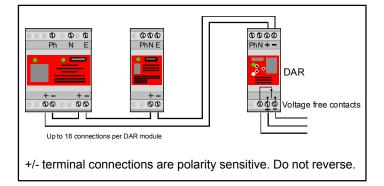
INSTALLATION INSTRUCTIONS

5. INTERCONNECTION

When connecting the DAR to a single opto-coupler output the + terminal of the SPD should connect to the + terminal on the DAR. The – terminal should connect to the – terminal.



When connecting the DAR to multiple opto-couplers the opto-couplers should be connected in series with + terminal of one connected to the – terminal of the next. The DAR + terminal should connect to + SPD terminal at one end of the series connection and the – DAR terminal connect to the – SPD terminal at the other end of the series connection.



5. STATUS INDICATION

	1	!	X
STATUS	Protection Operational	Protection Alarm	Fault Mode
DISPLAY	Normal	Normal O 8 Fault - 6	Normal O ® Fault O 6
EXPLANATION	Red indicator OFF Relay is energised	DSD in alarm mode or power to DSD has been removed Normal (green) indicator OFF Red indicator ON Relay is de-energised Power is supplied	Power to DAR removed Protection status unknown Normal (green) indicator OFF Red indicator OFF Relay is de-energised Power is OFF

6. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of the power supply to the DAR to provide protection to the unit itself and the wiring in case of fault conditions.

The fuse rating should be based on the wiring size used to connect to the DAR Ph & N terminals. Australian regulations AS3000-1991, Table B2 specifies the following upstream protection for single phase circuits, unenclosed in air.

Cable Size	HRC Fuse or	CB Rewirable Fuse
1.5mm ²	16A	12A
2.5mm ²	20A	16A
4mm ²	25A	20A
6mm ²	32A	25A

Where overcurrent protection of the appropriate rating or smaller is already fitted in the upstream circuit, overcurrent protection at the DAR will not be required

6. MAINTENANCE & TESTING

Before removing a DAR unit from service, ensure that the power has been removed. Maintenance, testing and replacement should only be undertaken by qualified personnel.

Testing of a DAR unit which is connected to a fully functional DSD unit can be accomplished by removing power to the DSD only. The DAR Status indication and output contacts should alter from the Normal to Fault condition.

Testing of the DAR unit alone may be accomplished by disconnecting the + / -connections to the unit. When power is applied the DAR "Fault" Status Indicator should be illuminated. By connecting the + / - terminals together, the "Normal" Status Indicator should be illuminated. The output contacts should alter to the appropriate state.

7. USE OF OTHER INTERFACES

Only DAR units are recommended for the interfacing of equipment to the DSD, TDS & TDF opto-coupler alarm output circuit(s). The direct connection of other equipment to these opto-coupler alarm outputs may not provide sufficient isolation or exceed the opto-coupler specifications. This may damage the SPD and/or the connected equipment. Warranty may be voided under such circumstances.

NOTE: In connecting to the SPD opto-coupler alarm output(s), do not reverse the +/- connections as damage may occur.

2.6. Carlo Gavazzi Monitoring Relays

Monitoring Relays True RMS 3-Phase, 3-Phase+N, Multi-function Types DPB01, PPB01







- TRMS 3-phase over and under voltage, phase sequence and phase loss monitoring relays
- Detect when all 3 phases are present and have the correct phase sequence (except for N versions)
- Available versions (W4) supplied between phase and neutral
- Detect if all the 3-phase-phase or phase-neutral voltages are within the set limits
- · Upper and lower limits separately adjustable
- Measure on own power supply
- Selection of measuring range by DIP-switches
- · Adjustable voltage on relative scale
- Adjustable delay function (0.1 to 30 s)
- Output: 8 A SPDT relay N.E.
- For mounting on DIN-rail in accordance with DIN/EN 50 022 (DPB01) or plug-in module (PPB01)
- 22.5 mm Euronorm housing (DPB01) or 36 mm plug-in module (PPB01)
- · LED indication for relay, alarm and power supply ON

Product Description

3-phase or 3-phase+neutral line voltage monitoring relay for phase sequence, phase loss, over and under voltage (separately adjustable set points) with built-in time delay function.

Supply ranges from 208 to 480 VAC covered by two multivoltage relays.

Ordering Key DPB 01 C M23 Housing Function Type Item number Output

Type Selection

Mounting	Phase sequence detection	Output	Supply: 208 to 240 VAC	Supply: 380 to 415 VAC	Supply: 380 to 480 VAC
DIN-rail	yes	SPDT	DPB 01 C M23	DPB 01 C M48 W4	DPB 01 C M48
Plug-in	yes	SPDT	PPB 01 C M23	PPB 01 C M48 W4	
Plug-in	yes	SPDT		PPB 01 C M48	
DIN-rail	no	SPDT	DPB 01 C M23 N	DPB 01 C M48 N W4	DPB 01 C M48 N
Plug-in	no	SPDT	PPB 01 C M23 N	PPB 01 C M48 N W4	
Plua-in	no	SPDT		PPB 01 C M48 N	

Power supply

Input Specifications

Input L1, L2, L3, N	DPB01: Terminals L1, L2, L3, N	Ranges Upper level	+2 to +22%
Note: Connect the neutral only	PPB01: Terminals 5, 6, 7, 11 Measure on own supply	Lower level	of the nominal voltage -22 to -2% of the nominal voltage
if it is intrinsically at the star centre		Note: The input voltage must not exceed the maximum	or the normal voltage
Measuring ranges 208 to 240 VAC	177 to 275 V _{L-L} AC M23 versions	rated voltage or drop below the minumum rated voltage reported above.	
380 to 415 VAC	323 to 475 V _{L-L} AC PPB01CM48 PPB01CM48N D/P PB01CM48W4 D/P PB01CM48NW4	Hysteresis Set points from 2 to 5% Set points from 5 to 22%	1% 2%
380 to 480 VAC	323 to 550 V _{L-L} AC DPB01CM48 DPB01CM48N		



Output Specifications

Output Rated insulation voltage	SPDT relay 250 VAC
Contact ratings (AgSnO ₂)	μ
Resistive loads AC 1	8 A @ 250 VAC
DC 12	5 A @ 24 VDC
Small inductive loads AC 15	2.5 A @ 250 VAC
DC 13	2.5 A @ 24 VDC
Mechanical life	30 x 10 ⁶ operations
Electrical life	10 ⁵ operations
	(at 8 A, 250 V, $\cos \varphi = 1$)
Operating frequency	7200 operations/h
Dielectric strength	
Dielectric voltage	2 kVAC (rms)
Rated impulse withstand volt.	4 kV (1.2/50 μs)

Supply Specifications

Power supply Rated operational voltage through terminals: L1, L2, L3, N (DPB01) 5, 6, 7, 11 (PPB01)	Overvoltage cat. III (IEC 60664, IEC 60038)
D/P PB01CM23, D/P PB01CM23N	208 to 240 V _{L-L} AC ±15% 45 to 65 Hz
D/P PB01CM48W4, D/P PB01CM48NW4, PPB01CM48, PPB01CM48N	380 to 415 V_{L-L} AC $\pm 15\%$ (220 to 240 V_{L-N} AC $\pm 15\%$) 45 to 65 Hz
DPB01CM48, DPB01CM48N	380 to 480 V _{L-L} AC ±15% (220 to 277 V _{L-N} AC ±15%) 45 to 65 Hz
Rated operational power	
DPB01CM23x, PPB01CM23x DPB01CM48x, PPB01CM48x	13 VA @ 230 ΔVAC, 50 Hz 13 VA @ 400 ΔVAC, 50 Hz Supplied by L1 and L2
DPB01CM48xW4 DPB01CM48xW4	13 VA @ 400 ΔVAC, 50 Hz Supplied by L1 and N

General Specifications

Power ON delay		1 s ± 0.5 s or 6 s ± 0.5 s
Reaction time Incorrect phase set total phase loss Voltage level Alarm ON delay Alarm OFF delay	quence or	< 200 ms (input signal variation from -20% to +20% or from +20% to -20% of set value) < 200 ms (delay < 0.1 s) < 200 ms (delay < 0.1 s)
Accuracy Temperature drift Delay ON alarm Repeatability		(15 min warm-up time) ± 1000 ppm/°C ± 10% on set value ± 50 ms ± 0.5% on full-scale
Indication for Power supply ON Alarm ON Output relay ON		LED, green LED, red (flashing 2 Hz during delay time) LED, yellow
Environment Degree of protection Pollution degree Operating tempera @ Max. voltage @ Max. voltage Storage temperatu	ture je, 50 Hz je, 60 Hz	IP 20 3 (DPB01), 2 (PPB01) -20 to 60°C, R.H. < 95% -20 to 50°C, R.H. < 95% -30 to 80°C, R.H. < 95%
Housing Dimensions	DPB01 PPB01	22.5 x 80 x 99.5 mm 36 x 80 x 94 mm
Weight		Approx. 120 g
Screw terminals Tightening torque		Max. 0.5 Nm according to IEC 60947
Approvals		UL, CSA (except for W4 versions)
CE Marking		Yes
EMC Immunity Emissions		Electromagnetic Compatibility According to EN 61000-6-2 According to EN 61000-6-3

Mode of Operation

Connected to the 3 phases (and neutral) DPB01 and PPB01 operate when all 3 phases are present at the same time, the phase sequence is correct (not N versions) and the phase-phase (or phase-neutral) voltage levels are within set limits.

If one or more phase-phase or phase-neutral voltages exceeds the upper set level or drops below the lower set level, the red LED starts flashing 2 Hz and the output relay releases after the set time period. In any case if phase-neutral measurement is selected both phase-phase and phase-neutral voltages are monitored. If the phase sequence is wrong or one phase is lost, the output relay releases immediately.

Only 200 ms delay occurs. The failure is indicated by the red LED flashing 5 Hz during the alarm condition.

Example 1 (mains network monitoring)

The relay monitors over and under voltage, phase loss and correct phase sequence. In case of N versions, the relay monitors over and under voltage.

Example 2 (load monitoring)

The relay releases in case of interruption of one or more phases, when one or more voltages drop below the lower set level or exceed the upper set level.

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Function/Range/Level and Time Delay Setting

Adjust the input range setting the DIP switches 3 and 4 as shown below.

Select the desired function setting the DIP switches 1 and 2 as shown below.

To access the DIP swiches open the grey plastic cover as shown below

Selection of level and time delay:

Upper knob:

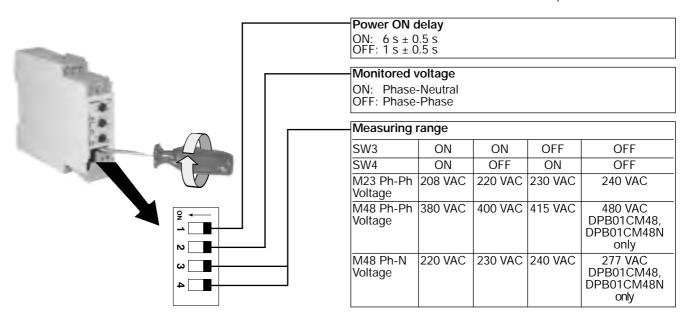
Setting of lower level on relative scale.

Centre knob:

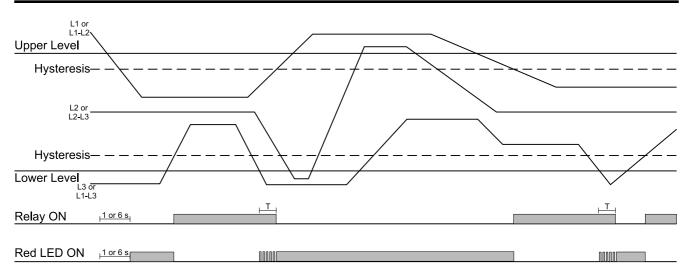
Setting of upper level on relative scale.

Lower knob:

Setting of delay on alarm time on absolute scale (0.1 to 30 s).

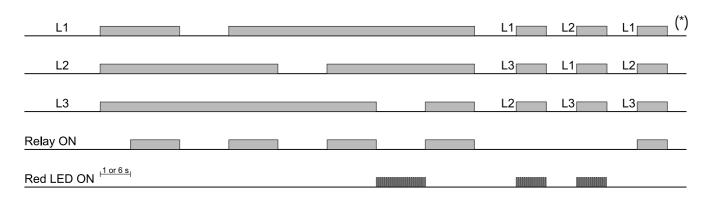


Operation Diagrams



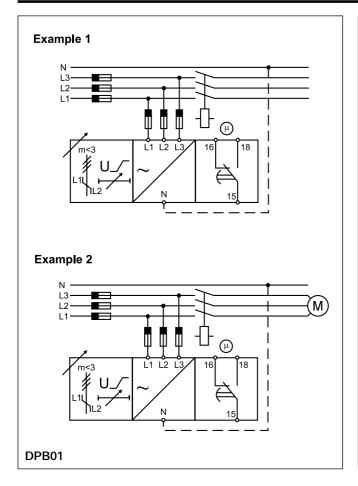


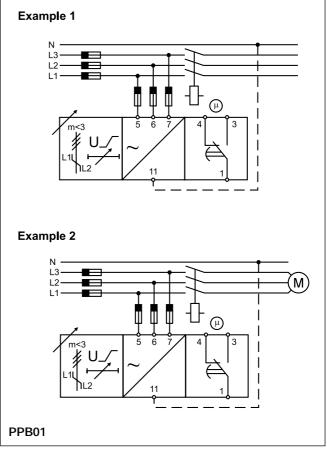
Operation Diagrams (cont.)



(*) N versions don't detect incorrect phase sequence.

Wiring Diagrams



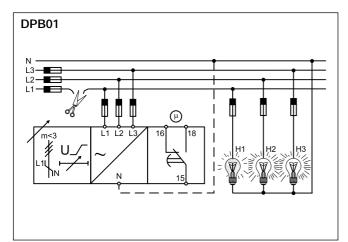


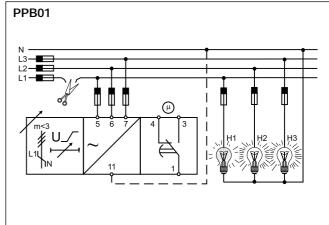


Note

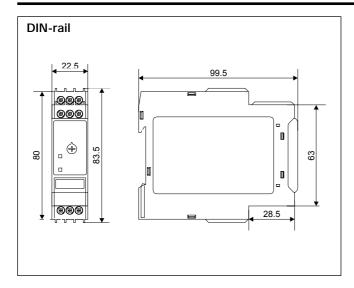
When DPB01 or PPB01 is used with phase indicator lamps (see examples in the following diagrams), the lamp H1 or H2 might be dimly lit when there is a phase loss in L1 or L2. This might happen if the lamps used are the typical low power indicator lamps, and there are no other loads present.

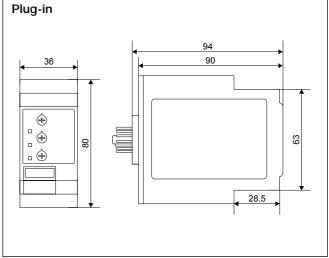
This fact can be avoided by using W4 models. Note that the neutral must be always connected to the device.





Dimensions





Q-Pulse Id: TMS172

2.7. Multitrode MTR Level Relay

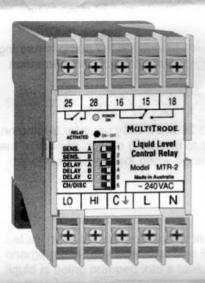


1 Introduction

The MultiTrode level control relay is a solid-state electronic module in a hi-impact plastic case with a DIN rail attachment on the back, making a snap-on-snap-off installation. Any number of relays can be easily added to the DIN metal rail then wired together to form a complex pumping system that other wise may have to be controlled and operated by a programmed PLC.

The relay is normally matched with the MultiTrode probe which works in conjunction with the relay and uses the conductivity of the liquid to complete an electrical circuit.

2 Electrical Overview



There are 10 screw terminals on the unit. Facing the relay as shown, we look at the bottom terminals (left to right):

- Lo (Charge mode). This is the point when the probe is dry the relay will turn on.
- Lo (Discharge mode). This is the point when the probe in the tank is dry the relay will turn off.
- Hi (Charge mode). This is the point when the probe in the tank is wet a relay will turn off
- Hi (Discharge mode). This is the point when the probe in the tank is wet a relay will turn on.
- C is common earth. All earth bonding must be terminated here for correct operation.
- "L" is "live" (240V AC)
- " N " is "neutral" (240V AC)

If the tank is plastic, or if you are conducting tests in a plastic bucket, or the vessel has no earth point inside, you must install an earth rod within the tank, vessel or bucket and make sure that it is bonded back to C on the relay unit.

3 DIP Switches

3.1 DIP Switches

(See Wiring Diagram for full program functions.)

3.1.1 DIP 1 & 2

DIP 1 and 2 control the Sensitivity, in other words the cleaner the liquid the higher the sensitivity setting must be. Concentrated acids, minerals are by their own chemical composition highly conductive, so a low level of sensitivity is required, purified water is almost an insulator against electrical current flow so a higher sensitivity inside the relay is required.

3.1.2 DIP 3, 4 & 5

DIP switches 3, 4 and 5, control delay on activation. For example, in discharge mode with DIP switches 3, 4 and 5 set to 10 seconds, when the Hi point becomes wet it will activate the motor and it will take 10 seconds of continual coverage of the probe sensor to make the relay close and start the pump. This is invaluable when the probe is in a turbulent part of a well where fluid is splashing around touching the sensors momentarily, and false activation cannot be tolerated.

3.1.3 DIP 6

DIP switch 6 controls the charge/discharge function. Set "ON" for charge, and "OFF" for discharge



3.2 Relay Contacts & their Applications

3.2.1 Contacts 15, 16 & 18

Contacts 15, 16, and 18 are used for electronic or visual notification of a change in state at the pump itself. Contacts 15, 16, and 18 are used for more advanced applications because they are a changeover relay, their state may be the same as contacts 25, 28 or the opposite. Both sets of contactors are triggered simultaneously. An example is when in discharge mode, (see Figure 1).

You have a gravity flow coming in so the fluid reaches the lower sensor PB1, contacts 15 and 18 are open (15 being common to both contact 16 and 18) contacts 25 and 28 are also normally open but contacts 15 16 in this current situation are closed, whether PB1 is wet or dry is of no concern all will stay the same. The level now rises to PB2 and both relays change state, contacts 25 and 28 close to turn on the pump, contacts 15 and 16 are open, with 15 and 18 closed.

In advanced applications this state change may be fed into a logic device to indicate the pump is running or the pump has stopped and perhaps light an LED or incandescent light source for visual confirmation that a change has occurred in the relay.

3.2.2 Contacts 25 & 28

Contacts 25 and 28 are used to control pump states. Contacts 25 and 28 are mostly used for turning on motors via a starting relay or solenoid, so, these sets of contacts react to the rising or falling levels of the fluid inside the tank, they will operate to turn on a pump in discharge mode when the top sensor is wet and in charge mode turn on the pump when the bottom sensor is dry.

4 Practical Overview

4.1 Discharge Mode - DIP switch 6 set to "OFF"

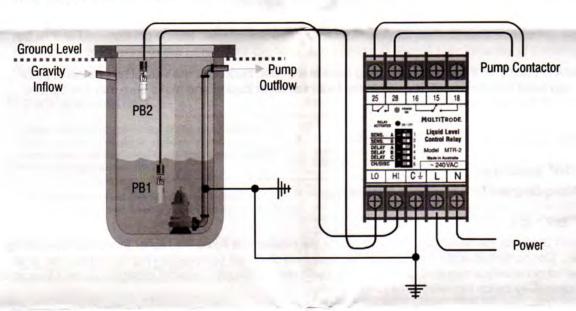


Figure 1 - Discharge Mode

Figure 1 shows two probes, (PB1 connected to Lo and PB2 connected to Hi). The pit is mostly underground and there is a gravity-fed inlet at the top left-hand side. The pit is empty with PB1 completely dry. Dipswitch 6 is set to "OFF."



The relay operation depends on the electrical conductivity of liquid in the pit, i.e. no liquid = no current flow. The level starts to rise and covers PB1.

This is a discharge operation so we do not want the relay to close and start a pump until the well is full so as the water rises it reaches PB2, the relay closes and the pump starts. The level now drops below PB2 but the pump still continues to run, the level continues to drop below PB1 the relay opens the pump stops.



4.2 Charge Mode - DIP switch 6 set to "On"

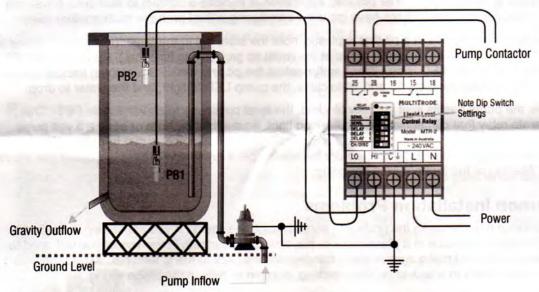


Figure 2 - Charge Mode

Note: "C" is connected to common bonded earth. The unit will not operate correctly if not earthed.

Let's look at the same relay but in a tank that is charging (DIP 6 is now on). See Figure 3, where liquid is being pumped into a tank, and discharging through a gravity feed, the tank is on steel stands "x" metres above the ground.



With the tank full, PB1 and PB2 will be wet, the relay is off, and the pump has stopped. Water is slowly fed out from the bottom, and now as PB2 (HI) becomes dry nothing happens; the water now drops to below PB1 (Lo), and the pumps restarts to fill the tank.

The pump will continue to fill the tank until PB2 (HI), becomes wet again.

4.3 MTRA Relay with Alarm (Discharge Applications Only)

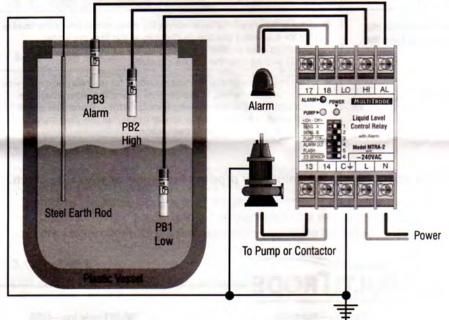


Figure 3 - MTRA Operation

The MTRA relay works in the same way as the MTR relay except the MTRA has a separate alarm output, and does not have a charge mode. The planned application is to close a contact to illuminate a warning alarm light. Various other applications have included introducing a third probe to latch another relay.

In Figure 2 we see three probes in a pit that is plastic, note the steel rod in the tank. (In a plastic vessel a steel rod must be used to create an earth return in the liquid so probes can function.) PB1, PB2, and PB3 are dry, and the relay power LED is on. When water enters the pit and wets PB1, nothing happens, water now reaches PB2 causing contacts 13 and 14 to close, the pump LED to light, and the water to drop.

If, for example, the pump has its inlet partially blocked, the level continues to rise and wets PB3. This closes a separate relay that can activate a red flashing light, an audible fog horn or send a 5 volt pulse into another device with the common cause to warn human beings that a spill is due to occur. If the pumps become unclogged and PB3 becomes dry the alarm opens again and breaks the circuit that stops the light from flashing or the foghorn from sounding.

5 Most Common Installation Problems

The relay requires a path between the probes to earth through the liquid. If you are testing in a plastic bucket, have installed the probe in a plastic tank or have no good earthing in the vessel you will need to install a separate earth and make sure all earth bonding comes back to the C terminal. Most problems like these are traced back to a lack of or poor earthing, or open circuits in the probe wiring.

Now is the time to check the relay by using "the bridge testing line technique" remember you must simulate a fluid flow to correctly ascertain a good relay or a bad one. (All DIPswitch settings from 1 to 6 should be off.)

Cut two pieces of insulated flexible copper wire one black one red 250 mm long, strip both ends back 10 mm on both cables, and join one black end and one red end. Insert the joined ends into C on the relay box, observing all safe electrical practises. You should have one black wire and one red wire free.

Set your relay for discharge mode (DIP switch 6 is off) with no sensors connected to the unit, connect the red wire to Lo – nothing should happen (if it does return the relay for replacement or repair*). Now connect the black wire to the Hi terminal the relay activated LED should light instantly (if it does not, the relay should be returned for repair*).

6 Troubleshooting

I have checked all the DIPswitches and settings but in discharge mode as soon as the bottom sensor gets wet the pump turns on then turns off almost straight away.	This is the most common problem encountered with relay set up and commissioning, the probe in the bottom of the tank is wired into the Hi terminal instead of the Lo terminal.
The installation went fine but now and again the pump will not turn on even though I am sure the probe is wet.	• Check the sensitivity level set on the relay, some times the level is set for foul water but due to changes in the flow the water becomes grey or clear, try changing the setting from $20K\Omega$ to $80K\Omega$ and monitor the results carefully.
All wiring is complete and all DIPswitches have been checked but the pump will not turn on at all.	 If you have completed the test schedule for the relay and it passed then check the wiring to the sensors – for this is now where the problem lies or in the earthing arrangements. If possible check the resistance between the sensor cable and the steel sensor on the probe to prove a solid connection.

^{*} Please contact your distributor or agent before returning any product for repair or warranty claim.



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2.8. Trio DR900-06A02-D0 Radio



TC-900DR USER GUIDE

41 Aster Avenue Carrum Downs 3201 Australia Tel: 61 3 9775 0505 Fax: 61 3 9775 0606

GENERAL

The Trio DataCom TC-900DR is a full duplex 900 MHz Radio featuring a fully integrated 4800/9600 bps data radio modem and antenna diplexer. Configuration of the unit is fully programmable, with parameters held in non volatile memory (NVRAM). All configuration parameters are accessible using the TC-DRPROG installation package, consisting of a programming lead, manual and software which will run on a PC under Windows 95/98/NT. It is essential that each unit is programmed to suit individual requirements prior to operation. For detailed information refer to the TC-900DR Handbook.

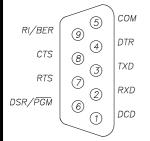
DATA CONNECTION

The data connection is via a DB9 connector labeled 'Port A' (shown below), which is wired as a DCE.

User Serial "Port A" Pin Assignment.

EXTERNAL VIEW OF 'PORT A

NOTE: Pin 6 and pin 9 provide a dual function which depends on the mode that the TC-900DR is operating in.



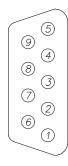
PIN NO. & FUNCTION

- 1. DATA CARRIER DETECT (DCD)
- 2. RECEIVE DATA OUTPUT (RXD)
- 3. TRANSMIT DATA IN (TXD) 4. DATA TERMINAL READY (DTR)
- 5. COMMON (COM)
- 6. PROGRAM PIN (PGM)
- 7. REQUEST TO SEND (RTS)
- 8. CLEAR TO SEND (CTS)
- 9. BIT ERROR RATE PIN (BER)

User Serial "Port B" Pin Assignment.

Port B can be used as a secondary data steam (independent of Port A) once configured by the programmer. Port B also has one connection that may be of use for installation. This connection (Pin 9) is Receive Signal Strength Indicator (RSSI) output. 0-5V where 1.5V typically indicates -110dBm and every 0.5V increase indicates an improvement of » 10dBm.

EXTERNAL VIEW OF 'PORT B'



PIN NO. & FUNCTION

- 1. DATA CARRIER DETECT (DCD)
- 2. RECEIVE DATA O/P (RxD)
- 3. TRANSMIT DATA O/P (TxD)
- 4. UNUSED
- 5. COMMON
- 6. DATA SET RECEIVE (DSR)
- 7. UNUSED
- 8. UNUSED
- 9. RECEIVE SIGNAL STRENGTH

NOTE: Port B Pin 9 output has a high impedance of around 50K OHMS and loading will decrease accuracy of the RSSI measurement.

POWER CONNECTIONS

The power required is 13.8VDC nominal, at 600mA (Tx) nominal. If the POWER LED indicator is not illuminated once power is applied, check the internal 1Amp fuse fitted within the unit.

Ext. view POWER CONNECTOR **PIN ASSIGNMENT** of socket **TOP PIN** +VE SUPPLY (13.8vdc) Тор **BOTTOM PIN GROUND**

AUXILIARY CONNECTOR

The auxiliary connector is primarily for use with the optional audio handset. The connections to this auxiliary 6 pin RJ11 connector are as follows:

PIN NUMBER	<u>FUNCTION</u>	External view
1	8 VOLTS	of socket ☐☐ Top
2	AUDIO OUT	J
3	GROUND	
4	MIC INPUT/SENSE	
5	GROUND	
6	MANUAL PTT	0 1

The optional audio handset is recommended as an aid in checking installations for radio path viability. This audio handset will only function when fitted prior to applying power to the unit.

The modem upon power up will check the presence of the handset and will inhibit data being transmitted so that voice communications can be established.

Once the path tests have been conducted the audio handsets MUST be REMOVED and the unit powered up with the handset removed before data communication can commence.

USER INDICATIONS

The TC-900DR provides 4 LED's that show status information to the user - POWER, RXSIG, SYNC, and TXMIT indications.

The POWER is indicated by a green LED and simply signifies that power has been applied to the unit.

The RXSIG LED (yellow) indicates the level of RSSI signal from the radio IF strip, compared to a threshold level set in the configuration data programmed by the user. If the signal is above the threshold, then the LED indicator is turned on.

In all operation modes except "Programmer mode", the SYNC LED (yellow) indicates when the modem has detected a valid data stream. The SYNC LED is activated, when the modem detects a valid HDLC flag sequence, and remains active until an invalid sequence of seven or more consecutive "1" bits is detected.

The SYNC LED will not be turned on if the RSSI signal strength (as indicated by the RXSIG LED) is below the minimum threshold. This prevents false SYNC detection from noise.

The TXMIT LED (red) indicator is connected directly to the modem's PTT output transistor. Whenever the radio is transmitting, this TXMIT LED indicator will be on.

SPECIAL MODES OF OPERATION

Part of the power-up/reset initialisation phase of the TC-900DR are tests to determine if the modem should enter one of 3 "special operation" modes. In these modes the TC-900DR won't operate in its standard run mode.

- Programmer mode.
- Bit error rate test mode.
- Handset mode.

These modes are only entered if the required setup conditions are present at power up. An error mode of operation can also be entered into, if during normal operation, an error condition occurs.

PROGRAMMER MODE

CABLE - Pins 2, 3, 4, 5 straight through with Pin 6 on the DB9 connector of Port A, connected to pin 5. When the modem is powered up with this fitted, the controller senses this and attempts to enter "Programmer mode" and the "SYNC" LED will flash approx. once per second. (Note, the TC-DRPROG programming software and lead has the required connections). Failure to supply the correct password in time, will cause the modem to abandon the "Programmer mode" attempt, and go on with it's normal power-up procedure.

BIT ERROR RATE TEST MODE

Pin 9 of the DB9 connector of Port A, is normally the Ring Indicate output line. However, if this pin is driven positive (connecting it to pin 6 [DSR] and pin 7 [RTS]), then the modem's data transmitter and receiver will enter the BER test mode. This will activate the RF transmitter, and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic "1" level in the unscrambled data. Any errors in the decoded bitstream, will be "0", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a "0" bit.

Note: As the TC-900DR is full duplex this test can operate in both directions simultaneously.

Every error bit detected, will activate the SYNC LED. For error rates of 1 in 10³ and above, the SYNC LED will be ON most of the time. A 1 in 10⁴ error rate will show the SYNC LED active for approximately 10% of the time. This function provides a crude indication of Bit Error Rate for installation purposes. Note: Error count messages (ET:XXXX) for every 10,000 bits are presented to Port A for the user. If pin 9 ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

HANDSET MODE

The DFM4-9 modem tests for the presence of a handset plugged into the handset auxiliary port at power up. If a handset is plugged in, the modem will not generate a data stream. However, it will continue to indicate received RF signal strength. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED. It is essential to remove the handset from the unit and reapply power to the unit in order to return to normal operation.

ERROR INDICATION MODES

There are 3 error conditions that cause the RXSIG & SYNC LEDs to be used for error indications and not their normal purpose. Two are fatal conditions, that cause the modem to restart after the duration of the error indication phase.

TRANSMIT POWER LOW

While the modem activates the radio transmitter, it periodically checks the transmit power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately 4 times per second. The TXMIT LED will also be on during this process. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function. Factory set to 100 milliWatts.

NVRAM READ ERROR

The DFM4-9DR modem accesses the non-volatile memory as part of it's initialisation phase, to read programming configuration data. If the communication protocol with the device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED operates ON and OFF twice, then the other. A total of five cycles of this occurs, then the modem restarts initialisation.

SYNTHESISER LOCK DETECT ERROR

If at any time during normal operation, BER mode, or handset mode, the TBB206 frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting.

One LED is turned ON (\$\circ\$), the LEDs are swapped, then both turned OFF (\$\circ\$). Then the latter LED ON again, swap LEDS, and then OFF. This will give the appearance of a sweeping motion between the LEDs. The following table shows all error condition displays.

Tx P\	NR Err	NVRAM Err		SYN	TH Err
RXSIG	SYNC	RXSIG	SYNC	RXSIG	SYNC
≎	•	٥	•	٥	•
•	٥	•	•	•	٥
≎	•	٥	•	•	•
•	٥	•	•	•	٥
٥	•	•	٥	٥	•
•	٥	•	•	•	•
٥	•	•	٥		repeat
•	٥	•	•		
continue			repeat		

MOUNTING AND ANTENNA CONNECTION

The TC-900DR should be mounted in a cool, dry, vibration free environment, whilst providing easy access to screws and connections. There are 4 mounting holes on the unit. The antenna should be an external yagi antenna but can be a ground independent dipole mounted via a feeder to the antenna connector (SMA type) for short range applications. However the whole radio modem should be clear of the associated data equipment to prevent mutual interference.

ASSEMBLY OF POWER LEAD

A small plastic bag containing a molex connector (M5557-2R) and two pins (M5556-TL) is provided in the packing box.

The pins are designed to take 18-24 (AWG) wire size with insulation range 1.3 - 3.10mm.

Please take care when crimping the pins.

04/01

2.9. Multitrode Level Probe

The MultiTrode Probe

MultiTrode probes are unsurpassed for rugged reliability, cost effectiveness and simplicity. Designed for the tough, turbulent conditions found in water, sewage and industrial tanks and sumps, the probes can be found in the simplest and the most complex water and wastewater management systems around the world.

- Low maintenance
- Simple installation
- Excellent in turbulence
- Short & long term cost savings
- Environmentally friendly
- Safe, low sensing voltage
- Unaffected by fat, grease, debris and foam
- Positive pump cut-out
- Safe MTISB Barrier

Reliable in all conditions

Operation is unaffected by build up of fat, grease debris and foam, which causes other systems such as floats, bubblers, pressure and ultrasonic transducers to fail. Turbulence does

not affect the probe operation. The rugged, streamlined design eliminates tangling and is ideal for confined spaces.

Positive pump cut-out

Operational consistency is important to longevity, low maintenance and cost control. The positive pump cut-out ensures pumps are turned off at the same level every time. This avoids damage due to pump over run and the cost of additional control equipment.

Safe for people and environment

The extra low sensing voltage ensures operators and maintenance staff are protected. All MultiTrode products are environmentally safe, containing no mercury or other harmful contaminants.

Cost savings

The low cost of equipment, installation and maintenance makes MultiTrode one of the most efficient level control systems available. Plus robust construction and longevity ensures continued cost savings when compared to other systems on the market.

Standard and custom probes

MultiTrode manufactures a wide range of standard probes, from a single sensor (200mm) to a ten-sensor probe (1000mm increasing to a maximum of nine metres). Custom probes can be manufactured to suit your requirements.

Installation

Installation is straightforward. Probes are easy to install without entering the wet area. The probe is simply lowered in from the top and suspended by its own cable, using the mounting kit supplied.

MTAK-1 Mounting Kit (Supplied)

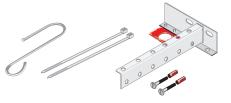
The mounting bracket is a standard accessory supplied with all multi-sensor probes (not standard with 0.2/1-xx single sensor probe).

The MTAK-1 mounting bracket has an integral cleaning device. All metal components are stainless steel.



MTAK-2 Mounting Kit (Optional extra)

This extended bracket provides up to 300mm extra wall clearance. This bracket is not included as standard with probes.



Ordering Examples and Information

Model Code	Probe Length (m/in)	Sensor Separation (mm/in)	Cable Length* (m/ft)	Number of Sensors
0.2/1-10	0.2/8	N/A	10/33	1
0.5/3-10	0.5/16	150/6	10/33	3
1.0/10-10	1/40	100/4	10/33	10
1.5/10-30	1.5/60	150/6	30/100	10
2.0/10-30	2/80	200/8	30/100	10
2.5/10-30	2.5/96	250/10	30/100	10
3.0/10-30	3/115	300/12	30/100	10
6.0/10-30	6/224	600/24	30/100	10
9.0/10-30	9/368	900/40	30/100	10

^{*}Cable Length 10m/33ft or 30m/100ft

Pr	Probe Length (meters)		•		Cable Length (meters)			
	2.5		10		10			



www.multitrode.com

MultiTrode Pty Ltd · Australia

Brisbane Technology Park 18 Brandl Street PO Box 4633 Eight Mile Plains Qld 4113 Tel: +61 7 3340 7000 Fax: +61 7 3340 7077

Q-Pulse Id: TMS172 sales@multitrode.com.au

MultiTrode Inc · USA

6560 East Rogers Circle
Boca Raton Florida 33487
Tel: +1 561 994 8090 Fax: +1 561 994 6282

sales@multitrode.net

MultiTrode Probe Immersion Table



PVC and AVESTA 254-SMO stainless steel comprise the major, exposed surfaces of the MultiTrode probe, and have been operated and tested in the following chemicals.

ACETIC ACID	50% Aqueous
ADIPIC ACID	Saturated Aqueous
ALUMINIUM SULPHATE	27%
AMMONIUM CARBONATE	50% Aqueous
AMMONIUM HYDROXIDE	All Concentrations
AMMONIUM PHOSPHATE	All Concentrations
AMMONIUM SULPHATE	All Concentrations
AMMONIUM SULPHIDE	All Concentrations
AMYL ALCOHOL	
ANILINE HYDROCHLORIDE	All Concentrations
BARIUM HYDROXIDE	All Concentrations
BEER	
BORAX	All Aqueous
BORIC ACID	All Aqueous
CALCIUM NITRATE	50% Aqueous
CHLORIC ACID	10%
CHROMIC ACID	5%
FORMIC ACID	Up to 50% Aqueous
GELATINE	All Concentrations
GLUCOSE	All Concentrations
GLYCERINE	All Concentrations
HYDROBROMIC ACID	50% Aqueous
HYDROCYANIC ACID	100%
HYDROFLUORIC ACID	1%
HYDROGEN PEROXIDE	30% Aqueous
HYDROGEN SULPHIDE	Moist Gas or Saturated Aqueous solution
LACTIC ACID	18% Aqueous
LEAD ACETATE	All Concentrations
MERCURY	100%
MILK	Sour
NITRIC ACID	Up to 40% Aqueous
	· · · · · · · · · · · · · · · · · · ·

	7
OXALIC ACID	5%
PHOSPHORIC ACID	Up to 30% Aqueous
POTASSIUM BICHROMATE	25%
POTASSIUM CHLORATE	36%
POTASSIUM CHROMATE	All Concentrations
POTASSIUM CYANIDE	All Concentrations
POTASSIUM PERMANGANATE	5-10%
POTASSIUM PERSULPHATE	Saturated
POTASSIUM SULPHATE	All Concentrations
SODIUM ACETATE	All Concentrations
SODIUM BICARBONATE	All Concentrations
SODIUM BISULPHATE	5%
SODIUM BISULPHITE	10%
SODIUM CHLORATE	30%
SODIUM FLUORIDE	5-10%
SODIUM NITRATE	All Concentrations
SODIUM PHOSPHATE	All Concentrations
SODIUM SILICATE	All Aqueous
SODIUM SULPHATE	All Concentrations
SODIUM SULPHIDE	5%
SODIUM SULPHITE	50%
SODIUM THIOSULPHATE	16-25%
SULPHUR DIOXIDE	Technically Pure Anhydrous
SULPHURIC ACID	98%
SULPHUROUS ACID	Saturated Aqueous
TANNIC ACID	All Aqueous
TARTARIC ACID	All Aqueous
TURPENTINE OIL	Technically Pure
VINEGAR	4-5%
YEAST	All Aqueous

Unless stated otherwise, all aqueous solutions are 100%.

Note: MultiTrode probes can be used in many other aggressive applications and the list above is by no means complete.

Leaders in Pump Station Management Technology

www.multitrode.com



Materials:

Sensors: Avesta 254 SMO high grade stainless steel alloy

Casing: uPVC premium quality extruded tube

Cable: PVC/PVC multi-core, purpose-manufactured

Resin: Fast cure, low viscosity, and solvent free

Compressive Strength (TM-45) 7 days at 25° C (77°F) = 60 N/mm^2 Elastic Modulus in Compression (TM-45) 7 days at 25° C = 60 N/mm^2

Flexural Strength (TM-46) 7 days at 25°C (77°F) = Specimen did not break under test

TG (TM-22) 7 days at 25°C (77°F) = 30°C (86°F)

Dimensions: 32 mm (1 1/4 in) diameter x specified length

Mounting: via the supplied suspension/cleaning bracket inside the wet well

Environmental Range: 0°C to +65°C (32°F to +149°F)

Cable: 10-core 3-core Single-core

Conductor Size 0.75mm² 0.75mm² 1.00mm²

Strands/Conductor 24 24 30

Ohms/km 25 25 20

Ohms/mile 40 40 32

Oversheath: 10-core 3-core Single-core

Nominal diameter 11.2 mm 6.8 mm 6.8 mm

Core Colours: White * White * White

Oversheath: Blue

Custom Probes:

MultiTrode can manufacture custom probes to suit a particular application. Custom probes are manufactured exactly to your requirements, within the following limits

No. of Sensors 25 sensors max.

Sensor spacing 76.2 mm (3 in) min.

Section length* 3m (115 in) max.

Cable length 400m (1500 ft) max.

* Note: Probes over 3m (10 feet) in length are made in sections.

Leaders in Pump Station Management Technology

www.multitrode.com

^{*} Mounting bracket not supplied with single-sensor probes

^{*} Other multi-core cables are available for non-standard probes

^{*} All multi-core cables are printed: "1-ONE-1", "2-TWO-2" = etc. every 200mm (7 in)

3. Drawings

3. Drawings

3.1. Point to Point Drawings

3.2. Tested Drawings

QUEENSLAND

Urban Utilities

PRV154 CORDELIA ST, SOUTH BRISBANE PRESSURE REGULATING VALVE SWITCHBOARD

	VARIABLE / LAYER	VALUE / ON	or OFF			
	PRV No. (01)	PRV154				
	StreetName (02)	CORDELIA ST				
	SuburbName (03)	SOUTH BRISE	BANE			
щ	Pin Gauge No. (04)	_		•		
NABI	Pout Gauge No. (OS)	+				
ΥA	Flowmeter No. (06)	-				
NS.	RadioPartNo. (07)	ER450-53A02	2-EHO			
DRAWING VARIABLE	DrawingNo. (08)	486/4/9-09	54			
,	Site Function (09)	PRESSURE R	EGULATIN	IG VALVE		
	SPARE (10)					
	1.1 Main PRV fitted	yes	Yes	No	No	
	1.2.1 Bypass PRV fitted	no	No	No	No	
	2.1 Radio fitted	yes	Yes	No	No	
	2.1.1 Side Antenna Mast fitted	yes	Yes	No	No	
	2.1.2 Rear Antenna Mast fitted	no	No	No	No	
	3.1 PSTN Modem fitted	no	No	No	No	
DRAWING LAYER	3.2 GSM Modem fitted	no	Yes	Yes	Yes	
/1 9	4.1 Flowmeter fitted	yes	Yes	No	Yes	
N.M.	5.1.1 Pressure Guage 1 fitted	yes	Yes	Yes	Yes	
DR/	5.2.1 Pressure Guage 2 fitted	yes	Yes	No	Yes	
	6.1 Sump Pump fitted	yes	Yes	No	No	
	7.1 RTU - MD331 fitted	no	No	No	Νο	
	7.2 RTU - eNet fitted	yes	Yes	Yes	Yes	
	7.3 RTU plg/skt fitted	yes	Yes	Yes	Yes	
PRESSURE REGULATING VALVE — Î Î						
PRESSURE GAUGE						

FLOWMETER:

ELECTRICAL DRAWINGS INDEX

DWG N°.	TITLE SHEET RE		REV	VISIONS		;	
486/4/9-0954-001	ELECTRICAL DRAWING INDEX	01	0	1			
486/4/9-0954-002	POWER DISTRIBUTION SCHEMATIC DIAGRAM	02	0	1			
486/4/9-0954-003	DIGITAL INPUTS AND OUTPUTS TERMINATION DIAGRAM	03	0	1			
486/4/9-0954-004	ANALOG INPUTS AND OUTPUTS TERMINATION DIAGRAM	04	0	1			
486/4/9-0954-005	PRV SWITCHBOARD GENERAL ARRANGEMENT	05	0	1			
486/4/9-0954-006	SWITCHBOARDS CONSTRUCTION DETAILS	06	0	1			
486/4/9-0954-007	PRV SWITCHBOARD EQUIPMENT LIST	07	0	1			
486/4/9-0954-008	SWITCHBOARD CABLE & LABEL SCHEDULE	08	0	1			
486/4/9-0954-009	SOLAR PANEL SWITCHBOARD GENERAL ARRANGEMENT	09	Α	0			
486/4/9-0954-010	SITE OVERALL LAYDUT	010	A	0			
486/4/9-0954-011	HALE STREET SOLAR PANEL SWITCHBOARD	011	Α	0			

NOTE:

P.MOSTERT 12.03

AS CONSTRUCTED DETAILS

I CERTIFY THAT THE "AS CONSTRUCTED" OFTAILS
SHOWN ON THIS PLAN ARE A TRUE AND ACCURATE

NAME of SIGNATORY:

COMPANY NAME:

FINISH DATE:



NAME SIGNATURE

QUEENSLAND URBAN UTILITIES DELEGATE (AUTHORISED FOR 12 MONTHS FROM DATE SHOWN)



1 03/12 DRAWING REVISED, ISSUED FOR CONSTRUCTION
0 03/11 FOR CONSTRUCTION

DESIGN W.O. No.

CONSTRUCTION W.O. No.

OVED. FUNDED BY Q.U.U. (/) EXTERNAL ()

DRAFTING CHECK P.HAGUE
CAD FILE 49-0954-SetO
Q.U.U. FILE No.

 07
 DESIGN
 R.P.E.Q. No.
 0

 Original Signed by R.JANFADA
 RPEO 5192
 12.

 DESIGN CHECK
 R.P.E.Q. No.
 DA

Original Signed by A.WITTHOFT

APPROVED BY SIGNATURE DATE

OF CONSTRUCTION MANAGER SIGNATURE DATE

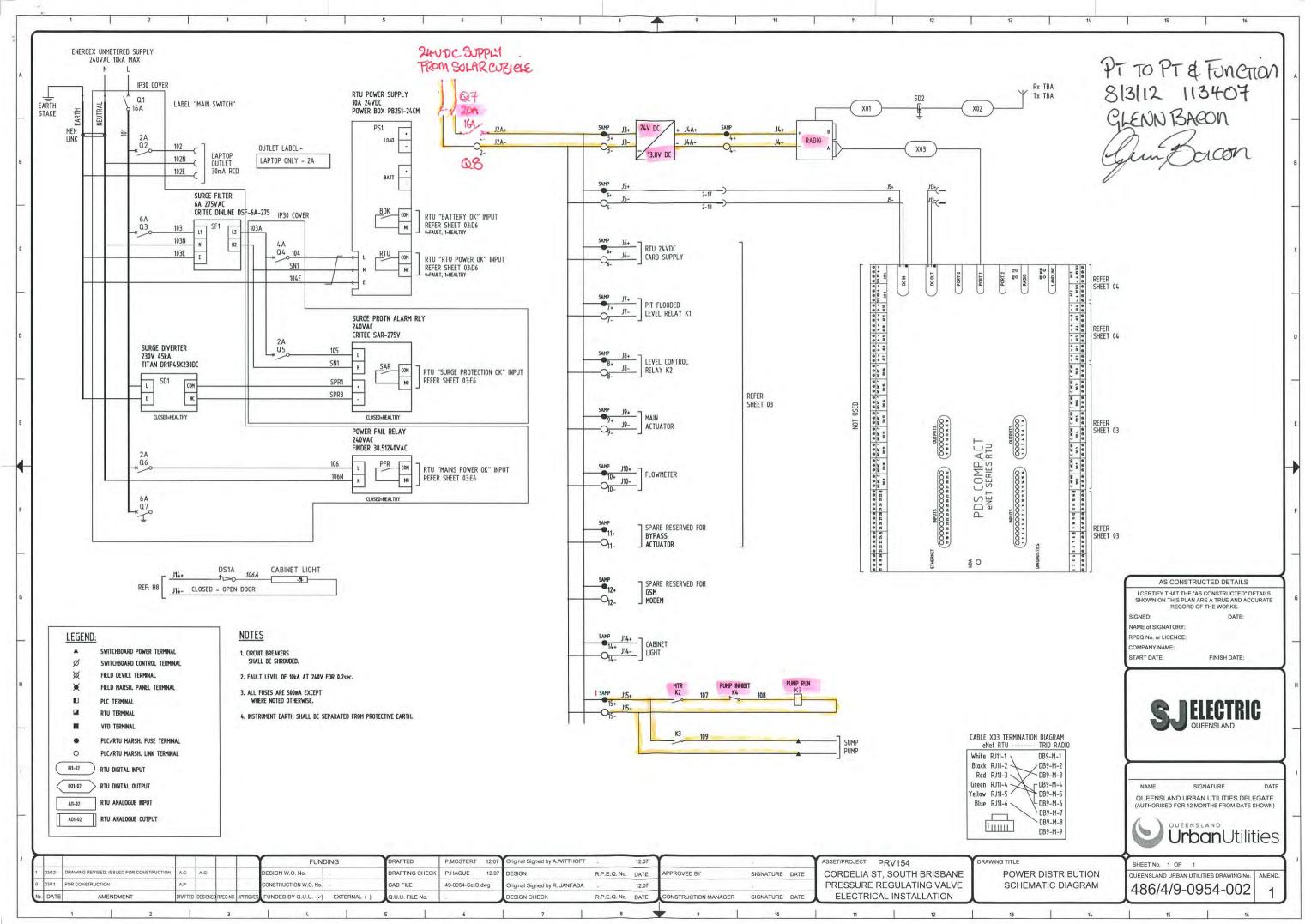
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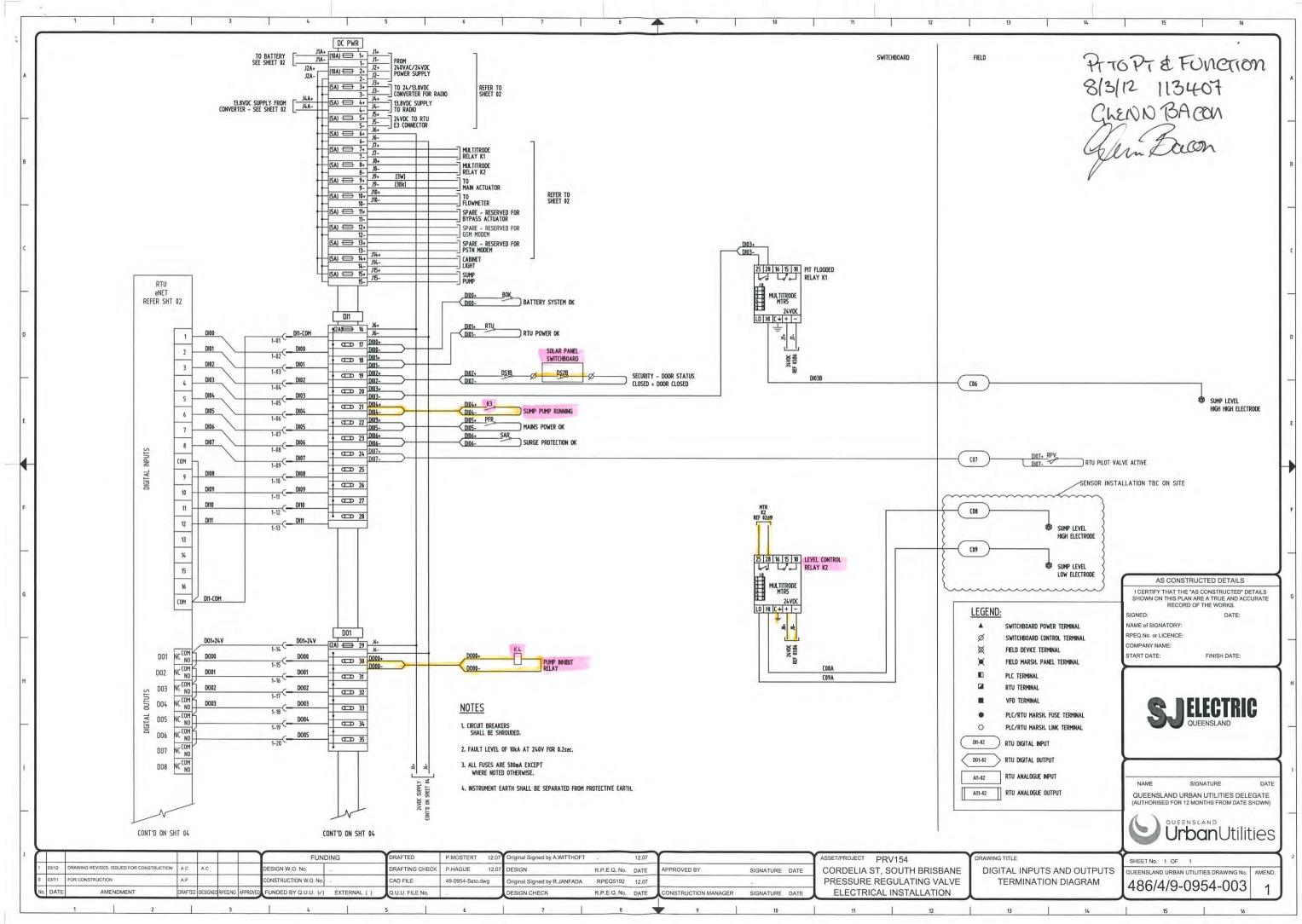
CORDELIA ST, SOUTH BRISBANE
PRESSURE REGULATING VALVE
ELECTRICAL INSTALLATION

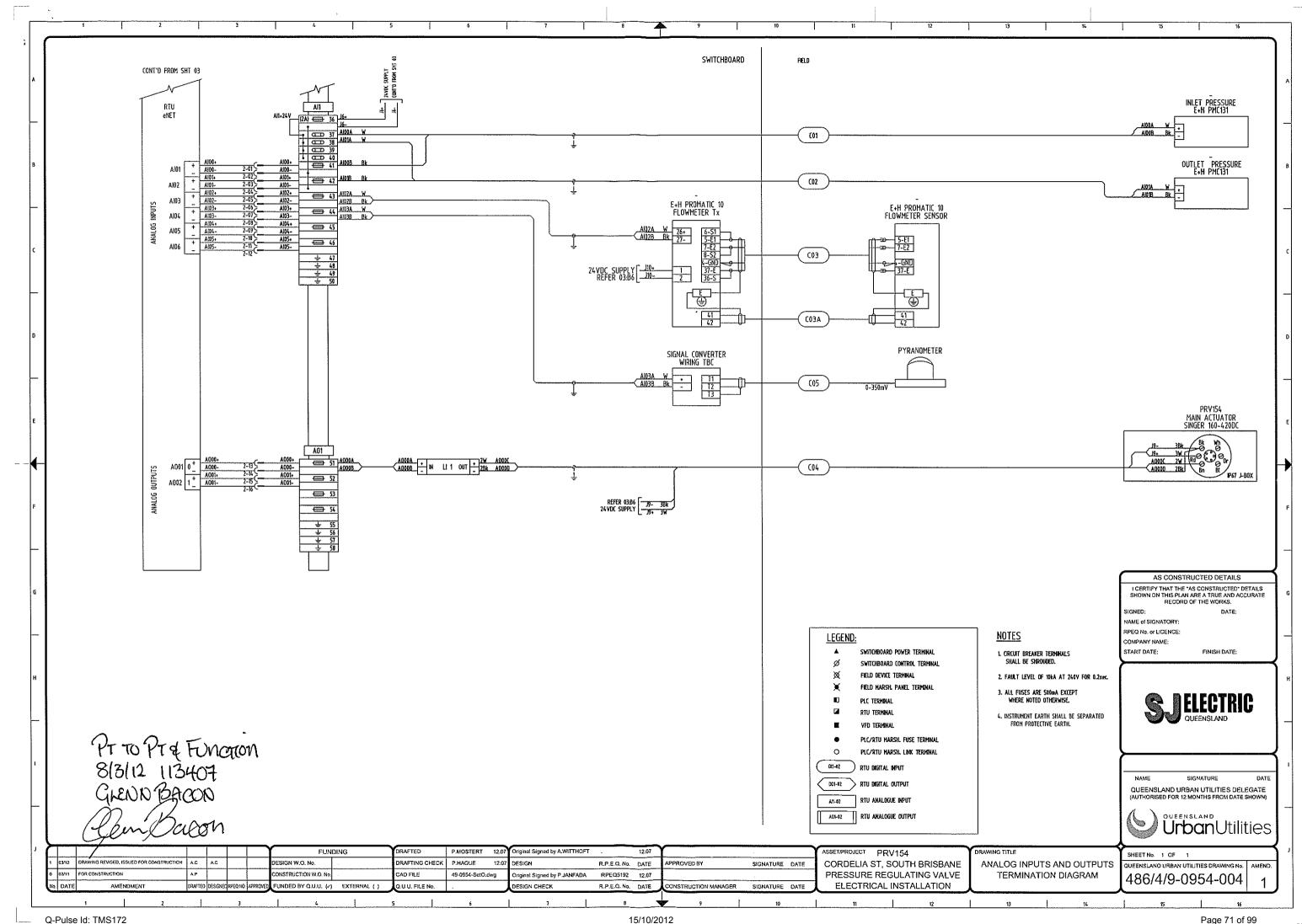
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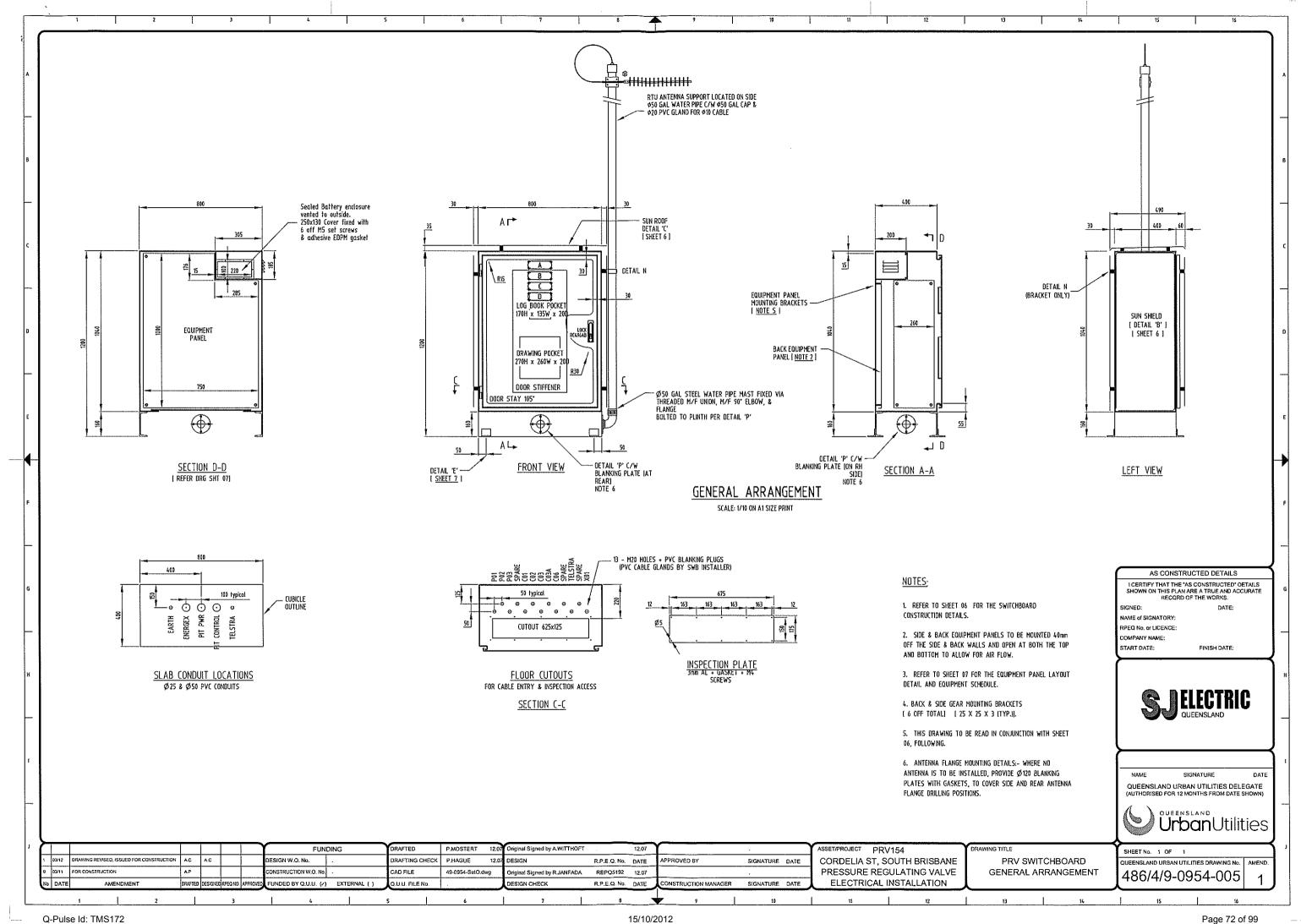
SHEET No. 1 OF 1 QUEENSLAND URBAN UTILITIES DRAWING No.

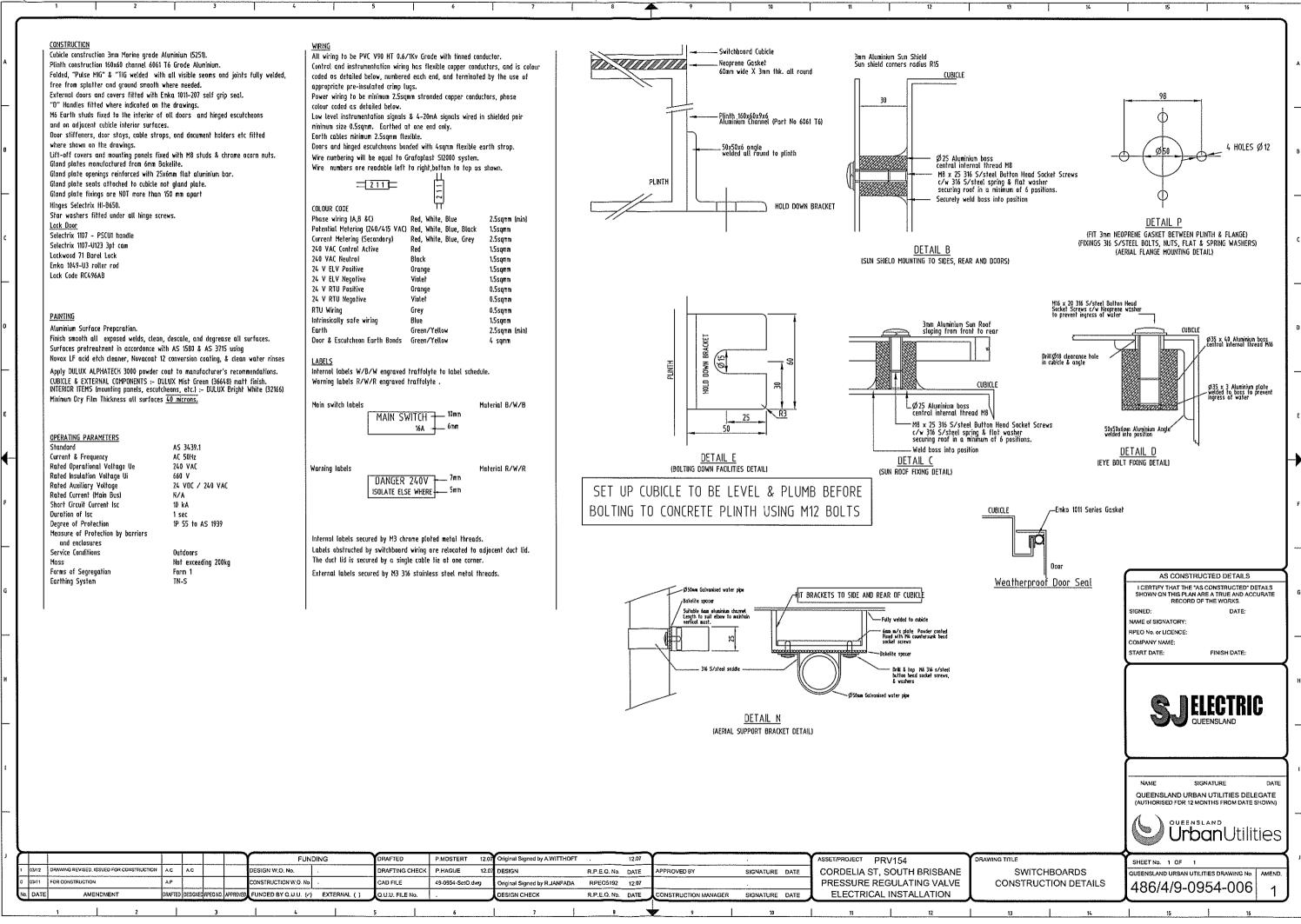
486/4/9-0954-001

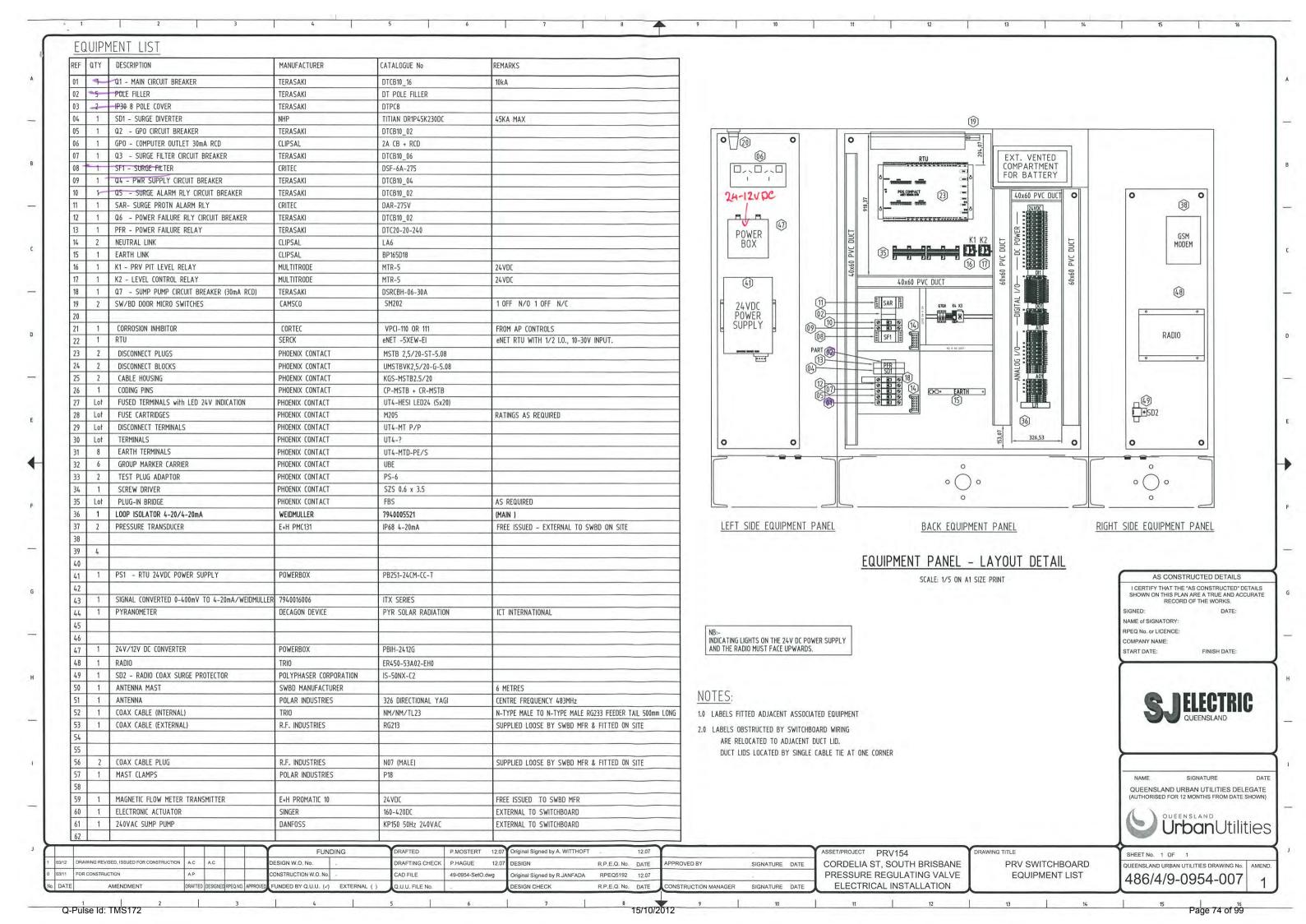












CARLE SCHEDILLE

Electrical Installation Contractor Electrical Installation Contractor Electrical Installation Contractor Switchboard Manufacturer
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FREE ISSUE
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/EL Electrical Installation Contractor
CTIVE Electrical Installation Cantractor

EQUIPMENT LABEL LIST

REF	TEXT HEIGHT mm / MATERIAL	TEXT LINE 1 / TEXT LINE 2
45	4mm / WBW TRAFFOLYTE	- INLET ZONE PRESSURE
45	4mm / WBW TRAFFOLYTE	- OUTLET ZONE PRESSURE
48	4mm / WBW TRAFFOLYTE	- FLOWMETER
49	4mm / WBW TRAFFOLYTE	SD2 - RADIO SURGE DIVERTER
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EQUIPMENT LABEL LIST

REF	TEXT HEIGHT mm / MATERIAL	TEXT LINE 1 / TEXT LINE 2
01	10mm / 4mm / WBW TRAFFOLYTE	MAIN SWITCH / Q1 - 16A
04	4mm / WBW TRAFFOLYTE	SD1 - SURGE DIVERTER
05	4mm / WBW TRAFFOLYTE	Q2 ~ LAPTOP GPO ~ 2A
06	4mm / WBW TRAFFOLYTE	2Amp LAPTOP ONLY
07	4mm / WBW TRAFFOLYTE	Q3 - SURGE FILTER - 6A
08	4mm / WBW TRAFFOLYTE	SF1 - SURGE FILTER
09	4mm / WBW TRAFFOLYTE	Q4 - 24V PWR SUPPLY - 4A
10	4mm / WBW TRAFFOLYTE	QS - SURGE ALM RLY - 2A
11	4mm / WBW TRAFFOLYTE	SAR - SURGE ALM RLY
12	4mm / WBW TRAFFOLYTE	Q6 - POWER FAIL RLY - 2A
13	4mm / WBW TRAFFOLYTE	PFR - POWER FAIL RLY
14	4mm / WBW TRAFFOLYTE	NEUTRAL
15	4mm / WBW TRAFFOLYTE	EARTH
18		
19	4mm / WBW TRAFFOLYTE	PS1 ~ 24YDC10A PWR SUPPLY
20	4mm / WBW TRAFFOLYTE	24/13.8VDC CONVERTER
21	4mm / WBW TRAFFOLYTE	BATTERY COMPARTMENT
22	4mm / WBW TRAFFOLYTE	RTU
24	4mm / WBW TRAFFOLYTE	K1 - PRV PIT LEVEL RLY
25		
28		
29		
45		

EXTERNAL LABELS

LABEL	TEXT	TEXT HEIGHT	PAINT FILL LETTERING	DIMENSIONS	QTY
A	PRV154	20mm	BLACK	150X35	1
В	<u>Warning</u> This site is monitored by the control room operator Please inform the operator before isolating station	8mm	BLACK	250X100	1
C	DANGER 240V	8mm	RED	120X1S	1
D	REMINDER: THIS IS AN UN-METERED SUPPLY AND ANY ALTERATIONS TO THESE CIRCUITS MUST BE NOTIFIED TO SUPPLY AUTHORITY BILLING DEPARTMENT.	3mm	BLACK	TO SUIT	1
A	PRY154A	20mm	BLACK	150X35	1

EXTERNAL LABELS 1mm THK. 316 GRADE STAINLESS STEEL. FIXED WITH M3 316 STAINLESS STEEL METAL THREADS.

AS CONSTRUCTED DETAILS

I CERTIFY THAT THE "AS CONSTRUCTED" DETAILS SHOWN ON THIS PLAN ARE A TRUE AND ACCURATE RECORD OF THE WORKS.

SIGNED: NAME of SIGNATORY;

RPEQ No. or LICENCE:

COMPANY NAME:

START DATE: FINISH DATE:



SIGNATURE

QUEENSLAND URBAN UTILITIES DELEGATE (AUTHORISED FOR 12 MONTHS FROM DATE SHOWN)



FOR CONSTRUCTION AMENDMENT

DESIGN W.O. No. ONSTRUCTION W.O. No. FUNDED BY Q.U.U. (/) EXTERNAL () DRAFTED DESIGNED RPEQ NO APPRO

DRAFTED P.MOSTERT 12.0 DRAFTING CHECK P.HAGUE CAD FILE 49-0954-SetQ.dwg Q.U.U. FILE No.

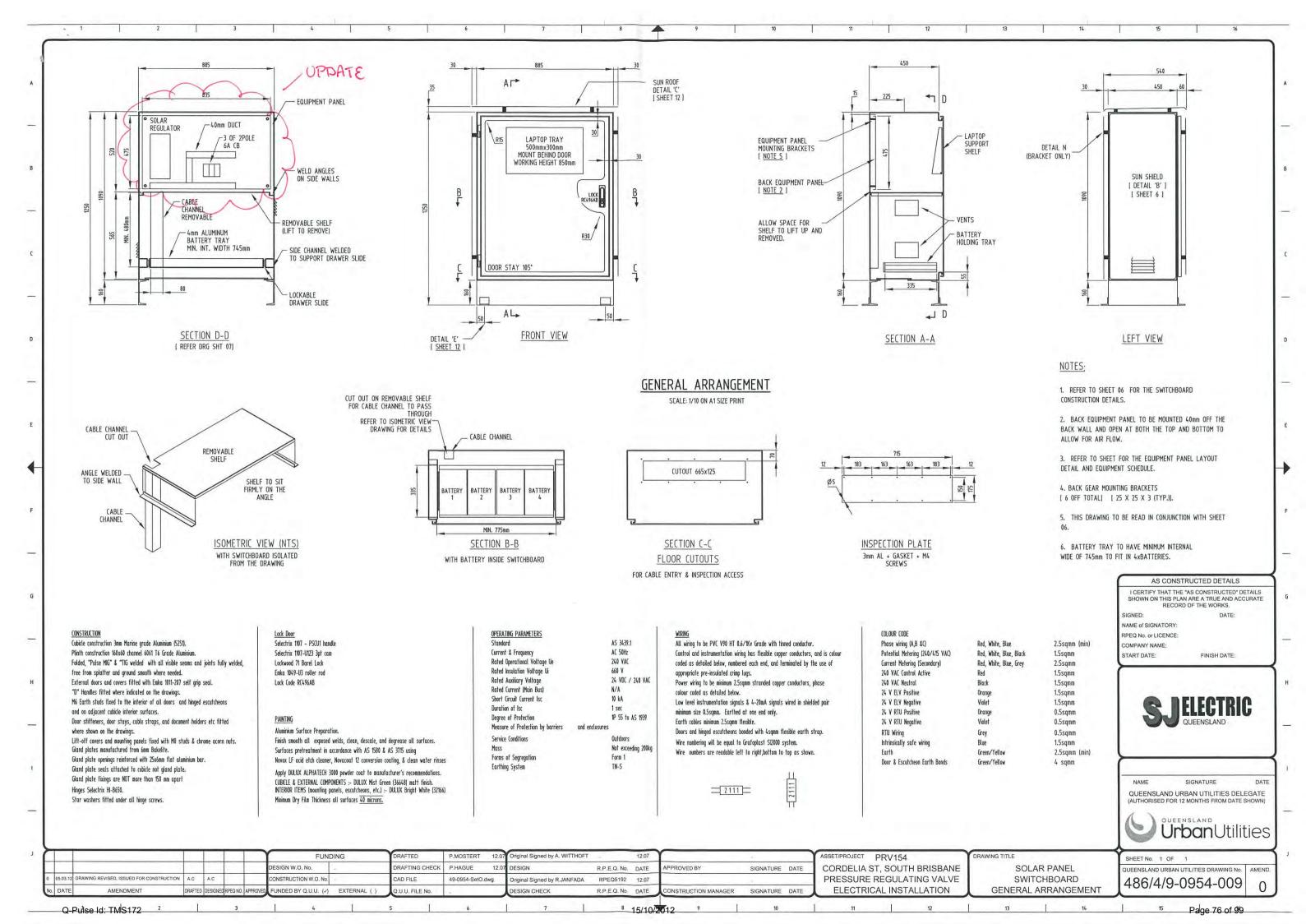
Original Signed by A.WITTHOFT 12.07 DESIGN R.P.E.Q. No. DATE Original Signed by R.JANFADA RPEQ5192 12.07 DESIGN CHECK R.P.E.Q. No. DATE

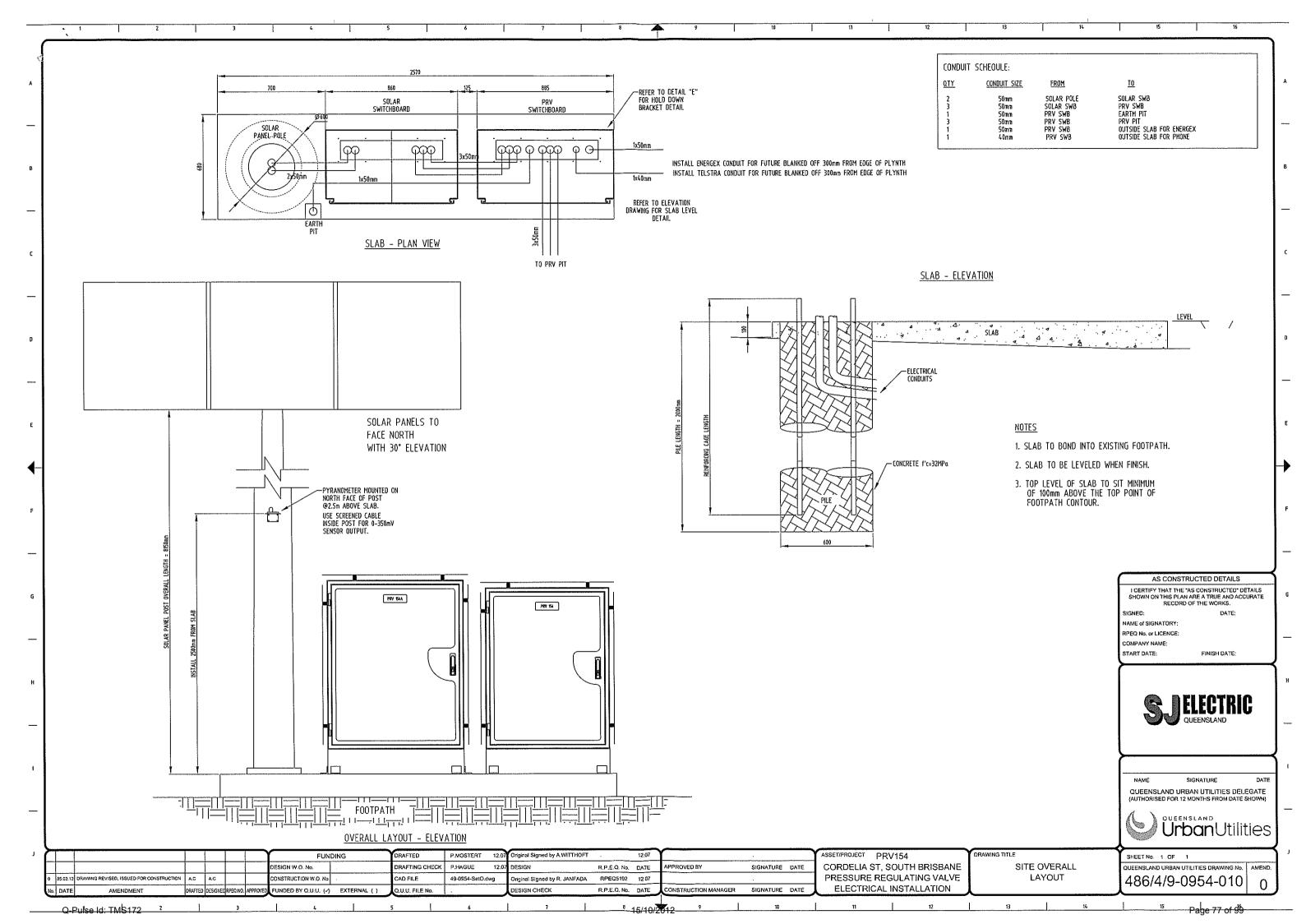
APPROVED BY SIGNATURE DATE CONSTRUCTION MANAGER SIGNATURE DATE ASSET/PROJECT PRV154 CORDELIA ST, SOUTH BRISBANE PRESSURE REGULATING VALVE ELECTRICAL INSTALLATION

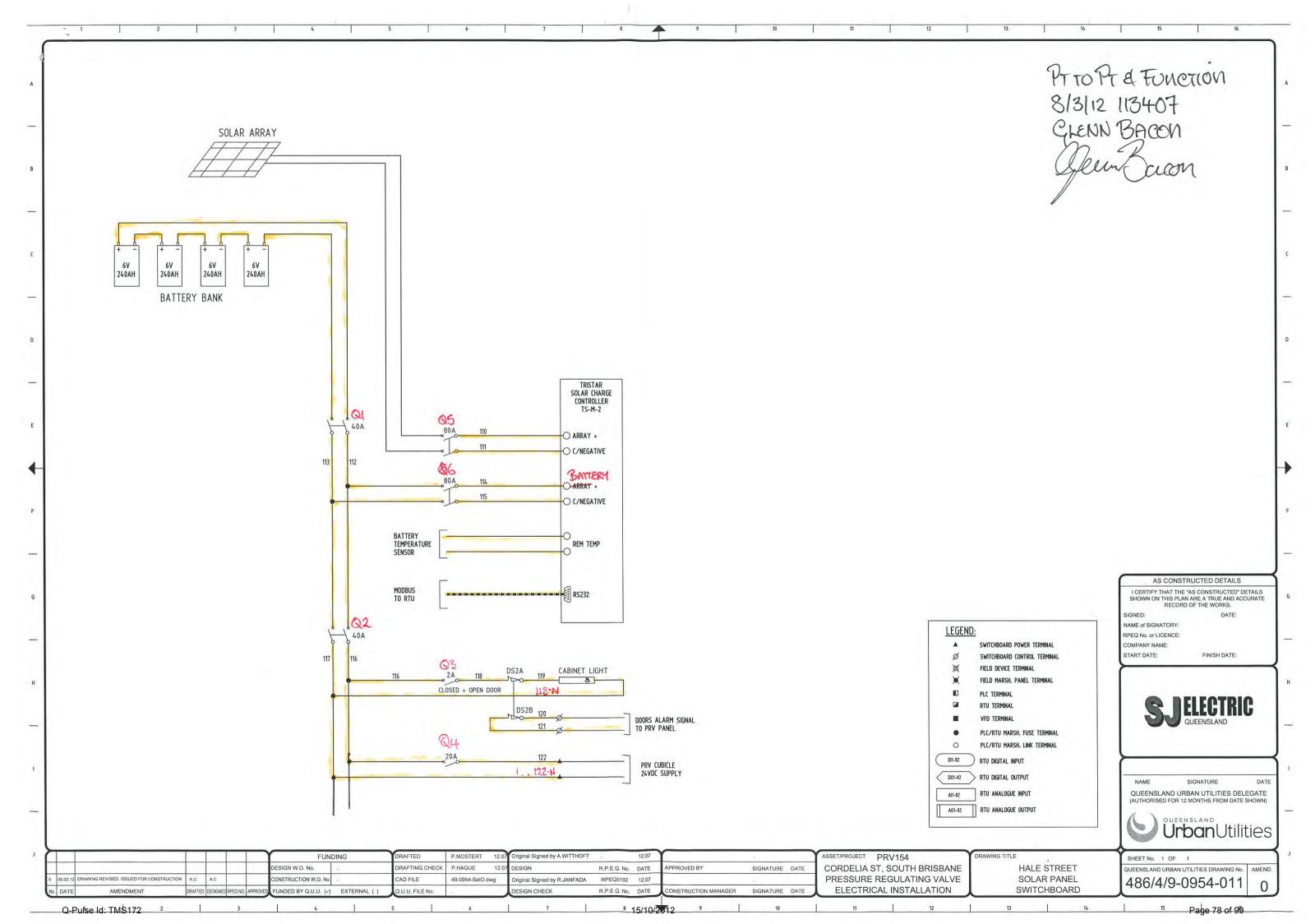
SWITCHBOARD CABLE & LABEL SCHEDULE SHEET No. 1 OF 1

QUEENSLAND URBAN UTILITIES DRAWING No. AMEND.

486/4/9-0954-008







3. Drawings3.3. As Built Drawings



PRV154, PRV154A CORDELIA ST, SOUTH BRISBANE PRESSURE REGULATING VALVE SWITCHBOARD

	VARIABLE / LAYER	VALUE / 0	N or OFF		
	PRV No. (01)	PRV154, PR	RV154A		
	StreetName (02)	CORDELIA S	T		
	SuburbName (03)	SOUTH BRIS	SBANE		
щ	Pin Gauge No. (04)	-			
DRAWING VARIABLE	Pout Gauge No. (05)	-			
X	Flowmeter No. (06)	-			
/ING	RadioPartNo. (07)	ER450-53A	02-EH0		
NA'	DrawingNo. (08)	486/4/9-0	954-		
_	Site Function (09)	PRESSURE	REGULATIN	IG VALVE	
	SPARE (10)				
	1.1 Main PRV fitted	yes	Yes	No	No
	1.2.1 Bypass PRV fitted	no	No	No	No
	2.1 Radio fitted	yes	Yes	No	No
	2.1.1 Side Antenna Mast fitted	yes	Yes	No	No
	2.1.2 Rear Antenna Mast fitted	no	No	No	No
	3.1 PSTN Modem fitted	no	No	No	No
YER	3.2 GSM Modem fitted	по	Yes	Yes	Yes
DRAWING LAYER	4.1 Flowmeter fitted	yes	Yes	No	Yes
N.	5.1.1 Pressure Guage 1 fitted	yes	Yes	Yes	Yes
8	5.2.1 Pressure Guage 2 fitted	yes	Yes	No	Yes
	6.1 Sump Pump fitted	yes	Yes	No	No
	7.1 RTU - MD331 fitted	no	No	No	No
	7.2 RTU - eNet fitted	yes	Yes	Yes	Yes
	7.3 RTU plg/skt fitted	yes	Yes	Yes	Yes

FLOWMETER

ELECTRICAL DRAWINGS INDEX

DWG N°.	TITLE	SHEET	F	RE\	/ISIC	NS
486/4/9-0954-001	ELECTRICAL DRAWING INDEX	01	0	1	2	
486/4/9-0954-002	POWER DISTRIBUTION SCHEMATIC DIAGRAM	02	0	1	2	
486/4/9-0954-003	DIGITAL INPUTS AND OUTPUTS TERMINATION DIAGRAM	03	0	1	2	
486/4/9-0954-004	ANALOG INPUTS AND OUTPUTS TERMINATION DIAGRAM	04	0	1	2	1-1
486/4/9-0954-005	PRV SWITCHBOARD GENERAL ARRANGEMENT	05	0	1	2	100
486/4/9-0954-006	SWITCHBOARDS CONSTRUCTION DETAILS	06	0	1	2	
486/4/9-0954-007	PRV SWITCHBOARD EQUIPMENT LIST	07	0	1	2	
486/4/9-0954-008	SWITCHBOARD CABLE & LABEL SCHEDULE	08	0	1	2	1
486/4/9-0954-009	SOLAR PANEL SWITCHBOARD GENERAL ARRANGEMENT	09	A	0	1	
486/4/9-0954-010	SITE OVERALL LAYOUT	010	Α	0	1	
486/4/9-0954-011	HALE STREET SOLAR PANEL SWITCHBOARD	011	A	0	1	

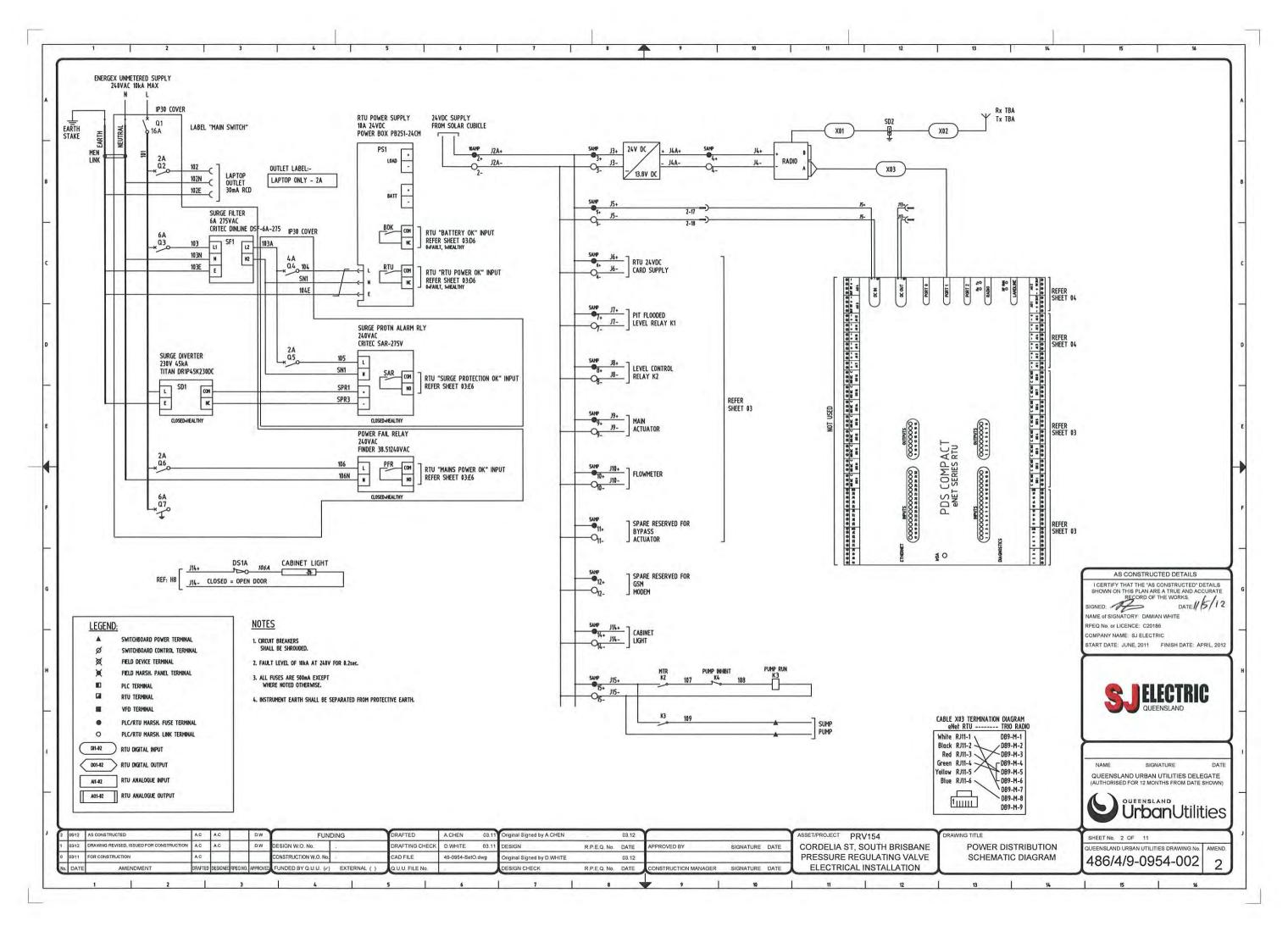
PEQ No. or LICENCE: C20186 MPANY NAME: SJ ELECTRIC QUEENSLAND URBAN UTILITIES DELEGATE **Urban**Utilities 486/4/9-0954-001

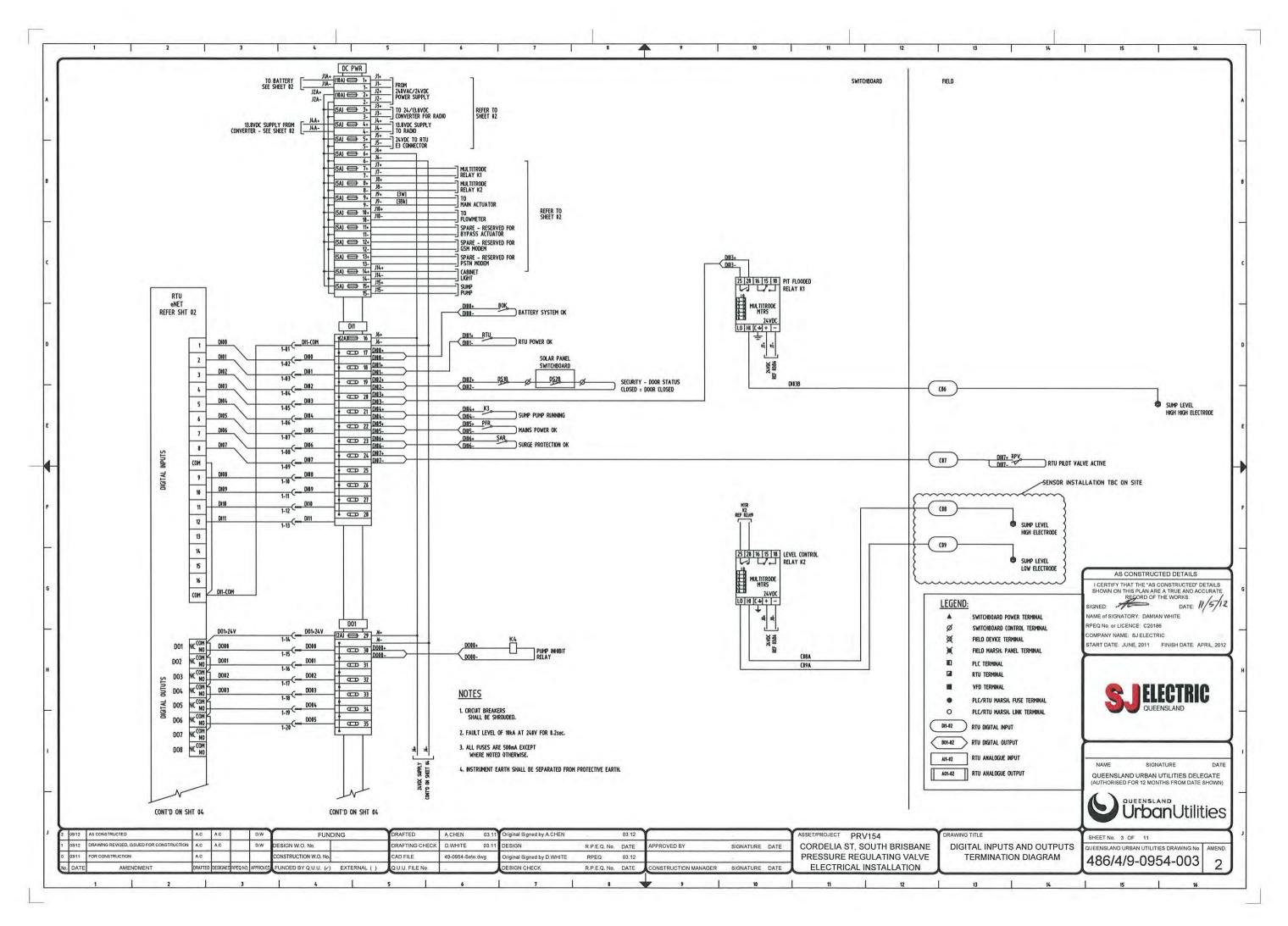
RAFTING CHECK D WHITE AD FILE RPEQ original Signed by D.WHITE

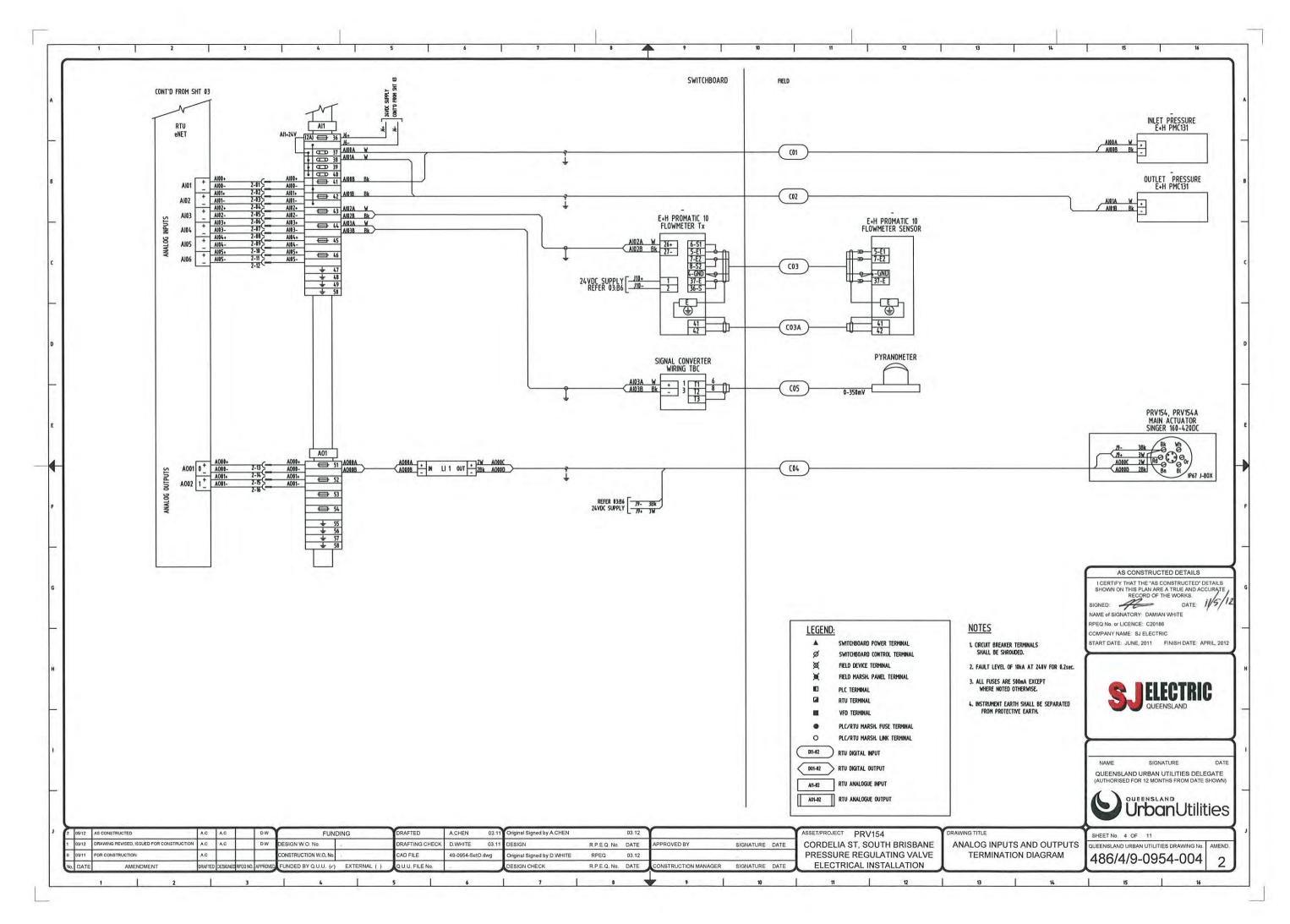
CORDELIA ST, SOUTH BRISBANE PRESSURE REGULATING VALVE ELECTRICAL INSTALLATION

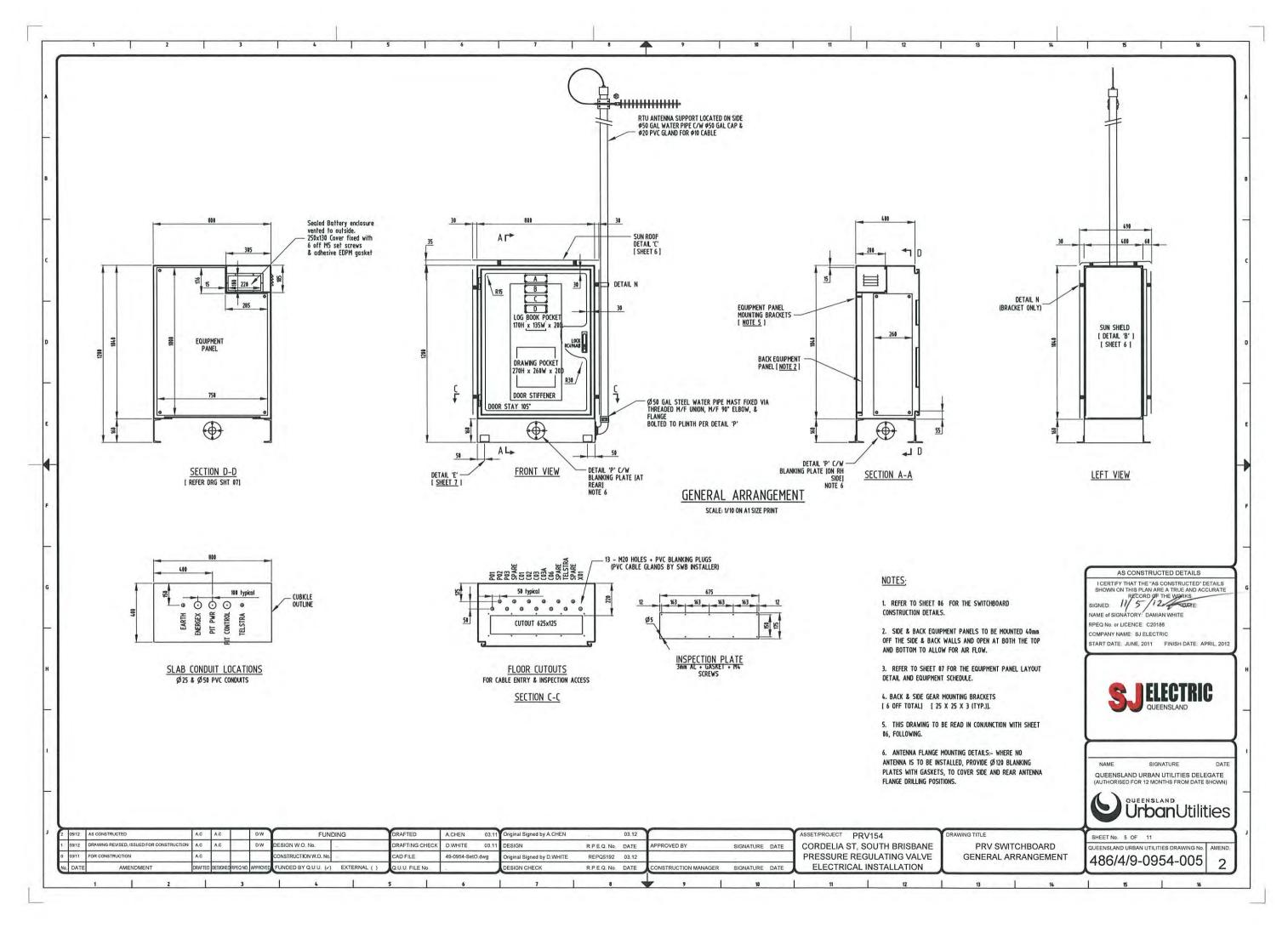
ELECTRICAL DRAWING

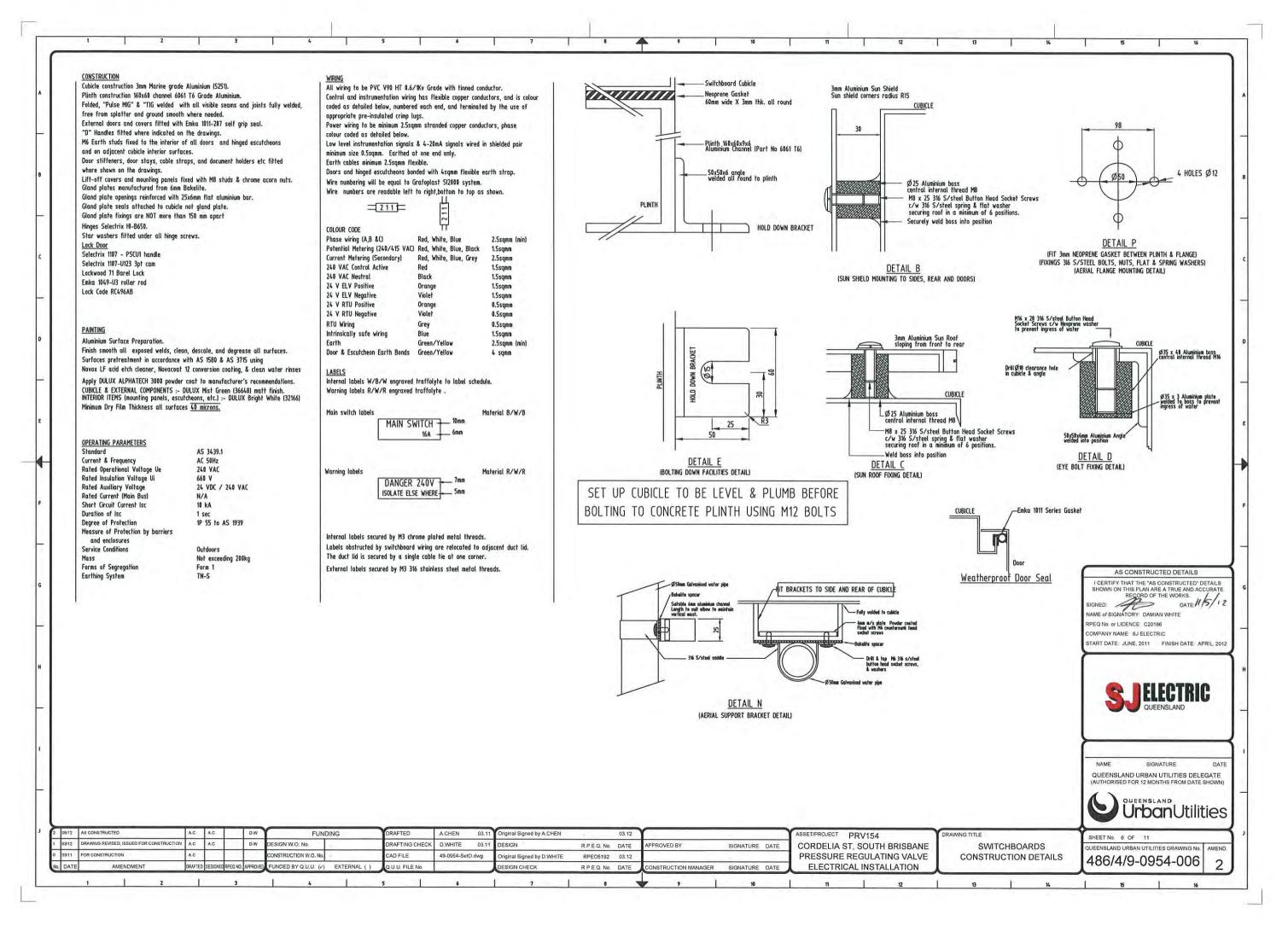
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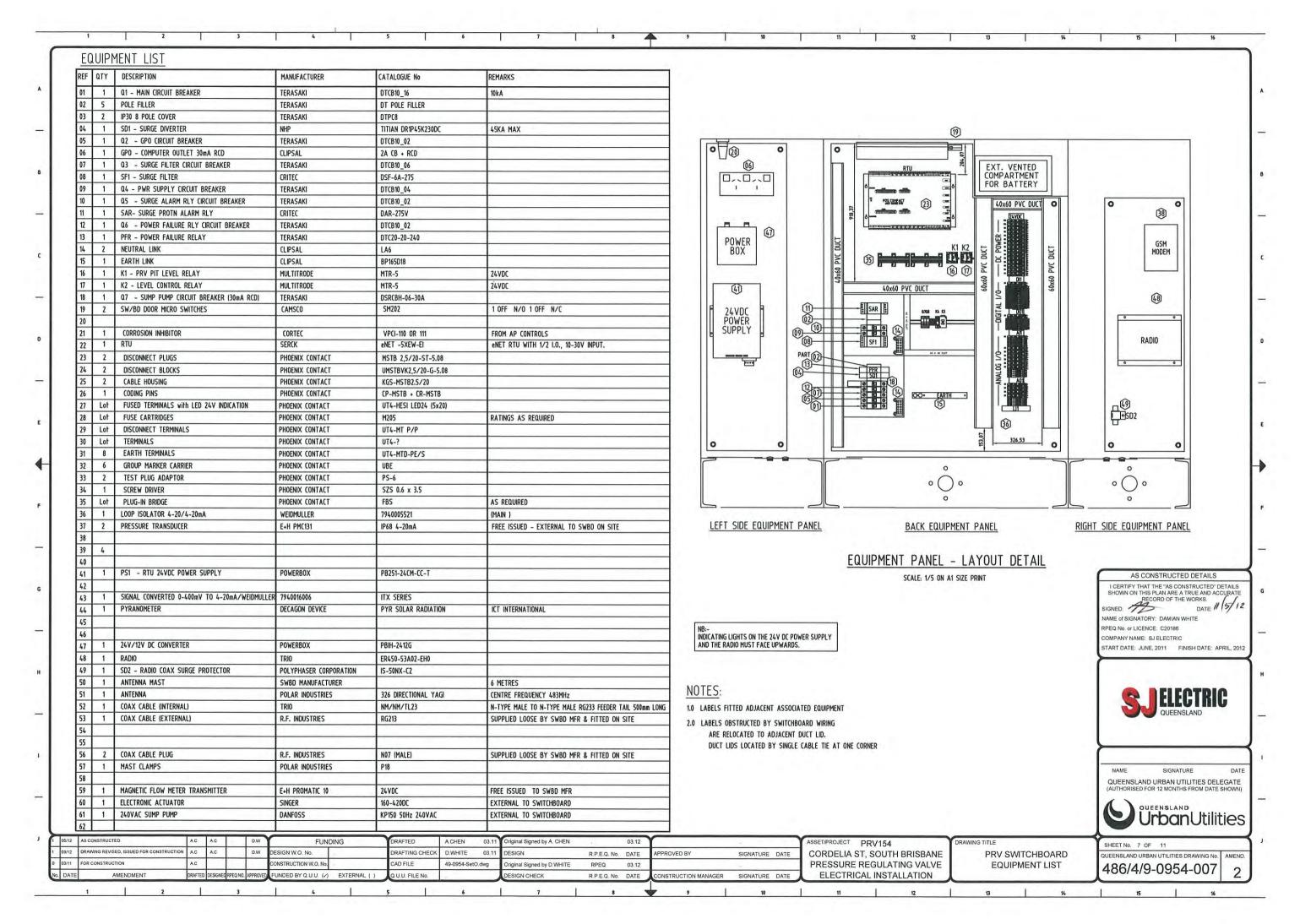


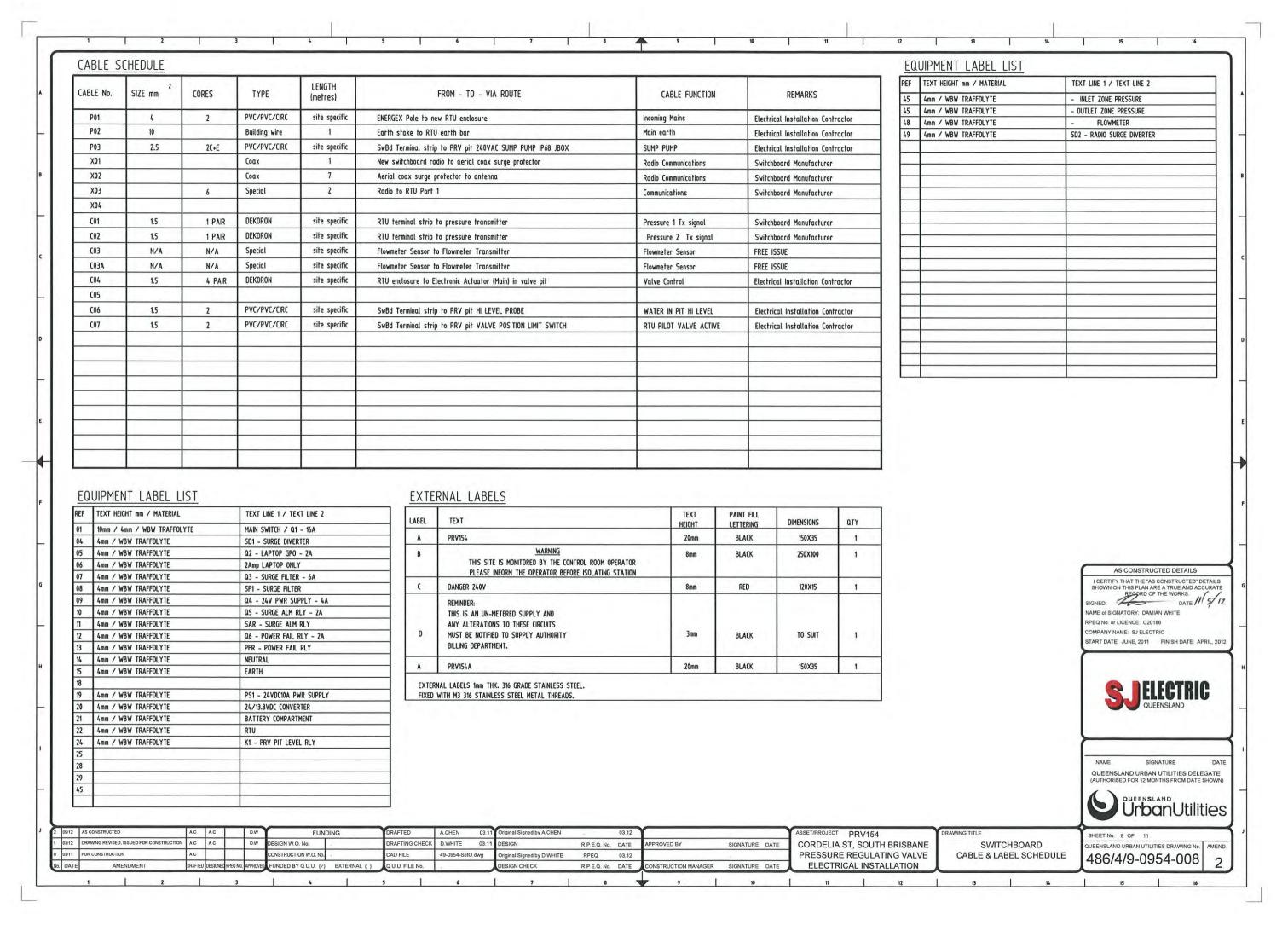


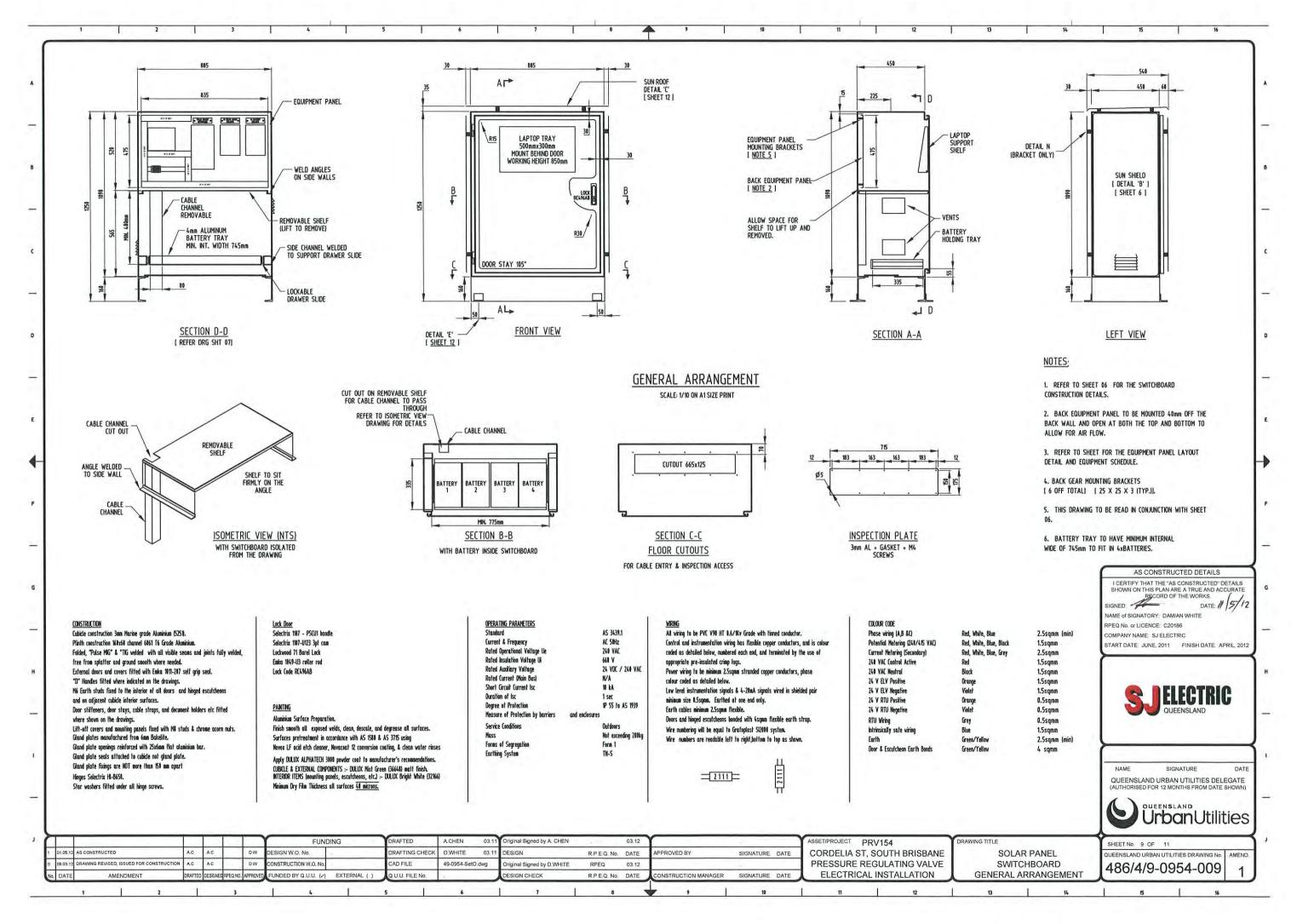


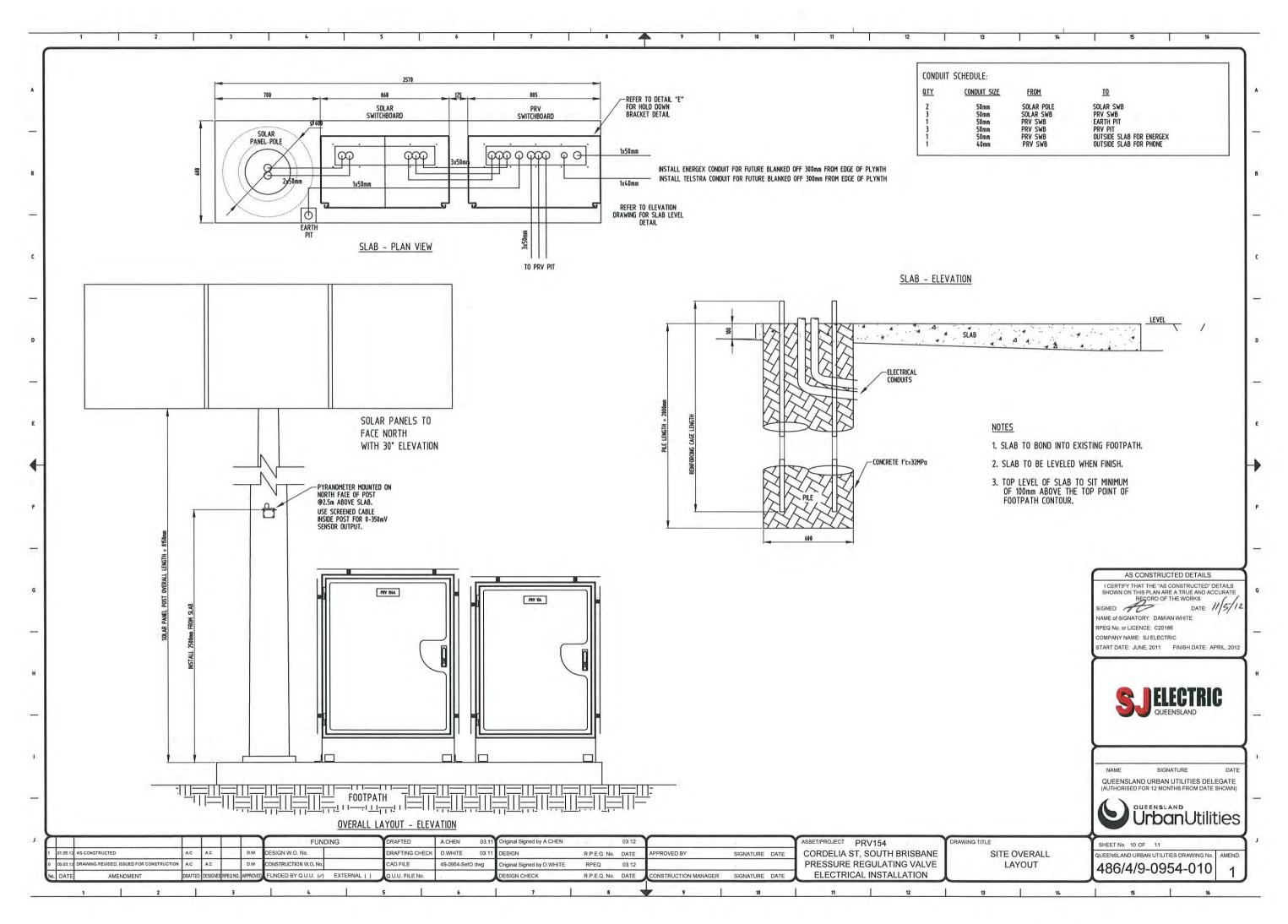


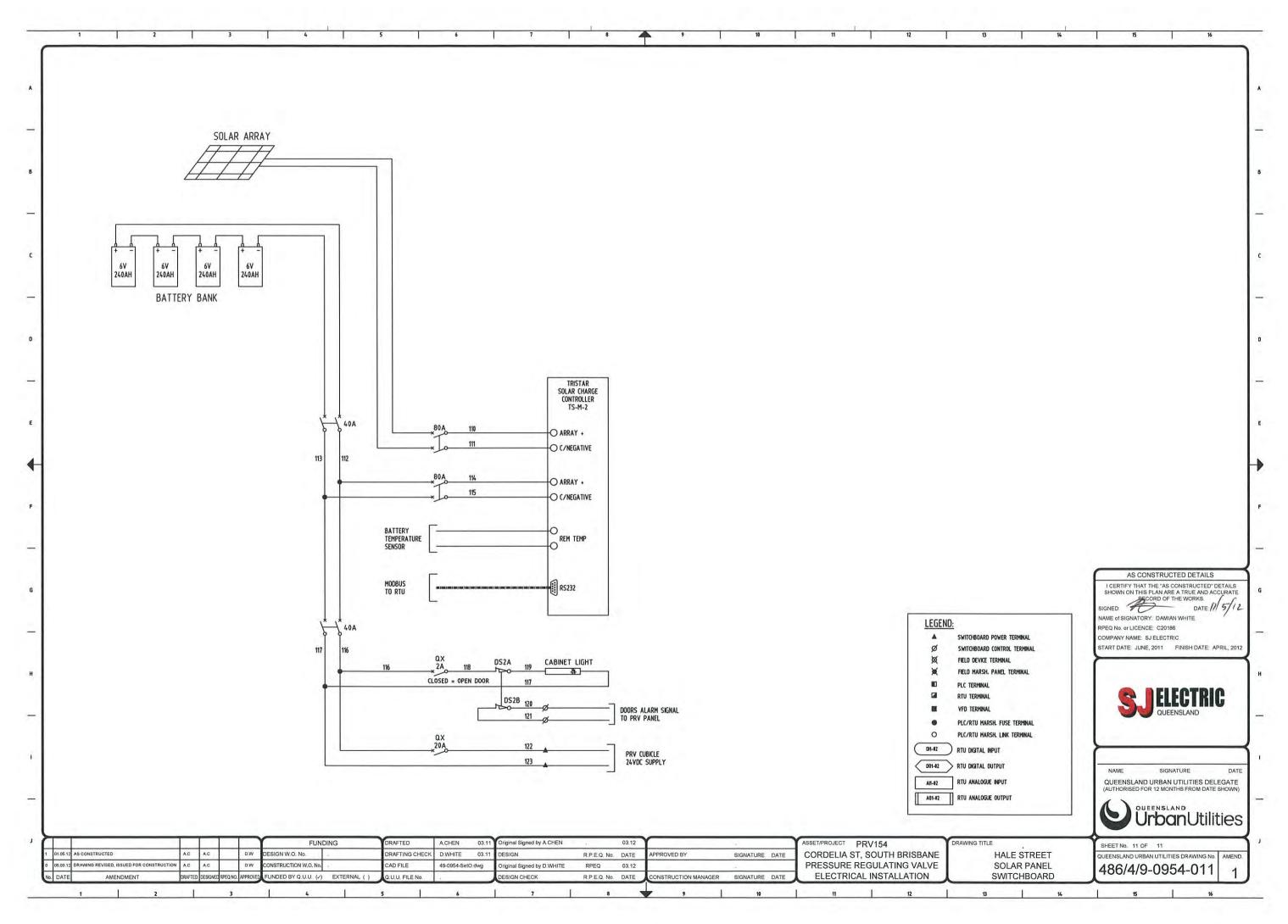












4. Inspection & Test Results

Ref: SJQF 502

Inspection and Test Check List

Date:	19	July	2007

TOO O	ractor / Order No.		ric Job No.	43400	0306
	No. 003 Date: 9(3(12	2	Co	rrespondi	ng ITP No. 001
eneral		1	11/16	NATION	CONTINUITY TEST
Built	By: CLEION tion Tested: WORKSHOP	Test Equ	ipment: M	IN PLA	AMP METED
Locat	tion Tostad: LADVCHOD	T K	UORTE O	3132A	IMP METER
Local	tion rested. WORKSHOP	Type:	OF IKONI	e Tac	10
Drg r	rev No:	Serial No	08007	466	
ieck Li	ist (Tick () acceptable items only, note deviations	under "REMA	RKS") (If not	applicable m	ark as N/A)
	Switch Board and Contro				
Item	Activity Description		Hold Points	Checked	By (Initial)
	Busbar		/	Сиссиси	Dy (Initial)
X	Correct size busbar to rated current load to meet A	AS 2067		()	
2	Appearance is good i.e. Straight & level	/		()	
3	Correct phase identification	/		()	
4	Correct hole sizes for joins and terminations			()	
5	All clearances have been meet			()	
6	Correct busbar support material has been used			()	
7	Busbar supports are at the correct distances apart			()	
8	Correct tensioning & blue sported at all joins & te	rminations		()	
9	Correct hole format in joining cubicle				
10	Sufficient clearances for terminating cable				
11	Heat shrink attached to flags for terminations	\			
12	All joins are dressed flat	1		()	
13	Busbar is insulated at supports	1		()	
	Cabling			,	
15	Correct size for demand of circuit			(V)/	03
16	Correct phase colouring			(1)	23
17	Correct termination & insulated			(1)	CB
18	Correct numbering			(V)/	CB
19	Correctly formed and neat			(\(\)	65
20	Correctly supported			$(\checkmark)_{/}$	33
21	All cable entry holes are insulated			(1)	GB
22	Check cable tray is mounted correctly & all sharp are removed	surfaces		(-),	
23	All cable ties are neatly trimmed				CB
24	All cable clear from busbar's			(-)	710
25	Check all analog inputs and outputs are shielded All shielded cables have been earthed			(-)	_
26	All Shielded cables have been earthed			(-)	

Inspection and Test Check List

Ref: SJQF 502 Date: 19 July 2007

ltem	Activity Description	Hold Points	Checked	By (Initial)
	Switchgear			
1	Check all main switches & circuit breakers are the	correct		12
	current rating		(V)	90
	ka rating.		(V)	GB.
	trip settings			(33)
	correct to cabling		(4)	CAD-
	• to labels.		(-)	(45)
	shunt trips		(-)	20
	inter locks		(-)	90
2	Check the fixings			Gb.
3	Check the number of poles		(8)	db
4	Check correct operation		(4)/	36
5	Correct mechanism		(1)	633
	Control Switches		``	40
6	Check correct number of positions		()	
7	Check correct size		()	
			()	
8	Check correct to labels		()	
9	Check mountings		()	
	Contactors			- NIP
10	Check for correct model no		(-)	m
11	Check for correct current rating to control		(V)/	95
12	Correct auxiliary contacts		(4)	(4)5
13	Correct phasing		(~)/	CB CB
14	Correct coil size		(~)	40
15	Check that it is accessible		(•)	GR
16	Check it has correct overloads		(-)/	-
17	Correct labelling		(1)	90
	Relays and Timers		/	
18	Check correct rated voltage		(V)	CB
19	Correct contacts		(V)	CB
20	Correct variances		(-)	
21	Dip switches in required position		(-)	_
22	Timers set to correct settings		(-),	
23	Correct operation		(~)	Cib
24	Correct auxiliaries		(\rightarrow)	1
	Transformers and Power Supplies		/	
25	Check for correct voltage ratings	3 L	(1)/	CB
26	Check for correct current ratings		(1)	Co
27	Check cabling is correct (no crossed voltage)		(1)	(3)
28	Check the secondary has been earthed when applie	cable	(1)	Cas
29	Check correct labelling		(1)	G15
30	Check mountings		(V),	35
31	Check for clearance around for heat extraction		(1)	CB
	arks/Remedial Action Required:			
	roved By: CLEW BASON		Date	2.
		Checked By: Zuvic	nt Pa	poiller
Elec	etrical Licence No. 113407	Signature:		Date:
the p	ne above signatories certify that the Electrical switcht prescribed procedure and that such work complies i 200 2007 and AS3008.1 1998	n every respect with the	n checked and requirements	tested in accordar of the Electricity Ac

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Ref: SJQF 502

Inspection and Test Check List

Date: 19 July 2007

	Activity Description	Hold Points	Checked	By (Initial)
	Fuses			
	Check that the cartridge is correct size		()	
2	Correct mountings		()	
3	Correct labelling		()	
4	Check that line side conductors are SDI and < 500mm		()	
	Current Transformers			
6	Correct ratio & size		()	
7	Correct direction of feed		()	
8	Correct earthing		()	
9	Correct cabling		()	
	Voltage / Current Monitoring Equipment			
10	Correct voltage / current range on meter to the installation		()	
11	Correct to ratio on Cts		()	
12	Voltmeter terminations are insulated			
13	Check that all meters are preset to zero			
14	Correct indication labels applied		()	
,	Indication Equipment			
15	Correct colour		()	
16	Correct voltage size with matching lamp attached			
17	Correct operation eg. Push to test		()	
18	Correct labelling			
	Terminal Blocks			
19	Correct size to cable		(1)	OR.
20	Correct colour coding		(./	02
21	Correct numbering		(-)	40
22	Correctly mounted with lock ends		(1)	Oh
23	Correct labels		()	72
	Neutral Links			40
24	Check that they are accessible	77	(V),	B
25	Correct labelling		(8)	73
26	Correct numbers stamped to match circuit identification		(1)	12
27	Correct cabling to circuit identification		(5)	33
28	Check that all neutral links & bar are insulated from the		/	- GP
	switchboard frame		(✓)	CB
	Earthing		/	
29	Check that all main earth bar is correct size		(v)/	GB
30	Check that the main earth is continuous		(\(\)	93
31	Correctly labelled		(🗸)	Co
32	Continuous for CT wiring		(-)/	
33	Check that all doors with equipment mount are electrically	1	1	COR
34	earth		(1)	90
34	Check all frames are earthed		(V)	Co

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Ref: SJQF 502

Inspection and Test Check List

Date: 19 July 2007

tem	Switch Board and Control Panels Construc			D- /1-1/1-1
Make	Activity Description Earthing Resistance & Continuity Test (Note all readings should be < .5 ohms) sure the MEN connection is removed and attach lead to main earth connection point than test with other lead between	Hold Points	Test Result	By (Initial)
1	The frame of each section		20·1 Ω	CR
2	The doors		(O''I Ω	63
3	All mounting bolts to all equipment		<0.1 Ω	CB
4	All brackets		(0.1 Ω	GB
5	All earth links		(0.1 Ω	CB
6	All bolts & threads for the mounting of escutcheon		Ω	~
7	All gland plates		Ω	
8	All cable trays		- Ω	-
9	All earth connection		<0.T Ω	CB
10	Earth secondary of transformers and power supplies		<0.1 Ω	(B)
11	Earth surge diverters		(O·1 Ω	GB
12	Current transformers		- Ω	
	Insulation Test	Hold Points	Test Result	By (Initial)
1	Make sure all control fuses and earths are removed from all electronic equipment before this test is carried out and Set insulation tester (meggar) to 500 volts before proceeding			
	Red - White		Ω	-
	Red - Blue		- Ω	~
	Red - Earth		7200 MΩ	95
	Red - Neutral		7200MΩ	415
	White - Blue		- Ω	Eller
	• White - Earth		- Ω	
	White - Neutral		- Ω	
	Blue - Earth		- Ω	
	Blue - Neutral		- Ω	
2	If all readings are clear the insulation tester is to be set at 1000 volts then proceed with the following			
	Red - White		Ω	
	Red - Blue		Ω	_
	White - Blue		Ω	

Inspection and Test Check List

Ref: SJQF 502 Date: 19 July 2007

(SJOF 502) Switch Board and Control Panels Construction Check List Checked By (Initial) **Activity Description** Item Points 2.5 KV Test This test is used to prove all busbar construction Make sure all control fuses and earths are removed from all electronic equipment before this test is carried out All the following tests must be set at a 1 minute time period, result 2 should be 0 Amps Hold Test Result By (Initial) **Points** 3 Test between: Red - White Red - Blue Red - Earth Red - Neutral White - Blue White - Earth White - Neutral Blue -Earth Blue - Neutral Supply Authority section Check supply authority main isolator lockable in the on position 1 Check all doors before the Ct's. Or meters are lockable 2 Check where the neutral link is located for the site connection if 3 metres are remotely mounted Check where the earth link is located for the site connection if 4 meters are remotely mounted Check double insulated cable for POT fuses are less than \$00 mm 5 Check double insulated cable are taken on line side of Ct.s 6 Check metre wiring is in building wire and correct size Check if Ct meter wiring is in steel conduit when closer than () 8 100mm to other conductors Check there is no equipment connected before on the line side of () 9 meters or Ct.s (i.e., surge diverters) Check list may vary if switch board is going interstate. Alter where () applicable Remarks/Remedial Action Required: Remedial Actions Completed Signature: Approved By: Checked By: Laurent Pavalle Signature: Electrical Licence No. 113407 Signature:

All the above signatories certify that the Electrical switchboard work listed has been checked and tested in accordance with the prescribed procedure and that such work complies in every respect with the requirements of the Electricity Act 2002, AS3000 2007 and AS3008.1 1998

Ref: SJQF 502

Date: 19 July 2007

Inspection and Test Check List

Switch Board and Control Panels Construction Check List (SJOF 502) **Hold Points** Checked By (Initial) **Activity Description** Item **Functional Test Hold Points** Checked By (Initial) Prior to connection of supply all inspection and test check lists must be completed Point to point test on all cables as per schematic and single (V) line drgs. (Leave spot for drawing. No's and Rev No's Check all Cts are not open circuit (-) By (Initial) **Hold Points** Test Result Connect supply (personal protection equipment must be used) Sheck polarity of connection V Red - White Red - Blue V Red - Earth V Red - Neutral V White - Blue V White - Earth White - Neutral V Blue -Earth V Blue - Neutral V **Hold Points** Checked By (Initial) (1) 4 Correct voltage / eurrent range on meter to the installation Check functional operation of switchboard following 5 (-)specific construction issue drawings (leave spot for drawing No's and Rev No's Check operation of all RCD's < .03s 6 Pre delivery check list SIA Check all punch list items are complete 1 Check if Compliance label is mounted and correct Check if heat shrinks is supplied when necessary 4 Check all load bolts are supplied 5 Check if m.e.n is mounted after testing All drawings have been as built red lined and supplied to drafting office 6 Photos have been taken of every section and given to 7 manager Test reports have been photo copied and placed in the client (-) 8 folder and SJ Electric folder As built drawings received back from drafting office, verify (-) 9 Rev No. Manuals placed in client folder 10 Switch Board wrapped with delivery details supplied 11 (V) Copy of red lined marked Drawing As built drawings placed in client folder. (Latest revision (-) 12 Remarks/Remedial Action Required: Remedial Actions Completed Signature: . Approved By: Checked By: Lair ont Signature Electrical Licence No. 11340 Signature:

All the above signatories certify that the Electrical switchboard work isted has been checked and tested in accordance with the prescribed procedure and that such work complies in every respect with the requirements of the Electricity Act 2002, AS3000 2007 and AS3008.1 1998

5. Compliance Certificates



A Division of the Trivantage Group

19 Elliot Street, Albion QLD 4010 P 07 3256 1522 F 07 3256 1533

E mail@sjelectric.com.au ABN 22573962619 REC 7623

www.trivantage.com.au

Ref: Test Certificate PRV154

TEST CERTIFICATE

SJ Electric (Qld) Pty. Ltd. 19 Elliot Street. Albion Qld. 4010 R.E.C. 7623

Attention:

Mr Glenn Rolfe

Contracts Manager

Major Projects and Commercial Services

Queensland Urban Utilities

GPO Box 13277 George Street, Brisbane Qld 4003

Work performed for Queensland Urban Utilities at PRV154 Corner of Cordelia Street and Montague Road South Brisbane under contract BW: 70103-06/07 Order No 60 (SJ Electric Job Number 43400306)

Installation Tested / Equipment Tested

- Solar Powered Supply Switchboard
- Pole with Solar Panel
- QUU free issued PRV switchboard
- New Main earth
- Conduits etc

All supporting test sheets attached.

Test Date 19/4/2012

For the electrical installation, this certificate certifies that the electrical installation to the extent it is affected by the electrical work has been tested to ensure it is electrically safe and is in accordance with the requirements of the wiring rules and the electrical safety regulation 2002. C.J. Holmes (endorsee to electrical contracting license 73286)

For the electrical equipment, this certificate certifies that the electrical equipment, to the extent it is affected by the electrical work, is electrically safe. C.J. Holmes (endorsee to electrical contracting license 73286)

Signed

Q-Pulse ld: TMS172 15/10/2012 Page JRUYANTAGE