BRISBANE CITY COUNCIL

## Sewerage Pump Station SP144

## Lavarack Av \#1

## Eagle Farm

Contract : BW 70103-013<br>Job Number: WT400035

Volume 1

## ELECTRICAL INSTALLATION

## OPERATIONS and MAINTENANCE MANUAL

INSTALLATION BY:
SJ Electric (Qld) Pty Ltd
19 Elliot Street
Albion Qld 4010

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SP144 Laverack Avenue Eagle Farm SPS Electrical Installation Volume 1 OM Manual
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## Page 1

### 1.1 General Workplace Health and Safety

- The Workplace Health and Safety Act (1995) sets out the laws about Workplace Health and Safety for all workplaces, workplace activities and specified high risk plant. The Electrical Safety Act (2002) sets out the laws covering electrical safety. Nothing in this document is designed, in any way, to undermine the authority of the Acts.
- All reasonable care must always be taken to ensure the plant is without risk to the health and safety of personnel operating and maintaining plant and equipment.
- Employers have an obligation to ensure the workplace health and safety of all personnel at work.
- It is employer responsibility to ensure that all persons entering or working on the premises use appropriate personal protective equipment.
- Personal protective equipment includes gloves, safety glasses, hard hats, ear protection, safe foot ware and, where necessary, specialist protective clothing for hazardous areas.
- Any item of equipment should always be isolated before maintenance or repairs commence to ensure that inadvertent operation of the item does not result in risk to the health and safety of any person.
- Where the item is isolated, any total or partial shutdown should not allow a hazardous situation to be created.
- Where the item cannot be isolated, another person should be stationed at the controls of the item and an effective means of direct communication should exist between the persons carrying out the maintenance and the person at the controls.


## Page 2

## General Operating Principles

- All persons working the premises must be qualified Electrical Engineers or electrical trades persons capable of performing the required tasks competently. All personnel must also be familiar with plant and equipment.
- Adequate information, instruction, training and supervision must be provided to enable personnel to perform work without risk to health and safety.
- Work in an orderly way.
- Plan work in advance to avoid hazardous situations.
- Warn others of any hazards.
- Make inquiries before starting work, particularly on any unfamiliar installation or equipment.
- Before any work begins ensure that any instructions received or given are fully understood.
- Concentrate on the task on hand.
- Do not distract others or allow yourself to be distracted by foolish actions.
- Work from a safe and convenient position that provides a maximum working space that you do not have to over reach, you cannot slip, trip or stumble and so endanger yourself and others.
- Keep the working area tidy and free of unwanted materials and equipment.
- Use insulated tools where possible.
- Inspect tools and equipment regularly and ensure that any necessary maintenance is carried out.
- Keep yourself in good health.
- Do not work if ill or over tired, to the extent that your concentration, movement or alertness is affected. Illness or fatigue can endanger yourself and others.


## Page 3

### 1.2 Project Overview

Contract BW70103-013 was for the manufacture and testing of ten (1) new pump station switchboards for various locations throughout Brisbane.

Equipment provided by SJ Electric ensures safe and efficient operation of the pump stations. Equipment supplied and installed by SJ Electric includes: -

- Switchboards
- Instrumentation
- Civil Works

The switchboard incorporates the latest technology in motor control, power monitoring, and instrumentation. It is important engineers, technicians and operators are familiar with the equipment installed before attempting any adjustments, modifications or maintenance.

The following Sections of this manual contain a comprehensive description of all equipment supplied, by SJ Electric. It is recommended that this manual be referred to before carrying out any work on any equipment.

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### 1.3 Plant Maintenance

To ensure proper operation of the plant the following should be observed: -

- The plant should be kept clean and tidy at all times. Not only is this of aesthetic value, it extends equipment life.
- Check that all plant and equipment is operating correctly. Correctly operating equipment promotes overall plant efficiency.
- All items and areas of equipment should be hosed down and cleaned regularly.


## WARNING

## - Avoid directly hosing any drive motor or electrical item.

- All maintenance, service, modifications and significant deviations from Normal operating conditions should be recorded in the Plant Service Log
- After a month of operation, check the tension of all bolts associated with the plant and thereafter periodically. Bolted connections on painted surfaces can loosen due to thinning of the paint underneath the bolt head-bearing surface. Motor mounting bolts and other bolted connections subjected to vibration should be periodically checked for loosening.


## WARNING

- Before starting work on any item ensure that the power supply is isolated, tagged off, and the item cannot be started.
- The importance of preventative maintenance cannot be over-emphasized. Regular maintenance and suitable care of the equipment will ensure a long and reliable service life of the equipment.
- Many stoppages can be avoided by following the recommended maintenance procedures. Do not wait until you hear the grinding of equipment that has broken down. If you see any item wearing down, replace it, before it causes damage to other associated items.

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## Preventive Maintenance

Maintenance procedures recommended to extend switchboard life are outlined as follows: -

- Switchboard exterior should be regularly wiped down with a solvent base cleaner such as "Spray \& Wipe". This will ensure longevity of the powder-coated surface.
- Accessible areas like distribution boards and motor starter panels should be cleaned with a vacuum cleaner to remove dust and foreign matter.
- PLC panels should be maintained as dust free as possible. Dusting with a dry rag is recommended - taking care not allows dust inside the I/O modules or processor.
- When removing or installing PLC modules care should be taken to ensure that power is turned off to the rack before modules are removed or installed.
- Connections and efficient operation of circuit breakers, contactors and isolators should be checked every 12 months - especially where connected to busbars.
- Busbar connections should be checked every 12 months.
- Globes for indicator lights should be checked on a weekly basis with any faulty lamps replaced.
- Cubicle Fans Filter should be inspected and cleaned frequently.


### 1.4 Electrical Control System

## General Description

The switchboards are manufactured from 3 mm aluminium and are suitable for location outdoors; the switchboards have been designed by Brisbane Water and contain several separate sections including:

- Incoming Section.
- Metering.
- Motor Starter Section.
- Distribution Section.
- RTU Section.


### 1.5 Control and Monitoring System.

The control and monitoring of the system is performed by the Brisbane Water telemetry system and was not included in this contract.

# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144

 Lavarack Av \#1 Eagle FarmEquipment Type: Circuit Breaker
Location: Main Incomer
Pump Circuit Breakers
Model Numbers: ..... XS 400
Manufacturer: ..... Terasaki
Supplier:
NHP Pty Ltd
25 Turbo Drive
Coorparoo QLD 4151
Ph: 0738916008Fx: 0738916139

## TemBreak MCCBs

## XS400 series thermal magnetic type

```
- Adjustment range 63-100\% of nominal current rating.
- Standards AS 2184/AS/NZS 3947-2.
- Adjustable thermal and magnetic trip.
```

XS400CJ ( 35 kA ) 3 pole


## Standard TemBreak circuit breaker Selection guide



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## Standard TemBreak circuit breaker Selection guide



| - | - | - | - | * | - |
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| 0 | O | 0 | - | - | - |
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| 0 | a | 0 | $\bigcirc$ | 0 | 0 |
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|  | : | : | : | - | : | : |  |

MCCB operational characteristics \& dimensions
Page

| Thermal - magnetic MCCB characteristics | $\mathbf{7 - 2}$ to $\mathbf{7 - 4}$ |
| :--- | ---: |
| Time / current characteristics thermal - magnetic MCCBs | $\mathbf{7 - 5}$ to $7-10$ |
| Electronic MCCB characteristics - settings | $\mathbf{7 - 1 1 \text { to } 7 - 1 4}$ |
| PTA - Pre-trip alarm option | $\mathbf{7 - 1 5}$ to $7-19$ |
| GF - Ground fault / 4th CT option | $\mathbf{7 - 1 8}$ to $\mathbf{7 - 1 9}$ |
| LED trip indication options | $\mathbf{7 - 2 0}$ to $7-22$ |
| Time / current characteristics electronic MCCBs | $\mathbf{7 - 2 3}$ |
| OCR checker for electronic MCCBs | $\mathbf{7 - 2 4}$ |
| TemCurve selectivity software | $\mathbf{7 - 2 5}$ to $7-50$ |
| MCCB dimensions with and without motors fitted | $\mathbf{7 - 5 1}$ |
| AC Watts loss - 3 pole MCCB |  |



## MCCB Technical data

## Thermal Magnetic MCCBs

Thermal-Magnetic MCCBs are available from 125 AF to 800 AF. Depending on the type of MCCB thermal and/or magnetic trip setting may be adjustable.

| MCCB type | Fixed thermal | Adjustable thermal | Fixed magnetic | Adjustable magnetic |
| :---: | :---: | :---: | :---: | :---: |
| XS125CS, XS125NS | - | - | - | - |
| XS125CJ, XS 125 NJ | - | - | - | - |
| XH125NJ, XH125PJ, TLI00NJ | - | - | - | - |
| XH160PJ | - | - | - | - |
| XE225NC | - | - | - | - - |
| XS250NJ, XH250NJ | - | - | - | - |
| XH250PJ | - | - | - | - |
| XS400CJ, XS400NJ, XH400PJ, TL250NJ | - | - | - | - |
| XS630CJ, XS630NJ, XH630PJ | - | - | - | - |
| XS800NJ | - | - | - | - |
| XH800PJ | $\cdot$ | - | - | - |

## Note: Yes

- No


## Access to setting dials

From 125 AF to 250 AF the thermal adjustment is visible from the front of the MCCB. At 400 AF and above a protective cover must be removed to gain access to the settings. To achieve access to the settings, the cover screw under the 'sealed' label must be removed. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver.
Once set, secure the cover and apply a new sealing label.


XH250NJ


XS400NJ


XS400NJ (cover removed)

## MCCB Technical data

## Thermal Adjustment

TemBreak MCCBs have a wide thermal adjustment range, one of the largest on the market. The rated current ' l ' is continuously adjustable from $63 \%$ to $100 \%$ of its nominal current 'In'. There are three main points of calibration marked at $63 \%, 80 \%$ and $100 \%$, as shown in the diagram below.

## Magnetic Adjustment

The magnetic adjustment is available on MCCBs of 400 AF and above. The magnetic setting ' 1 m ' is continuously adjustable from $500 \%$ to $1000 \%$ of its rated current ' 1 n '. There are five main points of calibration marked as multiples of $\mathrm{In}_{\mathrm{n}}$ 5, 6, 7.1, 8.5 and 10 . These are shown in the diagram below.


## Examples

1. $\mathrm{XS} 125 \mathrm{NJ} / 125 \mathrm{~A}$ MCCB set at $\mathrm{I}_{\mathrm{r}}=0.8$, the rated current is calculated as $125 \times 0.8=100 \mathrm{~A}$
2. XS400NJ/400A MCCB set at $I_{m}=6$, the magnetic setting is calculated as $400 \times 6=2400 \mathrm{~A}$
3. XS630NJ/630A MCCB set at $\mathrm{I}_{\mathrm{r}}=0.8$ and $\mathrm{I}_{\mathrm{m}}=5.0$

The rated current is calculated as $630 \times 0.8=504 \mathrm{~A}$
The magnetic setting is calculated as $630 \times 5=3150 \mathrm{~A}$
Note that the magnetic setting is a multiple of the nominal current In and not the rated current Ir.
All thermal and magnetic trip settings are expressed as AC RMS values.
All MCCBs are calibrated at $45^{\circ} \mathrm{C}$ unless otherwise specified.
Breakers with adjustable magnetic trip

|  | Rated <br> current (A) |  |  |  |  |  | Magnetic trip current (A) |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| Scale 10 | $\mathbf{8 . 5}$ | $\mathbf{7 . 1}$ | $\mathbf{6}$ | $\mathbf{5}$ |  |  |  |  |  |
| Breaker | 250 | 2500 | 2125 | 1775 | 1500 | 1250 |  |  |  |
| XS400CJ | 400 | 3400 | 2840 | 2400 | 2000 |  |  |  |  |
| XS400NJ | 400 | 4000 | 3400 | 2840 | 2400 | 2000 |  |  |  |
| XH400PJ | 400 | 4000 | 3400 | 2840 | 2400 | 2000 |  |  |  |
| XS630CJ | 400 | 6300 | 5355 | 4473 | 3780 | 3150 |  |  |  |
| XS630NJ | 630 | 6300 | 5355 | 4473 | 3780 | 3150 |  |  |  |
| XH630PJ | 630 | 8000 | 6800 | 5680 | 4800 | 4000 |  |  |  |
| XS800NJ | 800 | 8000 | 6800 | 5680 | 4800 | 4000 |  |  |  |
| XH800PJ | 800 |  |  |  |  |  |  |  |  |

Note: Settings; 3-poles can be adjusted simultaneously with one adjustment dial.

## MCCB Technical data

Time/current characteristic curves


Ambient compensating curves


## Example 1

The XS250NJ set at its maximum thermal setting of 250A experiences an overload of 1000A. What would be the tripping time?

## Solution

As the axis are 'percent' rated current the overload as a percentage to rated current is

$$
\frac{100 \mathrm{~A}}{250}=400 \%
$$

The maximum and minimum on the curve are the tolerance bands. Therefore at $400 \%$ overload the tripping time would be as follows:
Maximum trip time $\approx 30$ seconds
Minimum trip time $\approx 10$ seconds
Average trip time $\approx 20$ seconds
Due to strict quality control of the manufacturing and calibration processes, the characteristic curve of most MCCBs will follow the 'average' curve within the tolerance band.

## Example 2

The XS250NJ is calibrated at 250 A for $45^{\circ} \mathrm{C}$ ambient. If the temperature rose to $55^{\circ} \mathrm{C}$ what effect would this have?

## Solution

At $55^{\circ} \mathrm{C}$ the ambient compensating factor is $93 \%$,
i.e. $250 \times 0.93=232.5 \mathrm{~A}$

In other words the XS250NJ would act as an MCCB set at 232.5 A , in $55^{\circ} \mathrm{C}$.

## MCCB Technical data



Ambient compensating curves


XS125CJ, XS125NJ, XH125NJ, XH125NJ
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## XE225NC

Time/current characteristic curves


Ambient compensating curves


XH160PJ, XS250NJ, XH250NJ
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

```
XH250PJ, XS400CJ, XS400NJ,
XH400PJ
```

Time/current characteristic curves


Ambient compensating curves


XS630CJ, XS630NJ, XH630PJ

Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## XS800NJ, XH800PJ

Time/current characteristic curves


Ambient compensating curves


XM30PB
Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## TL30F

Time/current characteristic curves


Ambient compensating curves


## TL100NJ

Time/current characteristic curves


Ambient compensating curves


## MCCB Technical data

## TL250NJ

Time/current characteristic curves


Ambient compensating curves


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## MCCB Technical data

## Microprocessor based characteristics and adjustments

## Characteristics

The standard microprocessor based MCCB from Terasaki has the most flexible characteristics on the European market. In addition to the standard overload and short circuit protection, there are a number of options available to meet specific applications.


| Legend |  | Application |  |
| :--- | :--- | :--- | :--- |
| LTD | Long Time Delay | Overload protection, True RMS |  |
| STD | Short Time Delay | Short circuit protection and selectivity |  |
| INST | Instantaneous | Short circuit protection, fast acting | Standard for all |
| I2t RAMP |  | Provides easier grading with downstream fuses | TemBreak |
| Pick-up LED |  | Lights on LTD overload, flashes on PTA pick-up | MCCBs |
| Test Port |  | Facility for TNS-1 OCR checker for calibration checking |  |
| PTA | Pre-Trip Alarm | Useful for loadshedding application |  |
| GFT | Ground Fault Trip | Protection against ground faults |  |
| LEDs | Light Emitting Diodes | Indication of fault for faster diagnosis |  |
| HI-INST | High Instantaneous | High inrush applications, increased selectivity |  |

## Access to setting dials

To adjust the settings on the microprocessor TemBreak, the sealed label must be broken and the cover fixing screws removed. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver. Align the setting required between the black dots marked on the dial.


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## MCCB Technical data

Microprocessor based characteristics adjustments, operation, settings

Standard time current curves


Standard microprocessor adjustments


| Setting Dial |  | Available adjustments |  |
| :--- | :--- | :--- | :--- |
| Base current setting | $I_{0}$ | $0.63-0.8-1.0 \times \mathrm{In}_{n}$ | Amps |
| LTD pick-up | $\mathrm{I}_{1}$ | $0.8-0.85-0.9-0.95-1.0 \times \mathrm{I}_{0}$ | Amps |
| LTD setting | $\mathrm{T}_{1}$ | $5-10-15-20-25-30\left(\right.$ at $\left.\mathrm{I}_{1} \times 600 \%\right)$ | Secs |
| STD pick-up | $\mathrm{I}_{2}$ | $2-4-6-8-10 \times \mathrm{I}_{0}$ | Amps |
| STD setting | $\mathrm{T}_{2}$ | $0.1-0.15-0.2-0.25-0.3$ | Secs |
| INST pick-up | $I_{3}$ | $3-12-\times \mathrm{I}_{0}$ (continuously adjustable) | Amps |

Note: A special generator $T_{1}$ setting adjustment of $1-5 \mathrm{sec}$ (at $l_{1} \times 600 \%$ ), is also available. Please contact NHP for details.

## MCCB Technical data

## Adjustment of TemBreak (electronic type) tripping characteristics

Electronic models of TemBreak come standard with an 8 -bit microprocessor overcurrent relay (OCR). It is the OCR which provides the functions necessary for protection, while maintaining a high level of reliability.

Note: The ground fautt trip and pre-trip alarm cannot be used simultaneously in a single breaker.

The wide OCR adjustment range allows the circuit breaker to be set-up in order to trip under certain conditions. Adjustments can be made to the tripping current as well as the tripping time of the breaker,

Front view


Figure 1. Electronic OCR adjustment possible (with label removed).

## Adjustment method

Remove the sealing label, loosen and remove the cover fixing screws and remove the cover. To adjust the individual trip settings, turn the setting dial with a flat bladed screwdriver.

Note: Align the groove (end marked with dots) between the bands for the required setting.
For example, the diagram right shows $10=1.0$
The INST and GFT pick-up currents are continuously adjustable.


Secure the cover and apply the sealing label.


## (4) TERASAKI

## MCCB Technical data

## Microprocessor based characteristics - adjustments, operation and examples

## Overload adjustment

The rated current of the microprocessor based TemBreak is adjusted using two current multipliers. This process achieves high accuracy adjustment from $50 \%$ to $100 \%$. These are the LTD pick-up dial ( 11 ) and the Base Current ( 10 ) selector switch. The rated current (LTD pick-up) is achieved as follows:
$I_{\text {rated }}=\ln \times 10 \times l_{1}$
In the example shown on the right the rating would be:
$I_{\text {ratien }}=1250 \times 1.0 \times 1.0=1250 \mathrm{~A}$
In total there are 15 possible increments of adjustment between 50 and $100 \%$ as shown below.


Base current


Current dial

Breaker
rated current


## Example - Settings

In the example shown on the right, what are all the settings in Amps?

## Solution

Irating LTD pick-up $=\ln \times \operatorname{lo} \times 11$


## Example - Time/Current curves



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## MCCB Technical data

## Options (electronic type) TemBreak

Pre-trip alarm (PTA)
The PTA continuously monitors the true RMS value of the load current. When the load current exceeds the pre-set current (Ip) an LED gives local alarm that the MCCB is approaching an overload situation.
Should the current ip be exceeded for 40 secs a ( $\mathrm{N} / \mathrm{O}$ ) contact will close to provide remote indication and/or load shedding.

## PTA specifications

Pick up current (A): [1/]


Adjustable steps of $70,80,90,100 \%$ of the selected rated current [ 11 ].
Setting tolerance $\pm 10 \%$
Note: The long time-delay trip does not operate 'first' when the pick-up current is adjusted to $100 \%$ of the rated current [ 11 ].

PTA characteristics


Operating time (s) [Ip] Output contact

40 secs (fixed definite time-delay) setting tolerance is $\pm 10 \%$ Normally open contact, (1a) Integral lead is standard length ( 450 mm )

|  |  | Resistive load | Inductive load |
| :--- | :--- | :--- | :--- |
| Rating of <br> contact | 250 V AC | $125 \mathrm{VA}(2 \mathrm{~A} \mathrm{max})$ | $20 \mathrm{VA}(2 \mathrm{~A} \mathrm{max})$ |
|  | 220 V DC | $60 \mathrm{~W}(2 \mathrm{~A} \mathrm{max})$ | $10 \mathrm{~W}(2 \mathrm{~A} \mathrm{max})$ |
|  | Pick-up LED flickers |  |  |

Inductive load
20 VA (2 A max) $10 \mathrm{~W}(2 \mathrm{~A} \max )$

PTA indication

## MCCB Technical data

## Adjustment of TemBreak electronic type OCR with ground fault

## Ground fault trip

The GFT pick-up current is continuously adjustable from $10 \%$ to $40 \%$ of the rated CT current.
Notes: The ground fault trip and pre-trip alarm cannot be used simultaneously in a single breaker.
XS400SE, XH400SE are not available with ground fault function.
When a three pole breaker is used in a 3 phase, 4 wire system, a separate CT is required for the neutral line. (refer NHP).

## GFI specifications

Pick-up current (A): [IG]


Continuously adjustable from 10 to $40 \%$ of the rated CT current (lct) setting tolerance is $\pm 15 \%$

Is X lor
Time-delay (S): [TG]


The GFT has a definite time-delay characteristic and is adjustable in steps of $0.1,0.2,0.3,0.4,0.8 \mathrm{~s}$. Total clearing time is +50 ms and resettable time is -20 ms for the preset time delay
GFT characteristics

## 4th CI for GFI



| Rating (A) | Type |
| :--- | :--- |
| 2500 | UXOY0007A |
| 2000 | UXOY0006A |
| 1600 | UXOY0005A |
| 1250 | UXOY0004A |
| 1000 | UXOY0003A |
| 800 | UXOY0002A |
| 630 | UXOY0001A |



Dimensions (mm)

| Rating (A) | A | B | C | D | E | F | H | CH | M | N |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2500-1000$ | 140 | 110 | 50 | 10 | 80 | 85 | 145 | 75 | 85 | 35 |
| $800-630$ | 105 | 100 | 40 | 8 | 50 | 75 | 110 | 57 | 50 | 20 |

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## MCCB Technical data

## TemBreak electronic type with ground fault

External neutral sensor (4th CT)
External neutral sensors are required whenever optional earth fault is used on 3 phase 4 wire systems

The position and direction of 4th CT
NEUTRAL BAR
EARTH BAR

The direction of 4th CT


## MCCB Technical data

## Trip indicators

The LEDs when lit, indicate which trip function tripped the breaker eg, long-time-delay (LTD), short-time delay/ instantaneous (STD/INST) or ground fault (GFT) (control power required).

Note: If a pre-trip alarm (PTA) is fitted, the LED control power can be used (common).

Trip indicator display (1250 AF and above)


Trip indicator display (400 AF to 800 AF ) and OCR controller example: XS, XH400
An optional feature available with TemBreak electronic type are An external trip indicator box is required with 400AF models. fault indication contacts - these are voltage free and provide a signal of the cause of a trip (long time, STD/INST).


Notes: For dimensions of XS/XH800SE and PE refer to pages 7-40 and 7-41, add dimensions of OCR controller and trip indication box (above).

## MCCB Technical data

OCR controller (PTA and trip indication)

OCR controller mounting position


Dimension table (mm)

| Ampere <br> frame | Type of <br> MCCB | With UVT <br> controller | Without UVT <br> controller | B |
| :--- | :--- | :--- | :---: | :---: |
| $\mathbf{4 0 0}$ | XS400 | 34 | 97 | 48 |
| $\mathbf{X 3 0}$ | XH400/TL400NE | 34 | 97 | 48 |
| $\mathbf{X S 6 3 0 / X V}$ | 64 | 151 | 60 |  |
| $\mathbf{X H 6 3}$ | XS800/XV | 64 | 151 | 60 |
| $\mathbf{1 2 5 0}$ | XH51250SE/XV | 51 | 151 | 60 |
| $\mathbf{1 6 0 0}$ | XS1600SE/TL-NE | 51 | 114 | 72 |
| $\mathbf{2 0 0 0}$ | XS2000NE | 54 | 114 | 92 |
| $\mathbf{2 5 0 0}$ | XS2500NE | 54 | 180 | 115 |

OCR controller (PTA and trip indication)
The OCR controller is installed in the left hand side of the breaker (standard). This can also be installed externally to the breaker (please specify when ordering).
OCR controller specifications
Control power source
Rated voltage $100-120 \mathrm{~V} \mathrm{AC}$ or $200-240 \mathrm{~V} \mathrm{AC}$
Consumption 2 VA
Note: The permissible range of control power is $85-110 \%$ of the rated voltage.

OCR controller connection diagram ') ${ }^{2}$ )


OCR controller dimensions
(Installed external to the breaker)


[^0]${ }^{7}$ ) Connected cable size - Max $2.0 \mathrm{~mm}^{2}$.

## MCCB Technical data

## Time/Current curves <br> XS400, XH400, TL400NE, XV400

Time/current characteristic curves


## Overcurrent tripping characteristics

| CT rated current (A) ( $\mathrm{I}_{\mathrm{n}}$ ) | 250, 400 |
| :---: | :---: |
| Base current setting (A) (10) | $\left(I_{n}\right) \times(0.63-0.8-1.0)$ |
| Long time-delay pick-up current (A): ( $I_{1}$ ) | (10) $\times(0.8-0.85-0.9-0.95-1.0)$ Non-tripping at (1) setting $\times 105 \%$ and below. Tripping at $125 \%$ and above. |
| Long time-delay time settings (S) ( $\mathrm{T}_{1}$ ) | (5-10-15-20-30) at ( 11 ) $\times 600 \%$ current. <br> Setting tolerance $\pm 20 \%$ |
| Short time-delay pick-up current (A); ( $\mathrm{l}_{2}$ ) | (10) $\times$ (2-4-6-8-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings ( S ) ( $\mathrm{T}_{2}$ ) | Opening time ( $0.1,0.15,0.2,0.25,0.3$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time - 20 ms for the timedelay setting |
| Instantaneous trip pick-up current (A) (13) Continuously adjustable from (10) x (3 to 12) |  |
|  | Setting tolerance $\pm 20 \%$ |
| - Pre-trip alarm pick-up current (A) (1.) | (1) $\times(0.7,0.8,0.9 .1 .0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarm time setting (S) (Tp) | 40 fixed definite time-delay. Setting tolerance $\pm 10 \%$ |

[^1]XS630, XH630, XS800,
XH800, XV630, XV800
Time/current characteristic curves


Overcurrent tripping characteristics

| CT rated current (A) (b) | 630,800 |
| :---: | :---: |
| Base current setting (A) ( l ) | (h) $\times(0.63-0.8-1.0)$ |
| Long time-delay pick-up current (A): (h) | (b) $\times$ ( $0.8-0.85-0.9-0.95-1.0)$ Non-tripping at ( 1 ) setting x 105 \% and below. Tripping at 125 \% and above. |
| Long time-delay time settings (S) ( $\mathrm{T}^{\text {I }}$ ) | (5-10-15-20-30) at ( 1 ) $\times 600 \%$ current. <br> Setting tolerance $\pm 20 \%$ |
| Short time-delay pick-up current (A): (k) | (lo) $\times$ (2-4-6-8-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings (S) ( $\mathrm{T}_{\text {I }}$ ) | Opening time (0.1, 0.15, $0.2,0.25,0.3$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time - 20 ms for the time-delay setting |
| Instantaneous trip pick-up current (A) (b) | Continuously adjustable from ( $l_{0}$ ) $\times(3$ to 12 ) <br> Setting tolerance $\pm 20 \%$ |
| - Pre-trip alarm pick-up current (A) (b) | (l) $\times$ ( $0.7,0.8,0.2,1.0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarm time setting (S) (Tr) | 40 fixed definite time-delay. Setting tolerance $\pm 10 \%$ |
| - Ground fault trip pick-up current (A) (k) | Continuously adjustable from ( 1 l$) \times(0.1$ to 0.4$)$ <br> Setting tolerance $\pm 15 \%$ |
| - Ground fault trip time setting (S) (Ta) | Opening time ( $0.1-0.2-0.3-0.4-0.8$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time is - 20 ms for the time-delay settings |

Note: - Optional.
Underlined values will be applied as standard ratings unless otherwise specified when ordering.

## MCCB Technical data

## Microprocessor based characteristics and adjustments

XS1250SE, XS1600SE, XS2000NE, XS2500NE, TL630NE, TL800NE, TL1250NE \& XV1250

Time/current characteristic curves


Overcurrent tripping characteristics

| CT rated current (A) ( $\mathrm{I}_{\text {n }}$ ) | 1000, 1250, 1600, 2000, 2500 |
| :---: | :---: |
| Base current setting (A) ( 10 ) | ( l ) $\times$ (0.63-0.8-1.0) |
| Long time-delay pick-up current (A): (1) | (lo) $\times$ ( $0.8-0.85-0.9-0.95-1.0$ ) Non-tripping at (h) setting $\mathrm{x} 105 \%$ and below. Tripping at $125 \%$ and above. |
| Long time-delay time settings ( S ) ( $\mathrm{T}_{1}$ ) | (5-10-15-20-30) at ( 1 l$) \times 600 \%$ current. <br> Setting tolerance $\pm 20 \%$ |
| Short time-delay pick-up current (A): $\left(I_{2}\right)$ | (10) $\times$ (2-4-6-8-10) Setting tolerance $\pm 15 \%$ |
| Short time-delay time settings (S) $\mathrm{T}_{2}$ ) | Opening time ( $0.1,0.15,0.2,0.25,0.3$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time - 20 ms for the time-delay setting |
| Instantaneous trip pick-up current (A) ( 12 ) | Continuously adjustable from ( 10 ) $\times$ ( 3 to 12 ) <br> Setting tolerance $\pm 20 \%$ |
| - Pre-trip alarm pick-up current (A) (l) | (h) $\times(0.7,0.8,0.21 .0)$ Setting tolerance $\pm 10 \%$ |
| - Pre-trip alarm time setting (S) (T) | 40 fixed definite time-delay. Setting tolerance $\pm 10 \%$ |
| - Ground fault trip pick-up current (A) (16) | Continuously adjustable from ( $(\mathrm{k}) \times(0.1$ to 0.4$)$ Setting tolerance $\pm 15 \%$ |
| - Ground fault trip time setting (S) (I) | Opening time ( $0.1-0.2-0.3-0.4-0.8$ ) in the definite time-delay. Total clearing time is +50 ms and resettable time is - 20 ms for the time-delay settings |

Note: - Optional.
Underlined values will be applied as standard ratings unless otherwise specified when ordering.

## MCCB Technical data

## Time/Current curves - Mathematical analysis

## MCCB curves

A microprocessor MCCB has three major regions on its overcurrent tripping characteristic, namely Long Time Delay (LID) for overload protection, Short Time Delay (STD) and Instantaneous (INST), both for short-circuit protection.
The following is an insight into how these curves interact and could act as a guide for hand-drawing the curves. TemCurve Selectivity Analysis Software is available for computerised generation of curves (refer to page $7-24$ ).
Firstly consider the following basic characteristic curve shown in figure 1. The LID takes the form of a curve and has the following characteristic equation:

$$
(12-1), t=k
$$

where ' $k$ ' is a constant. To determine $k$, the calibration point of the LID should be used, i.e. $t=T_{1}$ at $I_{1}=6(600 \%)$.
IEC - 60947-2 states that a breaker must not trip below $105 \%$ of its rated current, and always trip at $130 \%$ of its rated current.
Terasaki microprocesssor MCCBs however are calibrated to trip between $105 \%$ and $125 \%$, giving them a higher degree of accuracy. If the middle point is taken then the pick-up of the MCCB is $115 \%$ of its rated current. The SID and INST parts of the curve can be drawn more easily as they are simply a series of horizontal and vertical lines determined by the $\mathrm{I}_{2}$ and $\mathrm{T}_{2}$ settings for the STD, and $I_{3}$ setting for the INST.

## Example

If we assume that we have:
XS1250SE with 1250A CTs and
$I_{0}=1, I_{1}=0.8, T_{1}=30$ secs,
$\mathrm{I}_{2}=8, \mathrm{~T}_{2}=0.2 \mathrm{sec}$ and
$\mathrm{I}_{3}=1_{2}$ (dial setting on OCR)
then the characteristic curve can be constructed as follows.
To draw the LID we firstly need to determine the constant $k$, as follows:
$\mathrm{k}=\left(\mathrm{l}^{2}-1\right) \mathrm{t}=\left(6^{2}-1\right) 30=1050$
giving the characteristic equation:
$\left(1^{2}-1\right) \mathrm{t}=1050$
By simple arithmetic the tripping times for each level of overload can now be determined.
For $400 \%$ overload (for the example this is equivalent to $1250 \times 1.0 \times 0.8$ $\times 4=400 \mathrm{~A}$ ).

$$
t=\frac{1050}{\left(1^{2}-1\right)}=\frac{1050}{\left(4^{2}-1\right)}=70 \text { secs }
$$

The STD and INST can be constructed as follows with
$I_{2}=I_{n} \times I_{0} \times I_{2}$
$I_{3}=I_{6} \times I_{0} \times I_{3}$
Please note that 20 ms is taken as an average time for the INST trip of the MCCB as it is the maximum time it will take the MCCB to trip. In practice the breaker will open much faster, particularly at high faults where the current limiting qualities of the MCCB become more effective.

Fig. 1




## MCCB Technical data

OCR checker, inspection and maintenance


The TemBreak (Electronic) OCR checker, Type TNS-1, is a portable easy-to-use instrument for field testing the trip functions.

It checks the pick-up current and tripping time value of the LTD, STD, INST and GFT functions.

Ratings and specifications

| Power source | $100-110 \mathrm{~V}, 220-240 \mathrm{~V} \mathrm{AC}$ single phase $50 / 60 \mathrm{~Hz}$ |
| :---: | :---: |
| Power consumption | 30 VA |
| Application | LTD function check (set current and trip time values) |
|  | STD function check (set current and trip time values) |
|  | INST function check (set current value) |
|  | GFT function check (set current and trip time values) |
| Measurement of set | Display 3-digit digital display |
| current values | Range $\quad 0.900 \mathrm{~mA}$ |
| Measurement of tripping time values | Range 0.00-99.9 seconds |
| Outline dimensions ( mm ) | $200 \mathrm{~W} \times 84 \mathrm{H} \times 130 \mathrm{D}$ |
| Weight | 2.7 kg |

[^2]?
-

[^3]
## NHE

## TemCurve

Selectivity Analysis Software

Our objective is to provide you with the tools necessary to ensure your time is managed as effectively and efficiently as possible.
TemCurve has been developed wholly by NHP for the Australian market, but will also be used within the Terasaki organisation throughout the world.

For further information please contact your local NHP office or agent.

## MCCB Technical data

## TemBreak XM30PB



Rear connected (optional)



Plug-in (optional)
Drilling plan


Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm
around the handle escutcheon.


## (1) TERASAKI

## MCCB Technical data

TemBreak XS125CS, CJ, NS, NJ, XH125NJ, PJ and TL30F MCCBs


## MCCB Technical data

TemBreak TL100F/TL100EM - TL100NJ
ASL: Arrangement standard line ㄴ: Handle frame centre line

## Outline dimensions (mm)



Note: Interpole barriers standard on TL100NJ.

## MCCB Technical data

Motor operators (XMB type) for XS125, XH125, TL100NJ, TL30F $\left.{ }^{1}\right)^{2}$ )


Rear connected (optional)


Plug-in (optional)


Notes: 1) For dimensions of 7MB-3BA2 used for TL100F refer to NHP.
${ }^{2}$ ) Dimensions for TL100NJ not showing length of MCCB. Refer page 7-27.
Above outline dimensions are for AC motors. Contact NHP for details for DC motors.

## MCCB Technical data

## TemBreak XE225NC

## Outline dimensions (mm)

ASL: Arrangement standard line
H: Handle frame centre line
Front connected (standard)


Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.5 mm around the handle escutcheon.

## Rear connected (optional)



Note: In the standard shipment mode, terminals on both the line side and the load side are in a horizontal orientation.

## (4) TERASAKI

## MCCB Technical data

## Motor operators for XE225NC



- Breakers with terminal bars available on request.

Rear connected (optional)


Note: In the standard selection mode, terminals on both the line side and load side are in a horizontal orientation.

## MCCB Technical data

## TemBreak XS250NJ



Breakers with terminal bars available on request.


## MCCB Technical data

## Motor operators (XMB type) for XS250NJ



- Breakers with terminal bars available on request.
Rear connected (optional)


Note: For dimensions and selection of motors for TL225F refer to NHP.

## MCCB Technical data

## TemBreak XH160PJ and XH250NJ



Note: Breakers with terminal bars available on request.
Rear-connected (optional)


Note: In the standard shipment mode, terminals on both the line side and the load side are in a horizontal orientation.


Plug-in (optional)
Details of connections


Drilling plan


# MCCB Technical data 

Motor operators for XH160PJ and XH250NJ


Rear connected (optional)

Note: In the standard selection mode, terminals on both
 the line side and the load side are in a horizontal orientation.
Plug-in (optional)


## MCCB Technical data

## TemBreak TL225F, TL250NJ



## MCCB Technical data

TemBreak XS400, XH400, XH250PJ, XV400


Rear connected (optional)


Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.

ASL: Arrangement standard line N: Handle frame centre line

Optional extension busbars


Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

Plug-in (optional)


## MCCB Technical data

TemBreak TL400NE

Outline dimensions (mm)
Front connected


ASL: Arrangement standard line
H : Handle frame centre line

Rear connected


Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.

## (4) TERASAKI

## MCCB Technical data

Motor operators (XMC type) for XS400, XH400, XV400, TL250NJ, TL400NE ${ }^{1}$ )

Outline dimensions (mm)

> ASL: Arrangement standard line H: Handle frame centre line

Front connected (standard)


Drilling plan


Rear connected (optional)


Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.


Note: ') TL250NJ and TL400NE length dimension not shown.
Refer pages 7-35 and 7-37.

## (4) TERASAKI

## MCCB Technical data

TemBreak 630 AF XS630, XH630


## (4) TERASAKI

MCCB Technical data
TemBreak 800 AF XS800, XH800


Rear connected (optional)
Drilling plan
Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the handle escutcheon.
Plug-in (optional)
Mounting block
Drilling plan


## MCCB Technical data

Motor operators (XMC type) for XS630, XH630, XS800, XH800

Outline dimensions (mm)
Front connected (standard)
ASL: Arrangement standard line
H : Handle frame centre line


| Types | B (mm) |  |  |
| :---: | :---: | :---: | :---: |
|  | A (mm) | 3 pole | N pole |
| XH, XV, XS800NE | 10 | 36 | 36 |
| XH, XV, XS630NE | 8 | 36 | 36 |



Rear connected (optional)


$\$ 15$ for accessory wiring when necessary
Note: In the standard selection mode, terminals on both the line side and the load side are in a horizontal orientation.

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the motor operator frame.

Plug-in (optional)


## (-) TERASAKI

## MCCB Technical data

TemBreak XS1250, XV1250


## MCCB Technical data

## Motor operators (XMD type) for XS1250, XV1250



Rear connected (optional)


Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the motor operator frame.

Plug-in (optional)


Drilling plan


## MCCB Technical data

TemBreak XS1600SE, TL630, TL800, TL1250NE


Rear connected with motor operator


## MCCB Technical data

Motor operators (XMD type) for XS1600SE types, TL630NE, TL800NE, TL1250NE


## (4) TERASAKI

## MCCB Technical data

Motor operators for XS1600 TL630NE, TL800NE, TL1250NE

Outline dimensions ( mm )
Front connected (standard)

## Drilling plan



ASL: Arrangement standard line
H: Handle frame centre line

Panel cut-out


Panel cut-out dimensions shown give an allowance of 1.0 mm around the motor operator frame.


## MCCB Technical data

## TemBreak XS2000NE

Outline dimensions (mm)
Front-connected (optional)


ASL: Arrangement standard line
H: Handle frame centre line Drilling plan



Panel cut-out dimensions shown give an allowance of 2 mm around the handle escutcheon.
Draw-out (optional)


## MCCB Technical data

## TemBreak XS2500NE

## Outline dimensions (mm)

ASL: Arrangement standard line
H: Handle frame centre line
Rear-connected (RC standard, no FC version)


Panel cut-out


- Panel cut-out dimensions shown give an allowance of 2 mm around the handle escutcheon.



Note: ${ }^{1}$ ) Use non-magnetic angle (SUS 304 etc )

Note: RC - Rear connected, FC - Front connected.

## MCCB Technical data

Motor operators (XMB type) for XS2000NE \& XS2500NE


Rear connected (standard)


Draw-out (optional)


## ( () TERASAKI

## MCCB Technical data

Motor operators XMB types for XS2000NE \& XS2500NE

Outline dimensions ( mm )
Front connected (standard)


Drilling plan
Note: ') Use non-magnetic angle (SUS 304 etc )


## MCCB Technical data

AC power watts loss - 3 Pole MCCBs


Notes: Standard terminal arrangements.
125-1600 front connection.
2000 and above rear connection.
${ }^{1}$ ) Watts loss figures are for 3 poles
e.g. An XH125NJ operating at 125 A , will have a total watts loss of 41 watts.
${ }^{2}$ ) Watts loss values are approximate and will vary according to ambient conditions and switchboard construction.

## NHP and PowerCad working together

PowerCad has established itself as the standard for electrical engmeering design software for electrical engineering building services.
PowerCad contains a suite of electrical design software which provides solutions ranging from basic cable sizing up to complete electrical design and modelling. There are 5 software packages which have a stepped level of features. These are: QuickCable-LT ${ }^{101}$, QuickCable ${ }^{\text {¹ }}$, PowerCalc ${ }^{1 m}$, PowerCaic- $H^{(m,}$, while the final and most powerful version is called PowerCad-5 ${ }^{14}$.


Theabove is a typical screen representation providing a circuit Whematic, along with an open window showing a protective device picture its various device OCR seltings, Cat. No, and outer device details

## PowerCad 5 - application

Starting with a network single line diagran), the designer is abte to assign the loads in the system from which the software calculates maximum demands, determines the appropriate cable sizes, and selects suitable protective devices and can finally undertake a powerful harmonic modelling function of the entire system. In order for the software to accurately model the protective devices in the system, Power Cad includes various device characteristic data as a library within its software, including Terasaki circuit breakers.

[^4]

PowerCad 5 features:

- Maximum demand
- Ciblesizing
- Gondai stang
- Fault-loop impedance
- Cable voltage drop calculations
- Cable thermal stress
- Short circuit calculations
- Let-through energy
- Harmonic analysis
- Harmonic mitigatior
- Power factor correction
- Network resonance
- L. V. Distribution Network Modelling
- Single Line diagram
- Single Line dragram export to AutoCad
- AutoCad interface for loads input
- Automatic mains is submains cable selections
- Automatic final subcircuit cable sizing
- Circuit breaker selection
- Co-ordination time-current curves
- Co-ordination curve on screen CB adjustment
- Substation sizing
- Motor Libraries and light fitting
- Liminare Libraries
- Extensive reporting with print preview
- Direct online support
- Standards AS/NZS. IEC. BS and CP5
- Generator sizing
- Harmonic active filtering
- Reactor passive filtering
- Transfer switches


## TECHNICAL DATA SHEET

For

## SEWERAGE PUMP STATION SP144

Lavarack Av \#1 Eagle Farm
Equipment Type: Motor Contactors
Location: Motor Starter Section
Model Numbers: ..... CA7-9
Manufacturer: Sprecher \& Schuh
Supplier:
NHP Pty Ltd25 Turbo DriveCoorparoo QLD 4151Ph: 0738916008
Fx: 0738916139


# Broad current range Compact dlimensions Maximum flexibilility 

## Series CA7 Contactors

## Controls Motors to 60HP (@460/575V)

As Little as 45mm Wide

## Reduces Panel Space



Compact dimensions with maximum performance! Our CA7 contactors control motors up to 60 HP , in frame sizes ranging from $45 \mathrm{~mm}\left(1-3 / 4^{\prime \prime}\right)$ to a maximum of $72 \mathrm{~mm}\left(2-3 / 4^{\prime \prime}\right)$ wide.

Because of its modular design, CA7 is flexible and easy to use. All CA7 contactors use the same accessories, reducing the need to stock additional inventory. They are also mechanically and electrically compatible with Sprecher + Schuh's CEP7 electronic
overload relay and KT7 motor circuit controller. This provides easy, clean installation for a variety of motor starter applications.

Whether part of a system or for individual use, the CA7 is the right contactor for the job.

## Series CA7



## Save space, save money

The CA7 contactor series includes ten contactors within four frame sizes. The two smallest sizes house capacities up to 25HP (@460V) and 30 HP (@575V). They measure only $45 \mathrm{~mm}\left(1-3 / 4^{\prime \prime}\right)$ in width! Even the largest of the contactors - the CA7-85, controlling motors to 60 HP - measures only $72 \mathrm{~mm}\left(2-3 / 4^{\prime \prime}\right)$ wide. The space you save with CA7 translates to smaller panels and lower cost.


Maximum flexibility
The CA7 contactor is designed for ultimate flexibility. Coil terminals can be supplied on the top or bottom, and are field-reversible to suit individual wiring needs. Auxiliary contacts can be mounted on the top and sides, for the most efficient use of panel space. In reversing applications where space may be tight, the mechanical interlock has a built-in auxiliary to save room.

Field-reversible coil terminals provide additional flexibility


Dual terminal technology provides additional wiring options, as well as increased reliability and a faster wiring process.
Dual wiring terminals speed installation

## State-of-the-art technology

CA7 contactors utilize the latest design technology. Combined with Sprecher + Schuh's CEP7 solid state electronic overload relay, the CA7 becomes the most accurate and reliable motor starter available. Mechanically linked contacts provide safety for all applications. In addition, snap-on electronic timers and a PLC interface are also available.


## Modular design

The CA7 contactor series includes universal accessories to fit every frame size. This provides incredible flexibility, and eliminates the need to purchase size-specific components.

Because of their modular design, CA7 contactors are easily joined to form complete starter combinations. The CA7 is specially designed for electrical and mechanical compatibility with our overload and motor circuit controllers.

## CA7 Selected Technical Data

| Catalog Number | $\begin{gathered} \text { AC-1 } \\ \text { Amp Rating } \\ 40^{\circ} \mathrm{C} \end{gathered}$ | Maximum Horsepower |  |  |  |  |  | $\begin{gathered} \text { Max. } \\ \text { Aux. } \\ \text { Contacts } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Single Phase |  | Three Phase |  |  |  |  |
|  |  | 115 V | 230 V | 200 V | 230 V | 460 V | 575 V |  |
| CA7-9 | 32 | 1/3 | 1 | 2 | 2 | 5 | 7-1/2 | 9 |
| CA7-12 | 32 | 1/2 | 2 | 3 | 3 | 7-1/2 | 10 | 9 |
| CA7-16 | 32 | 1 | 3 | 5 | 5 | 10 | 15 | 9 |
| CA7-23 | 32 | 2 | 3 | 5 | 7-1/2 | 15 | 15 | 9 |
| CA7-30 | 50 | 2 | 5 | 7-1/2 | 10 | 20 | 25 | 9 |
| CA7-37 | 50 | 3 | 5 | 10 | 10 | 25 | 30 | 9 |
| CA7-43 | 85 | 3 | 7-1/2 | 10 | 15 | 30 | 30 | 8 |
| CA7-60 | 100 | 5 | 10 | 15 | 20 | 40 | 50 | 8 |
| CA7-72 | 100 | 5 | 15 | 20 | 25 | 50 | 60 | 8 |
| CAT-85 | 100 | 7-1/2 | 15 | 25 | 30 | 60 | 60 | 8 |

See Sprecher + Schuh's general catalog for complete information and pricing on CA7 contactors.

Sprecher + Schuh US Division Headquarters 15910 International Plaza Dr., Houston, TX 77032 Tel: (281) 442-9000; Fax: (800) 739-7370 nww.ssusa.cc
ublication No: F-CA7-R1 1002

Sprecher + Schuh Canadian Division
3610 Nashua Dr., Unit 10, Mississauga, Ontario L4V 1L2 Tel: (905) 677-7514; Fax: (905) 677-7663 www.sscdn.cc

Attenti o prevent electrical shock, disconnect from power: $\quad \exists$ before installing. or servicing. Install in suitable enclosure. Keep free from contaminants ...-C37 /...-37
Achtung: Vor Installations- oder Servicearbeiten Stromversorgung unterbrechen, um Unfälle zu vermeiden: Die Geräte müssen in einem passenden Gehäuse eingebaut und gegen Verṣchmutzung geschützt werden.
Attenzione: Per prevenire infortuni, togliere tensione prima dell'installazione o manutenzione. Installare in custodia idonea.
Tenere lontano da contaminanti.
Attention: Avant le montage et la mise en service, couper f'alimentation secteur afin d'éviter tout accident. Prévoir une mise en coffret ou armoiré appropriée. Protéger le produit contre les environnements agressifs.
Atención: Desconectar la alimentación eléctrica antes de realizar e montaje y la puesta en servicio, con el objeto de evitar accidentes. Instalado en una caja o armario apropiado. Proteger el producto de los ambientes agresivos.


Min. distance lateral to grounded parts or walls $=6 \mathrm{~mm}$
Min. seitlicher Abstand zu geerdeten Teile oder Wände $=6 \mathrm{~mm}$
Distance latéral min. enver pièces mises à terre ou parois $=6 \mathrm{~mm}$ Distanza laterale min. verso pezzi a Distancia lateral min. a chasis o paredes $=6 \mathrm{~mm}$

##  <br> CE

EN 60947-1/-4-1 UL 508; CSA 22.2 No. 14;



|  |  |  |  <br> $\xi D D=\mathrm{No} 3$ <br> Pozidriv No 2 |
| :---: | :---: | :---: | :---: |
|  |  |  | (3) $1 \ldots$. <br> $\sum D D=$ No 3 <br> Pozidriy No 2 |



Technische Ånderungen vorehatten
22.221.950-01/05. 2007

Ausgabe 10

## sprecher + schuh

## Contact Block

## Performance \& Selection


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## Contact Block Considerations

A combination of many factors affect the dependability, life expectancy, and suitability of a contact block in any given application. Understanding the most important of those factors can help you select the best switch for your needs. In the pages that follow you'll gain a basic understanding of switch materials and properties, and how they affect switch performance.

## Contact Material

## Contact Construction

The contact material forms the surfaces that come in contact with each other to establish an electrical circuit. Typical contact materials include fine silver, nickel-silver, and silver alloys. Fine silver provides low electrical resistance between the movable and stationary contact interface. Silver alloys form harder surfaces to reduce wear and help prevent contact welding.

In low voltage applications (below 48 V DC and 0.1 A , or below 24 V AC and 0.4 A ) where excess oil or dust is present, the use of more noble alloys (such as palladium, gold, and their alloys) in the contact material is recommended. These alloys are highly reliable in this type of environment.

Silver alloys are susceptible to chemical attack which can affect reliability at low voltages. Noble metals resist chemical attack, but are susceptible to frictional polymer formation, which can affect reliability. Combining gold and palladium will resist frictional polymer formation.

The perimeter of the contact is often shaped like a circle or rectangle and may have little effect on contact performance. The shape of the faces where the fixed and movable contacts meet is more important. This interface should not have two flat surfaces meeting. If one of the contacts has a flat surface, the other contact should be a rounded surface to provide a more defined and controlled touch point.

Figure 1. Bifurcated Spanner Example


The bifurcated style of construction provides a higher degree of reliability than the butt spanner because it divides each movable contact into two sections at the tip of the spanner. This minimizes the chance of foreign materials accumulating on contact surfaces and preventing the completion of the circuit. Even if foreign material accumulates on one of the contact tips, the second tip will most likely touch a clean spot establishing the circuit. Typically, the bifurcated spanner is designed for use in full voltage applications, where the arc between the spanner and stationary contacts will burn off small amounts of contamination in most cases. To aid contact cleaning the contact spanner is designed to flex, which wipes the stationary surface and allows each finger to act independently.

## Contact Block Considerations

Figure 2. Pentafurcated and Quadfurcated Spanner Examples


In low voltage applications (below 48 V DC and 0.1 A or below 24 V AC and 0.4 A ) pentafurcated/quadfurcated styles of construction provide the highest degree of reliability. because they divide each movable spanner contact side into separate flexible fingers. Every part in the system is corrosion-resistant and the flexible spanner is designed to wipe the stationary contacts clean every time the circuit is opened or closed. This is important since the absence of an arc in low voltage environments means that contaminants will not be burned off, but will be eliminated by the wiping action. Therefore, the pentafurcated or quadfurcated are the most reliable styles of spanners available.

Some manufacturers use protrusions such as bars or nibs raised on the face of either the movable or stationary contact to help establish the circuit under low power conditions. These raised surfaces will tend to penetrate non-conducting films that may be present on contact surfaces. They may also lessen the chance of foreign matter preventing completion of the circuit. Such protrusions may, however, quickly burn away under arcing or higher current conditions.

Base materials to which the contact material is attached include copper alloys and steel. Copper alloy is preferable because of its thermal conductivity, electrical conductivity, and corrosion properties.

## Contact Size/ Volume Stationary vs. Movable

Contact size refers to the size of the face of the contact or the areas that meet to form the interface between the movable and stationary contacts. Volume is the total amount of contact material.

It is desirable to make one of the contacts smaller than the other so it stays within the perimeter of the other contact when switch action takes place: This arrangement provides greater assurance that alignment of contacts is maintained under repeated operation and resulting wear. Misalignment can cause severe contact wear and shorten switch life.

In the contact set, the movable contact is most often the smaller contact in both size and volume, so that its mass and resulting inertia can be minimized. Partly because of its low. volume, the movable contact operates at a higher temperature than the stationary contact. Consequently, the stationary contact will also contribute to a greater rate of wear on the movable contact. The stationary contact is generally attached to a more massive base structure that provides a better heat sink than the movable contact structure.

In alternating current applications, the higher temperature of the movable contact can cause material to be expelled from the surface of the contact. The higher temperature can cause transfer of material to the cooler surface of the stationary contact as well. In direct current applications, the relative polarity of the contacts has a major effect on how the contact material is transferred from one surface to the other.

## Contact Block Considerations

## Contact Reliability

Contact reliability pertains to the ability of contacts to establish a circuit across the interface between the stationary and movable contact set(s) each time the switch is operated. This reliability can be most often adversely affected by two conditions:

- Mechanical debris within the switch
- Non-conducting films that form on the contact surfaces

Mechanical debris or dirt can be introduced into the switch during assembly. Dirt and debris can also be interjected during installation or can be a product of switch action. The wear produced by internal switch components sliding past one another during operation can generate dirt. Care must be taken in the design of moving mechanisms to keep this wear to a minimum.

Non-conducting film and oxides can be formed from gaseous contaminants that enter the switch from an extemal environment as well as being formed from intemally generated reactants. Sealing methods have been developed to isolate the switch interior from the external environment. An understanding of the relationship of all the material used in the construction of a switch is required to eliminate the internally generated reactants. This requires knowledge of the post curing outgassing of any plastics, elastomers, paint, and other components used in the construction of the system. Some gases will react in the presence of an electric arc to form non-conducting films that will cause reliability problems if deposited on the contact face. The tendency of many thermoset plastics to continue to outgas for a period of time after curing has led to the use of thermoplastic materials in switch interiors.

Contact Resistance Contact resistance pertains to resistance across the interface between a pair of movable and stationary contacts. The higher the value of this resistance, the more difficult it is to establish a circuit when the contacts close. This is especially true in low power circuits. Higher resistance also contributes to contact heating.

The initial contact resistance of both fine silver contacts and noble contact materials (gold, palladium, and their alloys) is $10 \ldots 15$ milliohms. However, the resistance of noble contact materials will remain relatively constant during their lifetime compared to silver contacts, which typically increase over time. These resistance values could vary with the ambient conditions in the vicinity of the contacts themselves

Sealed switches have slightly higher initial contact resistances compared to silver contacts ( $80 \ldots 150$ milliohms, depending on type), but they remain stable over the life of the device.

## Switch Design Considerations

Single Break vs. Double Break

In addition to the physical characteristics of the materials used in manufacturing, design considerations also affect the performance of a switching mechanism. In this section you'll gain an overview of those switch design fundamentals and how they affect switch performance.

Figure 3. Single Break Design


Figure 4. Double Break Design


Single break and double break refer to the number of contact pairs that are used to make or break the electrical circuit. Single break means the electrical circuit is controlled by one set of contacts. Double break means the electrical circuit is controlled by two sets of contacts in series.

In a single break design, the contact pair tends to repeatedly make and break the circuit on the same spot on the contact faces. This helps to keep the contact touch point clean, enhancing the contact reliability.

The double break design provides twice the length of air gap in the electrical circuit using the same stroke of the actuating member as with the single break design. The result is the electrical arc that is created by the opening of the circuit will be extinguished sooner and with less actuator movement as compared to a single break design.

Also, since the energy in the arc created upon contact opening is distributed across two air gaps, there is less tendency for the contacts to weld in the double break design.

On the other hand, because of the nature of the double break design, the contact points of the spanner may vary slightly with each actuation. This variation may, over time, affect switch reliability.

## Contact Motion

Contact motion refers to the relative motion of the contact faces as they begin to touch one another. Various design techniques are utilized to increase the reliability of the contacts establishing the circuit as they meet.

A wiping or sliding action will help clear surfaces of dirt and oxides and break any nonconducting film that may have formed on contact surfaces. This type of action must be carefully controlled, especially with precious metal contacts, to avoid excessive mechanical wear of the contacts.

Contact tips on the end of the spanner must be capable of flexing and twisting to establish a seat on the surfaces of bifurcated/quadfurcated/pentafurcated stationary contacts. A sliding action of one contact against the other could cause continuity interruptions if the moving . contact slides up over a piece of debris.

## Switch Design Considerations

Spring Force

## Overtravel

The spring force discussed in the following paragraphs is the force provided within the contact block that retums the contact structure to its normal or unoperated state when the extemal force applied to the device operator is removed. This force holds the contact structure in its normal state until an external force is again applied to the device operator.

The amount of spring force is determined by the force required to insure contact reliability under the conditions in a variety of applications. Sufficient force is required to break through contaminants that may be present on the contact faces on the normally closed (N.C.) contacts. The force should insure that contacts stay stable under possible shock and vibration. Light welds created by contact arcing on the normally open (N.O.) contacts should be able to be broken by spring force. The spring force required to maintain circuit reliability is dependant on the contact material hardness. Greater force is required for harder materials.

Spring force directly affects the external force required to operate and to some extent contribute to internal switch friction. Consideration must be given to these factors when determining the spring force used

Overtravel in a switch pertains to the amount of travel occurring in a switch beyond what is required to operate. Overtravel allows for wear within the switch mechanism. It helps to insure the switch will continue to function as the contacts wear or erode. Overtravel also provides contact stabilization under conditions of shock and vibration.

Contact underlap and overlap refer to the relative action of the N.O. and N.C. contacts when the switch is actuated.

Underlap is the more common type of switch action. As the device operator is moved from its rest position to initiate $s$ witch action, the following events take place in order:

1. The N.C. contact opens.
2. There is a duration where no electrical continuity is present.
3. The N.O. contact closes.

In overlap type switch action, the N.O. contact makes its circuit before the N.C. contact breaks its.circuit. There is never a period of time when electrical continuity is absent:

1. The N.O. contact closes.
2. There is a duration where both circuits are active.
3. The N.C. contact opens.

The type of switch action selected is dependant on the requirements of the specific user circuit application.

## Switch Design Considerations

## Direct Drive

NFPA 79 and EN 418 both require that emergency stops must be a direct drive design. A direct drive design switch will have continuous mechanical linkage from the external operating member to the contact carrier. It will not employ the use of any resilient members or springs in the mechanical actuating path to open the N.C. contacts.

A special case of direct drive design is a switch that complies with IEC 60947-5-1. It is designed so that contact separation will take place even though the contacts may have been welded or "sticking" during fault circuit conditions. A direct drive switch is designed to allow contact separation even if the contacts have been lightly welded during fault circuit conditions. The manufacturer provides the fusing level requirements needed to protect these contacts from welding. The actuator movement and actuator force required affecting contact separation are specified by the switch manufacturer.

This type of switch construction is used to help ensure that contact action takes place when the external operating member is actuated. By avoiding the use of any springs in the actuating path, a solid connection is provided directly from the external mushroom operator to the contacts.

Contact opening should always take place at the same point in the actuating stroke and with the same operating force. By their nature, these types of switches fall into the slow break/slow make category of devices although some special designs have been developed that provide positive opening in snap action devices. With increased awareness of safety concerns and the movement toward designing devices that are used globally, greater emphasis has been placed on the direct drive feature.

Contact Action
Contact action refers to how contacts make and/or break the electrical circuit they intend to control. There are two basic types of contact action: slow make/slow break and snap action.

In slow make/slow break action, the contact carrier and contacts move at the same rate of travel as the actuating mechanism. This action is most often obtained with direct drive switch designs. Since the rate of movement of the contacts is solely dependant on the speed of the external actuator, it can result in slow separation of contacts and create a condition called "teasing".

In the teasing condition, the air gap created to break the electrical circuit opens so slowly that arcing occurs between the faces of the stationary and moveable contacts. This arcing is detrimental to the contacts because of accelerated contact wear and material transfer and can cause the contacts to weld rather than separate. The arcing can also cause circuit problems by introducing noise.

Snap action design incorporates a resilient member or springs between the actuator and contact carrier. The springs cause the contacts to move independently of the actuating mechanism. The mechanism is designed so that when actuator movement takes place, not only does the contact carrier movement take place, but energy is also built up in the spring system. Prior to the point in the travel of the actuator where contact separation takes place, the contact carrier and spring system are designed to go into an overcenter mode.

## Switch Design Considerations

## Mechanically <br> Linked Contacts

Time Delay

At the overcenter point, sufficient energy is available in the spring system allowing the carrier to move independently of any further actuator motion and the contacts snap open. This rapid opening prevents teasing and minimizes contact welding. Some snap action devices also incorporate direct opening action. The direct opening action occurs slightly later in the travel than the normal snapover point if the contacts were slightly welded.

This construction has also been known as "positively guided contactṣ". It combines a N.C. and N.O. contact combination to prevent N.C. and N.O. contacts from closing at the same time. This nomenclature is generally applied to control relays, but is also applicable to push buttons, pressure and temperature switches, and other control circuit devices. It is generally used for checking control circuit functions.

Time delay of a switching device is the interval between the time when the external operator of the switching device is actuated and the time when the contact action actually occurs.

In a switching device where time delay is provided, contact action takes place at a predetermined time interval after physical action has taken place to displace the external operator in a sufficient manner to operate the device. This time delay is fixed in some devices and adjustable in others to meet circuit requirements. Pneumatic timers are commonly used to perform this function.

A switching device that has been designed for stacking has provisions for attaching multiple contact elements to the operator.

Stacking provides a means for multiple circuits to be actuated from a single external operator. A switching device with this capability can perform multiple functions or combinations of functions depending on the type of external operator. A selector switch type operator with several positions in combination with multiple contact elements is one example of this type of device.

## Switch Design Considerations

Wiring Termination
The following are examples of some of the more common methods of termination used.

## Binding Head Screw

This screw has a larger than normal head. The underside of the screw head has a groove where the wire seats and is secured when the screw is tightened. It is most effective when used with solid wire. A cup washer can be added to accommodate stranded wire, but care must be exercised to ensure that all strands are secured

## Saddle Clamp

This is a U-shaped clamp with a screw in the center. The screw threads into a flat conductor on the switching device and the legs of the $U$ slide over the edges of the flat conductor in order to trap the wire.

## Figure 5.



The saddle clamp should be designed so it tilts to securely clamp a single wire on one side or a different wire size on each side of the clamp.

Barrel Type - This is similar to the saddle clamp design, but instead of a $U$-shaped clamp, the clamp is rectangular.

## Figure 6.



The screw is not threaded into the flat conductor but rather bears against its top surface. This causes the barrel to be drawn upward clamping the wire between the undersurface of the flat conductor and the lower portion of the barrel. A major advantage is the wire is easy to insert into the clamping area.

## Pressure Plate

A pressure plate is essentially a flat piece of material with a screw in the center. As with the saddle clamp, the screw threads into the flat conductor on the switching device. Even though the pressure plate is flat, it is designed to force the individual strands of wire to the center of the face plate that comes in contact with the conductor on the switching device where they are restrained. In addition, features are often designed into the body of the switching device that prevent any wire strands from escaping the pressure plate clamping action.

## Switch Design Considerations

## Stab Type

This type of termination is often termed quick-connect, push-on, fast-on, etc. The connection between the switching device and the wire is made with special complementary connection parts. The male part is normally built into the switching device and the female part is mechanically attached to the wire end. Termination is accomplished by mating the connector parts. This method provides a quick way to attach wires to the switching device and it is easy to remove the wires for service.

## PC Pin

These are switching devices that can be soldered directly to a printed circuit board or plugged with pin connectors into receptacles mounted on the board.

## Lugs and Ferrules

These devices are mechanically secured to the wire end. They make it easier to attach the wire to the switch terminal. They are normally used with stranded wire.

- Lugs provide a flat projection that is usually shaped like a fork or ring. The projection can be inserted under the head of the screw, inserted into saddle clamps, or slipped under pressure plates.
- Ferrules provide a pin type projection well suited for use with saddle clamps, pressure plates, and barrel type terminals.


## Solder

Solder can be applied to the end of stranded wire to prevent the individual strands of wire from separating. The end of the wire becomes solid when soldered and can be used with saddle clamps, pressure plates, and barrel type terminals. It should be noted that the solder end will be quite hard and will resist the crushing effect of clamping means. Because of the irregular shape obtained through soldering, only partial contact between the wire and the terminal could result.

## Spring-Clamp

This termination style is designed to minimize wiring time. The optimized spring-clamp is designed to reduce stress relaxation while maintaining contact force. An opening force is applied by a lever. The wire is then inserted and the opening force is removed. Upon force removal, the spring-clamp closes on the wire. This design is good for vibration environments.

Because of the large variety of termination options and the importance of establishing and maintaining a reliable connection between the switching device and the circuit, standards have been developed to address this area. The Underwriters Laboratories Pullout and Secureness test is used to insure that termination methods have sufficient strength to retain the wire under conditions of use. This test also determines if the wire strands have been damaged during the wiring process or are susceptible to breakage under conditions of use.

## Switch Design Considerations

## Finger-Safe

A finger-safe device provides a degree of protection from accidental, casual contact of live electrical parts by personnel. Only those components meeting or exceeding the requirements of IEC standard IP2X (listed under IEC 529) can be considered finger-safe.

Those standards describe a model test finger, along with guidelines for the manner in which the test finger is to be manipulated in the vicinity of the wiring terminals to determine if the switching device provides the required degree of protection.

Some switching devices achieve the finger-safe condition by basic device design while others require an external attachment.

The finger-safe feature is becoming more prevalent as safety issues take on added importance. Higher voltage levels pose a greater risk of injury and liability. A concern of finger-safe design is it may provide a false sense of security to personnel who have access to the area where electrical terminations are made.

## Special Considerations

Every switch serves as just one element in a complete system. Where and how that system operates plays a significant role in which switch will deliver the most cost-effective performance over time. In the section that follows, you'll gain a better understanding of some of the extraordinary issues involved in switch specification.

## Environmental Considerations

Careful consideration of the environment to which the switching device is subjected will help ensure proper operation and acceptable service life. Consideration of external environmental conditions of the operators includes temperature and humidity, shock and vibration, and exposure to washdown, cutting fluids, etc., encountered during operation.

In installations where an unfriendly external environment exists, the switching device should be housed in an enclosure designed to isolate it from the environment. Various enclosure ratings have been developed for use in specific environments and these ratings are regulated by industry standards. The external environment of the switching device can have a profound effect on the operation of the device and on its service life.

Conditions generated within enclosures can also have a negative effect on switch operation and life. Condensation, internally generated chemicals, or trapped dirt are some of the more common problems. In addition, since each switching device is made of a variety of materials, each produces its own internal environment. Caution must be taken during the design of the switching device to ensure the materials selected are proper for this kind of device and are compatible with one another.

The following information points out some key internal and external conditions affecting switching devices, as well as their effects.

## Temperature

All electrical devices have a maximum operating temperature rating and this rating is generally understood by the user. The maximum storage temperature and the effects of low temperature are not as well-understood.

Exceeding the high temperature limits can cause degradation of materials within the switch. This degradation can weaken switch parts or release gases from plastics and elastomers. A change in physical dimensions may occur, affecting operational travel and force. A very low temperature environment can cause sticking of the actuator and compromise the return action provided by the internal springs within the switching devices. Great care should be taken to exclude freezing liquids from the vicinity of the external operator or the switch may be inoperative under available levels of operating force.

Large fluctuations in temperature can lead to condensation of water or other liquids, and result in the problems relating to humidity, chemicals, and gases listed below (in those cases it is generally helpful to ventilate the enclosure).

## Humidity

Moisture can cause the formation of rust and corrosion on metallic parts as well as contribute to electrical problems such as arc tracking.

## Chemicals and Gases

This class of contaminants can cause degradation of material used in the product in a

## Switch Design Considerations

variety of ways. Corrosion of metallic parts and the degradation of physical properties of plastics and elastomers are among the most common effects. The formation of conductive films on the surface of the insulation can cause arc tracking.

## Dirt and Debris

Whether originating internally from wear or damage, or externally, this material can cause friction between moving parts, increase wear, and reduce switch life. Dirt on contacts increases resistance and contributes to contact reliability problems.

## Shock and Vibration

Consideration must be given to the shock and vibration to which the switching device is subjected. Severe shocks can cause unintended momentary contact operation that could result in circuit malfunction. Long term exposure to vibration can cause premature wear of the switch elements and generation of internal dirt. Even a poorly designed panel door can repeatedly subject a switching device to damaging shock and vibration.

It's also important to handle a switch with care during installation to avoid damaging shock.

## Physical Abuse

Improper handling of the switching device during shipping or installation can cause damage to device components that could affect operation.

Environmentally Sealed Devices

An environmentally sealed device isolates the contact area from the environment.
The most common type of construction has the contacts hermetically sealed within a glass envelope. Prior to sealing, the interior of the glass envelope is filled with an inert gas that keeps the environment around the contacts stable. This construction keeps out explosive gases or contaminants that could affect contact reliability. Since the contacts are not accessible for actuation by mechanical means, they are operated by means of magnetic flux.

A special version of the sealed switch known as a logic reed is used in logic circuits. The logic reed is characterized by very short contact bounce, typically less than 0.5 milliseconds.

Contact isolation can also be accomplished by mechanical means such as a flexible diaphragm. These methods do not, however, provide a true hermetic seal, and are more susceptible to wear and degradation.

## Switch Design Considerations

## Standards and Approvals

Standards have been developed by industry groups and governmental units to help ensure that switching devices meet certain requirements with regard to installation criteria, safe operation, load carrying ability, minimum mechanical and electrical life, etc.

Once a particular design has met the requirements of a specific standard, a marking may be affixed to devices constructed according to that design indicating that the standards of that particular agency have been met.

Users need to be aware of which standards pertain to the products used in their locations and which approvals are required. Requirements vary depending on the application and the governmental unit having jurisdiction. Some of the standards that apply to switching devices are listed below:

- UL 508
- NEMA ICS 5 part 1
- IEC 60947-5-1
- CSA 22.2 No. 14

Switch life can be defined in a variety of ways. It can be defined as the time when the switch physically fails and can no longer provide contact action. It can also be defined as the point when the operating characteristics change to such a degree that switch action is no longer reliable or the parameters fall outside those required for that application. Examples of the latter would be an increase in operating force or excessive travel to obtain contact action.

A switching device may wear out due to mechanical considerations. Repeated operations cause physical wear of parts due to friction, shock, and stress, and can lead to eventual component failure. Dirt and debris generated by the moving mechanism can cause binding and can be a source of contact contamination.

The electrical life of a switch is not necessarily related to its mechanical life. The electrical life of a switch is primarily load dependant, because the electrical load is the main source of heating in - and damage to - current carrying components. High current loads can also contribute to arcing at the contacts during contact action. This arcing action results in contact erosion and deformation and can lead to welding of the contacts. As a result, it is good practice to evaluate both mechanical and electrical life ratings before selecting a switching device.

The switch environment can cause corrosion. This may lead to friction, physical failure of components, and dirt or corrosion in the contact areas.

Low level switching and infrequent use may allow buildup of film on contact faces, affecting contact reliability. Logic reed switches or switches with precious metal contacts. are ideal in these applications.

## Special Considerations

Shock and Vibration

Shock and vibration refer to the physical conditions that are present in the environment where the switch operates. These conditions often introduce undesirable motion into the device mechanism.

Sources of shock can be the normal motion of the equipment where the device is mounted or the expected movement of the entire control system. Such motion may be repetitive in nature or may occur only periodically under specific situations such as startup, etc. The user may try to anticipate random, abnormal conditions which could result in a high shock situation. One-time mishandling during shipping and installation can cause damage that will affect operation.

Another source of high shock is the slamming of control panel doors where the switching devices are mounted. In order to minimize the effect of known vibration, the axis of actuation of the switching device should not lie on the same plane as that of the direction of normal equipment vibration.

Contact reliability can be affected by shock and vibration. Continual vibration causes mechanical wear and under load conditions, arcing can lead to welding of contacts. A severe shock can cause unintended, momentary contact operation that could result in circuit malfunction.

The mechanical wear caused by long term exposure to vibration can result in the generation of dirt and debris which affects contact reliability and causes added friction in the sliding portions of the mechanism.

Dielectric Strength
Dielectric strength is a measure of the ability of the insulation used in the switching device to withstand the application of a voltage across its surface or through its mass. This will determine the maximum electrical rating of the device.

Degradation of the dielectric strength of insulation can lead to failure of the device. Unintended electrical continuity may be established between circuit elements and ground. In either case, the result is a failure of the switch to perform its intended function.

The most common type of failure is due to arc tracking across the surface of the insulation. The combination of a particular insulation and environmental conditions such as moisture and/or certain gases in the presence of an electrical arc can result in the buildup of a conducting path.

## Special Considerations

Contact Block Ratings

The contact block rating of a switching device is the electrical load that the device is capable of switching. This rating is expressed in voltage and current and typically refers to the maximum values that can be switched in a specified number of operations. Although contact blocks are usually rated for maximum conditions, there is a practical low load limit that the contacts will switch in a reliable manner.

Exceeding the high loads can cause burning and pitting of the contacts leading to welding and contributing to arc tracking. If the load to be switched is of a very low energy level, any contaminants or non-conducting films on the contacts may prevent a circuit from heing established when the contacts are operated. If loads below 48 V DC and 0.1 A , or below 24 V AC and $0 . \dot{4} \mathrm{~A}$, are to be switched, the user must be cautious when selecting the contact materials. If the switching is within a typical Type $4 / 4 \mathrm{X} / 13$ environment, the quadfurcated/ pentafurcated blocks should be used for ultimate reliability. If the switching is within Class 1 and 2 Division 2 environment, without a sealing well or a conduit seal off, logic reed, sealed switch, or stackable sealed switch contact blocks should be used. If this type of switch is used at the high end of the rating, then caution should be exercised if these contacts are used for switching low energy loads. The feature built in for establishment of low energy loads may have been burned away during high load switching operations.

Due to the growing popularity of solid-state devices being used in control circuits, the trend in industry is toward lower energy loads.

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# TECHNICAL DATA SHEET 

## For

## SEWERAGE PUMP STATION SP144 Lavarack Av \#1 Eagle Farm

Equipment Type:

Location:

Model Numbers:

Manufacturer:

Supplier:

TDS-180-4S-277

Critec
Surge Diverter

Main Incomer

Energy Correction Options
PO Box 431
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Ph: 0733560577
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## EnITECH

## CRITEC ${ }^{\circledR}$ Transient Discriminating Surge Diverters


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## Surge Protection And Surge Ratings

The stress, which an SPD will experience under surge conditions, is a function of many complex and interrelated parameters. These include:

- Location of the SPD(s) within the structure - are they located at the main distribution board or within the facility at secondary board, or even in front of the end-user equipment?
- Method of coupling the lightning strike to the facility for example, is this via a direct strike to the structures LPS, or via induction onto building wiring due to a nearby strike?
- Distribution of lightning currents within the structure for example, what portion of the lightning current enters the earthing system and what remaining portion seeks a path to remote grounds via the power distribution system and equipotential bonding SPDs?
ype of power distribution system - the distribution of lightning current on a power distribution system is strongly influenced by the grounding practice for the neutral conductor. For example, in the TN-C system with its multiple earthed neutral, a more direct and lower impedance path to ground is provided for lightning currents than in a TT system.
- Additional conductive services connected to the facility - these will carry a portion of the direct lightning current and therefore reduce the portion which flows through the power distribution system via the lightning equipotential bonding SPD.
- Type of waveshape - it is not possible to simply consider the peak current which the SPD will have to conduct, one also has to consider the waveshape of this surge. It is also not possible to simply equate the areas under the current-time curves (also referred to as the action integral) for SPDs under different waveshapes.

Many attempts have been made to quantify the electrical nironment and "threat level" which an SPD will enperience at different locations within a facility. The new IEC ${ }^{\text {sh }}$ standard on lightning protection, IEC 62305-4
"Protection against lightning - Part 4: Electrical and electronic systems within structures" has sought to address this issue by considering the highest surge magnitude which may be presented to an SPD based on the lightning protection level (LPL) being considered. For example, this standard postulates that under a LPL I the magnitude of a direct strike to the structure's LPS may be as high as 200kA $10 / 350$. While this level is possible, its statistical probability of occurrence is approximately $1 \%$. In other words, $99 \%$ of discharges will be less than this postulated 200 kA peak current level.
An assumption is made that $50 \%$ of this current is conducted via the building's earthing system, and 50\% returns via the equipotential bonding SPDs connected to
a three wire plus neutral power distribution system. It is also assumed that no additional conductive service exists. This implies that the portion of the initial 200 kA discharge experienced by each SPD is 25 kA .

Simplified assumptions of current dispersion are useful in considering the possible threat level, which the SPD(s) may experience, but it is important to keep in context the assumptions being made. In the example above, a lightning discharge of 200kA has been considered. It follows that the threat level to the equipotential bonding SPDs will be less than 25kA for $99 \%$ of the time. In addition, it has been assumed that the waveshape of this current component through the SPD(s) will be of the same waveshape as the initial discharge, namely $10 / 350$, while in reality the waveshape have been altered by the impedance of building wiring, etc.

Many standards have sought to base their considerations on field experience collected overtime. For example, the IEEE* guide to the environment C62.41.1 and the recommended practice C62.41.2 present two scenarios of lightning discharge and different exposure levels under each of these depending on the location where the SPD is installed. In this standard, Scenario II depicts a direct strike to the structure, while Scenario I depicts a nearby strike and the subsequent conducted current into a structure via power and data lines. The highest surge exposure considered feasible to an SPD installed at the service entrance to a facility under Scenario I is $10 \mathrm{kA} 8 / 20$, while under Scenario II it is considered to be $10 \mathrm{kA} 10 / 350$ (exposure Level 3 ).

From the above, it is apparent that the selection of the appropriate surge rating for an SPD depends on many complex and interconnected parameters. When addressing such complexities, one needs to keep in mind that one of the more important parameters in selecting an SPD is its limiting voltage performance during the expected surge event, and not the energy withstand which it can handle.


Arotection zones defined by specific product application.

## Advanced Technologies - The ERICO ${ }^{\circ}$ Advantage

## Transient Discriminating Technology

To meet the fundamental requirements of performance, longer service life and greater safety under real world conditions, ERICO has developed Transient Discriminating (TD) Technology.
This quantum leap in technology adds a level of "intelligence" to the Surge Protection Device enabling it to discriminate between sustained abnormal over-voltage conditions and true transient or surge events. Not only does this help ensure safe operation under practical application, but it also prolongs the life of the protector since permanent disconnects are not required as a means of achieving internal over-voltage protection.

## Traditional Technologies

Conventional SPD technologies utilize metal oxide varistors and/ or silicon avalanche diodes to clamp or limit transient events. However, these devices are susceptible to sustained $50 / 60 \mathrm{~Hz}$ mains over-voltage conditions which often occur during faults to the utility system. Such occurrences present a significant safety hazard when the suppression device attempts to damp the peak of each half cycle on the mains over-voltage. This condition can cause the device to rapidly accumulate heat and in tum fail with the possibility of inducing a fire hazard.

## The Core of TD Technology

The secret to ERICO's Transient Discriminating Technology is its active frequency discrimination circuit. This patented device can discriminate between a temporary over-voltage (TOV) condition


and a very fast transient, which is associated with lightning or switching-induced surges. When the transient frequencies are detected, the patented Quick-Switch within TD activates to allow the robust protection to limit the incoming transient. The frequency discriminating circuit that controls the Quick-Switch helps ensure that the SPD device is immune to the effects of a sustained 50 or 60 Hz TOV . This allows the device to keep operating, in order to help provide safe and reliable transient protection, even after an abnormal over-voltage condition has occurred.

## Meeting \& Exceeding UL* Standards

The CRITEC* range of surge protection devices from ERICO ${ }^{\circ}$ employing TD Technology has been specifically designed to meet and exceed the new safety requirements of UL 1449 Edition 3. To meet the abnormal over-voltage testing of UL 1449 Edition 3, many manufacturers of SPD devices have incorporated fuse or thermal disconnect devices which permanently disconnect all protection from the circuit during an over-voltage event. Transient Discriminating Technology on the other hand will allow the SPD device to experience an abnormal overvoltage up to twice its nominal operating voltage and still remain operational even after this event! This allows the device to help provide safe, reliable and continuous protection to your sensitive electronic equipment. TD Technology is especially recommended for any site where sustained over-voltages are known to occur, and where failure of traditional SPD technologies cannot be tolerated.
The UL 1449 testing standard addresses the safety of an SPD device under temporary and abnormal overvoltage conditions, but does not specifically mandate a design that will give a reliable, long length of service in the real world. Specifically, UL 1449 tests that the SPD remains operational at $10 \%$ above nominal supply voltage, allowing SPD manufacturers to design products that permanently disconnect just above that. Most reputable manufacturer's designs allow for up to a $25 \%$ overvoltage, while ERICO's TD Technology gives even greater overhead.


## TDS 130

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS 130 Series

## Features

- CRITEC TD Technology with thermal disconnect protection
- Compact package, modular DIN rail mounting for limited space requirements
- Three modes of protection: L-N, L-PE \& N-PE odication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- $15 \mathrm{kA} 8 / 20 \mu \mathrm{~s}$ surge rating per mode
- CE, UL® 1449 Edition 3 Listed

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS130 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. The TDS130 is specifically designed for the protection of single phase power supplies within instrumentation and control applications. They are conveniently packaged for easy installation on 35 mm DIN rail within control
 panels.
CRITEC ${ }^{\circ}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of life. A visual indicator flag provides user-feedback in the event of such operation. The TDS130 provides a set of optional voltagefree contacts for remote signaling that maintenance is required.
The convenient plug-in module

and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


## Features

- CRITEC ${ }^{\text {TD }}$ Technology with thermal disconnect protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 50kA $8 / 20 \mu s$ maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, ULº 1449

Edition 3 Listed

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS 150 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS150 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.
CRITEC ${ }^{\bullet}$ TD technology helps ensure reliable and continued operation during sustained and abnormal
 over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A visual indicator flag provides userfeedback in the event of such operation. As standard, the TDS150 provides a set of voltage-free contacts for remote signaling that maintenance is required.
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


| Model | \|TDS1501SR150 | \|TDS1501SR240 | [TDS15015R277 | TDS1501SR560 |
| :---: | :---: | :---: | :---: | :---: |
| Item Number for Europe | 702404 | 702406 | 702407 | 702408 |
| Nominal Voltage, $\mathrm{U}_{\mathbf{n}}$ | 120-150 VAC | 220-240 VAC | 240-277 VAC | 480-560 VAC |
| Max Cont. Operating Voltage, $U_{s}$ | 170 VAC | 275 VAC | 320 VAC | 610 VAC |
| Stand-off Voltage | 240VAC | 1440VAC | 480VAC | 700VAC |
| Frequency | $0-100 \mathrm{~Hz}$ |  |  |  |
| Short Circuit Current Rating, ${ }^{\text {cos }}$ | 200kAIC |  |  |  |
| Back-up Overcurrent Protection | 125AqL, if supply > 100A |  |  |  |
| Technology | TD with thermal disconnect |  |  |  |
| Max Discharge Current, Ims | 50kA 8/20us |  |  |  |
| Nominal Discharge Current, $I_{n}$ | 25kA 8/20]s 120kA 8/20 |  |  |  |
| Protection Modes | Single mode (L-G, L-N or N-G) |  |  |  |
| Voltage Protection Level $U_{p}$ | $\begin{aligned} & 400 \mathrm{~V} \text { e } 3 \mathrm{kA} \\ & 1.0 \mathrm{kV} \text { In } \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} \text { ब } 3 \mathrm{kA} \\ & 1.2 \mathrm{kV} \text { © } \mathrm{In} \\ & \hline \end{aligned}$ | $\begin{aligned} & 800 \mathrm{~V} \cdot 3 \mathrm{kA} \\ & 1.6 \mathrm{kV} \text { e } \mathrm{ln} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.8 \mathrm{kV} \odot 3 \mathrm{kA} \\ & 2.4 \mathrm{kV} \odot \ln \end{aligned}$ |
| Status | N/O, N/C Change-over contact, 250V-/0.5A, max $1.5 \mathrm{~mm}^{2}$ (\%14AWG) terminals <br> Mechanical flag/remote contacts (R model only) |  |  |  |
| Dimensions $\mathrm{H} \times \mathrm{D} \times \mathrm{W}: \mathrm{mm}$ (in) | $90 \times 68 \times 18(3.54 \times 2.68 \times 0.69)$ |  |  |  |
| Module Width | 1 M |  |  |  |
| Weight: kg (lbs) | 0.12 (0.26) |  |  |  |
| Enclosure | DIN 43880 UL94V-0 thermoplastic, IP 20 (NEMA-1) |  |  |  |
| Connection | $\begin{aligned} & 525 \mathrm{~mm}^{2} \text { (\#4AWG) stranded } \\ & \leq 35 \mathrm{~mm}^{2} \text { ( }(2 \mathrm{~B} \end{aligned}$ |  |  |  |
| Mounting | 35 mm top hat DIN rail |  |  |  |
| Temperature | $-40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}\left(-40^{\circ} \mathrm{F}\right.$ to $\left.176^{\circ} \mathrm{F}\right)$ |  |  |  |
| Humidity | 0\% to $90 \%$ (1) |  |  |  |
| Approvals | CE, IEC ${ }^{61643-1, ~ U L ~}{ }^{\circ} 1449$ Ed 3 Recognized Component Type 2 |  |  |  |
| Surge Rated to Meet | ```ANSIMEEEE C62.41.2 Cat A, Cat B, Cat C ANSI`/EEE* C62.41.2 Scenario II, Exposure 2, 50kA 8/20\mus IEC 61643-1 Class II UL* 1449 Ed3 In 20kA mode``` |  |  |  |
| Replacement Module | ITDS150M150 | ITDS150M240 | 1T05150M277 | ITDS150M560 |

Features

- CRITEC TD Technology with thermal disconnect protection
- Compact design fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches ommon circuit reakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 100kA 8/20us maximum surge rating provides protection suitable or sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL 1449 Edition 3 Listed


## TDS1 100

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS1 100 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
The TDS1100 series of surge suppressors provide economical and reliable protection from voltage transients on power distribution systems. They are conveniently packaged for easy installation on 35 mm DIN rail within main distribution panelboards.
CRITEC ${ }^{*}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior
 at end-of-life. A visual indicator flag provides user-feedback in the event of such operation. As standard, the TDS1100 provides a set of voltage-free contacts for remote signaling that maintenance is due.
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.


| Model | T0S 1000258150 | [TDSIIC02SR280 | [IDSIT002SR27] | ITOSTI00232560 |
| :---: | :---: | :---: | :---: | :---: |
| Item Number for Europe | 702409 | 702411 | 1702412 | 702413 |
| Nominal Voltage, U $\mathrm{V}_{5}$ | $120-150 \mathrm{VAC}$ | 220-240 VAC | $1240-2717 \mathrm{VAC}$ | 480.560 VAC |
| MaxCont Operating Voltage. $\mathrm{US}^{\text {a }}$ | 170VAC | 275 VAC | 320VAC | 610VAC |
| Stand-ofi Votage | 240VAC | WGOVAC | 1480 VAC | 700VAC |
| Frequency | O-100 Hz |  |  |  |
| Short Crauit Cursent Rating, is | 200 kA |  |  |  |
| Back-up Overcurrent Protection | 125Agh iff suody | 100A |  |  |
| technology | t10 with thermal | isconnect |  |  |
| Max Discharge Current, ${ }_{\text {che }}$ | 100kA820]s |  |  |  |
| mpuse Current 1 - | $12.56410 / 35015$ |  |  |  |
| Nominal Discharge Curent. 1 . | 50148820]5 | [40kA 820 l |  |  |
| Frotection Modes | Single mode (l-G | L-NorN-G |  |  |
| Vortage Protection Level, ${ }_{\text {, }}$, | $\begin{aligned} & \begin{array}{l} 400 \mathrm{~V} 03 \mathrm{ka} \\ 1.0 \mathrm{kV} \\ \hline 100 \mathrm{kA} \end{array} \end{aligned}$ | $\begin{aligned} & 700 \mathrm{O} 3 \mathrm{3kA} \\ & 1.2 \mathrm{kV}=20 \mathrm{kA} \end{aligned}$ | [800V 3 3k <br> $1.6 \mathrm{kV} \odot 20 \mathrm{kA}$ | $\left[\begin{array}{l} 1.8 \mathrm{kVe} 3 \mathrm{kA} \\ 2.4 \mathrm{kV} e 20 \mathrm{kA} \end{array}\right.$ |
| Status | NO, NC Change Mechanical flag/ | $\begin{aligned} & \text { over contact, } 250 \mathrm{~V} \\ & \text { remote contacts ( } \mathrm{R} \end{aligned}$ | $\begin{aligned} & 0.5 A \text { max } 1.5 \mathrm{~mm}^{2} \\ & \text { podel only) } \\ & \hline \end{aligned}$ | 14AWG) terminalk |
| Dimenslons $\mathrm{H} \times \mathrm{DXW}: \mathrm{mm}$ ( I ) | $90 \times 68 \times 3513.54$ | $\times 2.68 \times 1.381$ |  |  |
| Modylewidet | 2 M |  |  |  |
| weight kg (1bs) | $0.24(0.53)$ |  |  |  |
| Encosure | DIN 43850, Ul94 | -0thermoplastic, | 20 (NEMA-1) |  |
| Connection | $\begin{aligned} & \frac{25 \mathrm{~mm}^{2}}{35} \mathrm{~mm}^{2} \text { (12AWG } \end{aligned}$ | stranded sollid |  |  |
| Mounting | 35 mm top hat 0 | 1rail |  |  |
| Tomperature | $-40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$ (-40 | fo 176\% |  |  |
| Humidity | +10.90\% |  |  |  |
| Approvals | CE, IEC-61643-1, |  | Ized Component | pe 2 |
| Surge Rated to Meet |  | 1. Cat A Cat 8, C 1.2 Scenarlo Il, Exp and Class II kA mode | ure $3,100 \mathrm{kA} 8 / 20$ | 10 kA 10350 ps |
| Reoplacement MoVModule | TOSSEOMISO | IIDS150M240 | 1105150M27] | IIDS150M560 |

## Features

- CRITEC TD

Technology with thermal disconnect protection

- Compact design
fits into DIN distribution panel boards and motor control centers
- 35 mm DIN rail mount - DIN 43880 profile matches common circuit breakers
- Indication flags and voltage-free contacts provide remote status monitoring
- Separate plug and base design facilitates replacement of a failed surge module
- 50kA $8 / 20 \mu \mathrm{~s}$ maximum surge rating provides protection suitable for sub-distribution panels and a long operational life
- Available in various operating voltages to suit most common power distribution systems
- CE, UL 1449

Edition 3 Listed

## CRITEC ${ }^{\circledR}$ TDS Surge Diverter - TDS350 Series

Surges and voltage transients are a major cause of expensive electronic equipment failure and business disruption. Damage may result in the loss of capital outlays, such as computers and communications equipment, as well as consequential loss of revenue and profits due to unscheduled system down-time.
CRITEC ${ }^{\bullet}$ TD technology helps ensure reliable and continued operation during sustained and abnormal over-voltage events. Internal thermal disconnect devices help ensure safe behavior at end-of-life. A
 visual indicator flag provides user-feedback in the event of such operation. As standard, the TDS provides a set of voltage-free contacts for remote signaling that maintenance is due.
The convenient plug-in module and separate base design facilitates replacement of a failed surge module without needing to undo installation wiring.

$53 \mathrm{~mm}\left(2.07^{\prime \prime}\right)$

| Model | TDS350TNC150 | TDS50120240 | [TDS350TNC277 | Tos350TT150 | TOS350T1277 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Item Number for Europe | 702414 | 702419 | 702417 | 702416 | 702418 |
| Nominal Voltage, $\mathrm{U}_{\mathbf{n}}$ | 120-150 VAC |  | 240-277 VAC | 120-150 VAC | 240-277 VAC |
| Max Cont. Operating Voltage, $\mathbf{U}_{\mathbf{8}}$ | 170/295VAC | 240/480VAC | 320/536VAC | 170/295VAC | 320/536VAC |
| Stand-off Voltage | 240/415VAC | 240/480VAC | 480/813VAC | 240/415VAC | 480/813VAC |
| Frequency | 0.100Hz |  |  |  |  |
| Short Crcuit Current Rating, , ${ }^{\text {cex }}$ | 200kAIC |  |  |  |  |
| Back-up Overcurrent Protection | 125AgL, if supply > 100A |  |  |  |  |
| Technology | TD with thermal disconnect |  |  |  |  |
| Max Discharge Current, las | 50kA $8 / 20 \mu \mathrm{~s}$ |  |  | 12.5kA 10/350 $/ \mathrm{s}$ N-PE 50kA $8 / 2015$ |  |
| Nominal Discharge Current, l | 25kA $8 / 20 \mathrm{Hs}$ |  | 20kA $8 / 20$ | 25kA8/20]s | 20kA 8/20 |
| Protection Modes | L-N | L-N, N-PE | L-N | L-N, N-PE |  |
| Voltage Protection Level, $\mathrm{U}_{\mathbf{p}}$ | $\begin{aligned} & \text { 400V } 3 \mathrm{kA} \\ & 1.0 \mathrm{kV} \mathrm{In} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 800 \mathrm{~V} \text { e 3kA } \\ & 1.6 \mathrm{kV} \mathrm{O} \mathrm{In} \end{aligned}$ | $\begin{aligned} & 400 \mathrm{~V}=3 \mathrm{kA} \\ & 1.0 \mathrm{kV} \text { In } \end{aligned}$ | $\begin{aligned} & \text { 800V }{ }^{8} 3 \mathrm{kA} \\ & 1.6 \mathrm{kV} \mathrm{O} \text { In } \end{aligned}$ |
| Status | N/O, N/C Change-over contact, 250V~/0.5A, max $1.5 \mathrm{~mm}^{2}$ (in14AWG) terminals Mechanical flag / remote contacts |  |  |  |  |
| Dimensions $\mathrm{H} \times \mathrm{D} \times \mathrm{W}$ : mm (in) | $90 \times 68 \times 53(3.54 \times 2.68 \times 2.07)$ |  |  | $90 \times 68 \times 70(3.54 \times 2.68 \times 2.76)$ |  |
| Module Width | 3 M |  |  | 4M |  |
| Weight kg ( (bs) | 0.36(0.79) |  |  | 0.5(1.10) |  |
| Endosure | DIN 43880, UL94V-0 thermoplastic, IP 20 (NEMA-1) |  |  |  |  |
| Connection | $\begin{aligned} & 525 \mathrm{~mm}^{2}(\mathrm{HAWG}) \text { stranded } \\ & \leq 35 \mathrm{~mm}^{2}(* 2 A W G) \text { solid } \end{aligned}$ |  |  |  |  |
| Mounting | 35 mm top hat DIN rail |  |  |  |  |
| Temperature | $-40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}\left(-40^{\circ} \mathrm{F}\right.$ to $\left.176^{\circ} \mathrm{F}\right)$ |  |  |  |  |
| Humidity | 0\% to $00 \%$ ( |  |  |  |  |
| Approvals | CE, IEC ${ }^{\circ} 161643-1$, UL $^{\circ} 1449$ Ed 3 Recognized Component Type 2 |  |  |  |  |
| Surge Rated to Meet | ANSiण1EEE C62.41.2 Cat A, Cat B, Cat C <br> ANSIथAEEE* C62.41.2 Scenario II, Exposure 2, 50kA 8/20 1 s <br> IEC 61643-1 Class II <br> UL® 1449 Ed3 $\ln 20 \mathrm{kA}$ mode |  |  |  |  |
| Replacement MOV Module | TDS150MM150 |  | TDS150M277 | TDSI50M150 | TDS150M277 |
| Replacement GDT Module |  |  |  | SGD112M |  |
| Replacement GDT Module (Europe) | - |  |  | 702403 |  |

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## WARNING

EDCO products shall be installed and used only as indicated in EnJCO's product instruction sheets and training materials. Instruction sheets are avallable at wwwerico.com and from wour ERICO customer service representative. Improper installation, misuse, misapplication or other fallure to completely follow Ekicos instructions and warninge may cause product nction, property damage, serious bodily injury and death.

## TECHNICAL DATA SHEET

For

## SEWERAGE PUMP STATION SP144

## Lavarack Av \#1 Eagle Farm

| Equipment Type: | Surge Filter |
| :--- | :--- |
| Location: | Main Incomer |
| Model Numbers: |  |
|  | TDF-10A-240V |
| Manufacturer: | Critec |
|  |  |
| Supplier: | Energy Correction Options |
|  | PO Box 431 |
|  | Kelvin Grove, QLD. 4059 |
|  | Ph: 07 3356 0577 |
|  | Fx: 07 3356 1432 |
|  | Web: www.ecoptions.com.au |

## Features

- CRITEC ${ }^{\ominus}$ Transient Discriminating (TD) Technology provides increased service life
- In-line series protection
- High efficiency low pass sine wave filtering - ideal for the protection of switched mode power supplies
- Three modes of protection: L-N, L-PE \& N-PE
- 35 mm DIN rail mount - simple installation
- LED status indication and opto-isolated output - for remote status monitoring
- CE, UL 1449 Ed. 3 Listed


## CRITEC ${ }^{\circledR}$ Transient Discriminating Filter

The TDF series has been specifically designed for process control applications to protect the switched mode power supply units on devices such as PLC controllers, SCADA systems and motor controllers. Units are UL® Recognized and available for 3A, 10A and 20A loads and suitable for $\mathbf{1 1 0 - 1 2 0} \mathrm{V}$ ac/dc and $\mathbf{2 2 0 - 2 4 0 \mathrm { Vac }}$ circuits.
The TDF is a series connected, single phase surge filter providing an aggregate surge capacity of $50 \mathrm{kA}(8 / 20 \mu \mathrm{~s})$ across L-N, L-PE, and N-PE. The low pass filter provides up to 65 dB of attenuation to voltage transients. Not only does this reduce the residual let-through voltage, but it also helps further reduce the steep voltage rate-of-rise providing superior protection for sensitive electronic equipment.



| Model | TDF3A120V | [TDF3A240V | [TDF10A120V | TDF10A240V | DF20A120V | DF20A240V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| tem Number for Europe | 700001 | 700002 | 700003 | 700004 | 700005 | 700006 |
| Nominal Voltage, $\mathrm{U}_{0}$ | 110-120V | 220-240 V | 110-120 V | 220-240 V | 110-120 V | 220-240 V |
| Distribution System | TN-C-S, TN-S |  |  |  |  |  |
| Max Cont. Operating | 170VAC | 340 VAC | 170VAC | 340 VAC | 170VAC | 340 VAC |
| Voltage, Uc |  |  |  |  |  |  |
| Stand-off Voltage | 240 V | 400 V | 240 V | 400 V | 1240 V | 400 V |
| Frequency | 0-60Hz | 50/60Hz | $0-60 \mathrm{~Hz}$ |  |  | 50/50Hz |
| Max Line Current, $h$ | 3A |  | 10 A |  | 120 A |  |
| Operating Current ${ }^{\text {OU }}$ | 135 mA | 1250 mA | 240 mA | 1480 mA | 240 mA | 480 mA |
| Max Discharge Current, | $\begin{aligned} & 10 \mathrm{kA} 8 / 20 \mu \mathrm{~s} \text { N-PE } \\ & 20 \mathrm{kA} 8 / 20 \mu \mathrm{~S} \text { L-N } \\ & 20 \mathrm{kA} 820 \mu \mathrm{~S} \text { L-PE } \end{aligned}$ |  |  |  |  |  |
| Protection Modes | All modes protected |  |  |  |  |  |
| rechnology | In-line series low pass sine wave filter TD Technology |  |  |  |  |  |
| Voltage Protection Level, $\mathrm{U}_{\mathrm{p}}$ | $\begin{aligned} & 500 \mathrm{~V} \text { e } 500 \mathrm{~A} \\ & 250 \mathrm{~V} \text { e } 3 \mathrm{kA} \\ & \hline \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} \text { 500A } \\ & 600 \mathrm{~V} \text { - 3kA } \end{aligned}$ | $\begin{aligned} & 500 \mathrm{~V} \text { e } 500 \mathrm{~A} \\ & 250 \mathrm{~V} \text { - } 3 \mathrm{kA} \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} \text { e 500A } \\ & 600 \mathrm{~V} \text { e 3kA } \\ & \hline \end{aligned}$ | $\begin{aligned} & 500 \mathrm{~V} \text { - 500A } \\ & 250 \mathrm{~V} \text { e 3kA } \end{aligned}$ | $\begin{aligned} & 700 \mathrm{~V} \text { e } 500 \mathrm{~A} \\ & 600 \mathrm{~V} \text { e 3kA } \end{aligned}$ |
| Filtering | -62dB e 100kHz $\quad-65 \mathrm{~dB} \mathrm{e} 100 \mathrm{kHz}$ |  |  |  | -53dB 9100 kHz |  |
| Status | Green LED. On=0k. Isolated opto-coupler output |  |  |  |  |  |
| $\begin{aligned} & \text { Dimensions } \mathrm{H} \times \mathrm{D} \times \mathrm{W} \text { : } \\ & \mathrm{mm}(\mathrm{in}) \end{aligned}$ | $\begin{aligned} & 90 \times 68 \times 72 \\ & (3.54 \times 2.68 \times 2.83) \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 90 \times 68 \times 144 \\ & (3.54 \times 2.68 \times 5.67) \end{aligned}$ |  |  |  |
| Module Width | 4.M |  | 8. M |  |  |  |
| Weight: kg (ibs) | 0.7 (1.54) |  | 1.48(3.25) |  | 1.57 (3.46) |  |
| Enclosure | DIN 43880, UL94V-0 thermoplastic, IP 20 (NEMA ${ }^{\circ}-1$ ) |  |  |  |  |  |
| Connection | $1 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ (\%18AWG to $\mathrm{P}^{\text {P }} 10$ ) |  |  |  |  |  |
| Mounting | 35 mm top hat DIN rail |  |  |  |  |  |
| Back-up Overcurrent | 3A |  | 10A |  | 20A |  |
| Protection |  |  |  |  |  |  |
| femperature | $-35^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}\left(-31^{\circ} \mathrm{F}\right.$ to $\left.131^{\circ} \mathrm{F}\right)$ |  |  |  |  |  |
| Approvals | C-Tick, CE (NOM 3A, 120V), CSA 22.2, UL 1283, ULe 1449 Ed 3 Recoonized Component Type 2 |  |  |  |  |  |
| Surge Rated to Meet | ANSI\%IEEE ${ }^{\circ} \mathrm{C}$ 2.41.2 ${ }^{\text {Cat A, Cat B, Cat C }}$ |  |  |  |  |  |

(1) Optocoupler output can be connected to DINUNE Alarm Relay (DAR275V) to provide Form C dry contacts.

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## Features

- In-line series protection
- EMI/RFI noise filtering - protects against industrial electrical noise
- Compact design
- fits into motor control and equipment panels
- Three modes of protection: L-N, L-PE \& N-PE
- 35 mm DIN rail mount - simple installation
- LED power indicator


## CRITEC® Dinline Surge Filter

The "two port" DSF series has been specifically designed for process control applications to protect the switched mode power supply units on devices such as PLC controllers, SCADA systems and motor controllers. The 30 V unit is suitable for 12 V and $\mathbf{2 4 V a c} / \mathrm{dc}$ signaling and control systems.
The 6A DSF series incorporates a space efficient, low pass, series filter which provides attenuation to high frequency interference. The larger 20A model provides status indication and a higher surge rating, making this ideal for the protection of higher risk equipment.


| Moder | DSF6ABM | [D356AT50V | [03F6A275V | [05F204275V |
| :---: | :---: | :---: | :---: | :---: |
| tem limmeri for Europa | 700050 | 701000 | 701030 | 170020 |
| Nominal Votrege, $\mathrm{l}_{6}$ | 24 | 110.120 | 220-240V |  |
| Distribution System | 1P\%2W+G |  |  |  |
| System Comptitility | THS, TINCS |  |  |  |
| maxcont. Operating Vote | 30VAC, 38 VOC | $1{ }^{150 \mathrm{VAC}}{ }^{275 \mathrm{VAC}}$ |  |  |
| neek |  |  |  |  |
| requency | 0.6012 | 5060 Hz |  |  |
| Maxume Current | 6 A |  |  | 120 A |
| Operating Cirrent ${ }^{\text {O }}$ U, | 7 mA |  |  |  |
| Max Discharge Current $\mathrm{l}^{\text {a }}$ | $4 \mathrm{4kA} 820 \mathrm{HS}$ |  |  |  |
| Protection Modes | Allmodes protected |  |  |  |
| Iedinology | In-line series filter MOV |  |  |  |
| Voltage Protection Leve, W, |  | 1400VO3kA [750VO3kA |  | Trovozka |
| ifltering |  |  |  | -3060 62 k +2 |
| statis | Lep power indicator |  |  | Status indicator |
| Pimensions $\mathrm{H} \times \mathrm{DxW}$. | $\begin{aligned} & 90 \times 68 \times 36 \\ & (3.54 \times 2.68 \times 1.12) \end{aligned}$ |  |  | 90x68 772 |
| mm(in) |  |  |  | (3.54 $\times 2.68 \times 2.83)$ |
| Modvlewith | 2M |  |  | 4 M |
| Welptt kg (ib) | $0.02(0.461)$ |  |  | 0.7(1.543) |
| Endosure | OIN 43880 , UL4W-0 thermoplastic, IP 20 (NEMA-1) |  |  |  |
| Connection | $1 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ (18AWG to H10AWG) |  |  |  |
| Mounting | 35 mm top hat Din rall |  |  |  |
| 3ack-up Overourrent Protection | 6A |  |  | 204 |
| Vemperature | -35 ${ }^{\circ}$ to $55^{\circ} \mathrm{C}(31 \mathrm{~F}$ to 1317) |  |  |  |
| Fumdity | 0xto $90 \%$ |  |  |  |
| Approwas |  | C-Tlck, ${ }^{\text {c }}$ |  |  |

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## INSTALLATION INSTRUCTIONS



MODEL NUMBER TDF-3A-120V
TDF-10A-120V
TDF-20A-120V
TDF-3A-240V
TDF-10A-240V
TDF-20A-240V

## 1. PREPARATION

DANGER: Electrical shock or burn hazard. Installation of this Transient Voltage Surge Suppressor should only be made by qualified personnel. Failure to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections to this electrical panel be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.

## CAUTION NOTES:

1. The installation of this Surge Protector should follow all applicable electrical codes, such as the National Electrical Code, or the Canadian Electrical Code.
2. Check to make sure line voltage does not exceed Surge Protector voltage requirement.
3. Prior to installation ensure that the TDF is of the correct voltage, current, and frequency rating for your application.
4. The earth terminal must be connected to a low impedance earth (< 10 ohms ) for correct operation.
5. Do not perform a "Flash Test" or use a Mega-Ohm Meter (Megger) to test circuits that are protected with TDF modules. Damage may occur to the TDF modules.
6. Follow all instructions to ensure correct and safe operation.
7. Do not attempt to open or tamper with the TDF units in any way as this may compromise performance and will void warranty.

## 2. INTRODUCTION

Transient Discriminating Filters (TDF) are packaged in "DIN 43 $880^{\prime \prime}$ profile enclosures for simple installation onto 35 mm DIN
rails. They can be selected for use on distribution systems with nominal RMS voltages of 120 Vac or 240 Vac at frequencies of $50 / 60 \mathrm{~Hz}$. The 120 Vac unit also operates on nominal 125 Vdc supplies.

## 3. QUICK INSTALLATION OVERVIEW

Install in the following manner:

1. Ensure that power is removed from the area and the circuits that will be connected.
2. Snap lock the TDF module to the DIN rail.
3. Install the appropriate upstream overcurrent protection.
4. Connect wiring to the indicated $V / p$ and o/p terminals.
5. Apply power and observe correct operation of the Status Indication, and alarm facilities if provided - see Section 11.

## 4. PROTECTION CONCEPTS

To optimize effectiveness of the TDF protection, the unprotected and protected wiring should be separated. Wiring from the exposed transient source to the TDF should be considered unprotected and kept approximately $12^{\prime \prime}$ ( 300 mm ) from all other wiring wherever possible. Wiring on the equipment side of the TDF should be considered protected.
The separation of protected and unprotected wiring is recommended to minimize the risk that transients conducted on unprotected wiring may cross couple onto protected circuits, and diminish the level of protection available from the TDF module.

The terminals on the TDF module are labeled "INPUT/LINE" (unprotected side) and "OUTPUT/LOAD" (protected side) assuming that the source of the transients is on the input side of the TDF module.

For applications where the transient source is on the load side of the TDF module, the TDF should be reverse connected with the INPUT/LINE terminals connected to the load side, toward the source of the transients.

## TRANSIENT DISCRIMINATING FILTER

## 5. MOUNTING

TDFs are designed to clip to 35 mm DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the TDF module spring clips to the bottom and the label text the correct way up.

NOTE: TDFs must be installed in an enclosure or panel that:

- prevents the TDF unit temperature from exceeding $122^{\circ} \mathrm{F}\left(50^{\circ} \mathrm{C}\right)$
- provides adequate electrical and safety protection
- prevents the ingress of moisture and water
- allows TDF status indicators to be inspected


## 6. GROUND FAULT CIRCUIT INTERRUPTION (GFCI)

Where GFCI protectors (RCDs/ELCBs) are used, it is preferable that the TDF modules be installed prior to these devices (i.e. upstream). If this is not done, nuisance tripping of the GFCls may occur during transient activity.

## 7. CONDUCTOR TERMINATION

Each TDF terminal is designed to accept wire sizes from 10 to 18 AWG ( $1.5 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ ) solid or stranded conductor. The wire insulation should be stripped back $5 / 16^{\prime \prime}(8 \mathrm{~mm})$.
NOTE: Do not use greater than ginlbs ( 1 Nm ) of torque when tightening the terminals. For UL compliance, where two wires may need to be terminated into one terminal, the permissible wire size is 18AWG each.

## 8. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of every TDF to provide protection to the unit itself, the load and the wiring in case of fault situations. The current rating of the breaker or fuse used should be determined according to below. However, the current rating should be less than the rating of the wiring. For example, if a 20A TDF were installed in a circuit with wiring that can carry 15A, then a 15A overcurrent device must be installed upstream to protect both the TDF and wiring from overload.

| MAX FUSE SIZES: | TDFRATING | FUSERATING |
| :---: | :---: | :---: |
|  | 3 A | 4 A |
|  | 10 A | 10 A |
|  | 20 A | 20 A |

## 9. STATUS INDICATION

TDF modules have a single Status Indicator on the front panel. When power is applied and full surge capacity is available, the Status Indicator will be illuminated. Should power be applied and the indicator fail to illuminate, the TDF should be replaced, as optimum protection is no longer provided.

## 10. MAINTENANCE \& TESTING

Before removing a TDF module from service, ensure that the power has been removed from the module. Replacement of a

TDF module should only be undertaken by qualified personnel.
NOTE: TDF units should be inspected periodically, and also following any periods of lightning or transient voltage activity. Check the Status Indicator and replace the module if it is not illuminated as detailed in Section 9 status INDICATION.

## 11. DINLINE ALARM RELAY (DAR)

The TDF status monitoring circuit which provides the visual Status Indicator, also provides a low voltage opto-coupler alarm output circuit. Should voltage free alarm contacts be required, the ERICO Inc, DINLINE ALARM RELAY (DAR) should be used.

The DAR module provides a fully isolated dry contact alarm output. One DAR can be used per TDF, or up to 16 TDFs can be connected in series to one DAR to provide a common dry contact alarm output.
Ensure that the voltage rating of the alarm wiring is rated in accordance with the other voltages present in the equipment. This would normally be the same voltage rating as that used for the TDF module input wiring.
It is recommended that the DAR unit be powered from the outputload side of the TDF being monitored, however the DAR can be powered from other circuits. This allows for example, one DAR unit to be connected to separate TDFs which are protecting a three phase circuit.

NOTE: Depending upon the usage of the DAR output contacts, failure of power to the DAR may be interpreted as a failure of one or more TDFs. Visual inspection of the DAR and TDF Status Indicator is required to clarify this situation.

## 12. USE OF OTHER INTERFACES

ERICO, Inc. DAR units are recommended for the interfacing of equipment to the TDF opto-coupler alarm output circuit. The direct connection of other equipment to the TDF opto-coupler alarm output circuit may not provide sufficient isolation or exceed the opto-coupler specifications. This may damage the TDF and/or the connected equipment. Warranty may be voided under such circumstances. However, the specifications for TDF alarm output has been provided for those who desire to use the TDF opto-coupler output directly.

The TDF alarm opto-coupler output is available on terminals 3 and 5 . Terminal 3 is the positive and 5 is the negative side. This output is an open collector transistor output of the optocoupler. When the opto-coupler is driven on, it should be arranged to have 2 mA flowing through it. For use with 24 Vdc circuits, a $12 \mathrm{k} \Omega$ current limiting burden resistor is required. For use with 12 Vdc circuits, a $5.6 \mathrm{k} \Omega$ current limit resistor is required. For use with 5 Vdc circuits, a $2.2 \mathrm{k} \Omega$ current limit resistor is required.

NOTE: In connecting to the TDF opto-coupler alarm output, do not reverse the +/-connections or exceed the maximum permissible ratings $(30 \mathrm{Vdc})$ as damage may occur.

# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144 Lavarack Av \#1 Eagle Farm

Equipment Type: Surge Filter Alarm Relay
Location: Main Incomer
Model Numbers: ..... DAR-275V
Manufacturer: Critec
Supplier:
Energy Correction Options PO Box 431
Kelvin Grove, QLD. 4059Ph: 0733560577Fx: 0733561432Web: www.ecoptions.com.au

## INSTALLATION INSTRUCTIONS



MODEL NUMBER DAR 275V

## 1. PREPARATION

DANGER: Electrical shock or burn hazard. Installation of this device should only be made by qualified personnel. Failure to lockout electrical power during installation or maintenance can result in fatal electrocution or severe burns. Before making any connections be sure that power has been removed from all associated wiring, electrical panels, and other electrical equipment.

## CAUTION NOTES

1. The installation of this device should follow all applicable electrical codes, such as the National Electrical Code.
2. Check to make sure line voltage does not exceed DAR275V voltage ratings.
3. Follow all instructions to ensure correct and safe operation.
4. Do not attempt to open or tamper with the DAR in any way as this may compromise performance and will void warranty. No user serviceable parts are contained.

## 2. INTRODUCTION

Selected DSD, TDS \& TDF DINLINE Surge Protection Devices include status monitoring circuits which provide visual status display of device capacity. They may also provide a low voltage opto-coupler alarm output circuit that can be connect to the DAR to provide potential free (Form C) change-over contacts. The DAR alarm contacts may be used to provide output to external alarm systems or remote monitoring circuits.
One DAR can be used per DSD/TDS/TDF opto-coupler alarm or up to 16 DSD opto-coupler alarms can be connected in series to the one DAR to provide a common output. It is recommended that the DAR be powered from the same power circuit that feeds the device(s) being monitored, however the DAR can be powered from other circuits. This allows for example, one DAR unit to be connected to separate SPDs that are protecting a three phase circuit.

Note. Depending upon the usage of the DAR output contacts, failure of power to the DAR may be interpreted as a failure of one or more of the SPDs being monitored. Visual inspection of the DAR and SPDs status displays would determine this.

## 3. MOUNTING

The DAR is designed to clip to 35 mm (top hat) DIN rails (standard EN50022). Unless otherwise mechanically restrained, use horizontal DIN rails with the DAR module spring clips to the bottom and the label text the correct way up.
NOTE: The DAR must be installed in an enclosure or panel that:

- prevents the DAR temperature from exceeding $131^{\circ} \mathrm{F}\left(55^{\circ} \mathrm{C}\right)$
- provides adequate electrical and safety protection
- prevents the ingress of moisture and water
- allows DAR status indicators to be inspected


## 4. ELECTRICAL CONNECTION

The interconnecting wiring should:

- be of size \#10 b \#14 AWG ( $2.5 \mathrm{~mm}^{2}$ to $6 \mathrm{~mm}^{2}$ ) solid or stranded conductor.
- The wire insulation should be stripped back $5 / 16^{\prime \prime}(8 \mathrm{~mm})$.
- NOTE: Do not use greater than ginibs ( 1 Nm ) of torque when tightening the terminals.


## CONNECTION TO TELECOMMUNICATIONS NETWORKS

The DAR is approved for use in Australia where the alarm contacts may be connected to private lines or building cabling associated with the telecommunications network. NO direct connection to the public switched network should be made.

## INSTALLATION INSTRUCTIONS

## 5. INTERCONNECTION

When connecting the DAR to a single opto-coupler output the + terminal of the SPD should connect to the + terminal on the DAR. The - terminal should connect to the - terminal.


When connecting the DAR to multiple opto-couplers the optocouplers should be connected in series with + terminal of one connected to the - terminal of the next. The DAR + terminal should connect to + SPD terminal at one end of the series connection and the - DAR terminal connect to the - SPD terminal at the other end of the series connection.


## 5. STATUS INDICATION



## 6. FUSING AND ISOLATION

Overcurrent protection must be installed in the upstream circuit of the power supply to the DAR to provide protection to the unit itself and the wiring in case of fault conditions.

The fuse rating should be based on the wiring size used to connect to the DAR Ph \& N terminals. Australian regulations AS3000-1991, Table B2 specifies the following upstream protection for single phase circuits, unenclosed in air.

| Cable Size | HRC Fuse or | CB Rewirable Fuse |
| :--- | :---: | :---: |
| $1.5 \mathrm{~mm}^{2}$ | 16 A | 12 A |
| $2.5 \mathrm{~mm}^{2}$ | 20 A | 16 A |
| $4 \mathrm{~mm}^{2}$ | 25 A | 20 A |
| $6 \mathrm{~mm}^{2}$ | 32 A | 25 A |

Where overcurrent protection of the appropriate rating or smaller is already fitted in the upstream circuit, overcurrent protection at the DAR will not be required

## 6. MAINTENANCE \& TESTING

Before removing a DAR unit from service, ensure that the power has been removed. Maintenance, testing and replacement should only be undertaken by qualified personnel.

Testing of a DAR unit which is connected to a fully functional DSD unit can be accomplished by removing power to the DSD only. The DAR Status indication and output contacts should alter from the Normal to Fault condition.

Testing of the DAR unit alone may be accomplished by disconnecting the $+/$-connections to the unit. When power is applied the DAR "Fault" Status Indicator should be illuminated. By connecting the $+/$ - terminals together, the "Normal" Status Indicator should be illuminated. The output contacts should alter to the appropriate state.

## 7. USE OF OTHER INTERFACES

Only DAR units are recommended for the interfacing of equipment to the DSD, TDS \& TDF opto-coupler alarm output circuit(s). The direct connection of other equipment to these opto-coupler alarm outputs may not provide sufficient isolation or exceed the opto-coupler specifications. This may damage the SPD and/or the connected equipment. Warranty may be voided under such circumstances.

NOTE: In connecting to the SPD opto-coupler alarm output(s), do not reverse the +/- connections as damage may occur

# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144

 Lavarack Av \# $\mathbb{1}$ Eagle FarmEquipment Type: Phase Failure Relay
Location: Common Control
Model Numbers: ..... 252-PS GW
Manufacturer: Crompton
Supplier: Crompton Instruments. PO Box 5108
Minto Business Center Minto NSW, 2566Ph: 0296032066Fx: 0296039335

## Page 1 of 2

Ref: IW250PMSH - Rev 6 - March 02

## Models Covered

| 252-PMM $\quad$ 252-PMT |  |
| :--- | :--- |
| 253-PH3 | $252-P M M$ |$\quad 252-\mathrm{PMT} \quad 252-P S G$

## Introduction

Thermistor Trip Relay (252-PMM \& 252-PMT).
The trip inputs are monitored within settable limits. In the event of the input moving outsidethese limits, the unit will initiate a trip sigñal via a double pole chángeover relay. An illuminated green LED indicates when the thermistor temperature is within normal working limits. The unit is . designed such that the atarm relay is energised when normal temperatures are reached.
Model 252-PMM has the facility for manual. resetting, so that the trip condition remains after normal operating temperature is reached, until manual intervention occurs.

Phase Balance Relay (252-PSF 8252 -PSG)
Trip inputs are monitored within settable limits. In the event of the input moving outside these limits, the unit will initiate a trip signal via a double pole changeover relay. An illuminated red LED indicates that the supply is within limits:

Speed Sensing Relay (263-PH3)
Trip inputs are monitored within settable limits. In the event of the input moving outside these limits, the unit will initiate a trip signal. The illuminated red LED's indicates that the single pole output relays are in an energised state anid at normal running speed all three relays should be energised. Units are factory adjusted for normal runing speed $=0.75 \mathrm{~mA}$. output. The meter adjust "óol on the product frontisused for this requirement, which also ensures the trip levels are set to the calibrated values. Terminal 8 is connected to terminal. 5 internally: Terminals 15 and 16 give a $0 / 1 \mathrm{~mA}$ signal proportional to speed.

No. 1 Relay energises on rising speed
No. 2 Relay energises on rising speed
No. 3 Rëlay de-energises on rising speed
This product is designed for use only with magnetic coil inductive sensors.

## Waming

- During normal operation; voltages hazardous to life may be present at some of the terminals of this unit. Installation and servicing shoutd be performed only by qualified, properly trained personnel' abiding by local regulations. Ensure all supplies are de-energised before attempting connection or other procedures.
- It is recommerided adjustments be made with the supplies de-energised, but if this is not possible, then oxtreme cautionishould be exeŕcised.:
- Teminals should not be user accessible after installation and extemal installation provisions must be sufficient to prevent hazards under fault conditions:
- This unit is not intended to function as part of a system providing the sole means of fault protection - good engineering practice dictates that any critical function be protected by at least two independent and diverse means.
Never open circuit the secondary winding of an energised current transformer:


## Protector Trip Relays

## DIN Rail $\&$ Wall Mounted 250 Series

 Thermistor Trip, Speed Sensing \& Phase Angle
## Installation

The Protector should be installed in a dry position, not in direct sunlight and where the ambient temperature is. reasonably stable and will not be outside the range 0 to 60 degrees Celsius. Mounting will normally be on a vertical suifface but other positions will not affect the operation. Vibration should be kept to a minimum:-The Protectors are designed for mounting on a 35mm rail to DIN 46277. Alternatively they may be screw fixed; a special adaptor is supplied to mount 252 types.

To mount a protector on a DIN rail, the top edge of the cutait on the back is hooked over one edge of the rail and the botiom edge carying the release dip clicked into place. Check that tie unit is 而mly fixed. Removal or repositioning may be actiseved by tevering down the release dip and lifting: the unit up and of the rail.

Connection diagrams should be carefully followed to ensure correct potanity and phase rotation where applicable. Extemal voltage transtomers may be used on 252-PSF and 252-PSG to extend the range:

252-PMM1 252-Part \& 253-PH3
Pick up, orpert and outpit leads should be kept separate from any other wining.

Setting Controls (252-PSF, 252PSG)
These products have wo calibration facilities that can beset to sufit operating requirements and they are lactory calibrated as follows:-

1. . \% unbalance set points

Voltages of and below 380 vodts $\mathrm{L}-\mathrm{L}$ are cafibrated to
$1.0 \%$ class index of rated voltage. Voltages above 380 volts L-L are calibrated to $1.5 \%$ class index of rated voltage.
2. Time Delay

For all voltage ranges $10 \%$ maximum delay:
3. Voltage Withstand

Continuous overload $=1: 35 \times$ rated voltage

## Setting Up (all other models)

The calibration marks around the controls are provided as a guide if the installer does not have access to accurate equipment. The maximum erior of the calibration marks is typically $10 \%$ of the span of the control concemed.

## Maintenance

The unit should be inspected to normal standards for this class of equipment. For exampte remove accumulations of dust and check all connections for tightness and corrosion: In the unlikely event of a repatr being necossary it is recommended that the unit be retumed to the factory or to the nearest Crompton Instruments Service Centre

## Electromagnetic Compatibility

This unit has been designed to provide protection against EM (electro-magnetic) interference in line with requirements of EU and other regulations. Precautions necessary to provide proper operation of this and adjacent equipment will be installation dependent and so the following can only be general guidance:-

- Avoid routing wining to this unit alongside cables and products that are, or could be, a source of interference.


## Page 2 of 2

Ref: IW250PMSH - Rev 6-Marct 02

Protector Trip Relays DIN Rail \& Wall Mounted 250 Series Thermistor Trip, Speed Sensing \& Phase Angle

- The auxiliary supply to the unit should not be suitject to excessive interference. In some cases; a supply line filter may be required.
- To protect the product against incorrect operation or permanent damage, surge transients must be controlled. It is good EMC praclice to suppress differential surges to 2 kV or less at the source. The unit has been designed to automatically recover from typical transients, however. in extreme circumstanices it mayibe recessary to temporaily disconnect the auxiliary supply for a period of greater than 5 seconds to restore correct operation.
- Screened communication and small signal leads are recommended and may be required. These and other connecting leads may require the fitting of RF suppression components, such as ferrite absomers, line fiters etc., if RF fields cause problems.
- it is good practice to install sensitive electronic instruments. that are pertorming critical functionsin EME enctosures that protect against electrical interference causing a disturbance in function.


The Information contained in theese instailation linstuctions is tor use onty by installers trained to make electrical power instiallations and is intended to describe the correct method of installation tor this procuct However, Tyco Electronics has no control over the lietd condithons, which influence producd instalation.
It is the user's responslblity to determine the sumataility of the installation method In the user's fieid conditions. Tyco Electrortics' only obligations are those in Tyco Elactronics' standard Conditions of Sala for thls product and in no case will Tyco Electiontes be liabte for einy other bxddental, indirect or consequential dameges ising from the use or misuse of the products. Crompton is a trade mark..

## TECHNICAL DATA SHEET

For

## SEWERAGE PUMP STATION SP144

 Lavarack Av \#1 Eagle FarmEquipment Type:<br>Level Relay<br>Location:<br>Common Control<br>Model Numbers:<br>MTR 240VAC<br>Manufacturer:<br>Multitrode<br>Supplier:<br>Multitrode Pty Ltd 130 Kinston Road Underwood. QLD 4119<br>Tel: 0733407000<br>Fax: 0733407077

## 1 Introduction

The MultiTrode level control relay is a solid-state electronic module in a hi-impact plastic case with a DIN rail attachment on the back, making a snap-on-snap-off installation. Any number of relays can be easily added to the DIN metal rail then wired together to form a complex pumping system that other wise may have to be controlled and operated by a programmed PLC.
The relay is normally matched with the Multitrode probe which works in conjunction with the relay and uses the conductivity of the liquid to complete an electrical circuit.

## 2 Electrical Overview



If the tank is plastic, or if you are conducting tests in a plastic bucket, or the vessel has no earth point inside, you must install an earth rod within the tank, vessel or bucket and make sure that it is bonded back to $C$ on the relay unit.

## 3 DIP Switches

### 3.1 DIP Switches

(See Wiring Diagram for full program functions.)

### 3.1.1 DIP 1 \& 2

DIP. 1 and 2 control the Sensitivity, in other words the cleaner the liquid the higher the sensitivity setting must be. Concentrated acids, minerals are by their own chemical composition highly conductive, so a low level of sensitivity is required, purified water is almost an insulator against electrical current flow so a higher sensitivity inside the relay is required.


### 3.2 Relay Contacts \& their Applications

### 3.2.1. Contacts $15,16 \& 18$

Contacts 15; 16; and 18 are úsed for electronic or visual rotification of a change in state at the pump itself. Contacts 15, 16, and 18 are used for more advanced applications because they are a changeover relay, their state may be the same as contacts $25 ; 28$ or the opposite. Both sets of contactors are triggered simultaneously. An example is when in discharge mode, (see Figure 1).
You have a gravity flow coming in so the fluid reaches the lower sensor PB1, contacts 15 and 18 are open ( 15 being common to both contact 16 and 18 ) contacts 25 and 28 are also normally open but … contacts 1516 in this current situation are closed, whether PB1 is wet or dry is of no concem all will stay the same. The level now rises to PB2 and both relays change state, contacts 25 and 28 close to turn on the pump, contacts 15 and 16 are open, with 15 and 18 closed.
In advanced applications this state change may be fed into a logic device to indicate the pump is running or the pump has stopped and perhaps light an LED or incandescent light source for visual confirmation that a change has occurred in the relay.

### 3.2.2 Contacts 25828

Contacts 25 and 28 are used to control pump states. Contacts 25 and 28 are mostly used for turning on motors via a starting relay or solenoid, so, these sets of contacts react to the rising or falling levels of the fluid inside the tank, they will operate to tum on a pump in discharge mode when the top sensor is wet and in charge mode tum on the pump when the bottom sensor is dry.

## 4 Practical Overview

### 4.1 Discharge Mode - DIP switch 6 set to "OFF"



Figure 1 - Discharge Mode
Figure 1 shows two probes, (PB1 connected to Lo and PB2 connected to Hi). The pit is mostly underground and there is a gravity-fed inlet at the top left-hand side. The pit is empty with PB1 completely dry. Dipswitch 6 is set to "OFF:"


The relay operation depends on the electrical conductivity of liquid in the pit, i.e. no liquid $=$ no curent, flow. The level starts to rise and covers PB1:

This is a discharge operation so we do not want the relayito close and start a pump until the well is full so as the water rises it reaches PB2, the relay closes and the pump starts. The level now drops below PB2 but the pump still continues to run, the level continues to drop below PB1 the relay opens the pump stops.

### 4.2 Charge Mode - DIP switch 6 set to "On"



Figure 2 -Charge Mode
Note:. $\because{ }^{4} C^{n}$ is connected to common bonded earth. The unit will not operate correctly if not earthed.
Let's look at the same relay but in a tank that is charging (DIP 6 is now on). See Figure 3 ; where liquid is being pumped into a tank, and
discharging through a gravity feed the tank is on steel stands " $x$ " metres above the ground.


With the tank full, PB1 and PB2 will be wet, the relay is off, and the pump has stopped. Water is slowly fed out from the bottom, and now as PB2 (HI) becomes dry nothing happens; the water now drops to below PB1 (Lo); and the pumps restarts to fill the tank.
The pump will continue to fill the tank until PB2 (HI), becomes wet again.

### 4.3 MTRA Relay with Alarm (Discharge Applications Only)



Scandurd
Figüre $3=$ MTRA: Operation

保

The MTRA relay works in the same way as the MTR relay except the MTRA has a separate alarm output, and does not have a charge mode. The planned application is to close a contact to illuminate a warning alarm light. . Various other applications have included introducing a third probe to latch another relay.
In Figure 2 we see three probes in a pit that is plastic, note the steel rod in the tank. (In a plastic vessel a steel rod must be used to create an earth return in the liquid so probes can function.) PB1, PB2, and PB3 are dry, and the relay power LED is on. When water enters the pit and wets PB1, nothing happens, water now reaches PB2 causing contacts 13 and 14 to close, the pump LED to light, and the water to drop.
If, for example, the pump has its inlet partially blocked, the level continues to rise and wets PB3. This closes a separate relay that can activate a red flashing light, an audible fog horn or send a 5 volt pulse into another device with the common cause to warn human beings that a spill is due to occur. If the pumps become unclogged and PB3 becomes dry the alarm opens again and breaks the circuit that stops the light from flashing or the foghorn from sounding.

## 5 Most Common Installation Problems

The relay requires a path between the probes to earth through the liquid. If you are testing in a plastic bucket, have installed the probe in a plastic tank or have no good earthing in the vessel you will need to install a separate earth and make sure all earth bonding comes back to the $C$ terminal. Most problems like these are traced back to a lack of or poor earthing, or open circuits in the probe wiring.
Now is the time to check the relay by using "the bridge testing line technique" remember you must simulate a fluid flow to correctly ascertain a good relay or a bad one. (All DIPswitch settings from 1 to 6 should be off.)
Cut two pieces of insulated flexible copper wire one black one red 250 mm long, strip both ends back 10 mm on both cables, and join one black end and one red end. Insert the joined ends into C on the relay box, observing all safe electrical practises. You should have one black wire and one red wire free.

Set your relay for discharge mode (DIP switch 6 is off) with no sensors connected to the unit, connect the red wire to Lo - nothing should happen (if it does return the relay for replacement or repair*). Now connect the black wire to the Hi terminal the relay activated LED should light iristantly (if it does not, the relay should be returned for repair*).

## 6 Troubleshooting

| I have checked all the DIPswitches and settings but in discharge mode as soon as the bottom sensor gets wet the pump turns on then turns off almost straight away. | - This is the most common problem encountered with relay set up and commissioning, the probe in the bottom of the tank is wired into the Hiterminal instead of the Lo terminal. |
| :---: | :---: |
| The installation went fine but now and again the pump will not turn on even though I am sure the probe is wet. | - Check the sensitivity level set on the relay, some times the level is set for foul water but due to changes in the flow the water becomes grey or clear, try changing the setting from $20 \mathrm{~K} \Omega$ to $80 \mathrm{~K} \Omega$ and monitor the results carefully. |
| All wiring is complete and all DIPswitches have been checked but the pump will not turn on at all. | - If you have completed the test schedule for the relay and it passed then check the wiring to the sensors - for this is now where the problem lies or in the earthing arrangements. If possible check the resistance between the sensor cable and the steel sensor on the probe to prove a solid connection. |

## * Please contact your distributor or agent before returning any product for repair or warranty claim.



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## TECHNICAL DATA SHEET

For

## SEWERAGE PUMP STATION SP144 <br> Lavarack Av \#1 Eagle Farm

| Equipment Type: | Radio |
| :--- | :--- |
| Location: | RTU Section |
| Model Numbers: | DR900-06A02-D0 |
| Manufacturer: | Trio |
| Supplier: | Brisbane Water |

## TC-900DR USER GUIDE

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## GENERAL

The Trio DataCom TC-900DR is a full duplex 900 MHz Radio featuring a fully integrated 4800/9600 bps data radio modem and antenna diplexer. Configuration of the unit is fully programmable, with parameters held in non volatile memory (NVRAM). All configuration parameters are accessible using the TC-DRPROG installation package, consisting of a programming lead, manual and software which will run on a PC under Windows 95/98/NT. It is essential that each unit is programmed to suit individual requirements prior to operation. For detailed information refer to the TC-9000R Handbook.

## DATA CONNECTION

The data connection is via a DB9 connector labeled 'Port ' (shown below), which is wired as a DCE

User Serial "Port A" Pin Assignment.
EXTERNAL VIEW OF 'PORT A
NOTE: Pin 6 and pin 9 provide a dual function which depends on the mode that the TC-900DR is operating in


PIN NO. \& FUNCTION

1. DATA CARRIER DETECT (DCD)
2. RECEIVE DATA OUTPUT (RXD)
3. TRANSMIT DATA IN (TXD)
4. DATA TERMINAL READY (DTR)
5. СОММОN (СОМ)
6. PROGRAM PIN ( $\overline{\mathrm{GGM}}$ )
7. REQUEST TO SEND (RTS)
8. CLEAR TO SEND (CTS)
9. BIT ERROR RATE PIN (BER)

## User Serial "Port B" Pin Assignment.

Port B can be used as a secondary data steam (independent of Port A ) once configured by the programmer. Port B also has one connection that may be of use for installation. This connection (Pin 9) is Receive Signal Strength Indicator (RSSI) output. $0-5 \mathrm{~V}$ where 1.5 V typically indicates -110 dBm and every 0.5 V increase indicates an improvement of » 10 dBm .
EXTERNAL VIEW OF 'PORT B'


PIN NO. \& FUNCTION

1. DATA CARRIER DETECT (DCD)
2. RECEIVE DATA OIP (RxD)
3. TRANSMIT DATA O/P (TXD)
4. UNUSED
5. COMMON
6. DATA SET RECEIVE (DSR)
7. UNUSED
8. UNUSED
9. RECEIVE SIGNAL STRENGTH

NOTE: Port B Pin 9 output has a high impedance of around 50 K OHMS and loading will decrease accuracy of the RSSI measurement.

## POWER CONNECTIONS

The power required is 13.8 VDC nominal, at 600 mA ( Tx ) nominal. If the POWER LED indicator is not illuminated once power is applied, check the internal 1Amp fuse fitted within the unit.

POWER CONNECTOR TOP PIN
BOTTOM PIN

## AUXILIARY CONNECTOR

The auxiliary connector is primarily for use with the optional audio handset. The connections to this auxiliary 6 pin RJ11 connector are as follows:

| PIN NUMBER |
| :--- |
| 1 |
| 2 |
| 3 |
| 4 |
| 5 |
| 6 |

FUNCTION 8 VOLTS AUDIO OUT GROUND MIC INPUT/SENSE GROUND MANUAL PTT

The optional audio handset is recommended as an aid in checking installations for radio path viability. This audio handset will only function when fitted prior to applying power to the unit.
The modem upon power up will check the presence of the handset and will inhibit data being transmitted so that voice communications can be established.
Once the path tests have been conducted the audio handsets MUST be REMOVED and the unit powered up with the handset removed before data communication can commence.

## USER INDICATIONS

The TC-900DR provides 4 LED's that show status information to the user - POWER, RXSIG, SYNC, and TXMIT indications.
The POWER is indicated by a green LED and simply signifies that power has been applied to the unit.
The RXSIG LED (yellow) indicates the level of RSSI signal from the radio IF strip, compared to a threshold level set in the configuration data programmed by the user. If the signal is above the threshold, then the LED indicator is turned on.

In all operation modes except "Programmer mode", the SYNC LED (yellow) indicates when the modem has detected a valid data stream. The SYNC LED is activated, when the modem detects a valid HDLC flag sequence, and remains active until an invalid sequence of seven or more consecutive " 1 " bits is detected.
The SYNC LED will not be turned on if the RSSI signal strength (as indicated by the RXSIG LED) is below the minimum threshold. This prevents false SYNC detection from noise.
The TXMIT LED (red) indicator is connected directly to the modem's PTT output transistor. Whenever the radio is transmitting, this TXMIT LED indicator will be on.

## SPECIAL MODES OF OPERATION

Part of the power-up/reset initialisation phase of the TC-900DR are tests to determine if the modem should enter one of 3 "special operation" modes. In these modes the TC-900DR won't operate in its standard run mode.

- Programmer mode.
- Bit error rate test mode.
- Handset mode

These modes are only entered if the required setup conditions are present at power up. An error mode of operation can also be entered into, if during normal operation, an error condition occurs

## PROGRAMMER MODE

CABLE - Pins 2, 3, 4, 5 straight through with Pin 6 on the DB9 connector of Port A, connected to pin 5. When the modem is powered up with this fitted, the controller senses this and attempts to enter "Programmer mode" and the "SYNC" LED will flash approx. once per second. (Note, the TC-DRPROG programming software and lead has the required connections). Failure to supply the correct password in time, will cause the modem to abandon the "Programmer mode" attempt, and go on with it's normal jower-up procedure.

## BIT ERROR RATE TEST MODE

Pin 9 of the DB9 connector of Port $A$, is normally the Ring Indicate output line. However, if this pin is driven positive (connecting it to pin 6 [DSR] and pin 7 [RTS]), then the modem's data transmitter and receiver will enter the BER test mode. This will activate the RF transmitter, and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic " 1 " level in the unscrambled data. Any errors in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a "0" bit.

Note: As the TC-900DR is full duplex this test can operate in both directions simultaneously.
Every error bit detected, will activate the SYNC LED. For error rates of 1 in $10^{3}$ and above, the SYNC LED will be ON most of the time. A 1 in $10^{4}$ error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for nstallation purposes. Note: Error count messages ( $E T: X X X X$ ) for every 10,000 bits are presented to Port A for the user. If pin 9 ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

## HANDSET MODE

The DFM4-9 modem tests for the presence of a handset plugged into the handset auxiliary port at power up. If a handset is plugged in, the modem will not generate a data stream. However, it will continue to indicate received RF signal strength. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED. It is essential to remove the handset from the unit and reapply power to the unit in order to return to normal operation. ERROR INDICATION MODES
There are 3 error conditions that cause the RXSIG \& SYNC LEDs to be used for error indications and not their normal purpose. Two are fatal conditions, that cause the modem to restart after the duration of the error indication hase.

## TRÁNSMIT POWER LOW

While the modem activates the radio transmitter, it periodically checks the transmit power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately 4 times per second. The TXMIT LED will also be on during this process. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function. Factory set to 100 milliWatts.

## NVRAM READ ERROR

The DFM4-9DR modem accesses the non-volatile memory as part of it's initialisation phase, to read programming configuration data. If the communication protocol with the device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED operates ON and OFF twice, then the other. A total of five cycles of this occurs, then the modem restarts initialisation.

## SYNTHESISER LOCK DETECT ERROR

If at any time during normal operation, BER mode, or handset mode, the TBB206 frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting.

One LED is turned ON ( 0 ), the LEDs are swapped, then both turned $\operatorname{OFF}(\bullet)$. Then the latter LED ON again, swap LEDS, and then OFF. This will give the appearance of a sweeping motion between the LEDs. The following table shows all error condition displays.

| TXPWR Err |  | NVRAM Err |  | SYNTH Err |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | $\bullet$ | 0 | $\bullet$ | 0 | $\bullet$ |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ | 0 |
| 0 | $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ | $\bullet$ | 0 |
| 0 | $\bullet$ | $\bullet$ | 0 | 0 | $\bullet$ |
| 0 | 0 | $\bullet$ | $\bullet$ | $\bullet$ | $\bullet$ |
| 0 | $\bullet$ | $\bullet$ | 0 |  | repeat |
| $\bullet$ | 0 | $\bullet$ | $\bullet$ |  |  |
| continue |  |  | repeat |  |  |

## MOUNTING AND ANTENNA CONNECTION

The TC-900DR should be mounted in a cool, dry, vibration free environment, whilst providing easy access to screws and connections. There are 4 mounting holes on the unit. The antenna should be an external yagi antenna but can be a ground independent dipole mounted via a feeder to the antenna connector (SMA type) for short range applications. However the whole radio modem should be clear of the associated data equipment to prevent mutual interference.

## ASSEMBLY OF POWER LEAD

A small plastic bag containing a molex connector (M5557-2R) and two pins (M5556-TL) is provided in the packing box.
The pins are designed to take 18-24 (AWG) wire size with insulation range 1.3-3.10mm.

Please take care when crimping the pins. 04/01


## TC-900DR

## 900 MHz <br> Full Duplex Data Transceiver

## User Manual

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## IMPORTANT NOTICE

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## Modifications

| Issue 1 | February 1993 (Preliminary) |
| :---: | :---: |
| Issue 2 | May 1993 Major Changes to Section 3 |
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|  | Removed Filter Alignment Setup Diagram |
|  | Inserted RSSI Level of Received Signal (typical) |
| Issue 4 | February 1994 |
|  | Minor Changes to all sections |
|  | Additions to Section 3 for Firmware V2.2 and Synchronous Operation |
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|  | Addition of section 5.2.6.1 and 5.2.6.4 |
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Issue 12 July 2000
Minor Change to Section 7

Issue $13 \quad$ February 2001
Change of Company Name

## SECTION 1

## INTRODUCTION

## 1 INTRODUCTION

### 1.1 GENERAL

The TC-900DR is a Full Duplex 900 MHz Radio, featuring a fully integrated 4800 or 9600 bps data modem.

The entire unit is housed in a robust metal enclosure that provides a compact and transportable means for the transmission of data over radio.

The product has been fully designed and developed in Australia, by an Australian owned and managed company.

The TC-900DR meets the ACA SP4/89 specification which covers radio data transmissions over point-to-point and point-to-multipoint systems.

It is ideally suited for applications such as :
, Transaction Processing.
, Public Utility Telemetry Systems.
, Alarm Monitoring.
" Supervisory Control and Data Acquisition.
„ Energy Distribution.
, Inventory Control
„ Common Carrier Data Services.
, Temporary Installations
The modem provides byte oriented packet data communications over narrow band FM systems, using digital filtered binary FSK modulation.

The TC-900DR can be supplied for use with $12.5 \mathrm{kHz}, 15 \mathrm{kHz}, 25 \mathrm{kHz}$ or 30 kHz channel spacings. Its operational parameters can be programmed with the TC-D Series installation programmer. This is a separate software package that runs on an IBM compatible PC under Windows 95/98/NT.

### 1.2 FACTORY QUALITY ASSURANCE

The TC-900DR has been designed and manufactured with particular emphasis placed on the following points:
\{ State of the art design techniques.
\{ Simple assembly/disassembly.
\{ Minimal alignment requirements.
\{ Manufactured using quality compenents.
All units have been manufactured using automated assembly procedures. This assures attention to detail and a high level of quality control.

All components used are of high quality, and conform to Trio DataCom's required specifications. The component suppliers provide batch, date and manufacturing criteria that are required to meet quality control standards.

Each unit is individually tested with an inbuilt self diagnostic program. It is then passed through a set of automatic test procedures with minimal human intervention. This ensures a consistently manufactured and performing product. Many of the alignments are factory set and should not require re-alignment in the field.

Trio DataCom's quality control does not finish here. Once each unit has passed its individual tests, it is placed in a cyclic heat/cooling chamber. This chamber is automatically cycled from $-10^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$, twice, over a twenty hour period. During this time, the modem controller - using external precision calibrated test equipment - monitors and stores frequency stability versus temperature data. The TC-900DR uses this information to achieve its temperature compensated, frequency stability level of 1 ppm .

Power output is measured during the temperature cycling. This is achieved by having the unit connected to a PC and various test equipment via a GPIB. Units that fail any of these tests are reported by the test program and corrective action taken before going through the complete cycle once again. Each unit shipped from the factory comes with a factory alignment printout which details:
, Configuration.
" Transmit frequency.
, Receive frequency.
„ Receiver sensitivity.
" Transmitter power output.
" Transmitter modulation.
In most cases, the radio transmitter as shipped from the factory will require no re-alignment.

It is this care and quality control that ensures that the purchaser of a TC-900DR radio modem, obtains a consistently manufactured and performance specified product, which has been "burned in" to minimise any operational failures.

### 1.3 FEATURES

Advanced microwave and digital techniques were employed during the design phase of the TC-900DR, ensuring an innovative and state of the art product.

Features include :
\{ Fully integrated full duplex radio and modem
( Built in antenna diplexer
\{ Power output $+30 \mathrm{dBm}(1 \mathrm{Watt}$ nom) at antenna connector
\{ Radio meets ACA SP4/89 requirements $2 / 90$
\{ In-built transparent remote diagnotics capability.
\{ Custom single chip modem - digital signal processing
\{ 4800 \& 9600 bps transfer rates, full duplex
\{ Selectable 110..19k2 asynchronous RS-232 host interface
\{ Unique collision avoidance facilities
\{ Integrated supervisory signalling channel
\{ Software selectable configuration parameters
\{ Configurable bit error rate testing
\{ Excessive temperature power fold-back
\{ Auxiliary port for use with an optional supervisory audio handset

### 1.4 SPECIFICATIONS

### 1.4.1 RADIO SECTION

Rx frequency range
Tx frequency range
Channel spacing

Frequency stability $\quad: \quad 1 \mathrm{ppm}\left(-10^{\circ} \mathrm{C}\right.$ to $65^{\circ} \mathrm{C}$ amb), [opt $-30^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ ]

Power output at Antenna connector

Duty cycle
Output impedance
Timeout timer
Tx key up time
Rx sensitivity

Rx intermodulation
Rx spurious responses
Tx spurious emissions
aging $<=1 \mathrm{ppm} /$ Annum
923 MHz to 933 MHz (see note 1 )
847 MHz to 857 MHz (see note 2)
Fully synthesized $12.5 \mathrm{kHz} / 25 \mathrm{kHz}$, [opt $15 / 30$ ] with programmable $1 / 2$ channel raster offset
$+30 \mathrm{dBm} \pm 1 \mathrm{dBm}$ ( 1 W nom) switchable under software control $200 \mathrm{~mW} / 1 \mathrm{~W}$

Continuous
50 Ohms
Programmable from 1 sec . to 28 minutes (max)
$: \quad<=$ to 1 mS (output _ 1 dB of power).
0.5 uV at antenna input for 12 dB SINAD at "delayed Rx signal" test point.
$>=70 \mathrm{~dB}$ spurious free dynamic range.
$<=-65 \mathrm{~dB}$.
$<=-65 \mathrm{dBc}$ (ref unmodulated carrier).

Full duplex with single antenna.

Note 1. The reciprocal frequency option for point-to-point operation or point to multi-point base repeaters is available as follows :

- Rx frequency range 847 MHz to 857 MHz .
- Tx frequency range 923 MHz to 933 MHz .

Note 2. The transmitter is normally supplied, with its frequency offset from the receiver by 76 MHz .

| 1.4.2 MODEM SECTION |  |  |
| :--- | :--- | :--- |
| User Ports | $:$ | DB-9 connector, EIA RS232, DCE, serial <br> asynchronous, $300 . .19 \mathrm{k} 2$ baud, $7 / 8$ bit, <br> no/odd/even parity. |
| Data Rate | $:$ | $4800 / 9600$ bps Full Duplex. |
| BER | $:$ | Less than 10E-6 @ -105dbm measured at antenna port |
| Data Format | $:$ | Narrow band digital filtered binary FSK Modulation, <br> using Trio DataCom's DFM4-9 digital modem chipset, <br> including Trio's unique supervisory signalling channel <br> C/DSMA collision avoidance scheme. |
| Synchronisation Delay : | 20 milliseconds. |  |

### 1.4.3 RADIO AND MODEM SECTIONS COMBINED

| Occupied bandwidth : | Meets ACA SP4/89 guidelines for point-to-point and <br> point-to-multipoint assignments. |  |
| :--- | :--- | :--- |
| Mean deviation | $:$ | $\pm 1.5 \mathrm{kHz}(4800 \mathrm{bps})$, <br> $\pm 2.75 \mathrm{kHz}(9600 \mathrm{bps})$ |
| Power requirements : | $14 \mathrm{Volts} \mathrm{AC} \mathrm{10VA} \mathrm{or} \mathrm{13.8VoltsDC(11} \mathrm{to} \mathrm{16V} \mathrm{Max} \mathrm{)}$. |  |
| Transmit current | $:$ | $<=$ to 600 mA. |
| Receive current | $:$ | 175 mA. |
| Size | $:$ | $241 \mathrm{~mm} \times 161 \mathrm{~mm} \times 65 \mathrm{~mm}$. |
| Weight | 1.3 Kg. |  |

### 1.4.4 CONNECTORS

| User RS-232 Connection | DB9 female wired as DCE (modem). <br> (AMP Part \# 747844-5) |
| :---: | :---: |
| Mating connectors | DB9 male solder type. <br> (AMP Part \# 747983-3) <br> Backshell to suit. <br> (AMP Part \# 205729-1). <br> Optional supplied to order |
| Antenna Connection | Gold plated SMA female bulkhead. (E.F.JOHNSON Part \# 142-0701-501) |
| Mating connector | SMA male to RG223 crimp type. (E.F.JOHNSON Part \# 142-0407-006) Optional supplied to order |
| AC/DC Power Connector | 2 pin locking ( 9 A rating). <br> (PCB SOCKET MOLEX Part \# M5569-2A2) |
| Mating connector | (RECEPTACLE MOLEX Par\# M5557-2R) (RECEPT PINS MOLEX Part \# M5556-TL). Supplied with standard unit. |
| Supervisory Audio |  |
| Handset Connector | 6 pin modular jack. <br> (AMP Part \# 520250-3) |
| Mating connector | 6 pin modular jack plug. <br> (AMP Part \# 5-641337-3). <br> Supplied with optional audio handset. |

### 1.5 OPTIONAL ACCESSORIES

Trio stock a large range of ancillary devices including coax cables, RF connectors, antennas, lightning protection, power supplies, etc.

Please contact Sales for futher information.

## SECTION 2

## HARDWARE TECHNICAL DESCRIPTION

## 2 HARDWARE TECHNICAL DESCRIPTION

### 2.1 GENERAL

The TC-900DR is a 900 MHz full duplex radio complete with radio modem and antenna diplexer. In this and subsequent descriptions to follow, references have been made to block diagrams, circuit diagrams and component loading diagrams.

These can be found in appendix $A$, at the rear of this manual.
The unit can be divided into five major sub-blocks :
Radio section.
Antenna diplexer section.
Audio handset.
Modem section.
Unit housing assembly.

### 2.2 RADIO SECTION

The radio section is built on a single PCB with approximate dimensions of $193 \mathrm{~mm} \times$ $152 \mathrm{~mm} \times 1.6 \mathrm{~mm}$.

This section consists of the following main blocks :
Receiver.
Transmitter.
Frequency control.
Interfaces.
Each of these blocks can be further broken down as follows :
Receiver.
Pre-amplifier.
Mixer.
45 MHz I.F. filter.
FM I.F. \& Demodulator
Audio processing.

- Data.
- Voice.

RSSI processing.
Transmitter.
Audio processing.

- Data.
- Voice.

Modulator.
Multiplier.
Mixer.
Power amplifier.
Control.

- PTT.
- Power.

Frequency control
Synthesiser.
Local oscillator.
AFC
Interfaces
Modem section.
Antenna diplexer.
Audio handset.

### 2.2.1 RECEIVER

The general form of the receiver circuitry is shown in diagrams "DR9 Macro Block Diagram" (drawing number TC01-05-19 sheet 3/3), and "900 MHz Radio - Block Diagram" (drawing number TC01-05-19 sheet 2/3).

### 2.2.1.1 PRE-AMPLIFIER

The receiver pre-amplifier obtains signal direct from the antenna diplexer port connector X 2 . It consists of two stages. The first stage is optimised to give a low noise figure, while the second is optimised to produce gain.

The central devices used are MRF5711 high frequency transistors. They provide the basis for a wide band amplifier that can receive from the lowest band frequency range of 852 to 854 MHz to the higher band frequency range of 928 to 930 MHz .

The RF selectivity is provided by the diplexer filter.
Strip line impedance matching networks are employed to ensure optimum performance of the amplifier.

The overall gain of the pre-amplifier is set to 20 dB .

### 2.2.1.2 MIXER

The receiver mixer consists of a 180 "rat race hybrid ring" followed by a passive Schottky mixer diode.

The mixer injection frequency is set 45 MHz from the required receive frequency, (high side injection for 930 MHz receive and low side for 850 MHz receive). This results in an I.F. frequency output of 45 MHz .

The level of the injection is set to 6 dBm by the amplifier stage Q3.

### 2.2.1.3 FIRST I.F. STRIP FILTER

The required receiver mixer product is filtered by the first I.F. filter. The filter is a bandpass crystal controlled device, centred on 45 MHz , and provides image rejection for the second IF Mixer.

The filter is aligned for optimum response by adjustment of inductors $L 4, L 3$ and $L 5$.

### 2.2.1.4 FM IF and DEMODULATOR

The heart of the demodulator section is an NE615D high performance low power mixer FM IF system IC.

This device incorporates a mixer/oscillator, two limiting intermediate frequency amplifiers, a quadrature detector, muting circuitry, logarithmic RSSI, and a voltage regulator.

The input to the device is from the output of the 45 MHz first IF strip filter. This is applied at $R F_{\text {in }}$ and $R F_{\text {bypass }}$ pins (U2-p1,p2).

This signal is applied internally to a Gilbert cell mixer, which is set to convert the signal down to 455 kHz .

The mixer injection is supplied by an internal oscillator, which is driven by an external oscillating signal applied at the XTAL OSC pins (U2-p3,p4).

The basic injection frequency is governed by the 44.545 MHz crystal XTAL1. This produces a mixer output product of 455 kHz .

The output of the mixer is available at MIXER OUT (U1-p20). This is applied to a 455 kHz centred bandpass filter. This acts as the "front end" filter, CF1.

The bandwidth and rolloff characteristics of this filter are set, depending on the required baud rate of the data being used on the modem, and the required channel spacing. Refer to Circuit Diagram for filter types.

The filtered output is then applied to the input of the internal IF amplifier, IF AMPIN (U1-p18). The bandwidth of the amplifier is about 40 MHz , with a gain of about 39 dB(uv). C10 and C11 provide IF amplifier decoupling.

The output is available at IF AMP OUT (U1-p16). This is applied to a 455 kHz centered bandpass filter. This acts as the "rear end" filter, CF2.

Again the filter selection depends on the required bandwidth. Refer to Circuit Diagram for filter types.

The filtered output is then applied to the input of the internal IF limiter, LIMITER IN (U1-p14). The bandwidth of the limiter is about 28 MHz , with a gain of about $62 \mathrm{~dB}(\mathrm{uv})$. C13 and C14 provide IF limiter decoupling.

The signal from the second limiting amplifier is passed to an internal Gilbert cell quadrature detector, as well as to LIMITER OUT (U1-p11).

One of the Gilbert cell ports is driven directly by the IF, the other by a tuned quadrature network, which is driven by the IF signal from LIMITER OUT. The tuned network is based around a ceramic resonator CF3. The Q of the network is varied depending on the required baud rate used by the modem. For 9600 baud the link LK3 is inserted, giving a higher damping factor than that required for 4800 baud, where the link is removed.

This gives the two input signals applied to the Gilbert cell a 90 degree phase relationship, the output of which is the demodulated audio/data signal.

The output signal is available at UNMUTED AUDIO OUT (U1-p9). A gated output is also available at MUTED AUDIO OUT (U1-p8).

### 2.2.1.5 AUDIO PROCESSING

### 2.2.1.5.1 DATA

The demodulated data signal output has been assigned to the UNMUTED AUDIO OUT pin (U1-p9). This ensures no interruption to the flow of data.

The signal is filtered by the C22, R20, R29 and C23 filter network. This is to remove any high frequency components produced at the output of the quadrature detector.

It is then amplified and DC level shifted by op-amp U1:C. The amount of DC bias applied to the signal can be varied by the potentiometer VR2. For correct processing by the modem, this level is set to 2 V . The AC level of the signal is set to about $1 \mathrm{~V}_{\mathrm{p} \text {-p }}$

### 2.2.1.5.2 AUDIO

The demodulated audio signal output has been assigned to the MUTED AUDIO OUT pin (U1-p8). This allows switching control of the audio passed to the handset earpiece.

The signal is filtered by R23 and C17. This is to remove any high frequency components produced at the output of the quadrature detector.

It is then buffered, amplified and level shifted by op-amp U1:D, and presented to the handset via coupling capacitor C20 and connector X3-p2.

The mute control signal is applied to the NE615 (FM IF system IC) MUTE IN pin (U2-p5). When active, the audio output signal from the IC is attenuated by greater than 60 dB .

### 2.2.1.6 RSSI

The RSSI output is presented by the NE615 at RSSI OUT (U2-p7). This signal is logarithmic with an output range greater than 90 dB . It is used for audio mute processing, and by the modem section as a data qualifier signal.

The signal is first passed through a unity gain buffer, op-amp $\cup 1$ : $B$, before it is split.
The RSSI level is compared with the setting of "audio mute adj" potentiometer VR1, by op-amp U1:A. The result is passed to the MUTE IN pin of the NE615.

This allows a suitable mute cutoff point to be set for the received audio sent to the handset earpiece.

The RSSI signal is also passed to the modem section for processing via R19 and connector X1-p21.

### 2.2.2 TRANSMITTER

The general form of the transmit circuitry is shown in diagrams "DR9 Macro Block Diagram" (drawing number TC01-05-19 sheet 3/3), and " 900 MHz Radio - Block Diagram" (drawing number TC01-05-19 sheet $2 / 3$ ).

### 2.2.2.1 AUDIO PROCESSING

### 2.2.2.1.1 DATA

The transmit data signal enters the radio section via connector J*3-p13, from the modem section. It is biased via R68 and R75 to a DC level of about 0.86 V . The signal is then passed through a level setting potentiometer VR2, used to set the level of transmit deviation.

It is then presented to the input of the modulator circuit.

### 2.2.2.1.2 VOICE

The transmit voice signal enters the radio section via connector $\times 3-\mathrm{p} 4$, from the microphone in the handset. The pre-amp in the microphone circuit is given some bias via R76.

The signal is first passed through a clipping circuit. This consists of back to back clamping diode pair D2, AC-coupled via C154. This ensures that a maximum transmit deviation level is imposed.

The modulator circuitry is based around a low power FM transmitter system IC,MC2833. Included in this device is a microphone amplifier and clipper. The audio is passed to the amplifier via R76 at the MIC AMP INPUT pin (U7-p5).

Feedback for gain is supplied by R76, and band limiting by C50. The amplifier output is presented at MIC AMP OUTPUT (U7-p4).

Further low pass filtering is provided by the network of R71, C49, R59.. and C42... C43 provides a rising response below 100 Hz . This filtering is needed to shape the base band signal, so as the transmit frequency spectrum stays within channel boundaries.

The audio is coupled into the modulator circuit at the MODULATOR INPUT pin of the MC2833 (U7-p3).

### 2.2.2.2 MODULATOR

The heart of the modulator section is an MC2833 low power FM transmitter system IC. This device is a one chip FM transmitter subsystem designed for FM communication equipment. It includes a microphone amplifier, a variable reactance modulator, a voltage controlled oscillator, and two auxiliary transistors.

Data is fed directly to the input of the reactance modulator at the MODULATOR INPUT pin (U7-p3). The audio channel is fed via an inbuilt clipper amplifier in the MC2833. The output of this variable reactance circuit is used to modulate the FM carrier.

The carrier frequency of the modulator is provided by an internal oscillator, which is driven by an external oscillating signal applied at the RF OSC pins (U7-p15,p16).

This oscillating signal is governed by the 20.166 MHz crystal XTAL3. The actual applied frequency is set by the modulating signal, which slightly varies ("pulls") the crystal frequency. This is achieved by connection of the crystals circuit to the output of the variable reactance circuit VARIABLE REACTANCE OUTPUT (U7-p1). This output is coupled to the crystal via a frequency trimming coil L6.

The output FM signal is presented at the RF OUTPUT pin (U7-p14).

### 2.2.2.3 MULTIPLIER

The output of the modulator is passed to a frequency tripler stage employing auxiliary transistor TR2. This places the carrier frequency at 60.5 MHz .

It then passes to a frequency doubler stage employing auxiliary transistor TR1, where the carrier is moved up to 121 MHz .

The signal is amplified through these stages to a level of about -4 dBm at 121 MHz .

### 2.2.2.4 MIXER

The transmit FM signal at 121 MHz when mixed with the VCO frequency by U 8 produces a transmitter signal 76 MHz from the receiver frequency.

The mixer employed is an MCL SBL-1X monolithic doubly balanced mixer (U8).
The transmit VCO signal is amplified to a level of about +6 dBm by Q 2 , and applied to the "L" input of the mixer. The 121 MHz signal is applied to the "I" input of the mixer.

To select the correct mixing product for the transmitter, a tunable filter using C78 and a coupled stripline circuit is used.

The output signal is then buffered by two MRF5711 transistors Q4 and Q5, to provide about +4 dBm of signal level, which is applied to the final amplifier section.

### 2.2.2.5 POWER AMPLIFIER

The power amplifier provides an overall gain of about 30 dB . This is achieved by three stages of amplification.

The first stage uses an MRF5711 transistor (Q8). This device is primarily designed for high gain, low-noise, small signal amplifiers, and is ideal for a transmitter pre amplifier. This stage provides about 13 dB of gain. The power control circuit acts on this stage to provide constant power at the PA. output connector.

The second stage uses an MRF8372 transistor (Q9). This device is primarily designed for wideband, large signal predriver stages, in the 800 MHz range. This provides a further 10 dB of gain.

The final stage uses two MRF8372 transistors (Q10, Q11) in a parallel configuration to provide the final output power. Each of these stages provides about 10 dB of gain. The output impedance is matched to 50 ohms via the use of balanced impedance strip lines.

The transmitted signal is presented at connector X 4 , at a level of about +32 dBm , where it is passed to the diplexer section.

### 2.2.2.6 CONTROL

### 2.2.2.6.1 PTT

PTT must be activated for the TC-900DR to transmit an RF signal. There are two sources of PTT, the audio handset, and the modem section.

PTT from the audio handset is referred to as "manual PTT". It enters the radio section via connector X3-p6. It is passed to the PTT control switch transistor Q12. PTT is active LOW, and turns on Q12 when applied.

PTT from the modem section enters the radio section via connector X1-p12, "/PTT". It is connected to the PTT control switch transistor Q12.

When PTT is not activated the transmitter is totally disabled. All stages of the transmit chain are turned off. This is to ensure that power consumption is kept to a minimum.

The PTT signal connects to the start of the transmit chain at the multiplier stage.
The internal transistors of the MC2833 IC, TR1 and TR2 have their bases effective grounded, turning off the devices. Similarly the mixer output buffer and amplifier transistors Q4 and Q5 are turned off as are the final amplifier stages employing Q8, Q9, Q11 and Q10.

When the PTT is activated, bias is applied to all these stages and transmission is possible.

Note : Tx enable must also be active to allow transmission.

### 2.2.2.6.2 TRANSMIT ENABLE

Transmit enable is a further control placed on the transmitter circuits. No transmission is possible unless the transmit enable signal is active. The signal enters the radio section via connector X1-p11, "ITX EN", from the modem section.

This signal basically enables the PTT switching transistor Q12, thus providing VCC for the 20.166 MHz oscillator section of the MC 2833 modulator IC , and bias to the handset microphone.

### 2.2.2.6.3 POWER

The RF power output of the TC-900DR can be set to two levels. Low power level is 200 mW , and high power is 1 W .

This level is controlled by two dc levels. One signal is a control level from the modem section, the other from an RF detector located at the output of the transmitter itself. These two signals are used in conjunction to hold the output power constant.

The signal from the modem section enters the radio section via connector $\mathrm{X} 1-\mathrm{p} 10$, "TXPWR". The signal is fed to an op-amp comparison circuit U9:A, via level setting potentiometer VR4.

The level is compared to that actually detected at the output of the transmitter, by the circuit based around diode D3. The comparator output is then used to bias the first stage of the P.A. section (Q8) of the transmitter, hence varying the transistor gain performance and ultimately the output RF power. This basic feedback network is required to keep the power at a constant level, regardless of any external conditions.

The detected output power level is also fed back to the modem section for monitoring and analysis via connector X1-p9, "TXPWR SENSE".

### 2.2.2.6.4 TEMPERATURE SENSE

A temperature sensing device is included in the radio section. The device used is an LM335 precision temperature sensor, U6. It is operated as a two terminal zener diode, with a breakdown voltage directly proportional to absolute temperature, with an output of +10 mV per degree kelvin.

The temperature data output is passed to the modem section for analysis and processing via connector X1-p14, "TEMP SENSE".

During the "Burn In" cycle, that the TC-900DR is passed through during production, the unit calibrates the output of the sensor to the test temperature. In particular it stores the hottest temperature reached by the test cycle (about 65C).

If the unit reaches this maximum temperature setting while operating in the field, the modem section of the TC-900DR will automatically signal the power control circuit to place the transmitter into low power mode $(200 \mathrm{~mW})$.

This low level of output power is retained until the temperature sensor signals the modem section, that the temperature has fallen back below the maximum temperature. When this occurs the transmitter is placed back to its previous power setting. A hysteresis is built into the microprocessor control circuitry to stop power jitter.

This scheme is referred to as "High Temperature Fold Back". It is used to protect the transmitter final power transistors from any damage that may be encountered under extreme temperature conditions.

### 2.2.3 FREQUENCY CONTROL

### 2.2.3.1 SYNTHESISER

The synthesiser section provides a local oscillator for use by the receiver and transmitter sections.

The synthesiser circuitry is based around a TBB206 PLL frequency synthesiser IC.
This device is a complex PLL circuit in CMOS technology for processor controlled frequency synthesis. The processor resides in the modem section, and three basic control lines are used to interface to the device. The enable "EN", data "DA" and clock "CL" control signals are passed to the TBB206 via connector X1-p16,p17,p18 respectively.

The reference frequency for the synthesiser is applied to the "RI" pin of the TBB206 (U3-p2). This reference is provided by a 12.000 MHz voltage adjustable temperature compensated crystal oscillator (VTCXO), XTAL2. This input has a sensitive preamplifier for a 16 -bit ( $R$ )eference divider. C33 provides AC coupling for the input.

The VCO frequency is applied to the "Fl" input pin of the TBB206 (U3-p8). This input has a highly sensitive preamplifier for a 12-bit $N$ divider and a 7 -bit A divider. C29 provides AC coupling for the input.

The actual signal applied to the "FI" input is from the output of a TBB202 dual modulus divider IC (U4-p4). This is to transform the actual VCO frequency of between 786 MHz and 996 MHz , down to a frequency acceptable for use by the "FI" input.

The divider ratio selected by the TBB202 is determined by the state of the "MOD" input pin (U4-p6). If the signal is HIGH, then a ratio of $1: 128$ is used. If the signal is LOW, a ratio of $1: 129$ is used. The state of this signal is controlled by the TBB206 synthesiser "MOD" output pin (U3-p7). The TBB206 drives this output LOW at the beginning of a cycle. When the A divider has reached its set value, the "MOD" output is set to HIGH. When the N divider reaches its set value, the output is set LOW again and the cycle is repeated.

The input to the TBB202 divider is from the VCO output via a strip line impedance matching network. The signal is applied to the "I1" pin (U44-p1).

The TBB202 can be placed into standby mode, when not in use. This is achieved by connection of the "STB" pin (U4-p7), to the multi function output port of the TBB206 synthesiser (U3-p6). This port is driven by the DFM4-9 modem IC located in the modem section.

The phase detector signal is provided on the "PD" pin of the TBB206 (U3-p12). This signal has especially short anti backlash pulses to avoid any "dead zones", and to neutralise any small phase deviations. This signal is passed to the loop filter of the VCO circuit.

A lock detect indication is given by the TBB206 synthesiser at the "LD" output pin (U3-p14). This signal is filtered and shaped by the network using R47 and C36, and presented to the modem section for monitoring and processing, via connector X1-p19.

### 2.2.3.2 VCO

The VCO used is an MQC309 series VCO. The exact device used depends on the required frequencies that the unit has to work with.

Two types are used :
A. MQC309 798 - Frequency range of 784 MHz to 816 MHz

Gives unit frequency ranges of :

- Transmit : 905 MHz to 937 MHz
- Receive : 829 MHz to 861 MHz
B. MQC309 978-Frequency range of 962 MHz to 994 MHz

Gives unit frequency ranges of :

- Transmit : 841 MHz to 873 MHz
- Receive : 917 MHz to 949 MHz

The 798 type employs low side injection to the mixers, whereas the 978 type employs high side injection.

The loop filter consists of R44, C40, C41 and R43.
The output of the VCO is passed to the receiver mixer via RXMIX, and to the transmitter mixer via TXMIX signal lines. Each of these is impedance matched by strip line circuits for optimum performance.

The layout and selection of all these components has been done in such a way so as to minimise VCO noise being impressed onto either the transmitted or received RF signals.

### 2.2.3.3 VCO TEMPERATURE COMPENSATION

Frequency temperature compensation is provided for by an input to the reference oscillator circuit.

During the "Burn In " cycle, that the TC-900DR is passed through during production, the unit calibrates the output of the temperature sensor to the test temperature and to any frequency variations that occur, and stores the results.

When the unit is operating in the field, the temperature of the unit is constantly being analysed. Should a frequency offset be required based on the calibration measurements, the modem section signals to the 12.000 MHz reference oscillator to vary its frequency slightly. This signal is passed to the radio section via connector X1-p15, "TEMP COMP". The voltage on this line "pulls" the reference oscillator XTAL2 onto a new frequency, which corresponds to the correct offset required.

Note : Because the temperature compensation for the installed VTCXO is held in the NVRAM of the modem it is imperative that modems and radio boards are maintained as matched pairs. Should either the VCO or NVRAM require replacement it is highly recommended that the unit be retumed to the manufacturer for re-calibration.

### 2.2.3.4 RECEIVER AFC

Automatic frequency control is provided for the received signal. The control signal is applied to the radio section from the modem section via connector X1-p22, "AFC CTL".

The basic injection frequency to the front end mixer of the NE615 FM demodulator IC (U2), is governed by the 44.545 MHz crystal XTAL1. The actual applied frequency can be set by the level of the AFC signal, which slightly varies ("pulls") the XTAL1 crystal frequency via the varactor diode DV1.

The modem section monitors the average DC level of the received signal (DATA signal X1-p13), which gives an indication of received frequency drift.

From this the modem section calculates the required compensation necessary and applies it to the "AFC CTL" signal line.

A reference signal is passed back to the modem section from the radio section via connector X1-p23, "AFC REF". This is processed by the modem section, and used to help determine the level of AFC signal level.

### 2.2.4 INTERFACES

### 2.2.4.1 MODEM SECTION

The radio section interfaces to the modem section via connector X 1 . Attached permanently to this connector is a 90 mm length of 26 way ribbon cable, fitted with a female 26 way connector at the other end. This attaches to connector JX3 on the modem section PCB.

Refer to interface diagram "RADIO MODEM INTERFACE", drawing number TC01-05-18 sheet 1/3.

CONNECTOR X1/JX3 SIGNAL DESCRIPTION PIN NUMBERS

| 1 | 13V8 POWER SUPPLY RAIL |  |
| :--- | :--- | :--- |
| 2 | 13V8 POWER SUPPLY RAIL |  |
| 3 | 13V8 POWER SUPPLY RAIL |  |
| 4 | GROUND |  |
| 5 | GROUND |  |
| 6 | GROUND |  |
| 7 | 8V POWER SUPPLY |  |
| 8 | 8V POWER SUPPLY |  |
| 9 | TXPWR SENSE | (o/p- TRANSMIT POWER SENSE) |
| 10 | TXPWR | (i/p-TRANSMIT POWER LEVEL) |
| 11 | ITX EN | (i/p-TRANSMIT ENABLE) |
| 12 | IPTT | (i/p-PRESS TO TALK) |
| 13 | DATA | (i/p-TRANSMIT DATA) |
| 14 | TEMP SENSE | (o/p-TEMPERATURE SENSOR) |
| 15 | TEMPCOMP | (i/p-TEMPERATURE COMPENSATION) |
| 16 | EN | (i/p-ENABLE FOR SYNTH) |
| 17 | DA | (i/p-DATA FOR SYNTH) |
| 18 | CK | (i/p-CLOCK FOR SYNTH) |
| 19 | LD | (o/p-LOCK DETECT FROM SYNTH) |
| 20 | DATA OUT | (o/p-RECEIVED DATA) |
| 21 | RSSI | (o/p-RSSI SIGNAL) |
| 22 | AFC CTL | (i/p-AFC CONTROL) |
| 23 |  | (UNUSED) |
| 24 | SUPPLY/MIC | (UNUSED) |
| 25 | TEST1 | (UNUSED) |
| 26 | TEST2 | (UNUSED) |

### 2.2.4.2 ANTENNA DIPLEXER

The interface between the radio section and the antenna diplexer section is via coaxial connectors X4 and X2, and low loss coaxial cables.

| CONNECTOR | SIGNAL DESCRIPTION |
| :--- | :--- |
| $X 4$ | TRANSMITTER OUTPUT |
| $X 2$ | RECEIVER INPUT |

### 2.2.4.3 AUDIO HANDSET

The interface between the radio section and the audio handset is via the modular- 6 pin connector X 3 .

CONNECTOR X3 PIN NUMBERS

2
3

4
5
6

## SIGNAL DESCRIPTION

8V POWER SUPPLY
AUDIO OUT ( $\mathrm{o} / \mathrm{p}$ - AUDIO TO EARPIECE)
GROUND
MIC (i/p - MICROPHONE AUDIO)
GROUND
MANUAL PTT (i/p - HANDSET PTT)

### 2.3 ANTENNA DIPLEXER SECTION

### 2.3.1 GENERAL

The antenna diplexer section of the TC-900DR is a separate plug in module, that "piggy backs" the radio section PCB.

The diplexer performs two major tasks. Firstly it couples both the transmit and receive RF paths to the antenna while providing high isolation between them, and secondly it provides image and spurious rejection for each of these paths, with high $Q$ bandpass filters.

The isolation between the transmit side and the receive side is greater than 50 dB .
The diplexer consists of two teflon PCB's bonded together using a critical temperature and pressure process. The top and bottom outer layers are connected via brass eyelets, that are pressed through the PCB. This eliminates the need for through hole plating of Teflon, which requires the use of dangerous chemicals.

The design is essentially two continuous ground planes, filled in between, with laminate dielectric, and stripline filter tracks which are centrally located between these ground planes.

The etching of the filter tracks is closely monitored and controlled to ensure an accuracy of better than $0.001^{\prime \prime}$ in track width and spacing.

The diplexer has been factory tested to ensure bandpass and performance characteristics are met. The diplexer has approximately 3 dB of loss at 930 MHz and 2 dB of loss at 850 MHz .

This diplexer requires no alignment in the field.

### 2.3.2 INTERFACES

The antenna diplexer connects to the radio section via low loss coaxial cables and connectors, and to the units antenna via a SMA connector.

Two versions of the diplexer are available, depending on the transmit and receive frequencies used. The difference between the two is the loading of the SMA connector.

TYPE-A CONNECTIONS (Transmit frequency $=930 \mathrm{MHz}$ range)

| DIPLEXER CONNECTOR |  |
| :--- | :--- |
| 850 MHz port |  |
| 930 MHz port | RF RECEIVE - RADIO SECTION X2 |
| ANT port | ANTENNA |

TYPE-B CONNECTIONS (Transmit frequency $=850 \mathrm{MHz}$ range)

DIPLEXER CONNECTOR
850 MHz port
930 MHz port
ANT port

SIGNAL DESCRIPTION AND DESTINATION RF TRANSMIT - RADIO SECTION X4

RF RECEIVE - RADIO SECTION X2
ANTENNA

### 2.4 AUDIO HANDSET SECTION

### 2.4.1 GENERAL

Refer to diagram "MTCU HANDSET MAIN PCB \& MIC PCB CIRCUIT DIAGRAM", drawing number 5015-A200-50.

The handset provides an audio link between units, to assist in link setup and commissioning. It is not intended for general use and the equipment is not licensed for voice operation only.

Caution : When the handset is inserted into the TC-900DR, reliable data transmission or reception is not possible. Unintentional voice traffic on a point to multi point system may cause data corruption to other units.

The data transmission section of the modem is totally disabled, if the handset is plugged in when the TC-900DR is turned on.

The handset contains two PCB's, a receive board and a microphone board, which are connected by a 10 way ribbon cable. Acoustic padding is also included in the handset for improved performance.

The microphone board contains an ECM30 electret microphone, along with a common emitter preamplifier stage (Q1), to provide transmit voice audio.

There are four indication LED's that are not used by the TC-900DR.
The receiver board contains a 78L05 5V voltage regulator (REG1). This is used to supply power to the LF353 receive amplifier (U2-p7), which drives a DH32-30 ohm earpiece.

The sidetone circuit provided by U2-p1 is disabled and not used by the TC-900DR. Similarly, the LED drivers are disabled.

The PTT switch places a ground connection onto its output signal line, for processing by the radio section.

### 2.4.2 INTERFACES

The audio handset connects directly to the radio section via the RJ11 connector, X3. Attached to the handset is an 8 way flexible curly cord.

| PIN NUMBER | HANDSET CONNECTOR | X3 PIN NUMBER | RADIO SECTION CONNECTOR X3 |
| :---: | :---: | :---: | :---: |
| 1 | LED CLK | - | UNUSED |
| 2 | LED DATA | - | UNUSED |
| 3 | 13V2 | 1 | 8V POWER SUPPLY |
| 4 | DGND | 3 | GROUND |
| 5 | PTT | 6 | MANUAL PTT |
| 6 | MIC | 4 | MIC |
| 7 | MIC RET | 5 | GROUND |
| 8 | EAR PHONE | 2 | AUDIO OUT |

### 2.5 MODEM SECTION

The modem section is built on a single PCB with approximate overall dimensions of $165 \mathrm{~mm} \times 152 \mathrm{~mm} \times 18 \mathrm{~mm}$.

It consists of the following main blocks
Modem control

- DFM4-9 modem.
- Reset and watchdog.
- Memory.
- External NVRAM.
- External RAM.

Host interface.
Radio interface.
Transmit signal conditioning.
Receive signal conditioning.

- Data recovery.
- Clock recovery.

User indications.
Power supply
Interfaces.

- Radio section.
- Port A.
- Port B.
- Power.


### 2.5.1 MODEM CONTROL

### 2.5.1.1 DFM4-9 MODEM

The modem section is controlled by a DFM4-9 Trio DataCom modem IC, (U5).
This device is specifically designed to provide data communications from a host computer over a radio channel.

The DFM4-9 is capable of full duplex operation, at data rates of 4800 baud or 9600 baud over the radio channel. The transmitter and receiver data rates may be set independently. The host computer interface provides two RS232 asynchronous serial ports, configurable for a variety of baud rates, and data formats.

In the standard delivery format of the modem, only one asynchronous serial port is operational. (Port A).

Advanced data recovery techniques are employed to ensure excellent performance in both good and noisy signal environments.

The data transmission method used, employs advanced optimal waveform shaping techniques. This maximises the recovered signal at the destination receiver, while remaining within the allocated RF channel bandwidths. The method uses computer generated Finite Impulse Response (FIR) techniques, to derive the transmitted waveform data.

The modem features a unique supervisory signalling channel, which embeds low speed data in the primary bit-stream, and is transparent to the user of the primary channel.

To drive the DFM4-9 modem clocking circuits, an external resonator is required. A 19.6608 MHz crystal (XTAL1) is applied to the OSC pins (U5-p9,10) of the device to achieve this.

A 4 way DIP switch is supplied to set up some configuration parameters of the modem. These are only read by the DFM4-9 at device power up. They connect to the "ESx" pins of the device (U5-p3, p5, p6,p7). Switches 1 and 2 are presently unused, switches 3 and 4 are defined in section 4.5.1.

### 2.5.1.2 RESET AND WATCHDOG

A MAX690 reset and watchdog IC (U3), is used to perform a variety of ancillary functions. This device provides a fixed length reset pulse for the proper initialisation of the modem chip on power up and reinitialisation. The MAX690 monitors the level of the VCC power supply line. If the voltage moves out of specification, the reset output is activated. This ensures that the modem chip recovers correctly in the event of a power failure. The reset signal is applied to the "RESET" pin of the modem (U5-p8).

The MAX690 provides a power monitoring function, which gives advance warning of imminent power supply failure. The DFM4-9 modem checks this signal, applied to its "PF" pin (U5-p2), before performing any transactions with the non-volatile memory, thus preventing accidental corruption of the contents of this memory. This "advance warning", is the length of time that the power supply capacitors hold their charge, after loss of power, before the Vcc supply rail drops below its cutoff level, and a reset pulse is generated.

The MAX690 also includes a "watchdog" timer. This timer must be strobed at a minimum rate, to prevent a reset pulse being generated. The DFM4-9 provides this signal at its "WDO" pin (U5-p22). Should the DFM4-9 modem operation go astray for some reason, it is probable that it will no longer perform this strobing function correctly. This condition is treated as irrecoverable and the MAX690 will timeout on its watchdog function and re-initialise the modem.

### 2.5.1.3 MEMORY

### 2.5.1.3.1 EXTERNAL NVRAM

The DFM4-9 modem, has a wide variety of configurable operating parameters, all of which are stored in an ST24C04 NVRAM IC, (U4). These parameters are read at power up, and determine the operating characteristics of the modem.

The NVRAM has 4096 bits of memory. It is accessed using the standard $I^{2} \mathrm{C}$, two wire, bus interface. A feature of this particular device, is a write protect function for one area of the memory.

This write protect feature prevents configuration data being inadvertently corrupted should some anomaly in modem operation occur. A hardware signal line is used to override this write protection feature, so that the configuration data may be changed by manual means. This signal can be accessed via the front panel connector, and is used when the TC-DFM9IP modem programmer is connected.

### 2.5.1.3.2 EXTERNAL RAM

External RAM is used to store data frames.
The RAM used may be either a $6264-8 \mathrm{~K}$ or $62256-32 \mathrm{~K}$ byte IC (U9). The standard TC-900DR is supplied with an 8K package. The DFM4-9 modem, tests the size of the attached RAM on power up.

All of the externally connected RAM is used to store packet data, and is allocated evenly between transmit and receive data. This memory is connected to the modem chip, by an 8 bit bus, and 3 control lines.

Two 8 bit 74HC573 latches (U8 and U10), are used to latch the memory address off the bus, before the data read or write cycle. The read/write control line to the RAM, is passed as the top address line in the MSB address latch.

The RAM read cycle operates as follows :

- The modem sets the two latch control lines, LADR_EN and HADR_EN, high.
- The high-address/R_select is then placed on the 8 bit bus.
- The HADR_EN line is set low to latch the data into U8.
- The lower eight address bits are placed on the bus.
- The LADR_EN line is set to low to latch the data into U10.
- The modem bus port is set to input mode.
- The RAM CE line is set low.
- The modem reads the data off the bus.

The RAM write cycle operates as follows:

- The modem sets the two latch control lines LADR_EN and HADR_EN, high.
- The high-address $/ W_{-}$select is then placed on the 8 bit bus.
- The HADR_EN line is set low to latch the data into U8.
- The lower eight address bits are placed on the bus.
- The LADR_EN line is set to low to latch the data into U10.
- The modem bus port is set to output mode.
- The modem writes the data to the bus.
- The RAM CE line is set low to write the data into the RAM.


## Note: WARNING

A modem containing a $32 K$ RAM package will not be compatible with a modem containing an 8K RAM package if end to end flow control is being used over the data link.

### 2.5.2 HOST INTERFACE

The host interface is provided by two RS232 ports, configured as DCE. These ports are presented to the user as 9 way female DMIN connectors, designated as PORT A and PORT B.

With the standard TC-900DR, only PORT A is operational.
The RS232 level translation is performed by two LT1081/MAX232 line transceivers (U1 and U2). These require a single five volt supply, and include internal charge pumps to generator the required +10 V and -10 V rails.

The four input and four output lines implement one full duplex serial port with RTS/CTS/DTR and DCD. This is PORT A. A second full duplex port with no handshake lines is provided on PORT B.

### 2.5.3 RADIO INTERFACE

The interface to the radio is via a 26 pin PCB header connector, X 4 .
The modem section has full control over the connected radio transceiver. It provides:

- Four lines for synthesiser control (used for RF channel selection).
- RSSI detection.
- Temperature sense input.
- Transmit power sense input.
- Temperature compensation for the synthesiser reference frequency.
- Receiver AFC.
- PTT control.
- Analogue lines for receive and transmit data signals.
- Regulated +13.8 V and +8 V power supplies.

Input to the receiver signal port, RXSIG, is offset by 2.0 V DC, with a signal level of $1 \mathrm{Vp}-\mathrm{p}$ AC.

The transmit signal output, TXSIG, has a signal level of $1 \mathrm{Vp}-\mathrm{p}$ for 4800 BPS , and $2 \mathrm{Vp}-\mathrm{p}$ for 9600 BPS , with a nominal DC offset of 2.0 V . This offset may vary by $\pm 1 \mathrm{v}$ according to the modulator temperature compensation requirements.

An ADC0834 four channel ADC (U6), is used to monitor various analogue quantities within the radio. The DFM4-9 modem communicates with the ADC by controlling 3 lines. An active high chip select, "ADCS" line (U5-p33), a data clock, "DCLK" line (U5-p35), and a serial data, "SD" line (U5-p36).

The state of the data line from the ADC is clocked into internal registers of the DFM4-9 on the rising edge of the clock line. The data stream consists of a four bit preamble, which includes the channel address. From the 5th clock pulse onward, the ADC drives the data line with the data of the conversion, MSB first. The transaction is terminated with the CS line being set to inactive low.

The first channel is used to monitor temperature, by measuring the voltage from an LM335 monolithic temperature sensor U6. The LM335 is situated in the radio section, adjacent to the 20.1666 MHz XTAL and VCXO synthesiser reference oscillator, and is fed into the modem section via connector X4-p14, ADC0.

The second channel is used to monitor RSSI, by measuring the RSSI output of the NE615 IF circuit. This signal is fed to the modem section from the radio section via connector X4-p21, ADC1.

The third channel is used to monitor the power level output by the RF transmitter, by measuring a voltage derived in the power control section of the radio. This is used to determine the "health" of the radio transmitter. This signal is fed to the modem section from the radio section via connector X4-p9, ADC2.

The fourth channel of the ADC, is used to measure the voltage of the +13.8 volt supply rail and to sense the presence of the audio handset at power up. The handset derives microphone bias from the modulator stage, and the voltage at this point is measured and compared with a fixed nominal value, to determine if the handset is connected at the time of TC-900DR power up. This signal is fed to the modem section from the radio section via connector X4-p24, ADC3. This 4th ADC channel is also multiplexed to measure the AFC control voltage so that an indication of received signal frequency can be made. U14:D is used to perform this switching function.

An auxiliary latch (U11) is provided to supply some of the output control to the radio section.

The latch receives data from the same data buss as the RAM. The lower six bits are fed to an R/2R ladder network DAC (RN2), which is used to present an analogue voltage to the radio's local oscillator synthesiser frequency reference. This correction voltage provides for excellent temperature stability of the radio. This signal is fed to the radio section via connector X4-p15, TEMP COMP.

The two top bits of the latch, drive auxiliary functions within the radio section.
Bit 6 is used to control the power of the RF transmitter in the radio section. This can be set to a HIGH level of 1 W , or to a LOW level of 200 mW . This signal is fed to the radio section via connector $\times 4-\mathrm{p} 10$, TXPWR.

Bit 7 provides the RF transmitter enable signal to the radio section. No RF signal can be transmitted unless this signal is set to active. This signal is fed to the radio section via connector X4-p11, TX EN.

### 2.5.4 TRANSMIT SIGNAL CONDITIONING

The transmit section of the DFM4-9 modem, outputs a byte of data, four times per bit period, on the "TDx" pins (TD1..TD7, U5-p56..49).

The parallel data is presented to an eight bit R/2R ladder network (RN1). This is a simple DAC which produces the transmit waveform at its output.

This signal is fed into opamp (U13:C) for amplification and filtering. This stage is a single pole low pass filter, used to attenuate clocking noise in the waveform. Two more filter stages follow, U13:B and U13:D.

By using 4 samples per bit, and an 8 bit resolution, precise control of the waveform shape is possible.

The gain and pole frequency of amplifier stage U13:C is switched by the DFM4-9 modem, via a 74 HC 4066 CMOS FET switches (U14:A). This is to produce the required waveform for the two data rates currently available. The bit rate output signal, "BRO" is provided at U5-p44.

For 4800 baud, components C43 and R45, are "included" in the feedback loop of the amplifier stage. When 9600 baud is selected, switch U14:A is turned OFF, and the components are "excluded" from the circuit.

### 2.5.5 RECEIVE SIGNAL CONDITIONING

The data receiver, consists of several functional blocks. Some of these are implemented by internal functions of the modem IC, and the remainder by external circuitry.

The incoming analogue signal, is routed to two separate sections of circuitry. One to process the received clock, the other to process the received data.

### 2.5.5.1 DATA RECOVERY

The data recovery is based around an "Integrating Data Slicer" circuit.
This circuit consists of a non-inverting, resetable integrator (U16:A, U12:C and U15:D), a dual peak detector ( $\mathrm{U} 12: \mathrm{A}, \mathrm{B}$ ) and a reference divider.

The received signal is passed into the modem section from the radio section via connector X4-p20, "RXSIG".

The signal is integrated by the non-inverting integrator formed by U16:A, and U12:C, and then forwarded on to a comparator ( $U 7: B$ ), where it is "squared up", ready to be read by the DFM4-9 modem.

An output signal is provided by the modem IC, to indicate the sampling point. In fact this signal, called "RxCLKOUT", is pulsed high immediately after the sampling operation has taken place.

The integrator is reset at the end of each bit period, by the 74 HC 4066 FET switch, U15:D, after the value of the bit has been read. The DFM4-9 provides this reset signal at the reset integrator "RxCLKOUT" pin (U5-p19).

The integrated receive signal, is then fed to the dual peak detector, where the positive and negative peaks of the integrated signal are detected, and stored on the capacitors C28 and C27.

The peak detector's attack time is determined by the output resistance of the opamps (U12:A,B) and the bulk resistance of the diodes (D7, D4). The decay time however is determined by the values of the hold capacitors (C28, C27) and the summing resistors (R24, R25).

Four diodes (D5, D6, D8, D9) are used to clamp the reference rail. If the incoming signal has a large DC shift, this clamping arrangement ensures that the data slicer reference level is quick to settle somewhere near its final operating point. This clamp however does impose a maximum allowable input signal level. Exceeding this level will cause the integrated signal to directly modulate the reference rail. The derived reference voltage level, is amplified and output back to the radio section, where it is used for AFC in the receiver.

### 2.5.5.2 CLOCK RECOVERY

The received clock signal is presented to the DFM4-9 modem at its "RXCLK" input (U5-p4).

Within the DFM4-9, a phase-locked-loop is used for data clock recovery, which relies on level transitions in the data signal.

This mechanism maintains the data sampling point in the center of the bit cells by comparing the signal's level transitions with an internal clock.

An error in the relative phase of the RXCLK signal and the internal clock, causes the internal clock to increase or decrease in speed, to bring the phase error to zero.

The phase-locked-loop clock recovery mechanism within the DFM4-9 modem, maintains the sampling point in the center of the bit cells, but the use of the integrator demands that this take place at the end of the bit cell. This means that the signal fed to the DFM4-9 modem RXCLK input must be delayed by half a bit period.

To obtain this, the received signal is passed through a half bit delay, low-pass filter (U16:D, U12:D, U7:A). The delay characteristics of this filter, are switchable between the available data rates of 4800 and 9600 baud operation, by five 74 HC 4066 FET switches. These switches are controlled by the "BRO" output of the DFM4-9.

### 2.5.6 USER INDICATIONS

There are four indication LED's supplied for user information. POWER, TXMIT, SYNC and RXSIG. The POWER LED is green, TXMIT LED is red and the other two are yellow.

The POWER LED (LED4), is driven from the $13 V 8$ power supply line. When supply is present the LED is activated.

The TXMIT LED (LED3), is activated when PTT is present. It is driven when the switching transistor Q3 is turned ON by the DFM4-9 modem "PTT" output going active (UX3-p38).

The SYNC LED (LED2), is activated when a valid data stream has been detected. It is driven when the switching transistor Q2 is turned ON by the DFM4-9 modem "SYNC" output going active (U5-p43).

The RXSIG LED (LED1), is activated when the received signal level is at a usable level. It is driven when the switching transistor Q1 is turned ON by the DFM4-9 modem "RXSIG" output going active (U5-p43).

### 2.5.7 POWER SUPPLY

The power supply is based around the use of three voltage regulators that supply +13 V 8 , +8 V and +5 V .

The incoming power is applied to a bridge rectifier (BR1),. Normally two legs of this bridge are linked out, so it provides only reverse polarity protection shunt diodes. A special manufacturing option allows for AC input, where the links are removed. A 2200 uF electrolytic capacitor (C2), provides filtering for $A C$ inputs.

This is then applied to an LT1086 low dropout regulator (REG1). The output of this is set to 13 V 8 and feeds the RF final amplifier, and the following two regulators.

The 8 V regulator (REG2) takes it's input directly from the 13 V 8 rail, its output is routed to the radio section, and provides supply for one of the amplifier devices.

The 5 V regulator (REG3) provides the supply rail for the modem section logic circuits. It takes it's input from the 13 V 8 rail via diode D1. Extra filtering capacitance is provided by C7.

### 2.5.8 INTERFACES

### 2.5.8.1 RADIO SECTION

The modem section interfaces to the radio section via connector JX3. The physical link between the two sections is achieved via a 90 mm length of 26 way ribbon cable.

Refer to interface diagram "RADIO MODEM INTERFACE", drawing number TC01-05-18 sheet $1 / 3$.

CONNECTOR JX3 SIGNAL DESCRIPTION
PIN NUMBER

| 1 | 13V8 POWER SUPPLY RAIL |  |
| :---: | :--- | :--- |
| 2 | 13V8 POWER SUPPLY RAIL |  |
| 3 | 13V8 POWER SUPPLY RAIL |  |
| 4 | GROUND |  |
| 5 | GROUND |  |
| 6 | GROUND |  |
| 7 | 8V POWER SUPPLY |  |
| 8 | 8V POWER SUPPLY |  |
| 9 | ADC2 | (i/p - TRANSMIT POWER SENSE) |
| 10 | TXPWR | (o/p - TRANSMIT POWER LEVEL) |
| 11 | TX EN | (o/p - TRANSMIT ENABLE) |
| 12 | IPTT OUT | (o/p - PRESS TO TALK) |
| 13 | TXSIG | (o/p - TRANSMIT DATA) |
| 14 | ADC0 | (i/p-TEMPERATURE SENSOR) |
| 15 | TEMPCOMP | (o/p- TEMPERATURE COMPENSATION) |
| 16 | EN | (o/p - ENABLE FOR SYNTH) |
| 17 | DA | (o/p - DATA FOR SYNTH) |
| 18 | CK | (o/p - CLOCK FOR SYNTH) |
| 19 | LD | (i/p-LOCK DETECT FROM SYNTH) |
| 20 | RXSIG | (i/p - RECEIVED DATA) |
| 21 | ADC1 | (i/p -RSSI SIGNAL) |
| 22 | AFC CTL | (o/p-AFC CONTROL) |
| 23 | SPARE | (UNUSED) |
| 24 | ADC3 | (FOR SUPPLY/HANDSET) |
| 25 | TEST1 | (UNUSED) |
| 26 | TEST2 | (UNUSED) |

### 2.5.8.2 PORT A

The modem section interfaces to the host user via the 9 way female DMIN type connector JX1.

CONNECTOR JX1 SIGNAL DESCRIPTION
PIN NUMBER

| 1 | DATA CARRIER DETECT | (DCD) |
| :--- | :--- | :--- |
| 2 | RECEIVE DATA OUTPUT | (RXD) |
| 3 | TRANSMIT DATA IN | (TXD) |
| 4 | DATA TERMINAL READY | (DTR) |
| 5 | COMMON | (COM) |
| 6 | DATA SET READY/prog mode | (DSR) |
| 7 | REQUEST TO SEND | (RTS) |
| 8 | CLEAR TO SEND | (CTS) |
| 9 | RING INDICATE/BER Test Mode | (RI) |

Note: Pin 6 and pin 9 provide a dual function which depends on the mode that the TC-900DR is operating in.

### 2.5.8.3 PORT B

For the standard delivery version of the TC-900DR, port B is normally not enabled. This port provides no handshake lines except DCD (parallel connected with DCD on Port A) and DSR which is wired active.

CONNECTOR JX1 SIGNAL DESCRIPTION
PIN NUMBER

| 1 | DATA CARRIER DETECT | (DCD) |
| :--- | :--- | :--- |
| 2 | RECEIVE DATA OUTPUT | (RXD) |
| 3 | TRANSMIT DATA IN | (TXD) |
| 4 |  |  |
| 5 | COMMON | (COM) |
| 6 | DATA SET READY/prog mode | (DSR) |
| 7 |  |  |
| 8 |  |  |
| 9 | RECEIVE SIGNAL STRENGTH INDICATOR | (RSSI) |

Pin 9 is used to output the RSSI signal for external measurement.
The RSSI output ranges from 0 to 5 Volts, where 5 volts indicates the strongest signal. It is important to note that this port output has a high impedance of around 50 K ohms and loading will decrease accuracy of the recorded measurement.

### 2.5.8.4 POWER

Power is supplied to the modem section via connector X 1 . Typically +13.8 V DC is applied to the top pin, with the common connected to the bottom pin.

## SECTION 3

## OPERATIONAL DESCRIPTION

## 3 OPERATIONAL DESCRIPTION

### 3.1 GENERAL

The Trio DataCom TC-900DR radio modem, is a full duplex 4800/9600 bits per second device, which converts digital data into an analogue form suitable for transmission over a radio channel. It uses specially filtered direct binary frequency modulation techniques to achieve this. It conversely, converts the analogue signal derived from a radio channel into a digital data signal.

The heart of the unit is the DFM4-9 modem IC. This performs all waveform shaping, randomising and de-randomising, NRZ/NRZI conversion, clock recovery, and HDLC framing and CRC error generation and checking. These functions are performed simultaneously, allowing full duplex operation at up to 9600 bps .

The modem is fully HDLC compatible. The user is provided with two RS232 compatible ports, which may each be configured with a standard PAD interface or SLIP/KISS protocol driver. The unit may also be configured for repeater operation.

It may be configured to use RS232 handshake lines, or XON/XOFF flow control on Port A.

The modem features a unique supervisory signalling channel, which embeds low speed data in the primary bit-stream, and is transparent to the user of the primary channel.

The supervisory signalling channel can be disabled if not required. It could be used to pass low speed data such as E and M status or C/DSMA control schemes.

The data rate of the supervisory signalling channel can be set independently for transmit and receive. It can range from about 40 to 533 bps with the primary channel rate at 4800 baud, and 80 to 1067 bps at a primary channel rate of 9600 baud.

NOTE: with the supervisory signalling channel active, the bit-stream is not compatible with standard HDLC interface devices (such as 8530).

The host user port may be configured for baud rates of 300 to 19 K 2 , with 7 or 8 bit character size, 1 or 2 stop bits, and parity off/odd/even.

The DFM4-9 modem includes several data tables which are used to generate waveforms with different characteristics. This is primarily for optimum performance at differing baud rates. A custom data table can be placed into the NVRAM of the modem, for specialised applications.

Configuration of the modem is fully programmable, with parameters held in non-volatile memory. All configuration parameters are accessible with the TC-DFM9IP Installation Program.

Configuration parameters include but are not limited to:
Supervisory Signalling Channel rate. XON/XOFF or RTS/CTS/DTR/DCD handshake mode. Default transmitter lead in delay. Constant specifying minimum RF RSSI for valid receive. Constant specifying minimum Tx power level.
Asynchronous serial port parameters.
User interface operating mode :

- User port interface protocol
- PAD Parameters


### 3.2 TC-900DR MODEM FIRMWARE REVISION VA2.3.0

### 3.2.1 FUNCTIONAL CHANGES AND ADDITIONS

The Diagnostics " M " command (serial port Mode) completed. The implementation of this command was not finished in time for VA2.2 release. This command is used to configure either of the two user ports, for character length, number of stop bits, parity odd/even/off.

1 Bit 7 is used to address which port is being referenced (set to " 0 " for Port $B$, or set to "1" for Port A).

2 Bit 6 determines the character size. Set to " 0 " for 8 bit, or "1" for 7 bit character size.

3 Bit 5 is set to "1" to enable parity, " 0 " to disable parity.
4 Bit 4 determines Odd (set bit to "1"), or Even (set bit to " 0 ") parity if Bit 5 is set.
5 Bit 3 determines the number of stop bits. Set to " 0 " for 1 stop bit, or set to " 1 " for 2 stop bits.

6 Bits 2, 1, and 0 are used to select the baud rate. The following table shows the available rates. The 19.2 K baud selection should only be made for Port A if Port $B$ is disabled. The last selection of 110 baud may be deleted from future firmware revisions.

| Bit | Bit 1 | Bit 0 | Baud Rate |
| :---: | :---: | :---: | ---: | ---: |
| 0 | 0 | 0 | 300 |
| 0 | 0 | 1 | 600 |
| 0 | 1 | 0 | 1,200 |
| 0 | 1 | 1 | 2,400 |
| 1 | 0 | 0 | 4,800 |
| 1 | 0 | 1 | 9,600 |
| 1 | 1 | 0 | 19,200 |
| 1 | 1 | 1 | 110 |

Channel Access Strategy 3 is now defined. This is selected by setting bits 1 and 0 ( TxCtrl 1 and TxCtr 10 ) in "Config1", both to " 1 ". This mode forces a randomly generated delay before transmission begins, even if the channel is perceived to be clear. This delay mechanism is similar to that used in Channel Access Strategy 2 when the channel is perceived to be busy. This operating mode is useful in systems that include remote terminals that generate reports at regular fixed intervals. In such a system, slight differences in this interval between two remotes, would cause them to become synchronised for some time, and thus transmissions from them would consistently
collide. Inserting a randomly generated delay before all transmissions will reduce the incidence of this effect.

The RS232 DCD handshake line now becomes active only during output of received data. Formerly, the DCD line indicated real time SYNC status of the modem data receiver. To facilitate the use of RS232 to RS422/RS485 converters, the DCD line is driven active a short time (approximately 0.5 mS ) before the received data is output to the user port, and lingers for approximately 2 to 3 character times (i.e. is proportional to baud rate of user port). The modem generates only one DCD function, which is available on pin 1 of both Port $A$ and Port B. Thus the DCD pin of both user ports will be activated when either port is outputting received data.

### 3.2.2 OTHER ENHANCEMENTS

Improvements in handling of the RS232 RTS line (Port A), makes the modem more tolerant in the timing of rapid OFF transitions of this handshake line, immediately after the end of the last character of a message. It has been observed that communications drivers in many PLCs turn their RTS output line OFF very shortly after the end of a message, resulting in the loss of the last character of the message with previous modem firmware revisions. This revision does not suffer this problem.

The random number generator used for the Channel Access Timer, has been improved to make it more random.

### 3.3 FACILITIES AND CONFIGURATION INFORMATION FIRMWARE VERSION 2.2

### 3.3.1 GENERAL

The TC-900DR provides fully transparent remote diagnostics facilities, and expanded data stream switching, which supports advanced stream trunking applications.

The diagnostics core, supports the reporting of current analogue conditions, including temperature, RSSI (Received Signal Strength Indication), RF transmitter power, AFC (i.e. received signal frequency offset), and supply voltage. Also, an extensive range of operating parameters may be changed remotely, including remote (RF) channel change.

Configuration options, allow various system topology's, so that the location of the system's diagnostics controller is flexible.

The data stream switching mechanism has been upgraded to allow either MUXIDeMUXing or multi-stream routing functions, independently for each port.

A few other minor upgrades to previous revisions of firmware are:

* Two different "ticker clocks" implemented, one running at 1 mS , and used for a) PAD Character Input Timers, and b) Channel Access Timer when running in Collision Avoidance mode. The other "ticker clock" runs at 10 mS , and is used for the PTT timer, and a host of other internal functions, not accessible by configuration programming
* When XON/XOFF flow control is enabled on PortA, the CTS output line continues to operate correctly, indicating the flow control state. XON/XOFF characters are generated in addition to, and reflect state changes on this line. As before, the DTR input line is ignored while XON/XOFF flow control is set, and the RTS line is not required to be true to validate transmit data.
* The modem stores data for transmission in buffer memory, which is limited. It also keeps track of frame boundaries of the stored data, and the number of frames it can manage is also limited by the amount of memory used to record the position of the frame boundaries. Thus it is possible that the modem can approach overflow before exhausting data buffer space, if frames are small. This flow control state is activated when the "frame boundary memory" approaches half full, for similar reasons used in data buffer management.
* If the Supervisory Signalling Channel is enabled in both transmit and receive directions, and PortA is configured in Repeater Mode, then the received Supervisory Signalling Channel data is also repeated, by being copied from the Supervisory Signalling Channel receiver to the Supervisory Signalling Channel transmitter.
* RSSI measurements are full eight bit conversion, so the "min_RSSI" configuration parameter lies in the range 0-255 (decimal). This is only important when setting this parameter without the aid of the DRPROG programmer.


### 3.3.2 INTERNAL DATA STREAM ROUTING

Essentially, all data streams travelling in both directions (transmit and receive), are examined and tested for a match with the diagnostics receive SID header code. If this match test is successful, then the data frame is copied into a buffer for the diagnostics core to process. The data frame also continues in the original direction as well. Thus diagnostics frames received from the radio channel (receive data), and from the stream switcher (transmit data, from one of the physical ports), are copied as they pass between the HDLC "device" and the data stream "switcher". Messages generated by the diagnostics core in response to received commands, are always sent back to the source of the command. That is, if a status request is received from the radio channel side of the modem, then the response is directed back out of the radio channel.

This dual access structure, allows the diagnostics controller to be located on either side of the modem, and thus supports any system topology.

### 3.3.3 DIAGNOSTICS REPEAT FUNCTION

Some applications will require that the "base" unit in a point to multi-point system repeats diagnostics frames. This will be the case where the system diagnostics controller is attached to a remote terminal in the system, and polls the system population from this point. The "base" unit must re-transmit diagnostics frames which are not addressed to itself. $A$ "diagnostics repeat" configuration bit enables this function.

### 3.3.4 DIAGNOSTICS FRAME STRUCTURE

Diagnostics data frames, are structured according to a defined protocol. A frame consists 1 st of the SID header code, which would normally (but not necessarily) be 00 . Following this is a three byte address of the destination unit, followed by a three byte source address. An addressed unit responding to a diagnostics command, will swap these two address fields around, in the response frame. The destination address in a diagnostics frame to a TC-900DR unit, is in fact the unique (factory) serial number of the unit. By convention, the diagnostics controller (a DOS based PC), will use a unique address for itself, outside the range of permissible TC-900DR addresses (e.g. 000000). Following the two address fields, is a single character command/response code, which is in turn followed by any operands that may or may not be required for the command/response. Total frame size is limited to 17 bytes. After the SID header, address fields, and command/response mnemonic, this allows up to nine bytes of data to be transferred per diagnostics frame.

### 3.3.5 DIAGNOSTICS COMMAND SET

The following is a list of the command set recognised by the diagnostics core in the TC-900DR Firmware. Also is tabulated the response to each command. The following examples use address 123456 for the TC-900DR unit address, and 000000 for the address of the system diagnostics controller. For the purposes of clarity only, each byte in the example messages is separated by a comma. Mnemonics are represented in quoted form to indicate an ASCll character (e.g. "C" is actually binary byte h'43).

## B Warm Boot Command.

This command forces the addressed unit to perform a "warm boot". Previous to this, the unit will have been halted (see " H " command), and one or more parameters changed with "P" and "W" commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " B "$
Response:- $\quad 00,00,00,12,34,56, " b "$

## C Calibration Constant Poll.

This command requests the addressed unit to reply with it's internal Analogue To Digital Converter (ADC) calibration constants. These are necessary to accurately interpret the data sent in Status Poll ("S") replies. This command has no operands, and the response mnemonic is " $c$ ". The form of the command and reply is:

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " C "$
Response:- $\quad 00,00,00,12,34,56, " c ", t t, r r, p p, f f, s s$
Where:-
$\mathrm{tt}=$ Temperature calibration code
$r r=$ RSSI calibration code
$\mathrm{pp}=$ Transmit Power calibration code
$\mathrm{ff}=$ Received Frequency Offset calibration code
ss $=$ Power Supply calibration code

## D Powered Up Response

This command is sent from the modem to the controller in response to a status poll ("S") immediately after the modem has been powered up. The modem will continue to send this command in response to a status poll until the controller acknowledges the command with a " $d$ ". The modem will then respond normally to a status poll.

This mechanism is used by the controller to determine whether it requires calibration data from the modem.

Syntax:-
Command:- 00,00,00,12,34,56"D"
Response:- $\quad 12,34,56,00,00,00 " d "$

## F Set New RF Synthesiser Frequency.

This command forces the unit to set the RF synthesiser to a new frequency, thus selecting another radio channel. This command has one operand, which defines the source of the synthesiser data. A value of zero, indicates that the frequency data has already been set with a parameter set command. Values from one to four select one of the channels stored in the NVRAM of the modem configuration. The addressed unit responds with an " $f$ " reply, before executing the channel change command (i.e. on the old channel).

Syntax:-
Command:- $\quad 12,34,56,00,00,00$, "F",nn
Response:- 00,00,00,12,34,56,"f"
Where:-
$\mathrm{nn}=00$ to 04 to select data source .

## H Halt Command.

This command forces the addressed unit to halt all internal operations, except diagnostics processing. This is necessary, when changing some parameters, before a warm boot command is issued to the re-configured unit.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " \mathrm{H"}$
Response:- $\quad 00,00,00,12,34,56, " h "$

This command forces the addressed unit to change the operating mode of one or both serial ports. Parameters such as character size, number of stop bits, parity etc. are changed with this command. It should be noted, that data may be lost while the operating mode of the serial ports is changed.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " M ", x x$
Response:- $\quad 00,00,00,12,34,56, " m "$
Where:-
$\mathrm{xx}=$ Serial port address bit and mode data

## P Parameter Set command

This command stores the contents of the operand string to a storage buffer. No other action is taken. This command should be immediately followed by a "W" command. See "W" command below. The parameter may be either a bit quantity, a byte quantity, a word quantity, or a string quantity. The diagnostics core in the modem firmware determines this from the parameter indentifier, which indexes an internal lookup table. String quantities are of indefinite length, and determined by the length of the operand string in the received "P" command. The "P" command response ("p"), echoes the complete received string. This is unique to the " P " and " W " commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " P ", n n, a a, b b, c c, \ldots$
Response:- $\quad 00,00,00,12,34,56, " p ", n n, a a, b b, c c, \ldots$
Where:-
$\mathrm{nn}=$ parameter identifier
$a a, b b, c c, \ldots$ are data value(s) for selected parameter

## R Parameter Readback command.

This command forces the addressed unit to read the state of the addressed parameter, and send this data back the the command originator (diagnostics controller) in a reply message. Again the size of the parameter (bit, byte, word, or string) is determined by the parameter identifier. String parameters are returned as a string of eight consecutive bytes.

Syntax:-
Command:- $\quad 12,34,56,00,00,00$, "R",nn
Response:- $\quad 00,00,00,12,34,56, " r ", n n, a a, b b, \ldots h h$

## $S \quad$ Status Poll.

This command requests the addressed unit to reply with the current value of analogue quantities, present temperature, last/present received RSSI, transmit power of last transmission, received frequency offset of last/present received signal, and present supply voltage.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " S "$
Response:- $\quad 00,00,00,12,34,56, " s "$, tt,rr,pp,ff,ss
Where:-
$\mathrm{tt}=$ Temperature conversion code
rr $=$ RSSI conversion code
pp = Transmit Power conversion code
ff = Received Frequency Offset conversion code
ss = Power Supply conversion code

## T. Diagnostics Watchdog Timer command.

This command forces the addressed unit to (re)set a special watchdog timer. The operand value is a word (16_bit) quantity. A zero value will disable the timer. A non-zero value will initialise the timer. This timer, while non-zero, will be decremented periodically. If the timer is decremented to zero, then the TC-900DR will perform a cold boot, thus restoring operating parameters from the NVRAM configuration memory. This command should be used in conjunction with parameter set and write commands. If a parameter change renders the unit in-operable, then either it will not continue to receive further "T" commands to reset the timer, or the system diagnostics controller may cease to send the timer reset commands, thus will eventually cause the unit to cold boot.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " T ", n n n n$
Response:- $\quad 00,00,00,12,34,56, " t "$
Where:-
nnnn = timer reset value (16 bit value)

V Request Firmware Version String command.
This command requests the addressed unit to reply with a string indicating it's firmware version number. Future firmware versions may provide further facilities that may then be used, by sending appropriate commands.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " V "$
Response:- 00,00,00,12,34,56,"v","A2.2.0"

## W Write Parameter command.

This command is used in conjunction with the " P " parameter set command. This parameter write command must be identical to the previous parameter set command. Providing they are identical (excepting the command mnemonic), then the operand is written to the selected modem operating parameter. Changing some parameters while normal operation continues could produce improper operation, possibly resulting in corrupted parameters, so the unit should be halted with a HALT command before such parameters are changed.

Syntax:-
Command:- $\quad 12,34,56,00,00,00, " W ", n n, a a, b b, c c, \ldots$
Response:- $\quad 00,00,00,12,34,56, " w ", n n, a a, b b, c c, \ldots$
Where:-
$\mathrm{nn}=$ parameter identifier
$a a, b b, c c, \ldots$ are data value(s) for selected parameter

### 3.3.6 PARAMETER SET

The following is a list of parameters which may be remotely set. Parameters marked with a "*", should only be changed while the unit is in a halted state, followed by a warm boot command. Parameters marked with a "\#", may only be referenced in an "R" readback command. Attempts to change these with " $P$ " and " $W$ " commands may produce unpredictable results.

| Parameter Identifier | Parameter Type(Size) | Parameter Name |
| :---: | :---: | :---: |
| 00 (^@) | undefined | not defined, reserved to facilitate future expansion |
| 01 (^A) | undefined | not defined, Trio DataCom test use only |
| 02 (^B) | byte | Drift_Offset |
| 03 (^C) | word | PTT_Time |
| 04 (^D) | string | Synthesiser Data for channel change |
| 05 (^E) | byte | min_RSSI |
| 06 (^F) | byte | Tx_LID |
| 07 (^G) | byte | Slot_Num |
| $08\left({ }^{\wedge} \mathrm{H}\right)$ | byte | Slot_Time |
| 09 (^) | word | SIDA1 and SIDA2 |
| OA (^J) | word | SIDB1 and SIDB2 |
| 0 B (^K) | word | SIDD1 and SIDD2 |
| $0 \mathrm{C}\left({ }^{\wedge}\right.$ ) | byte | KISS_adrA |
| OD (^M) | byte | KISS_adrB |
| 0 E (^N) | byte | EOMA_code |
| OF (^O) | byte | EOMB_code |
| 10 (^P) | byte | input_timeA |
| 11 (^Q) | byte | input_timeB |
| 12 (^R) | byte | frame_sizeA |
| 13 (^S) | byte | frame_sizeB |
| 14 (^) | bit * | SLIP/KISS_mode portA |
| 15 (^U) | bit * | SLIP/KISS_mode portB |
| 16 (^V) | bit | EOM_enable portA |
| 17 (^W) | bit | EOM_enable portB |
| 18 (^X) | bit * | KISS_mode portA |
| 19 (^Y) | bit * | KISS_mode portB. |
| 1A (^Z) | bit | RTS/CTS_interlock portA |
| $1 \mathrm{~B}{ }^{\wedge}{ }^{\text {( }}$ ) | bit * | PORTB_enable |
| 1C (^) | bit * | Repeat_Enable portA |
| 1D (^) | bit * | Repeat_Enable portB |


| 1E (^^) | bit * | (Not defined, reserved for Error Recovery Enable) |
| :---: | :---: | :---: |
| 1F ( ${ }^{\text {a }}$ ) | bit * | (Not defined, reserved for Error Recovery Enable) |
| 20 () | bit | LiveFrame portA |
| 21 (!) | bit | LiveFrame portB |
| 22 (") | bit | XonXoffMode portA |
| 23 (\#) | bit | XonXoffMode portB |
| 24 (\$) | byte | PORTA_Config |
| 25 (\%) | byte | PORTB_Config |
| 26 (\&) | bit | diags_repeat |
| 27 (') | bit | TxPWR_HI/LOW |
| 28 () | bit | SID_Enable |
| 29 ()) | bit | RTS2PTT |
| 2A (*) | bit | SYNC2PTT |
| 2B(+) | bit | SCDO_Default |
| 2C(,) | bit | SupChnFunc |
| 2D (-) | bit | TxCtrl1 |
| 2E (.) | bit | TxCtrio |
| 2F (/) | byte | Config1 |
| 30 (0) | byte \# | SMR1 (portA serial port mode) |
| 31 (1) | byte \# | SMR0 (portB serial port mode) |
| 32 (2) | byte \# | BRR1 (portA serial port baud rate) |
| 33 (3) | byte \# | BRR0 (portB serial port baud rate) |
|  |  | Additions for version A2.3.0 |
| 34 (4) | byte | err_limit (Frame Error output for Base Station) |
| 35 (5) | byte | err_flags |
| 36 (6) | word | good_cnt |
| 37 (7) | word | bad_cnt |
| 38 (8) | word | lost_sync_cnt |
| 39 (9) | word | lost_RSSI_cnt |
|  |  | Additions for version A2.3.1 |
| 3A (:) | byte | DCD_timeA |
| 3 B (;) | byte | DCD_timeB |
| 3C (<) | byte | Diags_Delay |

### 3.3.7 ADVANCED STREAM ROUTING FUNCTIONS

The TC-900DR provides advanced stream routing functions. For each port, there is allocated two SID (Stream IDentifier) codes, and a configuration flag that determines how these two codes are used.

With the flag off, SID×1 (where x is A or B for portA and portB respectively) defines the SID code of received frames that are de-multiplexed to the port, and SIDx2 defines the SID code that is inserted by the modem at the front of every frame it transmits. Thus only one data stream passes through the port, and the modem manages the insertion and extraction of SID header codes.

With the configuration flag on, SIDx1 and SIDx2 define a range of streams that will be passed from the received data to the port. SIDx1 defines the lowest stream, while SIDx2 defines the highest stream. The SID header codes remain on the received frames, and are passed to the port. For transmit data, the modem assumes that the SID header codes are already in place, being inserted by some external device, and no processing is performed on the transmit data. For this application, it is highly desirable that a SLIP (or KISS) driver be employed so that frame boundaries are defined.

These functions are independent for each port, so it is possible to construct (say), a multi-drop, multi-hop repeated data system, where one stream can be "peeled off" at each repeater site. There are many other possibilities, the TC-900DR product simply requiring suitable configuration to construct a vast range of network topologies.

### 3.4 FACILITIES AND CONFIGURATION INFORMATION VERSION 2

### 3.4.1 GENERAL

The TC-900DR, provides two independent user data streams, which are multiplexed onto the radio channel data stream. The stream switching protocol also provides for an embedded remote diagnostics facility.

The two (asynchronous) user ports can be configured for a variety of baud rates, character sizes, parity, and stop bits.

Flow control on user Port_A may be set to use RTS/CTS/DTR/DCD handshake lines, or XON/XOFF characters. Flow control for Port_B may be set to use XON/XOFF characters, or no flow control. Port_B is not supported by RTS/CTS/DTR handshake lines.

Data is transported in (HDLC) frames, protected by a 16 bit CRC error checking sequence, conforming to the CCITT standard. Received frames found to contain errors are discarded. The TC-900DR does not release received data frames to the user port, until completely received, and error checked.

Maximum frame size is configurable for each port independently, and may be set to any value between 4 and 255. Frame size limiting is disabled by setting this parameter to zero (0).

Each user port, is supported with PAD functions conforming to X 3 , or SLIP*1 $^{\star 1}$ or KISS* protocol interface.

For Point To Multipoint applications, a unique collision avoidance mechanism is available, with configurable channel access parameters.

All configuration parameters are held in a non-volatile memory. Normally, this memory can only be written when the radio modem is connected to a programmer.

### 3.4.2 BRIEF OVERVIEW OF MODEM INTERNAL OPERATION.

### 3.4.2.1 DATA TRANSMITTER

Each physical user port, is supported by a "driver", in this case a PAD (Packet Assembler/Dis-assembler) or SLIP/KISS. This function transfers the data from the port, to a buffer memory. This buffer not only stores the raw user data, but also keeps track of frame boundaries. Another functional block, retrieves that stored data, and feeds it to a third mechanism, which generates the data waveform which is applied to the radio transmitter modulator.

[^5]
### 3.4.2.2 DATA RECEIVER.

The receiver extracts data frames from the received signal, and stores the contents of the frames into buffer memory. It may also perform a steering function, if more than one port is enabled. A second function is to retrieve the stored data, and send it to the user port(s), consistent with some flow control regime.

### 3.4.3 SELECTING FRAME SIZE

The selection of maximum frame size is a compromise between channel through-put and data propagation time over the link.

The receiving modem collects and stores the incoming data frame, and on detecting the end of the frame, checks if an error has occurred. If not, then the stored data is released for transfer to the user data port. If an error has occurred, then the stored data is "flushed" from the data store. Thus a delay is introduced between the time the frame data begins to enter the destination radio modem, and the time this data begins to emanate from the user port. This delay is effectively the length of the data frame, which consists of the user's data, plus the framing overhead. This overhead will include at least 24 bits for the HDLC Flag and FCS (error checking data), plus another 8 bits if SID (Stream IDentifier) codes are enabled (refer to detailed description elsewhere in this document), plus the duration of the transmitter Lead-In-Delay, if the radio transmitter had to be started up to send the data. Thus larger frames reduce the proportional overhead, but increase the end to end propagation delay.

On the assumption that the radio transmitter was already on, and that the frames include the SID header, then every frame includes 32 bits of overhead.

Assuming that the user port is configured for 8 bit character size ( 8 bit data no parity, or 7 bit data and parity), and 1 stop bit, then each character is carried as a 10 bit sequence on the asynchronous user channel. On the radio channel data stream, user data is stripped of the start and stop bits used on the asynchronous user port, and transmitted as eight bit "octets", and so the character rate is $1 / 8$ th of the bit rate, while on the asynchronous user port, the character rate is $1 / 10$ th of the bit rate. For every 16 user characters 32 bits are stripped off, so if the maximum frame size parameter is set to 16 , and the nominal baud rates are the same, then the effective character rates on the asynchronous user channel and the synchronous radio data channel will be the same. This also assumes that the supervisory signalling channel is not enabled, and does not allow for the overhead introduced by the HDLC "dummy zero" stuffing mechanism.

### 3.4.4 CONFIGURING PAD PARAMETERS

The Packet Assembler/Dis-assembler (PAD) can be configured with a variety of parameters. Each user port is supported by an identical but independent PAD.

The configuration parameters of the PAD, control how the user data (to be transmitted) is framed. There are three distinct mechanisms that can cause the frame that will carry the user data to be closed.

The first of these is the Maximum Frame Size parameter, already discussed above. As each character is input to the modem, a counter is incremented, and when this counter reaches the set maximum frame size, the data storage mechanism that operates within the modem, will close the frame. This function may be disabled, by setting the parameter to zero.

The second mechanism, is the use of a specified End Of Message (EOM) character. This function is enabled/disabled by a flag in a configuration byte for the port driver. The EOM character may be any 8 bit character. When the EOM function is enabled, all incoming user data is compared to the selected EOM character code, and in the event of a match, the current frame is closed. Note that this match only triggers the frame closure mechanism. The matching character is not deleted from the user data stream, and in fact becomes the last user character in the frame.

The third mechanism, is the implementation of a timer. If the timer is enabled, each character received from the user port re-starts the timer. If the time duration between successive user characters allows the timer to expire, then the frame closure mechanism is invoked. The timer counts in units of "ticker clocks", which is a time interval generated by the modem internally, and is approximately 2.5 mS . The reload value for the timer can be set from 1 to 255 ticker clocks. The timer mechanism is disabled by setting the PAD timer parameter to zero.

There is a single bit configuration flag, that allows the radio modem to begin transmitting user data, even before the frame is deemed to be complete. In this case, as soon as there is any data in the storage buffer, the modem begins the transmission procedure. Providing that the input character rate is greater than or equal to the character rate on the synchronous radio channel, then there is no danger of an under-run condition, where the modem transmitter runs out of data before the PAD deems a frame end. However, should this occur, the modem data transmitter function simply closes the frame itself. Further data is carried in the next frame. This may or may not cause problems elsewhere in a system context. If higher protocol layers are employed (e.g. X.25, AX. 25 etc.), where address and control fields normally occupy fixed positions in data frames, then the above scenario should not be allowed to occur.

The major advantage of allowing the radio modem to begin the transmission procedure before the frame is deemed to be complete, is that it avoids a (store and forward) delay in the modem transmitter, similar to that required in the receiver. For applications where a transparent point to point link is all that is required, this mode provides the most time efficient transport mechanism.

In fact with the immediate transmission function enabled, there is little necessity to enable the EOM or timer functions of the PAD.

### 3.4.5 SUPERVISORY SIGNALLING CHANNEL: APPLICATIONS \& CONFIGURATION.

The reader is referred to drawing number TC01-05-18, which provides a diagramatic view of this section.

The Supervisory Signalling Channel (SSC) is implemented by the insertion of extra data bits in the primary bit-stream on the synchronous radio channel. These extra bits are inserted between primary data octets, at a rate which can be set to range from once every octet, to once every 15 octets. The SSC operates independently for transmit and receive directions, and can be disabled by setting the rate variable to zero.

The SSC, when enabled, can be configured either to provide end-to-end flow control for Port_A data, or implement the collision avoidance mechanism.

### 3.4.5.1 PORT_A END TO END FLOW CONTROL APPLICATION.

In this configuration, the SSC is used to carry flow control information for data on Port_A at each end of the link.

SSC data inserted into the transmitted bit-stream, relates to the flow of the primary data stream received. When handshake lines are employed, the DTR line locally controls the flow of receive data to the user port. The state of this line is also logically combined with the "fill" state of the receive buffer, and the result is then sent as SSC data in the transmit data stream. Thus the state of the transmitted SSC data bit is one ("1") if the DTR line is in a "false" state, OR the receive buffer is more than half (approximately) full. In the case where XON/XOFF flow control is used, the DTR line input is instead replaced with the state of the last received XON or XOFF control character.

SSC data extracted from the received bit-stream, is logically combined with the "fill" state of the transmit buffer, and the result is output to the CTS line of the modem. The CTS output line is set to "false" if the transmit buffer is more than half (approximately) full, OR the received SSC data bit is a one ("1"). Thus the CTS line is set to "false" if the local transmit buffer is more than half (approximately) full, OR the remote receive buffer is more than half full, OR the remote DTR input line is "false" (or equivalent XOFF received).

Data flow control is exercised only at the user port. No flow control is used on the radio channel, so once data is entered into the transmit buffer, it will be transmitted. This is the reason why the buffers are only allowed to become half full before the flow control mechanism engages. If the flow of receive data is stopped by deactivating the DTR line, the remaining data in the transmit buffer will not overflow the receive buffer. It should be noted that some hysteresis is used in the buffer occupancy tests, to prevent the CTS line from changing state too often, as some hosts (e.g. DOS machines) appear to get confused when this happens.

If the SSC is not configured for end to end flow control, or is disabled, then the flow control mechanisms still operate at a local level. That is, the CTS line (or equivalent XON/XOFF control regime) reflects the fill state of the local transmit buffer.

### 3.4.5.2 COLLISION AVOIDANCE APPLICATION.

When the SSC is allocated to transporting collision avoidance data, the transmitted SSC data reflects the state of the radio receiver. Other processes in the modem, measure the RSSI signal from the radio receiver, and compare this measurement to a preset threshold level. This threshold value is also held in the non-volatile configuration memory. The result of the comparison is copied to the modem pin that drives the RXSIG LED. The transition of the RXSIG signal from off to on, (re)starts an internal timer. This time is a fixed value of $35 \pm 5 \mathrm{mS}$. The SSC data transmitted, is simply a copy of the RXSIG pin state, until the timer terminates, and there-after, the modem data receiver must be "SYNC'd" to maintain the "1" state of the SSC transmit data. Thus the SSC data transmitted by the modem will indicate that the radio channel receiver is busy, using only RSSI for the first $35 \pm 5 \mathrm{mS}$, but after this time, data receiver SYNC is used to qualify this state. This prevents low level RF interference from effectively blocking the channel.

At the receiving end, the recovered SSC data is used by the radio modem to determine when the receiver of the destination station is free. This data can then be used to control it's channel access strategy. Channel access strategies are dealt with in more detail elsewhere in this document.

In such a data transport system, there is a single unit which performs the function of Master, and two or more stations which operate as Slaves. The SSC need only operate in one direction, that from Master to Slaves. In the reverse direction, the SSC can be disabled. That is the SSC in the Slaves is enabled in the data receiver only, while in the Master, it is enabled only in the data transmitter.

### 3.4.5.3 RECEIVED SSC DATA DEFAULT STATE

The received SSC data bit is stored in an internal latch. This latch is updated each time a SSC data bit is extracted from the incoming bit-stream. However, if the radio receiver looses signal, then a default state is forced into the latch. This default state is configurable.

For applications which use the SSC for collision avoidance, this configuration bit would normally be set to " 1 ", so that the remote station would not attempt channel access while the signal from the base is lost.

For applications which use the SSC for end to end flow control, setting the default state of the SSC receive data latch to " 0 ", would cause the CTS output line to indicate local flow control status only, until the destination unit enables it's transmitter, where-upon the received SSC data would reflect the state of the destination receive buffer and DTR input line. Alternatively, setting the default state to " 1 ", would ensure that the CTS output line would be in a "FALSE" state, until the destination unit enables it's transmitter, where-upon the received SSC data would reflect the state of the destination receive buffer and DTR input line.

An associated configuration bit, is one that allows the automatic activation of the radio transmitter, whenever the data receiver attains SYNC. When this configuration bit is set to "1", the modem will automatically activate the radio transmitter's PTT control line when the data receiver is SYNC'd. This could be used at the base end of a small point to multipoint network, using the SSC for flow control, and would not require the host connected to base, to specifically activate the radio transmitter to establish the end to end link.

### 3.4.6 SLIP/KISS PROTOCOL DRIVERS

In addition to a generic PAD, two other host interface protocols are supported, "Serial Line Interface Protocol", SLIP, which hails from the world of UNIX(tm), and an extension of SLIP, KISS "Keep It Simple Stupid", (a rather unfortunate phrase in the present context, but a protocol standard proposed by Phil Kahn, USA, specifically for the control of radio connected data terminals) which includes a facility to send commands which are addressed to the DCE device itself. These commands set operating parameters of the radio-modem DCE, such as transmitter lead-in delay, or radio channel (RF frequency).

Neither of these protocol standards, specify anything about the construction of data packets on the radio channel. Allocation of address, control, and information fields is the user's responsibility.

As standard, the modem is equipped with an 8 K ( 8192 bytes, 32 K optional) data storage memory to hold transmit and receive data. This memory is divided equally between transmit and receive buffer space, and equally between the two user ports, so the largest frame size is 4095 bytes, if only PortA is enabled, (or 2047 bytes each if both user ports are enabled), before the frame check sequence (FCS)is appended.

Additionally, the modem can store up to sixty four separate frames for each direction, again split between the two user ports if both are enabled, though the total byte count is still limited to 8192 total.

### 3.4.6.1 SLIP Protocol Description/Definition

The SLIP protocol, is a data transport protocol, originated and used extensively in UNIX(tm) based systems, and thus also closely associated with TCPIIP networked systems. Although not truly a "standard" it is so widely used that it has become the defacto standard for serial interface in UNIX and many other networked systems. SLIP is a method of framing messages containing binary data, on asynchronous channels. The asynchronous serial channel is configured for eight bit character size, no parity, and one stop.

A specific binary code called FEND (Frame End, hexadecimal value $=C 0$ ) is reserved to define a frame boundary. Should this same code occur in the data message to be transferred across the channel controlled under SLIP, then an escape sequence is used so that the message byte will not be confused for a FEND. This escape sequence, involves replacing the message hexadecimal CO code with a two byte sequence FESC, TFEND. FESC (Frame Escape) is the binary code hexadecimal DB, and TFEND (Transposed FEND) is binary code hexadecimal DC. Likewise, if the FESC character ever appears in the user data, it is replaced with the two character sequence FESC, TFESC (Transposed FESC). The TFESC is the binary code hexadecimal DD. The following table clarifies this.

| ABBREVIATION | DESCRIPTION | HEX.VALUE |
| :--- | :--- | :--- |
| FEND | Frame end | C0 (192) |
| FESC | Frame escape | DB (219) |
| TFEND | Transposed frame end | DC (220) |
| TFESC | Transposed frame escape | DD (221) |

As characters arrive at the SLIP receiver, they are appended to a buffer containing the current frame. Receiving a FEND .marks the end of the frame, and consequently, succeeding bytes are considered part of the next frame.

Receipt of a FESC code puts the SLIP receiver into "escaped mode", causing it to translate a following TFESC or TFEND back to a FESC or FEND code, appending it to the buffer, and resuming it's normal state. Receipt of any byte other than TFESC or TFEND while in escaped mode, is an error. No translation occurs, and the SLIP receiver leaves escaped mode. A TFESC or TFEND received while not in escaped mode is treated as an ordinary character and stored accordingly. Reception of consecutive FEND characters, causes no action to be taken (i.e. is not interpreted as zero length frames).

An example of a typical SLIP frame is shown below. The message consists of the string DA, C4, C0, C5, DB, 20, BD, DC, DD. The SLIP frame will be:-

$$
\begin{aligned}
& <\text { FEND }>, \text { DA }, C 4,<\text { FESC }>,<\text { TFEND }>, C 5,<F E S C>,<T F E S C>, 20, B D, D C, D D,<F E N D> \\
& ==> \\
& C 0, D A, C 4, D B, D C, C 5, D B, D D, 20, B D, D C, D D, C 0
\end{aligned}
$$

### 3.4.6.2 KISS Protocol Description/Definition

The KISS protocol is an extension of SLIP. It uses the same method of framing packets, using FEND, FESC, TFEND, and TFESC codes. However, the first byte in each frame is reserved as a control code, that defines the function/content of the frame, and also contains an address.

This addressing scheme allows up to sixteen "Terminal node controllers" (TNC's), to share a multidrop buss. The top nibble of the control code carries the TNC address, and the lower nibble carries the command code. Normally the address is set at zero for installations containing only one TNC. Note that some extensions have been proposed for the KISS protocol, that properly support addressed multidrop line operation of multiple TNCs, that the present TC-900DR modem firmware does not implement. The following table shows the commands defined by KISS, and the comment column indicates how the TC-900DR modem interprets them.

| COMMAND | FUNCTION | COMMENTS |
| :---: | :---: | :---: |
| 0 | Data Frame | The rest of the frame is data to be transmitted. |
| 1 | TxDelay | The next byte is the RF transmitter key-up delay in octets. |
| 2 | Slotnum | The next byte is the Slotnum parameter. |
| 3 | Slot-Time | The next byte is the "Slot" interval in "ticker clocks". |
| 4 | TxTail | The next byte is the time to hold up the RF transmitter after the closing FLAG has been sent. This command is obsolete, and not implemented in the TC-900DR. |
| 5 | FullDuplex | The next byte is zero for half duplex, non-zero for full duplex. This command is not implemented in the TC-900DR, as it always operates in full duplex mode. |
| 6 | SetHardware | Specific for each TNC. This parameter has values between 00 and 03 , and commands the TC-900DR to set RF channels 0 to 3 . Values above 3 are ignored by the present modem firmware, but may be used in future versions. |
| F | ExitKISS | Exit KISS and return control to higher level TNC control program. This command is not implemented in the TC-900DR. |

### 3.4.7 RF TRANSMITTER CONTROL AND CHANNEL ACCESS STRATEGIES

There are three conditions which cause the modem to activate the radio transmitter. These are: a) receiver SYNC if enabled, as described above; b) RTS if enabled, as described below; and c) the existence of a data frame ready for transmission. The first two mechanisms are absolute, and if enabled, cause an immediate activation of the radio transmitter. There are two configuration bits that control how the availability of a data frame, will activate the radio transmitter, and thus gain access to the channel. For the purposes of this description, these are referred to as Modes A, B, and C.

In Mode A, channel access is immediate. The radio transmitter is activated, and the modem then proceeds to send a preamble sequence, followed by the data. The preamble sequence is necessary for receiver synchronisation, and the length is a configuration parameter. Further discussion of these aspects of the modem configuration are dealt with elsewhere in this document.

In Mode B, the modem will attempt channel access only if the radio receiver is NOT receiving a signal (i.e. the measured RSSI level is below the minimum RSSI threshold as described elsewhere in this document). This method could be used for small point to multipoint systems, where the base station would enable it's radio transmitter on receiving a transmission. Typically this would be done at the base unit by enabling the SYNC-PTT function, as described above. This implements a basic collision avoidance system, without the use of the Supervisory Signalling Channel, which then remains available for flow control applications.

In Mode C, the modem will attempt channel access only if the data receiver is SYNC'd, and the SSC data is " 0 " (i.e. base receiver free). This is the full Collision Avoidance system as described in detail above.

In the latter two cases, if another data frame is ready for transmission at the time the present one is ending, then it is automatically appended as another frame, and the transmission continues. Obviously since the radio transmitter is already enabled, no preamble is required or sent. The modem itself does not limit the number of consecutive frames it will transmit. If data continues to be input to the modem, once channel access is gained, it continues to be transmitted. It is the responsibility of the user to manage any maximum channel access time in overall system design. However, if the PTT timer is enabled (dealt with in detail elsewhere in this document), and the set time is reached, then the modem will disable the radio transmitter PTT line. User data will now be lost.

For the two latter strategies, if channel access fails (i.e. signal at radio receiver in the former case, or SSC=1 in latter case), then the modem uses a timed delay mechanism before testing for channel availability again.

### 3.4.7.1 SELECTING "SLOTIME" AND "SLOTNUM" VALUES

This delay time is necessary to prevent multiple remotes from attempting to gain access to the channel as soon as it is signalled to be clear after another transmission has finished, as this would result in the transmissions from all these remotes colliding. Instead, when a modem fails to gain channel access, it generates a randomly selected delay time, and when this time has expired, it again tests for channel availability.

There are two parameters which are used to generate the delay time. The "Slotime" parameter defines the size of the time increment used in selecting the delay. This value defines a time counted in "ticker clocks" (approximately 2.5 mS ), and has an allowable range of 0 to 255 . The "SlotNum" parameter defines the upper limit of the random number generator. The random number generator selects an integer between one and the value of "SlotNum", and then multiplies this by the value of "Slotime" to derive the delay time. The "SlotNum" parameter has a maximum allowable range of 1 to 16 .

These two parameters together provide a very flexible method of tuning the channel access characteristics of a system, and should be regarded as system tuning parameters. In the absence of any knowledge of a system configuration, Trio DataCom's set default values for these to parameters to 4 and 16 for "Slotime" and "SlotNum" respectively.

### 3.4.7.2 PTT CONTROL BY RTS LINE

Applications relying on establishing a point to point link before data is transferred, would normally require some "manual" method of activating the radio transmitter. A configuration bit enables the RTS input line to be used as a PTT control. The modem is always generating a data signal. During the time when no user data is available, the modem continually generates an "idle" bit-stream of HDLC FLAGs. This sequence produces no data output at the receiving radio modem.

### 3.4.8 SELECTING FLOW CONTROL REGIMES

The type of flow control to be used on the radio modem port(s), depends on the user's application and capabilities of the equipment which the user interfaces to the TC-900DR.

Port_A, which is always active, can be configured to use the standard RS232 handshake lines RTS/CTS/DTR, or use XON/XOFF protocol.

### 3.4.8.1 PORT_A, HARDWARE HANDSHAKE FLOW CONTROL

If hardware handshake lines are configured, then RTS must be active to validate characters input to the modem for transmission. As each character is received (i.e. at the end of each character bit sequence) the state of the RTS input line is tested to validate the character. If the RTS line is tested "true", then the character is stored ready for transmission. If "false", then the character is discarded. The modem provides flow control of transmit data with the CTS line. The CTS line is set "false" to indicate that no more transmit data should be input. Normally, most terminals or hosts will still send one or two more characters after the CTS line is set "false", and this is normal and allowed for in the CTS control logic. In fact the modem will continue to accept and store transmit data (providing the RTS line is still active) even though it has set the CTS line to "false", however the user then risks the occurrence of an overflow condition. If the transmit buffer becomes full, then further data is discarded.

A configuration bit, further controls the state of the CTS output line in relation to the RTS input line. If the bit is clear, then the CTS output will always indicate the flow control state, regardless of the state of the RTS input. If the bit is set, the CTS line is conditional on the state of the RTS input. If the RTS input is "false", then the CTS output is also "false". If the RTS input is "true", then the CTS output indicates the flow control state. This latter configuration is typical of a "wired" modem.

The modem's internal data store holds both the raw user data, and records the position of frame boundaries (as defined by PAD operation) in the data. A limited amount of memory is allocated to storing the frame boundary data. When this memory space is full, the modem sets the CTS output to false, even though the character storage space may not be full. The frame boundary storage space is sufficient to hold data for 64 frames. If the modem has both ports (Port_A and Port_B) enabled, then this space is evenly divided between the two, or if Port_B is disabled, then up to 64 frames can be stored for Port_A. If data continues to be input when the CTS line has been set to "false" because no more frame boundaries can be recorded, then the frame closure mechanism may abort. This has the effect that a frame will not be closed when defined by PAD configuration. An example of this, is where the PAD is configured to close the frame on receiving a <CR $>$ (carriage return) EOM. If the frame boundary space is full, when a $<C R>$ is input, then the subsequent characters will be appended to the same frame. Another attempt to create a new frame will not occur until the same or another frame close condition (as defined by PAD configuration) occurs, in this case another <CR>. This logic avoids the unnecessary loss of data.

Situations where the data storage space or frame boundary storage space become full, would be rare, and would only be likely to occur if the transmitter could not gain access to the channel, or the input data rate exceeds the channel transmission rate for some time.

Normally the TC-900DR is manufactured with an 8 kilobyte memory for data storage. This memory space is divided equally between transmit and receive data storage. If both user ports are enabled, then each half is equally divided between the ports (i.e. $2 K / 2 K / 2 K / 2 K$ for Port_A transmit, Port_A receive, Port_B transmit, Port_B receive). If Port_B is disabled, then 4 K is available for each of the transmit and receive data storage functions for Port_A.

The DTR line controls the flow of receive data to the user port. While the DTR input line is "true", available received data is output from the port. If the DTR input is "false", then receive data output ceases.

### 3.4.8.2 PORT_A XON/XOFF FLOW CONTROL PROTOCOL

When XON/XOFF flow control is configured for Port_A, the CTS line is set "true", the RTS input line is not required to validate input data, and receive data is not dependent on the state of the DTR line. Instead of controlling the CTS line, the modem sends XON/XOFF characters (embedded in the receive data stream), to the port. The flow of receive data is controlled by the receipt of XON/XOFF characters in the transmit data stream. These control characters are trapped out of the transmit data stream, and are not transmitted.

The underlying flow control logic is the same as RTS/CTS/DTR control. An XON is sent instead of a "false" to "true" transition of the CTS line, and an XOFF is sent instead of a "true" to "false" transition on the CTS line. A received XON is recorded by an internal flag that emulates a "true" state on the DTR line, and a received XOFF is recorded by the flag to emulate a "false" state on the DTR line.

This method of flow control would be considered to be less reliable, since a lost XON or XOFF control character could cause either an overflow condition, or data flow to stop altogether.

### 3.4.8.3 PORT_B FLOW CONTROL

User Port_B can be configured for no flow control, or XON/XOFF flow control. When XON/XOFF flow control is configured, it operates identically to Port_A, except that this port has no CTS line to set "true". Flow control on Port_B operates at a local level only, since end to end flow control via the SSC is available only for Port_A.

If XON/XOFF flow control is disabled, then no flow control is used on Port_B, as there are no RTS/CTS/DTR lines implemented on Port_B. Users should be careful to avoid overflow conditions, to avoid loss of data.

It will now be obvious that the RTS input line on Port_A can be used by more than one function in the modem. RTS can have no function, or be used in Port_A flow control, and/or provide a manual PTT facility.

### 3.4.9 SETTING MINIMUM RSSI LEVEL

The data receiver of the modem is continually running. It will be in one of two states. It is not SYNC'd, and thus looking for HDLC FLAGs in the radio receiver signal, or it is SYNC'd, and recovering frame data to be checked and stored. If the radio receiver is not receiving a signal, then the recovered signal applied to the data receiver of the modem, will consist only of noise. To prevent the modem from erroneously locking onto noise, a minimum RSSI level must be present to validate the recovered signal applied to the modem data decoder. This threshold level, is stored in the non-volatile configuration memory. It should be set by applying a signal to the radio receiver, which produces a desired SiNaD result, a desired bit error rate, or more crudely, a predetermined absolute signal level into the antenna connector of the TC-900DR. The modem (operating in Test/Program mode) is then commanded to measure the RSSI level, which produces a response of a message indicating the measured level, in hexadecimal. This process should be repeated several times, then an average taken. The analogue to digital conversion performed in this way, is an eight bit conversion. In normal operation, the modem performs a six bit conversion when measuring the RSSI level, so the average of the levels measured in the test mode should now be divided by four. The result should now be stored in the configuration memory, at the address reserved for it.

### 3.4.10 SETTING PTT TIMER

The modem implements a PTT timer. This timer can be disabled entirely by setting the PTT Timer configuration value to zero. The timer value is a 16 bit number, that counts in "ticker clocks". If the timer is enabled, whenever the modem activates the PTT control to the radio transmitter, it initialises the timer with the configured value. The timer is decremented while the PTT control remains active, and if it terminates, the PTT control is deactivated. No other action is taken, and all other functions within the modem are oblivious to this condition, so data frames continue to be output, and thus lost. The PTT timer is to be considered an emergency override mechanism only, in case an error occurs in the operation of the user's host equipment and/or software. To reset this time-out state, conditions must be met that would cause the modem to normally deactivate the PTT control. The PTT timer will then be re-initialised the next time the PTT control is activated. The time-out period may be set in "ticker clock" ( 2.5 mS ) increments to over 160 seconds.

### 3.4.11 DATA STREAM SWITCHING, SELECTING AND ENABLING SID CODES

The TC-900DR radio modem includes a feature that provides data stream switching. This is achieved by placing a Stream Identifier code (SID) at the beginning of every frame. This code functions as a simple addressing function. If both user ports of the TC-900DR are enabled, then SID codes should also be enabled, so that data frames carry a code which identifies the originating port ( $A$ or $B$ ), thus the port to which the frame data should be directed when the frame is received at the destination station.

However this stream switching mechanism is not only confined to this simple application. The SID codes for each user port, are contained in the configuration memory, and are thus "soft". It would be possible to engineer a small (up to 256 stations) network using an individual SID code for each remote station. Since the modem receiver will discard frames which are headed by an SID code which is not recognised, only frames specifically addressed would be stored and passed on to the attached host. The SID code is allocated to the port, so the modem uses the same SID code both for transmission and receipt of frames. Therefore in such a system, the master would be configured with SID codes disabled. The host attached to the master would preface each message with the eight bit address of the destination remote. The message from the remote emanating from the port will have the SID code removed. A message received from a remote, will have the SID code of the sending station at the beginning as the first byte. The remote modem itself places this code at the head of the frame.

Another application of the stream switching feature, is a remote diagnostics facility. This is a facility which is planned for release in the next firmware version. A reserved SID code will be used to address a diagnostics function within the modem. A command/addressing protocol is being developed that employs the units own unique serial number for addressing. "Stay tuned for further updates!".

The SID code is placed in the first octet of each frame. This provides up to 256 unique codes. However, to avoid possible future compatibility problems where higher level protocols are in use on the same channel (e.g. AX.25, etc.), it is suggested that the SID codes used have bit0 set to "1". Such higher level protocols normally use extended addressing where more than one octet is used to carry the destination/source address. A frame using an SID code with bit0 set, will fail an address test and be discarded by such systems. Conversely, if this modem receives a frame containing a higher level protocol, bit 0 of the first octet will normally be set to " 0 ", so will not match any SID code stored in the configuration memory, and be discarded.

By default, Trio DataCom sets the SID codes to 03 and 05 for ports $A$ and $B$ respectively. We have also reserved SID code 00 for the diagnostics facilities.

### 3.4.11.1 Separate Tx And Rx SID Codes. (Firmware Revision V2.1 onwards)

Firmware revision V2.1.0 onwards allows the Transmit and Receive SID codes to be different. Normally the RxSID and TxSID parameters (separate for each port) would be programmed the same. By programming them to be different, means that a TC-900DR unit will receive frames carrying a SID code that matches the configured RxSID code, but transmit frames which carry a SID code that is specified by the TxSID code configuration parameter. Applications for this feature are in small point to multipoint systems, using a central "community" repeater.

### 3.4.11.2 Repeater Operation Mode. (Firmware Revision V2.1 onwards)

The TC-900DR radio modem may also be configured in a repeater mode. The repeater function is enabled as a protocol driver on a port. Thus each user port driver can individually be configured for repeater operation. Essentially, what this does is automatically routes the received data frames back to the transmitter. If SID codes are enabled, then the original SID codes are stored as part of the data frame, and thus the retransmitted frame is identical to that received. Note that only frames received error free will be repeated.

When a port driver is configured for repeater operation, the RxSID and TxSID codes stored in configuration data in the NVRAM are used to define a range of streams to be repeated. The RxSID code configuration parameter defines the lowest SID stream to be repeated, and the TxSID code configuration parameter defines the highest SID stream that will be repeated. Thus it is possible to configure a unit to perform a repeater function for two separate ranges of streams, by configuring both user ports with a repeater driver, or to configure one end of a data link to also be a repeater for a range of other streams.

### 3.4.12 SETTING TRANSMITTER LEAD_IN_DELAY

Whenever the radio transmitter is activated a timer is started. No data frames are transmitted until this timer terminates, so that the destination unit receiver has time to synchronise it's data receiver before frame data is begun. The radio transmitter is very fast, reaching final output power and frequency stability in a matter of a few hundred microseconds (other sections of this document deal with the receiver synchronising aspects). This timer counts in octets, not "ticker clocks" as most other timed functions do, so the actual time elapsed is a function of the radio channel bit rate. However, the synchronisation time is primarily a function of the number of bits to the receiver. Trio DataCom would suggest a value of 25 to 50 (decimal) for this parameter, but it's final value will depend on signal strength and quality at the receiving point, and should best be determined by test.

### 3.5 FACTORS AFFECTING MODEM SYNCHRONISATION TIME

### 3.5.1 (UN)SCRAMBLER AND HDLC STATE MACHINE

It can be shown, that the un-scrambler in the receiving unit will synchronise to the scrambler in the sending unit in 17 bits maximum.

The receiving unit must then detect an HDLC FLAG, which will take another 15 bits maximum. Thus the HDLC state machine and unscrambler should be synchronised in 32 bits maximum.

### 3.5.2 PHASE LOCKED LOOP

Before valid data can be read for the unscrambler, the phase locked loop (PLL) must lock. The time required for this to occur is affected by signal quality and content. The PLL relies on level transitions of the binary signal, on which to lock. It essentially compares the phase of an internal counter, with the phase of the incoming data bits. A detected phase error, will cause the internal counter to speed up or slow down, to reduce the phase error. The greater the error, then the greater the speed adjustment to the internal counter.

If the incoming data stream has few transitions, then the internal counter will "catch up" to it quicker, since it's speed is adjusted less often. The PLL will synchronise to within $90 \%$ of the correct phase (from 0\%), in 16 to 36 bits time, depending on the number of transitions.

In practice, even though the PLL has not reached $90 \%$ lock, meaningful data will still be obtained as long as a good strength, clean signal is available.

### 3.5.3 ERROR CONTROL

Having recovered the raw data, the modem then applies the bit-stream to a de-ramdomiser, which is based on a recursive tapped shift register, described by the polynomial:

$$
X^{17}+X^{12}+1
$$

The output of the de-randomiser is then fed through another conversion function, to convert the NRZI data to NRZ.

The data is now an HDLC data stream, conforming to ISO3309. It is then applied to a function which detects HDLC FLAGs, and extracts "dummy zeros", which were inserted by the transmitter. Frame boundaries are detected at this point.

The modem calculates and appends a 16 bit Cyclic Redundancy Checksum (CRC) word to the end of each frame. This calculation uses the polynomial:

$$
X^{16}+X^{12}+X^{5}+1
$$

This is sometimes referred to as CRC-CCITT since it is a CCITT standard.

The 1's complement is taken of the calculation result and this FCS is appended to the end of the data frame and sent MSB first. (Refer to ISO 3309 for more information)

At the receiver, this calculation is repeated on the received data, and the result checked. A detected error, will cause the receiver to discard the entire frame. A higher protocol level (determined by the user) will detect the lost packet, and initiate a re-send of the packet.

In terms of the reliability of this FCS, it can be claimed that the following will be detected: 2

All single bit errors.
All double bit errors.
Any odd number of errors.
Any burst error less than 16 bits long.
Most large burst errors.
From here emanates the original frame data, provided the FCS was correct. If not then the frame data is discarded. The data is stored in externally addressed memory, connected to the modem IC. Maximum data packet size is determined by the amount of available memory. Normally the modem is fitted with an 8K CMOS RAM, of which half ( 4096 bytes) is allocated to the receiver. The modem can be fitted with an external memory up to 32 K with no other modifications. The receiver section of the modem can store up to 32 separate data packets.

How this data is handled from this point on, depends on the user protocol implemented by the modem on the user interface.

### 3.5.4 TRANSMISSION FORMAT AND TIMING

The data to be transmitted is input to the modem, via the user interface protocol implemented on the user interface. The modem stores the data packet(s) in externally addressed memory, connected to the DFM4-9 modem IC. Maximum data packet size is determined by the amount of available memory. Normally the modem is fitted with an 8 K CMOS RAM, of which half ( 4096 bytes) is allocated to the transmitter. The modem can be fitted with an external memory up to 32 K with no other modifications. The transmitter section of the modem can store up to 32 separate data packets.

Most of the transmitter functions are performed internally in the modem IC, with only a DAC (Digital to Analogue Converter) and final low pass filter implemented by external circuitry.

The data is placed into an HDLC frame (consistent with ISO3309), complete with dummy zeroes where required. During transmission, a CRC calculation (CRC-CCITT) is performed, and when the end of the data packet is reached, this FCS (Frame Check Sequence) is appended to the end of the frame, before the closing HDLC FLAG.

Where two or more consecutive frames are sent, only one FLAG octet is used to delimit the frames. All frames are composed of an integral number of octets.

| "Data and Computer Communications" | William Stallings |  |
| :--- | :--- | :--- |
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Data from the HDLC formatting stage is fed through a function, to convert the NRZ data to NRZI format.

The NRZI encoded data stream is now fed to a data randomiser, to ensure that there is no DC component to the data stream. This is based on a recursive seventeen bit shift register with two taps.

### 3.5.5 COLLISION AVOIDANCE SCHEME

The unique supervisory signalling channel facility available in this product is ideally suited to the implementation of a highly effective collision avoidance mechanism. This is a highly desirable feature in a multipoint data network, in that it allows vastly increased usage of the available channel capacity.

For instance, take a point-to-multipoint network, with a central base station, and a large number of remote data terminals scattered around the central station.

This is a split frequency duplex channel, where the central station is able to transmit on frequency F1, and simultaneously receive on frequency F2. Remote stations transmit on frequency F2, and receive on frequency F1.

If a transmission by one remote station is "crashed" by a transmission by another remote station, then the base station may not get the message correctly, and thus not acknowledge it. If there is no control over when the remote stations transmit, then because the remote stations cannot "hear" each other, their transmissions will begin to collide more often as the data traffic increases. This type of system will suffer a total blockage as the total traffic requirement approaches about $50 \%$ of the channel capacity.
Now, if the base station could quickly inform all other remote terminals, when the base receiver is busy because one of the remote terminals is transmitting, then this message can be delivered to the base receiver without being "jumped on" by another terminal blindly "crashing in". The next terminal can then deliver it's message when the receiver is signaled to be free. Of course collisions are still possible, but the occurrence of these can be dramatically reduced by this type of scheme.

Now to implementation specifics. The supervisory signalling channel in the modem, can be set independently for transmit and receive directions. For the purposes of this collision avoidance scheme, the supervisory signalling channel is only required in the base transmit direction. In the reverse direction, the supervisory signalling channel is disabled. The base transmitter is active full time, sending only FLAGs when it has no real data to send. The base controller, then indicates to the whole population of remote terminals, the current status of the base receiver, in the value of the supervisory signalling channel data bits.

The remote data terminals are programmed so that they will not begin a transmission if the received supervisory signalling channel data indicates that the base receiver is currently busy. This would result in remote terminals queuing for access to the base receiver. To prevent all these remote terminals all beginning a transmission as soon as the base indicates a free receiver, a "windowed" timing mechanism would be implemented, with a random factor added in the terminal's selection of a "window".

There are many factors that would determine the quantification of system variables, but this short description serves to illustrate a basic approach.

### 3.6 TEMPERATURE COMPENSATION

Periodically, the modem controller reads the voltage on the temperature transducer mounted on the radio section. This value is then used in a table look-up procedure, to derive correction data to be applied to the modulator circuitry via a transmit waveform offset voltage. This is provided by the output of the six bit DAC (UX8/RN2), which is fed to the correction voltage input of the 12 MHz reference oscillator.

The offset table is constructed in the temperature calibration cycle performed during the factory testing procedure. The radio-modem is temperature cycled twice from -10C to +65 C . During this time, the necessary data is determined to correct the temperature induced frequency errors. At the end of the cycle, the final database is constructed and written to the non-volatile memory.

### 3.7 USER INDICATIONS

The TC-900DR provides three LED's that show status information to the user - RXSIG, SYNC, and TXMIT indications.

In all operation modes of the modem except "Programmer mode" (see the section below on special modes of operation), the RXSIG LED indicates the level of the RSSI signal from the radio IF strip, compared to a threshold set in the configuration data read from the non-volatile memory. If the signal is above the threshold, then the LED indicator is turned on. There is no hysteresis applied in this process.

In normal operation, the SYNC LED indicates when the modem has detected a valid data stream. The SYNC LED is activated, when the modem detects a valid HDLC flag sequence, and remains active until an invalid sequence of seven or more consecutive "1" bits is detected. The SYNC LED will not be turned on if the RSSI signal strength (as indicated by the RXSIG LED) is below the minimum threshold. This prevents false SYNC detection from noise. While the modem is SYNC'd, it does not continue to measure RSSI levels.

The TXMIT LED indicator is connected directly to the modem's PTT output transistor. It is active whenever the PTT line to the radio section is active low.

### 3.8 SPECIAL MODES OF OPERATION

### 3.8.1 GENERAL

Part of the power-up/reset initialisation phase of the TC-900DR modem, is a set of tests to determine whether the modem should enter a special operation mode.

There are three of these "special" modes. Whilst in these modes the TC-900DR will not operate in its standard run mode.

- Programmer mode.
- Bit error rate test mode.
- Handset mode.

These modes are only entered if the required setup conditions are present at power up of the TC-900DR. An error mode of operation can also be entered into, if during normal operation of the TC-900DR modem, an error condition occurs.

### 3.8.2 PROGRAMMER MODE

Pin 6 on the DB9 connector of Port $A$, is normally the DSR line. This pin is pulled high by a resistor to +13.8 v , so that to a connected DTE the DSR signal implies that this DCE is ready.

However, if this pin is connected to pin 5 when the modem is powered up, the controller senses this, and attempts to enter "Programmer mode". The modem sends out of the serial port, an ASCII "?" (question mark) character, and waits for the programmer to reply with a password. The SYNC LED toggles on and off with every output of the "?" prompt until the correct password is entered. This mode is sustained for approximately 30 seconds. Failure to supply the correct password in time, will cause the modem to abandon the "Programmer mode" attempt, and go on with it's normal power-up procedure. This password protection scheme provides some defense against unauthorised tampering with the TC-900DR modems configuration data.


### 3.8.3 BIT ERROR RATE TEST MODE

Pin 9 of the DB9 connector of Port A, is normally the Ring Indicate output line. The modem includes a resistive pulldown to ground to show a negative condition on this line. However, if this pin is driven positive (typically by connecting it to pin 6), then the modem's data transmitter and receiver will enter the BER test mode.

It will activate the RF transmitter and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic " 1 " level in the unscrambled data.

A test point on the modem section PCB, is available to monitor this point with a frequency counter. (In fact this test point is always active, and may be used to monitor the received data decoded by the DFM4-9 modem IC at any time). Any errors in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a " 0 " bit.

An internal timer is used to generate a time equivalent to 1000 bits. Every error bit detected, will activate the SYNC LED, and restart the timer. If and when the timer expires, the SYNC LED is deactivated. Thus, for error rates of 1 in 103 and above, the SYNC LED will be ON most of the time. A 1 in 104 error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for installation purposes.

Other functions performed in this state include RXSIG indication, and temperature compensation. The state of pin 9 is constantly monitored in this mode. If the pin ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

### 3.8.4 HANDSET MODE

The DFM4-9 modem tests for the presence of a handset plugged into the handset audio port at power up.

This is done by measuring the voltage on channel 4 of the analogue to digital converter (UX10-p6). This signal is passed into the modem section from the radio section via connector X4-p24, "ADC3".

If a handset is plugged in, then the measured voltage will be about 2 V , but if it isn't installed, then the voltage will be about 4 V . The measured voltage is compared to 3 V to determine whether the handset is plugged in. If this test succeeds, then the modem will not generate a data stream. However, it will continue to indicate received RF signal strength, and perform temperature compensation. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED.

### 3.8.5 ERROR INDICATION MODES

### 3.8.5.1 GENERAL

There are three error conditions that will cause the RXSIG and SYNC LEDs to be used for error indications and not their normal purpose. Two of these are fatal conditions, that cause the modem to restart after the duration of the error indication phase.

### 3.8.5.2 TRANSMIT POWER LOW

While the modem activates the radio transmitter, it periodically checks the transmit power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately four times per second. The TXMIT LED will also be on during this process. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function.

### 3.8.5.3 NVRAM READ ERROR

The DFM4-9DR modem accesses the non-volatile memory as part of it's initialisation phase, to get configuration data. If the communication protocol with the device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED operates ON and OFF twice, then the other. A total of five cycles of this occurs, then the modem restarts it's initialisation from scratch.

### 3.8.5.4 SYNTHESISER LOCK DETECT ERROR

If at any time during normal operation, BER mode, or handset mode, the TBB206 frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting. One LED is turned ON ( 0 ), the LEDs are swapped, then both turned $\operatorname{OFF}(\bullet)$. Then the latter LED ON again, swap LEDS, and then OFF. This will give the appearance of a sweeping motion between the LEDs.

The following table shows all error condition displays for comparison.

| Tx PWR Error |  | NVRAM Error |  | TBB206 Error Synthesiser |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | - | 0 | - | 0 | - |
| - | 0 | - | $\bullet$ | - | 0 |
| 0 | - | 0 | - | $\bullet$ | - |
| - | 0 | $\bullet$ | - | - | 0 |
| 0 | - | $\bullet$ | 0 | 0 | - |
| - | 0 | $\bullet$ | - | - | - |
| 0 | - | - | 0 |  | repeat |
| - | 0 | $\bullet$ | - |  |  |
| continue |  |  | repeat |  |  |

### 3.9 SYNCHRONOUS OPERATION MODE FIRMWARE REVISION: V2.1

### 3.9.1 GENERAL

The TC-900DR when operating in Synchronous mode, implements a V. 24 like interface. The unit uses a special wiring harness that converts the two 9 pin "D" connectors on the end panel of the TC-900DR to a standard 25 pin " D " connector for user interface.

Synchronous Mode implements a bit level interface. Data is carried on a bit by bit basis. No framing or error detection is performed. Modem operation is full duplex.

Current implementations of SYNC mode, do not provide a DCD signal in the 25 pin RS232 interface.

### 3.9.2 DATA RECEIVER

While sufficient RF signal is present into the radio receiver, the data decoder is continually extracting data bits from the received signal, and outputting these to the user interface connector. If the received RF signal into the radio receiver falls below the minimum threshold, then the data decoder stops.

### 3.9.3 SETTING MINIMUM RSSI LEVEL

The data decoder of the modem is continually running while sufficient RF signal is present into the radio receiver. If the radio receiver is not receiving a signal, then the recovered signal applied to the data decoder of the modem, will consist only of noise. To prevent the modem from erroneously locking onto noise and producing "garbage" at the RxD pin, a minimum RSS| level must be present to validate the recovered signal applied to the modem data decoder. This threshold level, is stored in the non-volatile configuration memory. It should be set by applying a signal to the radio receiver, which produces a desired bit error rate, a desired SiNaD result, or more crudely, a predetermined absolute signal level " into the antenna connector of the TC-900DR. The modem (operating in Test/Program mode) is then commanded to measure the RSSI level, which produces a response of a message indicating the measured level, in hexadecimal. This process should be repeated several times, then an average taken. The analogue to digital conversion performed in this way, is an eight bit conversion. In normal operation, the modem performs a six bit conversion when measuring the RSSI level, so the average of the levels measured in the test mode should now be divided by four. The result should now be stored in the configuration memory, at the address reserved for it. The DR9_PRGM programmer available from Trio DataCom Pty Ltd facilitates this process.
*Use a signal generator modulated with a sine wave frequency of half the nominal bit rate of the unit (e.g. for a 4800 BPS unit, use 2400 Hz modulation).

### 3.9.4 DATA RECEIVER CLOCK OUTPUT

The receive section of the modem, includes a clock line driven by the modem. This signal is used to synchronise the transfer of receive data to the user system. The RCO (Rx_Clock_Output, pin17 in the DB25 connector) line changes from ON (TRUE) to OFF (FALSE) as the RxD (Receive_Data, pin3 in the DB25 connector) line outputs the next bit, and from OFF (FALSE) to ON (TRUE) in the nominal centre of the bit cell. This conforms to the V. 24 specification.

### 3.9.5 OTHER RS232 RECEIVER CONTROL LINES

The DSR (Data_Set_Ready) line is driven true by the modem. This line is in fact merely tied to the internal +13.8 volt rail via a 4 K 7 resistor. The DTR (Data_Terminal_Ready) input is unused in Synchronous mode.

### 3.9.6 DATA TRANSMITTER

The transmit data input is continually sampled and coded for transmission. This process consists of sampling the data input, randomising the bit pattern so that the DC component of the transmitted stream is zero, and generating a waveform suitable for application to the modulator of the FM radio transmitter.

### 3.9.7 DATA TRANSMITTER CLOCKS

The modem transmit data interface, includes two clock lines. One clock line, TCO (Transmit_Clock_Out, pin15 in DB25 connector) is driven by the modem, the other, TCI (Transmit_Clock_In, pin24 in the DB25 connector) can be enabled to allow the external user to supply a transmit data clock. This is implemented by synchronising the internal clock generator to the user's clock (within a small frequency range). This function is essentially a Phase Locked Loop, and effectively adjusts the phase of the internal clock to match that of the input clock. If the user clock source stops, then the modem will continue to generate the internal clock at it's nominal rate. In accordance with specification V.24, the state of the transmit data line (TxD, pin2 in the DB25 connector) is sampled on the ON to OFF transition of the clock, the bit cell boundary occurs with the OFF to ON transition of the clock.

### 3.9.8 TRANSMITTER RTS/CTS LINES

Two other control lines are included in the transmitter interface. The RTS (Ready_To_Send) input line, is used to control the radio RF transmitter. The CTS (Clear_To_Send) output line is driven by the modem, to indicate that the modem transmitter is ready to accept transmit data. The RTS to CTS time is determined by an internal timer. A configuration parameter is used to load the internal timer when the RTS line is activated, which must expire before the modem activates the CTS line. This time is necessary to allow the remote receiver to settle and synchronise to the data stream, before the user at the transmitting end begins sending data. However it should be noted, that the CTS signal does not perform any flow control function within the modem.

### 3.9.9 PHASE SYNCHRONISM WITH GLOBAL CLOCKS

When data is transferred over more than short distances, and synchronism must be maintained to some external global master clock (e.g. Telecom DDN network), then the propagation delay, and thus phase shift of the data becomes significant. A facility is provided, to introduce a phase delay in the transmitted data stream, of up to $3 / 4$ of a bit, in $1 / 4$ bit steps. This delay is adjusted so that minimum phase offset results at the receiver of the destination station.

### 3.9.10 TRANSMIT TIMER

The modem implements a transmit (PTT) timer. This timer can be disabled entirely by setting the PTT Timer configuration value to zero. The timer value is a 16 bit number, that counts in increments of 2.5 milliseconds. If the timer is enabled, whenever the modem activates the PTT control to the radio transmitter, it initialises the timer with the configured value. The timer is decremented while the RTS line remains active, and if it terminates, the PTT control is deactivated. No other action is taken, and all other functions within the modem are oblivious to this condition, including the CTS line, so data continues to be "carried", and thus lost. The PTT timer is to be considered an emergency override mechanism only, in case an error occurs in the operation of the user's host equipment and/or software. To reset this timeout state, the RTS line must be taken from ON to OFF. The PTT timer will then be re-initialised the next time the RTS line is activated. The timeout period may be set in 2.5 mS increments to over 160 seconds.

### 3.9.11 LED INDICATORS

### 3.9.11.1 Received Signal Strength Indication. RXSIG LED

In all operation modes of the modem except "Programmer Mode" (see section below on special modes of operation), the RXSIG LED indicates the level of the RSSI signal from the radio IF strip, compared to a threshold set in the configuration data read from the non-volatile memory. If the signal is above the threshold, then the LED indicator is turned on. There is no hysteresis applied in this process.

### 3.9.11.2 Data Carrier Detect Indication. SYNC LED

In "Synchronous" operation mode (V2.1.x), prior to modem hardware revision "D", and firmware revision "V2.1.4", the SYNC LED is superfluous and not driven.

Note that firmware revision V2.1.5 onwards should only be used in SYNC mode.
From modem hardware Revision D onwards, the SYNC LED drive is used to generate a DCD function in the user interface connector, and requires firmware revision V2.1.4 onwards (i.e. firmware revision V2.1.4 onwards drives the SYNC LED ON 20 mS after the "leading edge" of the RxSig LED).

This means that the SYNC LED drive should always show this function and not be. allowed to show low Tx Power (see Error indication modes section 3.8.5.2). To facilitate this the Min Tx Pwr parameter in the TC-900DR modem should be set to zero, when the modem is built for synchronous operation.

### 3.9.11.3 Radio Transmitter Active Indication. TXMIT LED

This LED indicator is connected directly to the modem's PTT output drive. It is illuminated whenever the PTT line to the radio board is active.

### 3.9.12 SPECIAL MODES OF OPERATION

### 3.9.12.1 Programmer Mode

Part of the power-up/reset initialisation phase of the modem, are tests to determine whether the modem should enter a special operation mode. The first, is a test for "Programmer Mode". Pin6 on the DB9 connector of Port A, is normally the DSR line. To this end, this pin is pulled high by a resistor to +13.8 v , so that to a connected DTE this signal says that this DCE is ready. However, if this pin is connected to pin5 (Com) when the modem is powered up, the modem senses this, and attempts to enter "Programmer Mode". The modem sends out of PORTA, an ASCII "?" (question mark) character, and waits for the programmer to reply with a password. Failure to supply the correct password in time, will cause the modem to abandon the "Programmer Mode" attempt, and go on with it's normal power-up procedure. This password protection scheme provides some defence against unauthorised tampering with the radio/modem's configuration data.

### 3.9.12.2 Bit Error Rate Test Mode

The next test, is one for "Bit Error Rate Test Mode". Pin9 of the DB9 connector of Port A, is normally the Ring Indicate output line. The modem includes a resistive pulldown to Gnd to show a negative condition on this line. However, if this pin is driven positive (typically by connecting it to pin6), then the modem's data transmitter and receiver will enter the BER test mode. It will activate the RF transmitter and generate a scrambled bit pattern which should be decoded at a receiver as a constant logic "1" level in the unscrambled data. A test point on the modem PCB, is available to monitor this point with
a frequency/event counter. (In fact this test point is always active, and may be used to monitor the received data decoded by the modem IC). Each error bit in the decoded bitstream, will be " 0 ", and the receiver portion of the modem in this mode, will activate the SYNC LED every time it sees a "0" bit. An internal timer is used to generate a time equivalent to 1000 bits. Every error bit detected, will activate the SYNC LED, and restart the timer. If and when the timer expires, the SYNC LED is deactivated. Thus, for error rates of 1 in $10^{3}$ and above, the SYNC LED will be ON most of the time. A 1 in $10^{4}$ error rate will show the SYNC LED active for approximately $10 \%$ of the time. This function provides a crude indication of Bit Error Rate for installation purposes. Other functions performed in this state include RXSIG indication, and temperature compensation. The state of pin9 is constantly monitored in this mode. If the pin ceases to be driven positive, then the BER Test mode is terminated, and the modem restarts it's initialisation phase.

### 3.9.12.3 Order_Wire/Handset Mode

Failure of the BERT Mode test, brings the modem to test for the presence of a handset plugged into the handset audio port. This is done by measuring the voltage on channel 4 of the analogue to digital converter. If a handset is plugged in, then the measured voltage will be about 2 volt, but if it isn't installed, then the voltage will be about 4 volt. The measured voltage is compared to 3 volt to determine whether the handset is plugged in. If this test succeeds, then the modem will not generate a data waveform to the radio transmitter. However, it will continue to indicate received RF signal strength, and perform temperature compensation. The handset has a PTT button, and this signal is connected across the modem's PTT output. Thus the handset PTT switch will activate the TXMIT LED.

### 3.9.12.4 Error Indication Modes

There are three error conditions that will cause the RXSIG and SYNC LEDs to be used for error indications and not their normal purpose. Two of these are "fatal" conditions, that cause the modem to restart after the duration of the error indication phase.

### 3.9.12.5 Transmit Power Low

While the modem activates the radio transmitter, it periodically checks the level of the radio transmitter output power. If the power measurement is less than a threshold set in the non-volatile memory, then the RXSIG and SYNC LEDs are made to alternate, approximately four times per second. Of course, the TXMIT LED will also be on in this case. This indication condition will persist for the duration of the transmission. As soon as the transmission is discontinued, the error indication will cease, and the two LEDs revert to their normal function. The user should be aware that from Revision D of the modem PCB, this state will cause incorrect operation of the DCD output line. As stated above, the Min Tx Pwr parameter should be set to zero.

### 3.9.12.6 NVRAM Read Error

The modem accesses the non-volatile memory as part of it's initialisation phase, to get configuration data. If the communication protocol with the memory device is violated, or the non-volatile memory CRC checksum is found to be incorrect, then the modem indicates this by flashing the RXSIG and SYNC LEDs twice alternately. That is, one LED winks on and off twice, then the other. A total of five cycles of this occurs, then the modem restarts it's initialisation from scratch.

### 3.9.12.7 Radio Frequency Synthesiser, Lock Detect Error

If at any time during normal operation, BERT mode, or handset mode, the frequency synthesiser indicates an out of lock condition, the modem enters an error indication mode for a short time before restarting. One LED is turned ON, the LEDs are swapped, then both off. Then the latter LED ON again, swap LEDS, and OFF. This will give the appearance of a sweeping motion between the LEDs. The following table shows all three modes for comparison.

| Tx PWR Error |  | NVRAM Error |  | TBB206 Error Synthesiser |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RXSIG | SYNC | RXSIG | SYNC | RXSIG | SYNC |
| 0 | - | 0 | - | 0 | - |
| - | 0 | - | - | - | 0 |
| 0 | - | 0 | - | - | $\bullet$ |
| - | 0 | - | - | - | 0 |
| 0 | $\bullet$ | - | 0 | 0 | - |
| - | 0 | - | - | - | - |
| 0 | - | - | 0 |  | repeat |
| - | 0 | - | $\bullet$ |  |  |
| continue |  |  | repeat |  |  |

3.9.13 WIRING ADAPTOR HARNESS FOR TC-900DR SYNCHRONOUS MODEL

| PORT A | 1 (DCD) | (RCO) |  | DB25F |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 (RxD) | (RxD) | 3 |  |
|  | 3 (TxD) | (TxD) | 2 |  |
|  | 4 (DTR) | (DTR) | 20 |  |
|  | 5 (Com) | (Com) | 7 |  |
|  | 6 (DSR) | (DSR) | 6 |  |
|  | 7 (RTS) | (RTS) | 4 |  |
|  | $8 \text { (CTS) }$ | (CTS) | 5 |  |
|  | $9(\mathrm{RI})$ |  |  |  |
| PORT B | 1 (DCD) | (DCD) | 8 |  |
|  | 2 (RxD) | (TCO) | 15 |  |
|  | 3 (TxD) | (TCI) | 24 |  |
|  | 4 |  |  |  |
|  | 5 (Com) |  |  |  |
|  | 6 (DSR) |  |  |  |
|  | 7 |  |  |  |
|  | 8 |  |  |  |
|  | 9 (RSSI) |  |  |  |

## SECTION 4

## ALIGNMENT PROCEDURE

## 4 ALIGNMENT PROCEDURE

### 4.1 GENERAL

This section details operational performance and alignment procedures that may be required for the TC-900DR. During servicing it may also be necessary to measure specific performance parameters as a means of verifying the presence of a fault condition.

### 4.2 TEST EQUIPMENT REQUIRED

The following list of test equipment is required to carry out all of the procedures detailed below.

- Frequency counter accurate to better than 100 Hz at 1 GHz
- FM Signal generator. 455 kHz to $1 \mathrm{GHz} .-120 \mathrm{dBm}$ to +10 dbm .

Synthesised in 100 Hz steps.

- Spectrum analyser 10 MHz to 1 GHz . Dispersion down to $2 \mathrm{kHz} / \mathrm{cm} .80+$ dB dynamic range. IF b/w down to 1 kHz .

RF Power meter to 1 GHz . -20 to +30 dbm . Accuracy $\pm 0.25 \mathrm{~dB}$.

- Digital volt meter.
- HP3406 RF Millivoltmeter or similar.
- RF Test leads, MCX male and SMA male.
- Audio noise and distortion test set.
- Audio oscillator.
- Surface mount repair tools.


### 4.3 TEST POINT LOCATIONS

Both the radio section PCB and the modem section PCB contain numerous test points. They are easily located on the PCB's, and are detailed below.

### 4.3.1 MODEM SECTION PCB

| TEST POINT |  | SIGNAL |  |
| :--- | :--- | :--- | :--- |
| TP1 |  | DESCRIPTION |  |
| TP2 |  | TXCLK |  |
| TP3 | BER TST |  | Transmit clock |
| TP4 | SYNC |  | Synchronised output |
| TP5 | RxCLKOUT |  | Integrator reset |
| TP6 | RxCLK | Receive clock |  |
| TP7 | RxDATA | Receive data |  |
| TP8 | DATA OUT | Transmit data |  |
|  | INTEGRATOR | Rx integrator reset |  |

### 4.3.2 RADIO SECTION PCB

## TEST POINT SIGNAL DESCRIPTION

FINAL PA SECTION

TP31
TP25
TP27
TP14
TP15
TP20
TP28
TP29
TP26
TP33
TP30

TXPWR-2 Bias to Q8
TXPWR-3 Bias to Q8
TXPWR-4 Bias to Q9
+8v Power Supply
TXEN Transmit enable
RxMIXOUT Rx mixer bias
TXPA-1 Bias to Q10
TXPA-2 Bias to Q11
+13V8 Power supply
PWR CONT Power control supply
PTT+8V Press to talk
121 MHz SECTION
TP13 DATA Tx data input
TP17 $\quad 60.5 \mathrm{MHz} \quad$ Modulated 60.5 MHz
TP16 $\quad 121 \mathrm{MHz} \quad$ Output of doubler
TP18 $\quad 121 \mathrm{MHz} \quad$ Modulated 121 MHz
TP32 MIC Tx Mic audio input
NE615 IF SECTION
TP6 $\quad 415 \mathrm{kHz}$ I/P 455 filter input/second mixer output
TP9 QUAD Quad detector
TP8 DATA Rx data out
TP10 AUDIO Rxaudio out
TP7
RSSI RSSI output
TP4 MUTE Mute control output
TP1 2nd L.O Second Xtal oscillator
TP2 2nd L.O Second Xtal oscillator
TP3 IF Input 45 MHz IF filter input
TP5 IF Output $\quad 45 \mathrm{MHz}$ IF filter output
TP19 VCO VCO oscillator injection
SYNTHESISERNCO SECTION
TP12 LOCK DET Synthesiser lock detect
TP11 +5 V Synthesiser +5 v supply

| AUXILIARY HANDSET $\operatorname{INTERFACE}$ SECTION |  |  |
| :---: | :---: | :---: |
| TP21 | MIC | Tx mic audio input |
| TP22 | PTT | Manual press to talk |
| TP23 | +8 V | Handset +8 V supply |
| TP24 | AUDIO OUT | Rx audio output |

### 4.4 ADJUSTMENT POINTS

All adjustment points are located on the radio section PCB. The following is a list of these adjustable components.

| COMPONENT | ADJUSTMENT |
| :--- | :--- |
| XTAL2 | VCO reference frequency |
| VR3 | Deviation level set |
| L10 | Tripler filter |
| L9 | Doubler filter |
| L7 | 121 MHz filter |
| L8 | 121 MHz final filter |
| L6 | Tx frequency set (121MHz Osc) |
| VR4 | Tx power control adjust |
| C78 | Tx mixer tunable filter |
| VR1 | Rx daudio mute adjust BIAS offset adjust |
| VR2 | 45 MHz filter alignment |
| L3 | 44.545 oscillator adjust |
| L1 | 45 MHz filter alignment |
| L4 | 45 MHz filter alignment |
| L5 |  |

### 4.5 LINK OPTIONS

Several options are set in the TC-900DR modem by the setting of links on the radio section PCB. Listed below is an option table for the various combinations.

| LINK NUMBER | SETTING |  | DESCRIPTION |  |
| :--- | :--- | :--- | :--- | :--- |
|  | IN2 |  | AFC option disabled |  |
|  | OUT | AFC option enabled | (factory standard) |  |
|  | LK4 | IN |  | PWR control disable |

### 4.6 HOUSING

The TC-900DR has been designed with the serviceability of the unit in mind. Construction of the unit is robust yet easily dismantled. The unit is primarily assembled in an aluminium extrusion with a central chassis that is fixed to the front panel.

### 4.6.1 DISASSEMBLY PROCEDURE

To disassemble the unit, simply remove the two silver screws on the underside of the unit and the six black screws located on the front panel (the front panel of the unit has the two DB9 connectors protruding from it). Ensure you do not loose the attached nylon washers, as these prevent the Lexan front panel label being damaged upon replacing and tightening the six screws. Simply slide the unit out of the extrusion clasping front panel and the complete unit is exposed to you.

Caution: When re-assembling be careful not to foul the ribbon cable against the case when sliding the unit into its case as this may inadvertently damage the cable.

### 4.6.2 MODEM AND POWER SUPPLY PCB

All components and connections to the modem section PCB are accessible without removing the PCB from the chassis. If access to the rear of the PCB is required, firstly remove two nuts that clamp the $C$ TO-220 power supply regulator to the front panel. Once this is removed, simply remove the four screws securing the PCB to the chassis.

The PCB is now free to work on, and can be folded out so as to service the unit in an open accessible condition whilst still connected to the radio section PCB. If required, the modem section PCB can be separated from the radio section PCB by simply unplugging the ribbon cable.

NOTE: Regulators will need to have heat-sinks fitted if unit is to be operated in this condition for excessive time periods.

### 4.6.3 ANTENNA DIPLEXER

The antenna diplexer is mounted on top of the radio section PCB. It is easily removed by firstly disconnecting the two miniature RF connectors (MCX type) from the PCB.

Care should be taken when unplugging these connectors so as not to damage them, it is important to remove and insert connectors in a vertical direction.

Secondly, remove the nut securing the antenna output connector from the central mounting chassis. The last two remaining screws must be removed which secure the diplexer to two metal PCB standoffs on the radio section PCB. The diplexer can now be removed.

Testing of the radio section PCB can be continued without the antenna diplexer, by connecting to the receiver and transmitter ports separately.

Miniature MCX RF Connectors are available from Trio DataCom if required.

### 4.6.4 RADIO SECTION PCB

The radio section consists of a two sided PCB which has surface mount components on one side and conventional components on the other. Several critical test points are accessible on the component side of the PCB which minimises removal of the PCB from the chassis.

To remove the PCB from the chassis, fifteen screws must be removed. Upon removal of these screws, the PCB can be manoeuvred from the chassis and once again can fold out so as to be serviceable as a complete unit.

NOTE: It is essential that all RF Deck mounting bolts are fitted and secure upon reassembly as many of these bolts provide inter-stage isolation and secure grounding ensuring the product meets all specifications.

Once service of the unit is complete, reassembly is simply the reversal of the above procedures.

Care should be taken when sliding the complete chassis assembly back into the extrusion. Ensure that the ribbon cable connecting the modem and radio section PCB's is carefully "tucked" away within its designated slot so as not to damage the cable.

### 4.7 ALIGNMENT DESCRIPTION

CAUTION - As the TC-900DR is capable of full duplex operation, care should be taken to avoid damage to sensitive test equipment such as signal generators or spectrum analysers. It is recommended that a 30 db 2 Watt pad be connected between the unit and any test equipment prior to testing.

This section is for alignment/adjustment of the RF Deck and should be read in conjunction with Section 2 (Hardware Technical Description) and Section 7 (Fault Finding) if faults or difficulties are experienced.

For initial alignment, proceed in the following order :
Reference oscillator \& synthesiser.
121 MHz Tx modulated injection oscillator.
Tx final stage/Power control.
Receiver and audio mute

### 4.7.1 REFERENCE OSCILLATOR AND SYNTHESIZER

1 Check VCXO (XTAL2) for reference frequency o/p at a level of 550 mV rms with an RF Millivoltmeter, and the VCO o/p for an RF level of around 150 mV rms.

2 Check that the TBB202 dual modulus prescaler (U4) is producing an output of approximately 7 MHz and a level of 550 mV rms at the "IF" $/ / \mathrm{p}$ to the TBB206 synthesiser I.C.(U3-p8)

3 Ensure that the synthesiser has been programmed to a frequency within the range of the VCO, and check that the VCO is locked by observing a high (5V) level on Lock detect output of the synthesiser I.C.(U3-p14). Note that very short duration pulses to ground is normal.

4 Program the synthesiser with the following VCO frequencies according to VCO type and ensure lock occurs at both ends of the frequency range. These frequencies are 2 MHz beyond the published specification.
VCO TYPE: MQC-798
Maximum 786 MHz VCO $=907 \mathrm{MHz}$ Tx or 831 MHz Rx
Minimum 814 MHz VCO $=935 \mathrm{MHz}$ Tx or 859 MHz Rx
VCO TYPE: MQC-978
Maximum $\quad 996 \mathrm{MHz}$ VCO $=875 \mathrm{MHz}$ Tx or 951 MHz Rx
Minimum $\quad 960 \mathrm{MHz}$ VCO $=839 \mathrm{MHz}$ Tx or 915 MHz Rx
5 Program the VCO to a given frequency within the range as specified above and measuring the VCO o/p frequency, adjust the 12 MHz (VCXO) reference trimmer to bring the frequency within 250 Hz of the VCO frequency.
Note: Unit is temperature compensated at factory and no field adjustment of Ref. Oscillator is possible. If VCO frequency is not correct $( \pm 1500 \mathrm{~Hz})$, consult factory for service advice.
Note ensure that the VCXO control input is within its active range (1-4 Volts).

6 Check the VCO power o/p by monitoring the Rx mixer bias at TP20, where approximately 200 mVDC should be measured.

7 With a spectrum analyser set to the VCO frequency and a dispersion of about 5 or 10 kHz per cm , check that the reference sidebands are less than -60 dBc in the adjacent channel.

8 Check VTCXO Reference frequency is $F(t x)+121 \mathrm{MHz}$ for 853 remote units or $\mathrm{F}(\mathrm{tx})-121 \mathrm{MHz}$ for master units. If Reference is out by more than $\pm 1.5 \mathrm{kHz}$, drift offset should be applied via the programmer or unit should be returned for factory service. attempting to alter Reference trimmer will void temperature compensation process and should only be done in an emergency and as a temporary measure.

### 4.7.2 121 MHZ MODULATOR

## Note - make sure the transmitter is loaded with a suitable attenuator on the antenna or $T x$ o/p socket before energising

1. For Initial alignment set all coil cores to their nominal positions as per the table below :

Miller coils
L9 5 turns from top of coil can
L10 2 turns
L7 4 turns
L8 5 turns
L6 0 turns
To prevent the final transmitter stages from producing excessive power whilst low level stages are being aligned, it is suggested that the Tx post mixer tunable filter be de-tuned. Energise the transmitter via manual PTT from the auxiliary handset.
2. Tune L7 through L10 for peak o/p. For initial alignment this can be done by monitoring the 121 MHz level at TP18 initially and then at the input to the SBL-1X transmit mixer (U8), where a level of about 75 mV should be measured by an RF millivoltmeter (e.g HP11960).

Typical RF millivoltmeter readings for each stage are :
TP17 $\quad 125 \mathrm{mV}$ RF $=0.25 \mathrm{VDC}$ on HP11960 probe.
TP16 $40 \mathrm{mVRF}=0.06$ VDC on HP11960 probe.
TP18 550 mV RF $=1.0 \mathrm{VDC}$ on HP11960 probe.
$121 \mathrm{MHz} \mathrm{i} / \mathrm{p}$ to mixer $\quad 75 \mathrm{mVRF}=0.13 \mathrm{VDC}$ on HP11960 probe.
Note: The signal at TP17 is present as long as "Tx En" is active. The subsequent test points require PTT to also be active.

If the complete transmit chain is known to be operative then the $121 \mathrm{MHz} \mathrm{o/p} \mathrm{can}$ be peaked by first de-tuning C 78 on the tunable Tx filter until the Tx power o/p is less than 100 mW and then tuning Inductors L.7 to L. 10 for maximum output at the Tx frequency.
3. With the radio section links set for the desired data rate (see link table above), set the peak deviation as per the chart below with VR3, and center frequency to 121.000 MHz with L6. NOTE: THESE ADJUSTMENTS ARE INTERACTIVE. ENSURE ALL COILS ARE SECURE
BAUD RATE DEVIATION LEVEL
$4800 \mathrm{bps} \quad \pm 1.5 \mathrm{kHz}$ peak
$9600 \mathrm{bps} \quad \pm 2.75 \mathrm{kHz}$ peak
4. Note that temperature compensation is applied to the 121 MHz oscillator so attempting to adjust either VR3 or L6 will upset compensation and should only be done as a temporary measure. Return unit to factory for repair if errors $> \pm 500 \mathrm{~Hz}$ are detected.

### 4.7.3 TX FINAL

NOTE: It is essential that all RF Deck mounting bolts are fitted and secure upon reassembly as many of these bolts provide inter-stage isolation and secure grounding ensuring the product meets all specifications.

1 Ensure the 121 MHz Tx injection is operating correctly.
2 Check Q2,4,5,8, are all biased correctly as per the voltage chart. Temporarily disable the Tx power control circuitry by shorting LK4 located on the top side of the board near the ribbon cable.
Energise the transmitter via the manual PTT on the auxiliary handset.
3 Tune the Tx filter tuning capacitor C78 for a peak output power measured at Antenna port or X 4 .

4 With full drive, Q9 driver collector current as seen across TP26//TP27 should be approximately $45 \mathrm{~mA}(100 \mathrm{mVDC})$, and NOT MORE THAN 55 mA ( 120 mVDC ).

5 With full drive at Q9 each final transistor should be drawing around 175 $\mathrm{mA}(385 \mathrm{mVDC})$ as seen across TP26/TP29 or TP28. The output power measured directly at the final connector should be between +32 and +34 dbm without power control.

6 Re-enable the power control circuitry and with the 'Txpwr' control line set at +5 VDC , set VR4 for $+32 \mathrm{dbm}+/-0.25 \mathrm{~dB}$ at the tx o/p socket X 4 . Check that the current in EACH final collector does NOT EXCEED 225 mA .

7 Check with the spectrum analyser that the Tx o/p is free from spurious signals.
Note 1. Prior to the diplexer the VCO level is nominally about -20 dbc.
Note 2. Close in mixing products (less than $+/-30 \mathrm{MHz}$ ) must be greater than 65 db below the carrier, as they are not attenuated by the diplexer filters.

## D.C. Voltages of Radio Section

| RF Output Power set to +32 dbm at X 4 (diplexer input) with 13.8 VDC supply |  |  |  |
| :--- | :--- | :--- | :--- |
| Transistor | Base | Emitter | Collector |
| Q2 | 1.66 VDC | 0.92 VDC | 6.96 VDC |
| Q4 | 1.79 VDC | 1.06 VDC | 6.46 VDC |
| Q5 | 1.80 VDC | 1.08 VDC | 7.51 VDC |
| Q8 | 1.05 VDC | 0.31 VDC | 4.02 VDC |
| Q9 | 0.47 VDC | 0 VDC | 13.35 VDC |
| Q10 | 0.28 VDC | 0 VDC | 13.05 VDC |
| Q11 | 0.29 VDC | 0 VDC | 13.16 VDC |
| Q12 | 7.17 VDC | 7.97 VDC | 7.88 VDC |
| Q1 | 7.29 VDC | 7.97 VDC | 7.91 VDC |
| Q13 | 4.56 VDC | 3.84 VDC | 7.97 VDC |
| Q7 | 1.14 VDC | 0.41 VDC | 6.68 VDC |
| Q6 | 1.13 VDC | 0.40 VDC | 7.52 VDC |
| Q3 | 1.06 VDC | 0.33 VDC | 7.59 VDC |

### 4.7.4 RECEIVER

The receiver section requires little or no alignment once factory aligned.

### 4.7.4.1 No AFC Models (Xtal $1=45.455 \mathrm{MHz}$ )

1 Adjust L1 for 45.455 MHz measured with pickup loop near L1.
2 In emergency adjust coils L3, L4 and L5 for best SINAD at TP8.
3 Adjust audio mute VR1 to mute handset audio at 10dB SINAD
4 Adjust VR2 for 2.0 VDC at TP8 whilst receiving data off-air.

### 4.7.4.2 AFC Models

Monitor 44.545 MHz with pickup at L 1 . Test for $44.545 \pm 1.5 \mathrm{KHz}$
Consult factory for alignment or service information.

## SECTION 5

## INSTALLATION AND COMMISSIONING

## 5 INSTALLATION OVERVIEW

All Data Radio Modem devices needs to be properly installed and commissioned in order to function reliably. It is important that installers are familiar with RF products / installations and are geared up with appropriate tools necessary to confirm the ongoing reliability of a communications system.

This chapter is intended as a short form checklist to ensure such radio devices are installed correctly and that important tests are made and recorded at each site for future reference should a problem eventuate.

Installers should check that each data radio has been programmed to suit their specific requirements before installation.

### 5.1 GENERAL

Installations play a critical role in network performance. Although this is a known fact, installations are often performed poorly or given little regard. It is essential that the installation is performed in a professional manner with careful attention and consideration to the following items :

1. Adequate primary power cable - relative to the length of cable to minimise voltage drop.
2. Shielded data cable between the unit and any external data equipment.
3. Low loss coax used for antenna feed line.
4. Careful termination of RF connectors.
5. A suitable antenna for the requirement.
6. Suitable placement of the antenna.
7. Adequate signal strength from the base station / other radio communications device.

### 5.2 INSTALLATION

The following information should assist when installing and commissioning data radio systems.

### 5.2.1 DATA CONNECTION

In industrial environments connection to any external device should be by shielded data cable with the shield connected to the connector shell to minimise data corruption, and/or radio interference.

### 5.2.2 MOUNTING

The radio modem should be mounted in a cool, dry, and vibration free environment. Mounting of the unit should be in a location providing easy access to screws and all connections.

### 5.2.3 POWER CONNECTIONS

The power required for $5 \mathrm{Watt}(\mathrm{Tx})$ at 13.8 VDC , is typically 2.0 Amps . As the Tx key up current is significant, the gauge of primary power wiring should be considered. It is suggested that a minimum of 18 gauge stranded copper wire be used for distances of up to two metres and a minimum of 14 gauge for longer distances up to 5 metres.

Ensure correct polarity to avoid costly repairs.

### 5.2.4 COAX CABLE CONNECTION

It is important to select the correct cable and connectors for each application as a poor selection can seriously degrade the performance of the unit.

As an example, for each 3 dB of cable and connector loss, half the transmitter power is lost and twice the receiver signal power is required to produce the same bit error rate.

In some installations where strong signals are present, a compromise of cable and connector cost may be acceptable.
It is essential that all connector terminations are performed as per the manufacturers specifications (especially at 900 MHz and above) and if connectors are to be used outside, it is essential that a sealant such as amalgamating tape be used to seal connectors. DO NOT use acetic cure silicon to seal the connectors.

It is also important that coax cables are not stressed by tight bends, kinking or excessive flexing. Ensure that coax cables have sufficient strain relief and are secure. If large diameter rigid or semi rigid cable is used, it is recommended to use a short length of high quality RG58 or RG223 cable between the unit and main cable feed.

The following chart is a guide to losses in various types of coaxes at 400 MHz and 900 MHz over distance, please consider this when installing the unit.

| CABLE TYPE | LOSS RELATIVE TO DISTANCE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 dB |  | 3 dB |  | 6 dB |  | $9 d B$ |  |
|  | 450 MHz | 900 MHz | 450 MHz | 900MHz | 450 MHz | 900 MHz | 450 MHz | 900 MHz |
| RG58C/U | 2.3m | 1.6m | 7 m | 5 m | 14m | 10 m | 20m | 15m |
| RG223/U | 3.1 m | 2.3m | 9 m | 7m | 18m | 14m | 28m | 21m |
| RG213/U | 6.1 m | 4 m | 18m | 12m | 37m | 24m | 55m | 37m |
| $\begin{aligned} & \hline \text { HELIAX } \\ & \text { LDF4-50A } \\ & \hline \end{aligned}$ | 19m | 14m | 57m | 43m | 114m | 87m | 171m | 130m |
| $\begin{aligned} & \mathrm{HELIAX} \\ & \text { LDF5-50A } \\ & \hline \end{aligned}$ | 38m | 25m | 114m | 75m | 229m | 150m | 343 m | 225m |

### 5.3 ANTENNA INSTALLATION

The selection of antennas and their placement is one of the most important factors when installing a radio based network. People often use a simile, it is like putting square wheels on a Mercedes Benz..... very true comparison.

Antennas are generally mounted to a vertical pole with either vertical or horizontal polarisation as per the licence requirement.

Antennas should be mounted as high as practical and away from metal surfaces which can cause reflections.

Determining the type of antenna is very important and as a typical generic example, Point to Multipoint (PTMP) systems generally employ high gain ( 3,6 , or 9 dB gain) omni directional antennas at the base station sites and either omni directional whips (unity gain) or preferably high gain directional yagi antennas ( 9 or 14 dB gain) at the remote sites.

### 5.3.1 YAGI ANTENNAS

Yagi antennas not only provide signal gain and directivity, but also provides protection from interfering signals which are outside the beam width of the antenna. Yagi antennas are essential when communicating over very long distances.

Yagi antennas are polarised and must be mounted either vertically (elements pointing from the ground to the sky) or horizontally (elements in parallel with the horizon).

As a general rule, Point to Multipoint remote units are vertically polarised, while Point to Point links are horizontally polarised.

When mounting yagi antennas with vertical polarisation, it should be noted that the dipole (loop section of antenna) has a drain hole. The small drain hole on one end of the dipole must be pointed towards the ground so that water will drain out of the antenna.

### 5.3.2 OMNI DIRECTIONAL ANTENNAS

Omni directional antennas provide a radiation pattern of equal strength through $360^{\circ}$ in the horizontal plane. This makes them ideal for base antennas in point to multipoint systems because they can reach the remote antennas.

Omni directional antennas are also used at remote sites (although yagi antennas are preferred) and are typically ground independent "whip" type antennas. The main reason for using whips at remote sites is for aesthetics as they are far less obtrusive than a yagi.

Regardless of the type, antennas need to be mounted properly and in a suitable location as covered below.

### 5.3.3 ANTENNA PLACEMENT

Antenna placement is of paramount importance and plays a big part of the antennas and in turn systems performance.

When choosing antenna locations the aim is to find the largest path of unobstructed space and locate the antennas within that space. It is important to locate antennas as high as possible and definitely clear of any moving obstructions.

Where possible it is important to avoid mounting antennas:

1. Against or adjacent to steel structures.
2. In an area which will have constant intermittent obstructions - people walking past, vehicles driving past etc. That is, mount antennas well above such moving obstructions.
3. Near any electrical equipment.
4. Near metal beams, structures etc
5. Inside any metal enclosures, tin sheds / warehouses etc. - note meshed wire fences act like a "brick wall" to RF transmissions.
6. Away from guard rails or support beams.

Note: Sometimes installations in such environments are unavoidable and where this is the case, certain care can be taken to still ensure a reliable installation. Please consult Trio for assistance on a case by case basis.

If tests indicate poor signal strength then the antennas at one or both ends of the link should be raised, and/or moved clear of obstructing objects, or if directional antennas are employed they should be checked for correct directional orientation and polarisation (horizontal or vertical signal orientation).

### 5.3.4 REFLECTIONS AND OUTPUT POWER

Ideally, the propagation path should be clear Line of Site (LOS).
The biggest problem with UHF radio when used within "steel" buildings or obstructed paths is the large presence of signals randomly reflected from the surrounding obstructions or "steel" walls. These signals cannot be eliminated, but by maintaining a 10 to 20 dB margin between the wanted and unwanted signals, problems should not be experienced. The simplest way to do this is to use directional gain antennas.

These antennas will provide attenuation to all signals arriving from a direction other than the direct path. Where steel walls or structure exist immediately behind the antenna location, the high front to back ratio of such antennas will negate such high level reflections. Power output should be set at the minimum level required to achieve a 25 dB fade margin, in order to minimise the amount of RF being reflected, and to avoid saturating the receiver front end and therefore reducing the margin between wanted and unwanted signals.

### 5.4 COMMISSIONING - RSSI LEVEL

When commissioning a data radio network, it is important to ensure that the incoming received signal strength (RSSI) is adequate to provide reliable communications.

Note: A good signal path should allow for approximately $30 d B$ fade margin.
Received signal strength (RSSI) of the incoming signal is available as an analogue output on Trio data radio modems. This RSSI output ranges from 0 to approx 4 Volts, where 4 Volts indicates the strongest signal. The actual values of received signal strength can be determined by comparing the output voltage against the calibrated graph supplied in the handbook.

By referring to the RSSI chart alignment of aerials can be optimised to achieve the greatest signal strength (highest output voltage).

Note: Be sure to stand clear of aerials when measuring this output voltage, touching or standing in close proximity to aerials will give inaccurate readings.

### 5.4.1 CHECKING DATA COMMUNICATIONS

If the host computer and remote equipment are capable of performing data integrity tests then connect the host and terminal data equipment to the radio modems.

Remove and re-apply power to each radio modem to ensure they are both in data comms mode, and run data tests on the link.

### 5.4.2 BIT ERROR RATE (BER) TESTING

If the connected data equipment is NOT capable of running data integrity tests then the TC-4500S modems can be put into a BER test mode, whereby the data channel can be tested in each direction to a reasonable level without external test equipment. To run a link test with the radio modems themselves, they must BOTH be put into BER test mode.

To place the unit in BER mode connect pin 6 and pin 9 of port A together and apply power..

The transmitter can be activated by driving the RTS pin (7) of port A positive. The unit will then send a predefined pseudo random sequence which is tested for accuracy by the receiving unit and any errors displayed on the front panel 'SYNC' lamp.

Each error bit will illuminate the lamp for approximately 1000 bits duration, therefore error rates above 1 in 1000 will show an almost constant error indication.

To return the unit to normal data transmission mode simply power it up without pin 9 connected to pin 6.

For further information on radio path problems please contact Trio DataCom for detailed advice.

Note : BER testing is not viable in an operational point to multi-point environment as the $B E R$ test will interfere with other operative units.

### 5.4.3 OUTPUT POWER - VSWR

Upon installation of equipment an output power measurement should be done using a suitable power meter. Forward and reflected power should be measured at the antenna port and recorded for future reference. The reflected power measurement should be as a minimum $3: 1$ of the forward power. If this is not the case, investigate possible causes such as poor terminations, faulty antenna etc.

### 5.4.4 DATA CONNECTION

The data connection is via a DB9 connector labelled 'Port A', which is wired as a DCE as shown below. The port labelled 'Port $B$ ' is not used for the standard configuration but can be enabled by the programmer for use as a totally independent second data channel. In industrial environments connection to the modem should be by shielded data cable with the shield connected to the connector shell to minimise data corruption, and radio interference.

- User Serial "Port A" Pin Assignment

PIN NO. \& FUNCTION
EXTERNAL VIEW OF 'PORT A'

1. DATA CARRIER DETECT (DCD)
2. RECEIVE DATA OUTPUT (RXD)
3. TRANSMIT DATA IN (TXD)
4. DATA TERMINAL READY (DTR)
5. COMMON (COM) $\qquad$
6. PROGRAM PIN (PGM)
7. REQUEST TO SEND (RTS)
8. CLEAR TO SEND (CTS)
9. BIT ERROR RATE PIN (BER)

NOTE: Pin 6 and pin 9 provide a dual function which depends on the mode that the $T C-450 D R$ is operating in.

## - User Serial "Port B" Pin Assignment.

Port B of the TC450DR is essentially unused in its standard configuration but can be enabled by the Programmer for use as a totally independent second data channel. This port is essentially used for specific applications and only has one connection that may be of use for installation purposes. This connection (Pin 9) is Receive Signal Strength Indicator (RSSI) output.

This RSSI output ranges from 0 to 5 Volts, where 5 Volts indicates the strongest signal. It is important to note that this Port output has a high impedance of around 10 K ohms and loading will decrease accuracy of the recorded measurement.

PIN NO. \& FUNCTION

1. DATA CARRIER DETECT
2. RECEIVE DATA O/P (RxD)
3. TRANSMIT DATA OIP (TxD)
4. DATA TERMINAL READY (DTR)
5. COMMON
6. DATA SET READY (DSR)
7. REQUEST TO SEND (RTS)
8. CLEAR TO SEND (CTS)
9. RECEIVE SIGNAL STRENGTH

EXTERNAL VIEW OF `PORT B'


### 5.5 GENERAL CHECKLIST

The following is a simple commissioning checklist which should be used at every site not only to ensure correct installation, but also as a reference list for problems which may eventuate.

| TRIO SITE COMMISSIONING CHECK LIST / RECORD |  |  |
| :--- | :--- | :--- |
| Company: | Operator: |  |
| Site Location: | Date: |  |
| Link to: | Serial \#: |  |
| Radio Type: | Config File Name: |  |
| Antenna Type / Gain | Path Distance |  |
| Tx Power at Radio | Measured RSSI Volts |  |
| Reflected Power | Fade Margin |  |
| VSWR | Line of Site to Base |  |
| Tx Power at Antenna | DC volts at Radio (Tx) |  |
| Site QA Inspection: |  |  |
|  |  |  |
|  |  |  |
| Notes: |  |  |
|  |  |  |
| Signed |  |  |

## SECTION 6

## FAULT FINDING

## 6 FAULT FINDING

This section is to assist with difficulties that may be experienced when installing or working on the TC-900DR.

### 6.1 MODEM/GENERAL

The following is a list of possible problem areas, and suggested checks that can be made to isolate any general problem that may have occurred.

1. POWER SUPPLY
a) Check for +13.8 Volts at supply input.
b) Check fuse on Modem PIS PCB (1 Amp SLO-BLOW).
c) Check supply volts:

Modem PIS i) 13.8 Volts
ii) 8 Volts
iii) 5 Volts

RF Deck i) 13.8 Volts
ii) 8 Volts
iii) 5 Volts
2. ANTENNA
a) Check antenna, cable and connectors for damage or water
b) Check forward and reflected power at antenna connector of unit.

VSWR should be <= 1.5:1
3. PROGRAMMING

Check programming information. e.g.
i) Transmit and receive frequencies are within the operating band of the unit
ii) User interface configuration.
4. INTERFACE
a) Check connections to Port A (DB9 Connector).
b) Check cable to host communications.
c) Interface commands to unit are incorrect or communications are not established correctly.
5. POOR TRANSMITTER PERFORMANCE
a) Check correct transmit frequency programmed.
b) Check transmitter carrier frequency.
c) Check transmitter deviation.
d) Check RF output power level.

## 6. POOR RECEIVER PERFORMANCE

a) Check correct receive frequency programmed.
b) Check receive sensitivity.
c) Check audio output level and DC bias to modem.
d) Check mute threshold.

### 6.2 RECEIVER

The following is a list of problem areas, and suggested checks that can be made to isolate any receiver specific problems that may have occurred.

### 6.2.1 RECEIVE SENSITIVITY LOW

1 Check mixer drive level by measuring DC bias developed across R27.
2 Check for correct DC bias conditions and supply volts on RF Amp, Local Osc buffer, and IF Strip, compared to voltage charts.

3 Ensure 44.545 MHz oscillator (part of NE615 IF IC) is within $\pm 250 \mathrm{~Hz}$. This is best carried out by using a communications test set such as an IFR1200 or similar in receiver mode with frequency error displayed.

4 Ensure that the local oscillator is netted to frequency by monitoring the Tx mixer injection with a pick up loop connected to a sensitive frequency counter of high stability. Adjust the VCXO frequency reference until correct L.O. frequency is observed. Note that the VCO and synthesiser use the VCXO as the frequency standard. Measure the Synthesiser LOCK signal to ensure the VCO is in phase lock.

5 With a 50 ohm signal generator tuned to 455 kHz , apply signal via a 1 nF capacitor to the inputs of the 1st and second IF Amp sections of the 615 IF IC and compare the level required to produce the correct RSSI level.
6 With a 50 OHM signal generator tuned to 45.000 MHz , apply signal to the points defined on the IF test chart and compare RF level required to produce the reference RSSI level as specified at TP4.

7 Apply signal frequency to the RF input connector at X2 and compare the level required to produce RSSI reference level at TP4 with that shown in the IF Level Chart.

8 Reconnect the Antenna Diplexer and apply the signal generator to the Antenna terminal of the diplexer. Adjust the generator level to provide the same Rx mixer bias from applied RF signal as was noted in 7) above. The level required should be no more than 3 dB ( Rx diplexer path loss) greater.

Note that the RSSI signal provided by the IF IC is a fairly accurate logarithmic scale between 0.5 and 4 VDC , providing about 0.5 VDC for each 10 dB of signal applied to the input of the IF Strip, and can be used as a reasonable measure of signal providing it is unmodulated and on center frequency at 455 kHz .

### 6.2.2 RECEIVER LEVEL CHART

The following chart lists the level (terminated) of a 50 OHM signal generator to produce 2.0 VDC of RSSI at TP4 when applied as specified to the point shown and at the frequency indicated.

| FREQUENCY | CONNECTION POINT AND APPLICATION | NOM LEVEL |
| :--- | :--- | :--- |
| 455 kHz | Pin 20 of IC U2 NE615 via 1 nF | -72 dBm |
| 455 kHz | Pin 18 of IC U2 NE615 via 1 nF | -74 dBm |
| 455 kHz | Pin 1 (i/p) of IF Fitter CF2 via 1 nF | -58 dBm |
| 455 kHz | Pin 14 of IC U2 NE615 via 1 nF | -43 dBm |
| 45 MHz | Rx i/p at X2 via coax direct | -49 dBm |
| 45 MHz | Mixer i/p following R.F. Amp | -62 dBm |
| 45 MHz | Mixer diode (D1) o/p across C100 | -61 dBm |
| 45 MHz | Junction of 1st \& 2nd 45 MHz crystal filter | -77 dBm |

### 6.3 TRANSMITTER

The following is a list of problem areas, and suggested checks that can be made to isolate any transmitter specific problems that may have occurred.

## 1. NO TRANSMIT

1. Check PTT circuit.
2. Check unit is programmed within its operational range.
3. Check if manual PTT (Rear Aux connector) keys transmitter.
4. Check if any transmitter output is present. Tuning required?

## 2. TRANSMITTER SPURIOUS EXCESSIVE

The probable cause is dependent upon the nature of the spurious as follows:
Carrier $\pm 910 \mathrm{kHz}$. - IF detector signal $(2 \times 455)$ modulating or mixing with carrier. Check 1 n bypass on reference $\mathrm{i} / \mathrm{p}$ to power control op-amp. Check bypasses on collectors and supply lines of low level transmitter stages, and L.O. buffer.

Carrier $\pm 20.166$ and/or 40.333 . - Excessive harmonics of 20.166 crystal oscillator in 121 MHz FM driver IC (U7). Check all pins of IC (U7) for correct DC conditions. Check all tuning inductors for 'normal $Q$ ', as 'soft' tuning will almost surely indicate an incorrect or faulty capacitor, or inductor.

Carrier $\pm$ VCXO reference frequency (approximately 7 MHz ). - Reference signal modulating VCO, or mixing with carrier in L.O.buffers. - Check Synthesiser supply bypasses, check for defective joints or components in and around the resistive divider at output of VCO.

Note that it is imperative that low frequency divider products be attenuated before they can reach the base/emitter junctions of the L.O. buffer transistors where they can mix with the VCO frequency.

Note also that poor SMD solder joints will provide nonlinear conductance and give rise to frequency mixing in this area. Check for faulty components or poor joints around the Synthesiser to VCO frequency control area, or VCO supply line bypassing.

Excessive Transmitter power radiated or conducted to the area of the VCO can also cause spurious effects and may enhance the levels of otherwise acceptable levels of spurious. If this is suspected, check that ALL chassis securing bolts are fitted and tight on the RF deck, and that ALL bypass capacitors and chokes are fitted and correct in and around the final Tx stages.

## 3. TRANSMITTER POWER LOW OR UNSTABLE :

1 Firstly - Ensure that ALL RF Deck mounting bolts are fitted and secure.
2 Check that the feed resistors used for current indication on all stages of the final are of correct value and firmly in circuit.

3 Check that the Tx L.O. buffer and post mixer buffers are correctly biased as per the voltage charts.

4 If necessary disconnect the final stages from the Tx post mixer buffers by removing the solder bridge between Q5 and Q8, and with an appropriate instrument measure the RF power available from the Tx buffers to the final pre-driver.
Note that the o/p impedance of the buffer is 50 OHM and must be measured by a 50 OHM instrument. It is highly recommended that a measuring spectrum analyser be used here as this instrument will also display the relationship between the wanted signal and other spurious or unwanted mixing products.
The nominal display seen at this point by a spectrum analyser is shown on the spectrum charts attached.

5 To test the final stages separate from the buffers - inject a signal from a 50 OHM generator at Tx frequency into pre-driver (Q8) via C122. The level required to drive the final to full output is shown on the Tx level chart.

6 Check that the current drawn by the driver transistor as measured across the feed resistor (TP28 to TP27) is within spec, and if not check and or replace the driver transistor or associated components as necessary.

7 Check that the current drawn by each final transistor as indicated by the voltage across the 2.2 OHM ( $2 \times 4.7$ ohm in parallel) collector feed resistors (TP26 to TP28 and TP29) is within the range stated in the voltage charts, and that both are within $10 \%$ of each other. If in error check components around final pair and replace final transistors as necessary.
NOTE it is possible for power transistors to be partly defective due to current or thermal abuse, and the fact that the devices are actually drawing current does not always indicate that they are producing full power at the collector.

## TX LEVEL CHART :

| Frequency | Connection Point \& Application | Level Remarks |
| :---: | :---: | :---: |
| Base band | Data from modem section TP13 (4800 baud) | 2 VD.C |
| Base band | Applied data signal to modulator U7 pin 3 (4800 baud level from modem) | $1 \mathrm{~V}_{\text {p-p }}$ |
| Base band | Audio signal to modulator TP32 | 0.84 VD.C <br> $60 \mathrm{mV}_{\mathrm{p}-\mathrm{p}}$ for VR3 set for maximum value $400 \mathrm{mV}_{\text {p.p }}$ for VR3 set for minimum value |
| Base band | Audio signal to modulator U7- pin 4 | $\begin{aligned} & 1.3 \mathrm{VD.C} \\ & 0.5 \mathrm{~V} \cdot \mathrm{p} \end{aligned}$ |
| 121 MHz | Signal level at TP18:A | -5 dBm |
| Final Tx frequency | Output to diplexer connector X 1 | $3 W$ at maximum power setting |

## SECTION 7

## APPENDIX A

## DRAWINGS

## 7 APPENDIX A DRAWINGS

TC01-08-12 Data Radio Mounting Details
TC01-08-11 Data Radio Assembly Details
TC01-04-05 Data Radio Basic Modem 9K6/4K8 Component Loading Details
TC01-00-05 450DR / 900DR Packet Modem (2 sheets)
TC01-08-10 PWB Manufacturing Details 900DR Data Radio - Radio Board (2 sheets)
TC01-00-10 Data Radio Project Sheet
TC01-00-10 Data Radio Final PA (AFC Fitted)
TC01-00-10 Data Radio 121 MHz OSC (AFC Fitted)
TC01-00-10 Data Radio - Synthesiser - VCO (AFC Fitted)
TC01-00-10 Data Radio - NE6154K8/9K6 (AFC Fitted)
TC01-04-15 850-930 MHz Antenna Diplexer Component Side Assembly
TC01-05-10 Radio Board Top Side (C/S) Test Point \& Adjustment Location Details
TC01-05-10 Radio Board Bottom Side (S/S) Test Point \& Adjustment Location Details

TC01-05-16 Duplex Radio BER/S $+\mathrm{N} / \mathrm{N}$ vs Sig
TC01-05-17 AFC Alignment Setup - Block Diagram
TC01-05-12 4800/9600 BPS Modem Functional Diagram
TC01-05-23 Asynchronous Modem Functional Diagram
TC01-05-19 Macro Block Diagram
TC01-05-18 Radio Section - Modem Section Interface
DR9-BLOK 900 MHz Radio Block Diagram
RSSI Level cf Received Signal (typical)

## SECTION 8

## APPENDIX B

## GLOSSARY of TERMS and ABBREVIATIONS

## 8 APPENDIX B GLOSSARY

ADC: Analogue to digital converter.
AFC: Automatic frequency control.
BER: Bit error rate.
bps: Bits per second.
C/DSMA: Carrier or data sense, multiple access scheme.
COM: Common.
CRC: Cyclic redundancy checksum.
CTS: Clear to send.
DAC: Digital to analogue converter.
DCD: Data carrier detect.
DCE: Data communications equipment.
DFM4-9: Trio DataCom digital modem chipset.
DIP: Dual in line package.
DOTAC: Department of Transport and Communications.
DSR: Data set ready.
DTR: Data terminal ready.
FCS: Frame check sequence.
FEND: Frame end.
FESC: Frame escape.
FIFO: First in first out.
FIR: Finite impulse response.

FM: Frequency modulation.
FSK: Frequency shift keying.
GPIB: General purpose interface bus.
HADR_EN: High address enable signal.
$I C: \quad$ Integrated circuit.
I.F.: Intermediate frequency.
$\mathrm{i} / \mathrm{p}: \quad$ Input.
KISS: Keep it simple stupid.
LADR_EN: Low address enable signal.
MSB: Most significant bit.
NVRAM: Non volatile RAM.
NRZ: Non return to zero.
NRZI: Non return to zero - inverted.
o/p: Output.
PCB: Printed circuit board.
PLL: Phase locked loop.
PMP: Point-to-multipoint.
ppm: $\quad$ Parts per million.
PTP: Point-to-point.
PTT: Press to talk.
RF: Radio frequency.
RI: Ring indicate.
R_select: RAM read select signal.
SIO: Serial input/output.
RSSI: Receive signal strength indication.
RTS: Request to send.
Rx: Receive.
RXD: Receive data output.
SCADA: Supervisory control and data acquisition.
SLIP: Serial line interface protocol.

TC-900DR: Trio DataCom 900MHz full duplex data transceiver.
TC-DFM9IP: Trio DataCom TC-900DR parameter programming software suite.
TFEND: Transposed Frame End.
TFESC: Transposed Frame Escape.
TNC: Terminal node controller.
Tx: Transmit.
TXD: Transmit data in.
VCO: Voltage controlled oscillator.
W_select: RAM write select signal

# TECHNICAL DATA SHEET <br> For <br> <br> SEWERAGE PUMP STATION SP144 <br> <br> SEWERAGE PUMP STATION SP144 <br> Lavarack Av \#1 Eagle Farm 

Equipment Type: Impulse Suppressor
Location: RTU Section
Model Numbers: ..... IS-50NX-C2
Manufacturer: Polyphaser
Supplier: Brisbane Water


# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144

 Lavarack Av \# $\mathbb{1}$ Eagle FarmEquipment Type: Radio/DC Converter
Location: RTU Section
Model Numbers: ..... PB1H-2412G-CC
Manufacturer: Powerbox
Supplier: Brisbane Water

## PBIH Series

15-150 WATTS DC/DC SINGLE OUTPUT

## Features

- Wide selection of models
- 4 input voltage ranges
- High efficiency
- Low output ripple
- Proven reliability
- Good thermal margins



| OPERATING |  |
| :---: | :---: |
| Efficiency | 70\%-89\% |
| Safety isolation (1 minute) | Type - 12, 24, 48 V input <br> Input - Output: 1500VAC <br> Input-Case: 1500VAC <br> Output-Case: 500VAC <br> Type- 110 V input <br> Input- Output: 2000VAC <br> Input-Case: 2000VAC <br> Output- Case: 500VAC |
| Insulation resistance | 50M (500VDC) Input - Case |
| Parallel operation | Consult sales office for details |
| Remote control | PBIH-R Series: Open link: output normal Short link: output off |
| ENYIRONAENTAL |  |
| Operating temperature | $0^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ full load |
| Cooling | Convection cooled |
| Storage temperature | $-20^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Humidity | 85\% |
| Shock | 30G, PBIH-F, G and J |
| Vibration | ( $5 \mathrm{~Hz}-10 \mathrm{~Hz}, 10 \mathrm{~mm}$ ). <br> ( $10 \mathrm{~Hz}-50 \mathrm{~Hz}$ ) 2G, PBIH-F, G and J |
| STANDARDS AND APPROUALS |  |
| Safety | Designed to UL1950 |
| C.tick | AS/NZS CISPR11 Group 1, Class A |
| MECHANICAL |  |
| Weight | PBIH-F : 250g <br> PBIH-G: 380g <br> PBIH-J:410g <br> PBIH-M : 800g <br> PBIH-R : 1.4 kg |

## PBIH Series

## 15-150 WATTS DC/DC SINGLE OUTPUT

## Selection Table

| MODEL NUABER | INPUT | OU | PUT | OUTPUT POWER |
| :---: | :---: | :---: | :---: | :---: |
| PBIH-1205F | $9.2-16 \mathrm{~V}$ | 5 V | 3A | 15W |
| PBIH-1212F | $9.2-16 \mathrm{~V}$ | 12 V | 1.2A | 15W |
| PBIH-1215F | $9.2-16 \mathrm{~V}$ | 15V | 1A | 15W |
| PBIH-1224F | 9.2 -16 V | 24 V | 0.62A | 15W |
| PBIH-2405F | 19-32V | 5 V | 3A | 15W |
| PBIH-2412F | 19-32V | 12 V | 1.2A | 15W |
| PBIH-2415F | 19-32V | 15 V | 1A | 15W |
| PBIH-2424F | 19.32 V | 24 V | 0.62A | 15W |
| PBIH-4805F | 38.63 V | 5 V | 3A | 15W |
| PBIH-4812F | 38-63V | 12 V | 1.2A | 15W |
| PBIH-4815F | 38.63 V | 15 V | 1A | 15W |
| PBIH-4824F | $38-63 \mathrm{~V}$ | 24 V | 0.62A | 15W |
| P8IH-11005F | 85-140V | 5 V | 3A | 15W |
| PBIH-11012F | 85.140 V | 12 V | 1.2A | 15W |
| PBIH-11015F | 85.140 V | 15 V | 1A | 15W |
| PBIH-11024F | 85.140 V | 24 V | 0.62A | 15W |
| PBIH-120SG | $9.2 \cdot 16 \mathrm{~V}$ | 5 V | 5A | 25W |
| PBIH-1212G | $9.2-16 \mathrm{~V}$ | 12V | 2.1 A | 25W |
| PBIH-1215G | 9.2-16V | 15 V | 1.7 A | 25W |
| PBIH-1224G | 9.2 -16V | 24 V | 1.1A | 25W |
| PBIH-1248G | 9.2 -16V | 48 V | 0.5A | 25W |
| PBIH-2405G | 19-32V | 5 V | 5A | 25W |
| PBIH-2412G | 19-32V | 12 V | 2.1 A | 25W |
| PBIH-2415G | 19-32V | 15 V | 1.7 A | 25W |
| PBIH-2424G | 19-32V | 24 V | 1.1A | 25W |
| PBIH-2448G | 19.32 V | 48 V | 0.5A | 25W |
| PBIH-4805G | $38-63 \mathrm{~V}$ | 5 V | 5A | 25W |
| PBIH-4812G | 38.63 V | 12 V | 2.14 | 25W |
| PBIH-4815G | $38-63 \mathrm{~V}$ | 15 V | 1.7A | 25W |
| PBIH-4B24G | 38-63V | 24 V | 1.1A | 25W |
| PBIH-484BG | 38-63V | 48 V | 0.5A | 25W |
| PBIH-11005G | $85-140 \mathrm{~V}$ | 5 V | 5A | 25W |


| MODEL NUMBER <br> PBIH-11012G | INPUT$85-140 \mathrm{~V}$ | OUTPUT |  | OUTPUTPOWER25W |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 12 V | 2.1A |  |
| PBIH-11015G | $85-140 \mathrm{~V}$ | 15 V | 1.7 A | 25W |
| P81H-11024G | $85-140 \mathrm{~V}$ | 24 V | 1.1 A | 25W |
| PBIH-11048G | $85-140 \mathrm{~V}$ | 48 V | 0.5A | 25W |
| PBIH-1205J | $9.2-16 \mathrm{~V}$ | 5 V | 8A | 50W |
| PBIH-1212J | $9.2-16 \mathrm{~V}$ | 12 V | 3.3A | 50W |
| PBIH-1215J | $9.2-16 \mathrm{~V}$ | 15 V | 2.7A | 50W |
| PBIH-1224J | $9.2-16 \mathrm{~V}$ | 24 V | 1.7A | 50W |
| PBIH-1248J | $9.2-16 \mathrm{~V}$ | 48 V | 0.8A | 50W |
| PBIH-2405J | 19-32V | 5 V | 10A | 50W |
| PEIH-2412J | 19-32V | 12V | 4.3 A | 50w |
| PBIH-2415J | 19.32V | 15 V | 3.4A | 50W |
| PEIH-2424J | 19-32V | 24 V | 2.5A | 50w |
| PBIH-2448J | 19.32 V | 48 V | 1 A | 50w |
| PBIH-4805J | 38-63V | 5 V | 10A | 50W |
| PBIH-4812J | 38.63 V | 12 V | 4.3 A | 50w |
| PBIH-4815J | 38.63 V | 15 V | 3.4A | 50W |
| PBIH-4824J | 38-63V | 24 V | 2.5A | 50W |
| PBIH-4848J | 38-63V | 48 V | 1A | 50W |
| PBIH-11005J | $85-140 \mathrm{~V}$ | 5 V | 10A | 50w |
| PBIH-11012J | 85-140V | 12 V | 4.3A | 50W |
| PBIH-11015J | $85-140 \mathrm{~V}$ | 15 V | 3.4A | 50W |
| PBIH-11024J | 85.140 V | 24 V | 2.5 A | 50W |
| PBIH-11048J | $85-140 \mathrm{~V}$ | 48 V | 1A | 50W |
| PBIH-1205M | $9.2-16 \mathrm{~V}$ | 5 V | 18A | 100W |
| PBIH-1212M | 9.2 -16V | 12 V | 9A | 100W |
| PBIH-1215M | $9.2-16 \mathrm{~V}$ | 15 V | 7A | 100W |
| PBIH-1224M | $9.2-16 \mathrm{~V}$ | 24 V | 4.5A | 100W |
| PBIH-1248M | 9.2-16V | 48 V | 2A | 100W |
| PBIH-2405M | 19-32V | 5 V | 20A | 100W |
| PBIH-2412M | 19-32V | 12 V | 9A | 100W |
| PBIH-2415M | 19-32V | 15 V | 7 A | 100W |


| HOODEL NUMBER | INPUT | OU | PUT | OUTPUT POWER |
| :---: | :---: | :---: | :---: | :---: |
| PBIH-2424M | 19-32V | 24 V | 5A | 100W |
| PBIH-2448M | 19-32V | 48 V | 2A | 100W |
| P81H-4805M | 38-63V | 5 V | 20A | 100W |
| P81H-4812M | 38.63 V | 12 V | 9 A | 100w |
| PBIH-4815M | 38-6.3V | 15 V | 7A | 100W |
| PBIH-4824M | 38-6.3V | 24 V | 5A | 100W |
| PBIH-4848M | 38-63V | 48 V | 2A | 100W |
| PBIH-I1005M | 85.140 V | 5 V | 20A | 100W |
| PBIH-11012M | 85-140V | 12 V | 9 A | 100W |
| PBIH-11015M | B5-140V | 15 V | 7 A | 100W |
| PBIH-11024M | 85.140 V | 24 V | 5A | 100W |
| PBIH-11048M | 85.140 V | 48 V | 2A | 100W |
| PBIH-1205R | $9.2-16 \mathrm{~V}$ | SV | 27A | 150W |
| PBIH-1212R | 9.2-16V | 12 V | 13A | 150W |
| P81H-1215R | $9.2-16 \mathrm{~V}$ | 15 V | 10A | 150W |
| P8IH-1224R | $9.2-16 \mathrm{~V}$ | 24 V | 6.5 A | 150W |
| PBIH-1248R | 9.2 -16V | 48 V | 3.3A | 150W |
| PBIH-2405R | 19-32V | 5 V | 30A | 150W |
| PBIH-2412R | 19-32V | 12 V | 14A | 150W |
| PBIH-2415R | 19-32V | 15 V | 11A | 150W |
| PBIH-2424R | 19-32V | 24 V | 7 A | 150w |
| PBIH-2448R | 19.32 V | 48 V | 3.5A | 150W |
| PBIH-4805R | 38-63V | 5 V | 30A | 150W |
| PBIH-4812R | 38.63 V | 12 V | 14 A | 150W |
| PBIH-4815R | 38.63 V | 15 V | 11A | 150W |
| PBIH-4824R | 38-63V | 24 V | 7 A | 150W |
| PBIH-4848R | 38.63 V | 48 V | 3.5A | 150W |
| PBIH-11005R | $85-140 \mathrm{~V}$ | 5 V | 30A | 150W |
| PBIH-11012R | $85-140 \mathrm{~V}$ | 12 V | 14A | 150W |
| PBIH-11015R | 85-140V | 15 V | 11 A | 150W |
| PBIH-11024R | $85-140 \mathrm{~V}$ | 24 V | 7A | 150W |
| PBIH-11048R | 85-140V | 48 V | 3.5A | 150W |

PBIH-F


- Dimensions in mm

| terminal No. |  |
| :---: | :---: |
| 1 | $0 \vee(D C$ in $)$ |
| 2 | $+V(D C$ in $)$ |
| 3 | FG |
| 4 | NO Connection |
| 5 | $-V$ out |
| 6 | $+V$ out |

## 圈 PBIH Series

15-150 WATTS SINGLE OUTPUT

| Terminal | Connection |
| :---: | :---: |
| 0 | FG |
| 1 | $D C+V$ in |
| 2 | $O V$ in |
| 3 | LFG |
| 4 | NO |
| 5 | NO |
| 6 | $-V$ out |
| 7 | $+V$ out |

PBIM-J


| Terminal | Connection |
| :---: | :---: |
| 1 | FG |
| 2 | $\mathrm{DC}+\mathrm{V}$ in |
| 3 | OV in |
| 4 | LFG |
| 5 | $-V$ out |
| 6 | $+V$ out |
| 7 | NC |

PBIH-M


| Terminal | Connection |
| :---: | :---: |
| 1 | $+V$ out |
| 2 | $+V$ out |
| 3 | $-V$ out |
| 4 | $-V$ out |
| 5 | FG |
| 6 | $-V$ in |
| 7 | $+V$ in |

PBIH-R


| Terminal | Connection |
| :---: | :---: |
| $\mathbf{1 , 2}$ | $+V$ out |
| 3 | $+S$ |
| 4 | $-S$ |
| 5,6 | $-V$ out |
| 7 | Remote |
| 8 | Control |
| 9 | $D C+V$ in |
| 10 | $D C O V$ in |
| 10 | FG |

# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144

Lavarack Av \#1 Eagle Farm
Equipment Type: Modem/Power Supply
Location: RTU Section
Model Numbers: ..... PB251-24CM-CC-TT
Manufacturer: Powerbox
Supplier: Brisbane Water

## PB251 Series

## 220-330 WATTS DC UPS

## Features

- Ultra-low noise output
- Independent battery charging output
- DC output OK \& battery OK alarms \& LEDs
- Battery-LVD and alarm
- Over-temperature protection
- Battery fuse fail LED


Specifications

| INPUT |  |
| :--- | :--- |
| Voltage: | 190 to 264 vac, or 190 to 400 VDC |
| Line regulation: | $0.2 \%$ typical |
| Current: | 1.4 A maximum |
| Inrush current: | 10 A maximum |
| Frequency: | 45 to 65 Hz |


| Safety | Complies with AS/NZS 60950, class 1, <br> NSW Office of Fair Trading Approval N20602 |
| :--- | :--- |
| EMC | Emissions comply with AS/NZS CISPR11, |
|  | Group 1, Class B. Complies with ACA EMC |
|  | Scheme, Safety \& EMC Regulatory Compliance <br>  <br>  <br>  <br>  <br> Marked <br> solation I/p-o/p <br> V/p-ground <br> o/p-ground |


| ALARMS \& BATTERY FUNCTIONS |  |
| :---: | :---: |
| Converter ON/OK alarm |  |
| green LED | ON=PSU OK |
| Battery low (\& fuse) alarm | 10.2 to 12.6 V for 12 V battery, adjustable 20.4 to 25.2 V for 24 V battery, adjustable Indicated by voltage-free changeover relay contacts \& green LED: ON=BATT OK |
| Low voltage disconnect | 9.6 to 12 V for 12 V battery, adjustable 19.2 to 24 V 2 for 4 V battery, adjustable |
| Charger over-load protection | Auto-resetting electronic circuit breaker |
| Reverse polarity protection | Internal battery fuse |
| Battery to load voltage drop | 0.2 to. 0.25 V typical |
| MECHANICAL |  |
| Case size | $264 \mathrm{~L} \times 172 \mathrm{~W} \times 67 \mathrm{Hmm}$ |
| Case size with heatsink | $264 \mathrm{~L} \times 186 \mathrm{~W} \times 67 \mathrm{Hmm}$ |
| Rack size | $232 \mathrm{D} \times 19^{\text {* }} \mathrm{W} \times 2 \mathrm{RUH}$ |
| Weight | 1.9 kg |
| Weight with heatsink | 2.1 kg |
| Weight (rack mounted version) | 5.5 kg |

## Selection Table

| MODEL <br> NUMBER | OUTPUT |  |  | OUTPUT <br> POWER | Note: Non standard battery charging current available on request. ie PB251-12CM-H-10 for 10A. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | VDC | $\mathrm{I}_{\text {load }}$ | $\mathrm{I}_{\text {Batt }}$ |  |  |
| PB251-12CM | 13.8 V | 16A | 2A | 220W |  |
| PB251-12CM-H | 13.8 V | 20A | 2 A | 275w |  |
| PB251-24CM | 27.6 V | 11A | 2A | 300W |  |
| PB251-24CM-H | 27.6 V | 12A | 2 A | 330W |  |
| PB251-12RML | 13.8 V | 20A | 4A | 275w |  |
| PB251-12B | 13.8 V | 20A | 4 A | 275W |  |
| P8251-24RML | 27.6 V | 12A | 2A | 330W |  |

## PB251 Series

275-330 WATTS DC UPS

Technical Illustrations


PB251-*RML \& -12B MECHANICAL OUTLINE

NOTES:

2 Mountry slots ave ivilatie for Ws hardinare.
3. inper connectur i a a toA Class 1 IfCceszo inter
4. 2 meler IEC mains coed with Autbalan plog is suppled with unit
5. P6251-128 alamm reminal Is 0875 female.
6. PE2S1-128 suqut and tantiery connecier is Hrose pa HS $2 \mathrm{BR}-4 \mathrm{~A}$

1. Mashy connecior s Heve pa HS $28 \mathrm{P}-4 \mathrm{~A}$ (not suppled.
T. PE251, wh Mi alam and outpot terminals are M3. 5 serews
sulable for ting or fork hog sp to 8 mm wide.


FRONT VEW




## Passt-128 alanm CONELCTOA



Your dependable power partner - www.powerbox.corn.au

# TECHNICAL DATA SHEET 

## For

## SEWERAGE PUMP STATION SP144

## Lavarack Av \# $\mathbb{1}$ Eagle Farm

Equipment Type: Level Probe
Location:
Common Control
Model Numbers:020130FSP
Manufacturer: Multitrode
Supplier:
Multitrode Pty Ltd130 Kinston Road
Underwood. QLD 4119Tel: 0733407000Fax: 0733407077

## The MultiTrode Probe

MultiTrode probes are unsurpassed for rugged reliability, cost effectiveness and simplicity. Designed for the tough, turbulent conditions found in water, sewage and industrial tanks and sumps, the probes can be found in the simplest and the most complex water and wastewater management systems around the world.

- Low maintenance
- Simple installation
- Excellent in turbulence
- Short \& long term cost savings
- Environmentally friendly
- Safe, low sensing voltage
- Unaffected by fat, grease, debris and foam
- Positive pump cut-out
- Safe - MTISB Barrier

Reliable in all conditions Operation is unaffected by build up of fat, grease debris and foam, which causes other systems such as floats, bubblers, pressure and ultrasonic transducers to fail. Turbulence does not affect the probe operation. The rugged, streamlined design eliminates tangling and is ideal for confined spaces.

## Positive pump cut-out

Operational consistency is important to longevity, low maintenance and cost control. The positive pump cut-out ensures pumps are turned off at the same level every time. This avoids damage due to pump over run and the cost of additional control equipment.

## Safe for people and environment

The extra low sensing voltage ensures operators and maintenance staff are protected. All Multifrode products are environmentally safe, containing no mercury or other harmful contaminants.

## Cost savings

The low cost of equipment, installation and maintenance makes MultiTrode one of the most efficient level control systems available. Plus robust construction and longevity ensures continued cost savings when compared to other systems on the market.
MULTITRODE

## www.multitrode.com

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## Standard and custom probes

MultiTrode manufactures a wide range of standard probes, from a single sensor ( 200 mm ) to a ten-sensor probe $(1000 \mathrm{~mm}$ increasing to a maximum of nine metres). Custom probes can be manufactured to suit your requirements.

## Installation

Installation is straightforward. Probes are easy to install without entering the wet area. The probe is simply lowered in from the top and suspended by its own cable, using the mounting kit supplied.

## MTAK-1 Mounting Kit (Supplied)

The mounting bracket is a standard accessory supplied with all multi-sensor probes (not standard with $0.2 / 1-\mathrm{xx}$ single sensor probe).
The MTAK-1 mounting bracket has an integral cleaning device. All metal components are stainless steel.


## MTAK-2 Mounting Kit (Optional extra)

This extended bracket provides up to 300 mm extra wall clearance. This bracket is not included as standard with probes.


Ordering Examples and Information

| Model <br> Code | Probe <br> Length <br> $(\mathbf{m} / \mathrm{in})$ | Sensor <br> Separation <br> $(\mathbf{m m} / \mathrm{in})$ | Cable <br> Length* <br> $(\mathbf{m} / \mathrm{ft})$ | Number of <br> Sensors |
| :---: | :---: | :---: | :---: | :---: |
| $0.2 / 1-10$ | $0.2 / 8$ | $\mathrm{~N} / \mathrm{A}$ | $10 / 33$ | 1 |
| $0.5 / 3-10$ | $0.5 / 16$ | $150 / 6$ | $10 / 33$ | 3 |
| $1.0 / 10-10$ | $1 / 40$ | $100 / 4$ | $10 / 33$ | 10 |
| $1.5 / 10-30$ | $1.5 / 60$ | $150 / 6$ | $30 / 100$ | 10 |
| $2.0 / 10-30$ | $2 / 80$ | $200 / 8$ | $30 / 100$ | 10 |
| $2.5 / 10-30$ | $2.5 / 96$ | $250 / 10$ | $30 / 100$ | 10 |
| $3.0 / 10-30$ | $3 / 115$ | $300 / 12$ | $30 / 100$ | 10 |
| $6.0 / 10-30$ | $6 / 224$ | $600 / 24$ | $30 / 100$ | 10 |
| $9.0 / 10-30$ | $9 / 368$ | $900 / 40$ | $30 / 100$ | 10 |

*Cable Length $10 \mathrm{~m} / 33 \mathrm{ft}$ or $30 \mathrm{~m} / 100 \mathrm{ft}$

| Probe Length <br> (meters) | Sensor <br> Points | Cable Length <br> (meters) |
| :---: | :---: | :---: |
| 2.5 | 10 | 10 |

## MultiTrode Probe Immersion Table

## multitrode <br> WATER • WASTEWATER • PUMP STATION • TECHNOLOGY

PVC and AVESTA 254-SMO stainless steel comprise the major, exposed surfaces of the MultiTrode probe, and have been operated and tested in the following chemicals.

| ACETIC ACID | 50\% Aqueous |
| :---: | :---: |
| ADIPIC ACID | Saturated Aqueous |
| ALUMINIUM SULPHATE | 27\% |
| AMMONIUM CARBONATE | 50\% Aqueous |
| AMMONIUM HYDROXIDE | All Concentrations |
| AMMONIUM PHOSPHATE | All Concentrations |
| AMMONIUM SULPHATE | All Concentrations |
| AMMONIUM SULPHIDE | All Concentrations |
| AMYL ALCOHOL |  |
| ANILINE HYDROCHLORIDE | All Concentrations |
| BARIUM HYDROXIDE | All Concentrations |
| BEER |  |
| BORAX | All Aqueous |
| BORIC ACID | All Aqueous |
| CALCIUM NITRATE | 50\% Aqueous |
| CHLORIC ACID | 10\% |
| CHROMIC ACID | 5\% |
| FORMIC ACID | Up to 50\% Aqueous |
| GELATINE | All Concentrations |
| GLUCOSE | All Concentrations |
| GLYCERINE | All Concentrations |
| HYDROBROMIC ACID | 50\% Aqueous |
| HYDROCYANIC ACID | 100\% |
| HYDROFLUORIC ACID | 1\% |
| HYDROGEN PEROXIDE | 30\% Aqueous |
| HYDROGEN SULPHIDE | Moist Gas or Saturated Aqueous solution |
| LACTIC ACID | 18\% Aqueous |
| LEAD ACETATE | All Concentrations |
| MERCURY | 100\% |
| MILK | Sour |
| NITRIC ACID | Up to 40\% Aqueous |


| OXALIC ACID | 5\% |
| :---: | :---: |
| PHOSPHORIC ACID | Up to 30\% Aqueous |
| POTASSIUM BICHROMATE | 25\% |
| POTASSIUM CHLORATE | 36\% |
| POTASSIUM CHROMATE | All Concentrations |
| POTASSIUM CYANIDE | All Concentrations |
| POTASSIUM PERMANGANATE | 5-10\% |
| POTASSIUM PERSULPHATE | Saturated |
| POTASSIUM SULPHATE | All Concentrations |
| SODIUM ACETATE | All Concentrations |
| SODIUM BICARBONATE | All Concentrations |
| SODIUM BISULPHATE | 5\% |
| SODIUM BISULPHITE | 10\% |
| SODIUM CHLORATE | 30\% |
| SODIUM FLUORIDE | 5-10\% |
| SODIUM NITRATE | All Concentrations |
| SODIUM PHOSPHATE | All Concentrations |
| SODIUM SILICATE | All Aqueous |
| SODIUM SULPHATE | All Concentrations |
| SODIUM SULPHIDE | 5\% |
| SODIUM SULPHITE | 50\% |
| SODIUM THIOSULPHATE | 16-25\% |
| SULPHUR DIOXIDE | Technically Pure Anhydrous |
| SULPHURIC ACID | 98\% |
| SULPHUROUS ACID | Saturated Aqueous |
| TANNIC ACID | All Aqueous |
| TARTARIC ACID | All Aqueous |
| TURPENTINE OIL | Technically Pure |
| VINEGAR | 4-5\% |
| YEAST | All Aqueous |

Unless stated otherwise, all aqueous solutions are 100\%.

Note: $\quad$ MultiTrode probes can be used in many other aggressive applications and the list above is by no means complete.


## TECHNICAL DATA SHEET

## For

## SEWERAGE PUMP STATION SP144

 Lavarack Av \#1 Eagle FarmEquipment Type: Soft Starter
Location: Drive section
Model Numbers: ..... MSF-017
Manufacturer: Emotron
Supplier:Siemens Ltd.885 Mountain HighwayBayswater Vic 3153
Tel: 137222
Fax: 1300360222

Valid for the following Soft starter Models: MSF-017 to MSF-1400

## MSF SOFT STARTER

INSTRUCTION MANUAL

Document number: 01-1363-01
Edition: $\mathbf{r} 2$
Date of release: 2001-04-20
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## SAFETY INSTRUCTIONS

## Safety

The soft starter should be installed in a cabinet or in an electrical control room.

- The device must be installed by trained personnel.
- Disconnect all power sources before servicing.
- Always use standard commercial fuses, slow blow e.g. type gl, gG, to protect the wiring and prevent short circuiting. To protect the thyristors against short-circuit currents, superfast semiconductor fuses can be used if preferred. The normal guarantee is valid even if superfast semiconductor fuses are not used.


## Operating and maintenance personnel

1. Read the whole Instruction Manual before installing and putting the equipment into operation.
2. During all work (operation, maintenance, repairs, etc.) observe the switch-off procedures given in this instruction as well as any other operating instruction for the driven machine or system. See Emergency below.
3. The operator must avoid any working methods which reduce the safety of the device.
4. The operator must do what he can to ensure that no unauthorised person is working on the device.
5. The operator must immediately report any changes to the device which reduce its safety to the user.
6. The user must undertake all necessary measures to operate the device in perfect condition only.

## Installation of spare parts

We expressly point out that any spare parts and accessories not supplied by us have also not been tested or approved by us.

Installing and/or using such products can have a negative effect on the characteristics designed for your device. The manufacturer is not liable for damage arising as a result of using non-original parts and accessories.

## Emergency

You can switch the device off at any time with the mains switch connected in front of the soft starter (both motor and control voltage must be switched off).

## Dismantling and scrapping

The enclosure of the soft starter is made of recyclable material as aluminium, iron and plastic. Legal requirements for disposal and recycling of these materials must be complied with.

The soft starter contains a number of components demanding special treatment, as for example thyristors. The circuit board contain small amounts of tin and lead. Legal requirements for disposal and recycling of these materials must be complied with.

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## 1. <br> GENERAL INFORMATION

### 1.1 Integrated safety systems

The device is fitted with a protection system which reacts to:

- Over temperature.
- Voltage unbalance.
- Over- and under voltage.
- Phase reversal
- Phase loss
- Motor overload protection thermal and PTC.
- Motor load monitor, protecting machine or process max or min alarm
- Starts per hour limitation

The soft starter is fitted with a connection for protective earth $\stackrel{1}{=}$ (PE).

MSF soft starters are all enclosed IP 20, except MSF-1000 and MSF-1400 which are delivered as open chassi IP00.

### 1.2 Safety measures

These instructions are a constituent part of the device and must be:

- Available to competent personnel at all times.
- Read prior to installation of the device.
- Observed with regard to safety, warnings and information given.

The tasks in these instructions are described so that they can be understood by people trained in electrical engineering. Such personnel must have appropriate tools and testing instruments available. Such personnel must have been trained in safe working methods.

The safety measures laid down in DIN norm VDE 0100 must be guaranteed.

The user must obtain any general and local operating permits and meet any requirements regarding:

- Safety of personnel.
- Product disposal.
- Environmental protection.

NOTE! The safety measures must remain in force at all times. Should questions or uncertalntles arlse, please contact your local sales outlet.

### 1.3 Notes to the Instruction Manual



WARNING! Warnings are marked with a warning trlangle.

## Serial number

The information given in these instructions only applies to the device with the serial number given on the label on the front page. A plate with the serial number is fixed to the device.

## Important

For all enquiries and spare parts orders, please quote the correct name of the device and serial number to ensure that your inquiry or order is dealt with correctly and swiftly.

NOTE! These Instructions only apply to the soft starters having the serlal number given on the front page, and not for all models.

### 1.4 How to use the Instruction Manual

This instruction manual tells you how to install and operate the MSF soft starter. Read the whole Instruction Manual before installing and putting the unit into operation. For simple start-up, read chapter 2 . page 8 to chapter 3. page 10.

Once you are familiar with the soft starter, you can operate it from the keyboard by referring to the chapter 13. page 79. This chapter describes all the functions and possible setting.

### 1.5 Standards

The device is manufactured in accordance with these regulations.

- IEC 947-4-2
- EN 60204-1 Electrical equipment of machines, part 1, General requirements and VDE 0113.
- EN 50081-2, EMC Emission
- EN 50081-1, EMC Emission with bypass
- EN 50082-2, EMC Immunity
- GOST
- UL508


### 1.6 Tests in accordance with norm EN60204

Before leaving the factory, the device was subjected to the following tests:

- Through connection of earthing system;
a) visual inspection.
b) check that earthing wire is firmly connected.
- Insulation
- Voltage
- Function


### 1.8 Unpacking of MSF-310 and larger types

The soft starter is attached to the plywood box/loading stool by screws, and the soft starter must be unpacked as follows:

1. Open only the securing plates at the bottom of the box (bend downwards). Then lift up the box from the loading stool, both top and sides in one piece.
2. Loosen the three ( 3 pcs ) screws on the front cover of the soft starter, down by the lower logo.
3. Push up the front cover about 20 mm so that the front cover can be removed.
4. Remove the two ( 2 pcs) mounting screws at the bottom of the soft starter.
5. Lift up the soft starter at the bottom about 10 mm and then push backwards about 20 mm so that the soft starter can be removed from the mounting hooks* at the top. The hooks are placed under the bottom plate and cannot be removed until the soft starter is pulled out.
6. Loosen the screws ( 2 pcs ) for the mounting hooks and remove the hooks.
7. The hooks are used as an upper support for mounting the soft starter.


Fig. 2 Unpacking of MSF-310 and larger models.
2. DESCRIPTION

### 2.1 General

The MSF is installed directly between the mains and the supply cable to the motor. If a mains contactor is used it can be activated by the integrated K1 relay.


The MSF is developed for soft starting, stopping and braking three-phase motors.

There are 3 different kinds of soft starting control methods:

## - Control method 1-Phase

The single phase controlled soft starters provide only a reduction in starting torque no control of current or torque. These starters need a main and bypass contactor as well as external motor protections. This is a open loop voltage controller. These starters are mainly in the power up to 7.5 kW .

- Control method 2-Phase

The two phase starters can start a motor without a mains contactor, but in that case voltage still is present at the motor when it's stopped. These starters are mainly in the power up to 22 kW .

- Control method 3-Phase

In the three phase Soft Starters there are different technologies:

- Voltage control
- Current control
- Torque control


## Voltage control

This method is the most used control method. The starter gives a smooth start but doesn't get any feedback on current or torque. The typical settings to optimize a voltage ramp are: Initial voltage, ramp time, dual ramp time.


Fig. 3 Voltage control

## Current control

The voltage ramp can be used with a current limit which stops the voltage ramp when the set maximum current level is reached. The maximum current level is the main setting and must be set by the user depending the maximum current allowed for the application.


Fig. 4 Current control

## Torque control

Is the most sufficient way of starting motors. Unlike voltage and current based systems the soft starter monitors the torque need and allows to start with the lowest possible current. Using a closed loop torque controller also linear ramps are possible. The voltage ramp can not hold back the motor starting torque this results in a current peak and unlinear ramps. In the current ramp there will be no peak current, but a higher current for a longer period of time during the start compared to torque control. Current starting doesn't give linear ramps. The linear ramps are very important in many applications. For an example, to stop a pump with an unlinear ramp will give water hammer. Soft starters which doesn't monitor the torque, will start and stop to fast if the load is lighter than the setting of current or ramp time.


Fig. 5 Torque control
2.2 MSF control methods

MSF Soft Starters control all three phases supplied to the motor. It manages all the 3 possible starting methods where the closed loop Torque control is the most efficient way of starting and stopping motors.

### 2.2.1 General features

As mentioned above soft starters offer you several features and the following functions are available:

- Torque controlled start and stop
- Current limit control at start
- Application "Pump"
- External analogue input control
- Torque booster at start
- Full voltage start (D.O.L)
- Dual voltage ramp at start and stop
- Bypass
- Dynamic DC-brake or Softbrake
- Slow speed at start and stop
- Jogging forward and reverse
- Four parameter sets
- Analogue output indicating current, power or voltage
- Viewing of current, voltage, power, torque, power consumption, elapsed time etc.
- Integrated safety system acc. to $\S 1.1$, page 6 , with an alarm list.

3. HOW TO GET STARTED


Fig. 6 Standard wiring.
This chapter describes briefly the set-up for basic soft start and soft stop by using the default "Voltage Ramp" function.


WARNING! Mounting, wiring and setting the device Into operation must be carred out by properly tralned personnel. Before set-up, make sure that the Installation Is according to chapter 6. page 24 and the Checkllst below.

### 3.1 Checklist

- Mount the soft starter in accordance with chapter 6 . page 24.
- Consider the power loss at rated current when dimensioning a cabinet, max. ambient temperature is $40^{\circ} \mathrm{C}$ (see chapter 12 . page 74).
- Connect the motor circuit according to Fig. 6.
- Connect the protective earth.
- Connect the control voltage to terminals 01 and 02 (100-240 VAC or 380-500 VAC).
- Connect relay K1 (PCB terminals 21 and 22) to the contactor - the soft starter then controls the contactor.
- Connect PCB terminals 12 and 13 to, e.g., a 2 -way switch (closing non-return) or a PLC, etc., to obtain control of soft start/soft stop. ${ }^{1}$ )
- Check that the motor and supply voltage corresponds to values on the soft starter's rating plate.
- Ensure the installation complies with the appropriate local regulations.

1) The menu 006 must be put to 01 for start/stop command from keyboard.

### 3.2 Main functions/Applications



WARNING! Make sure that all safety measures have been taken before switching on the supply.

Switch on the control voltage (normally $1 \times 230 \mathrm{~V}$ ), all segments in the display and the two LED's will be illuminated for a few seconds. Then the display will show menu 001. An illuminated display indicates there is supply voltage on the PCB. Check that you have mains voltage on the mains contactor or on the thyristors. The settings are carried out according to following:

The first step in the settings is to set menu 007 and 008 to "ON" to reach the main functions 020-025 and motor data 041-046.

NOTE! The main functlon is chosen according to the application. The tables in the applications and functlons selectlon (table 1, page 15), glves the Information to choose the proper maln function.

### 3.3 Motor Data

Set the data, according to the motor type plate to obtain optimal settings for starting, stopping and motor protection.

NOTE! The default settings are for a standard 4-pole motor acc. to the nominal power of the soft-starter. The soft starter will run even If no speclfic motor data ls selected, but the performance will not be optimal.

| 0 | 4 | 1 |
| :--- | :--- | :--- | |  |  |  |
| :--- | :--- | :--- |
|  | 4 | 0 |
|  | 4 | 0 |




NOTE! Now go back to menu 007 and set it to "oFF" and then to menu 001.

### 3.4 Setting of the start and stop ramps

The menu's 002 and 003 can now be set to adjust the start ramp up time and the stop ramp down time.


Estimate the starting-time for the motor/machine. Set "ramp up time" at start ( $1-60 \mathrm{sec}$ ).
Key "ENTER $\&$ " to confirm new value.
Key "NEXT $\rightarrow$ ", "PREV $\leftarrow$ " to change menu.


Set "ramp down time" at stop (2-120 s). "oFF" if only soft start requires.

### 3.5 Setting the start command

As default the start command is set for remote operation via terminal 11, 12 and 13 . For easy commissioning it is possible to set the start command on the start key on the keyboards. This is set with menu 006.


Menu 006 must be set to 1 to be able to operate from keyboard.

NOTE! Factory default setting Is remote control (2).
To start and stop from the keyboard, the "START/ STOP" key is used.

To reset from the keyboard, the "ENTER $\leftarrow /$ RESET" key is used. A reset can be given both when the motor is running and when the motor is stopped. A reset by the keyboard will not start or stop the motor.

### 3.7 Starting



WARNING! Make sure that all safety measures have been taken before starting the motor In order to avold personal infury.

Start the motor by pressing the "START/STOP" key on the keyboard or through the remote control, PCB terminal 11,12 and 13 . When the start command is given, the mains contactor will be activated by relay K1 (PCB terminal 21 and 22), and the motor then starts softly.


Fig. 7 Example of start ramp with main function voltage ramp.

### 3.6 Viewing the motor current

Set the display to menu 005. Now the Motor current can be viewed on the display.


NOTE! The menu 005 can be selected at any tlme when the motor Is running.

## 4. APPLICATIONS AND FUNCTIONS SELECTION

This chapter is a guide to select the correct soft starter rating and the selection of the Main function and additional functions for each different application.

To make the right choice the following tools are used:

- The norm AC53a.

This norm helps selecting the soft starter rating with regard to duty cycle, starts per hour and maximum starting current.

- The Application Rating List.

With this list the soft starter rating can be selected depending on the kind of application used. The list use 2 levels of the AC53a norm. See table 1, page 15.

- The Application Function List.

This table gives an complete overview of most common applications and duties. For each applications the menu's that can be used are given. See table 2, page 17.

- Function and Combination matrix.

With these tables it is easy to see which combinations of Main and additional functions are possible, see table 3, page 19 and table 4, page 19.

### 4.1 Soft starter rating according to AC53a

The IEC947-4-2 standard for electronic starters defines AC53a as a norm for dimensioning of a soft starter.

The MSF soft starter is designed for continuous running. In the Applications table (table 1, page 15) two levels of AC53a are given. This is also given in the technical data tables (see chapter 12. page 74).


Fig. 8 Rating example AC53n.
The above example indicates a current rating of 210 Amps with a start current ratio of $5.0 \times$ FLC (1050A) for 30 seconds with a $50 \%$ duty cycle and 10 starts per hour.

NOTE! If more than $\mathbf{1 0}$ starts/hour or other duty cycles are needed, please contact your supplier.


Fig. 9 Duty cycle, non bypass.

### 4.2 Soft starter rating according to AC53b

This norm is made for Bypass operation. Because the MSF soft starter is designed for continuous operation this norm is not used in the selection tables in this chapter.


Fig. 10 Rating example AC53b.


Fig. 11 Duty cycle, bypassed
The above example indicates a current rating of 210 Amps with a start current ratio of $5.0 \times$ FLC (1050A) for 30 seconds with a 24 -minute period between starts.

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### 4.3 MSF Soft starter ratings

According to the norms AC53a and AC53b a soft starter can have many current ratings.

NOTE! Because the MSF soft starter Is designed for continuous operation the norm AC53b is not used in the appllcation rating Ilst.

With help of the Application Rating List with typical starting currents and categories in the AC53a level (see table 1, page 15 and table 2, page 17) it is easy to select the proper soft starter rating with the application.

The Application Rating List uses two levels for the AC53a norm:

- AC53a 5.0-30:50-10 (heavy duty)

This level will be able to start all applications and follows directly the type number of the soft starter. Example: MSF 370 is 370 Amps FLC and then 5 time this current in starting.

- AC 53a 3.0-30:50-10 (normal/light duty)

This level is for a bit lighter applications and here the MSF can manage a higher FLC.
Example: MSF 370 in this norm manage 450 Amps
FLC and the 3 times this current in starting
NOTE! To compare Soft Starters it's Important to ensure that not only FLC (Full Load Current) is compared but also that the operating parameters are Identical.

### 4.4 The Application Ratings List

Table 1 gives the Application Ratings List. With this list the rating for the soft starter and Main Function menu can be selected.

Description and use of the table:

## - Applications.

This column gives the various applications. If the machine or application is not in this list, try to identify a similar machine or application. If in doubt pleas contact your supplier.

- AC53a ratings.

The rating according to AC53a norm is here classified in 2 ratings. The first for normal/light duty
(3.0-30:50-10) and the second for heavy duty (5.0-30:50-10)

- Typical Starting current.

Gives the typical starting current for each application

- Main Function menu.

The Main Function menu is advised here. " 25 ; $=1$ ", means: progran selection 1 in menu 25.

- Stop function.

Gives a possible Stop function if applicable. " $36 ;=1 / 38-40$ ", means: program selection 1 in menu 36 , also menus 38 to 40 can be selected.

## EXAMPLE:

Roller Mill:

- This is an application for heavy duty,
- Typical starting current of $350 \%$.
- Main function Torque ramp start (menu 25) will give the best results.
- Stop function Dynamic Brake (menu 36, selection 1) can be used.
- As well as the Slow Speed at start and stop (menu $38-40$ ) can be used for better start and stop performance.

Table 1 Applications Rating List


### 4.5 The Application Functions List

This list gives an overview of many different applications/duties and a possible solution with one of the many MSF functions.

Description and use of the table:

- Application /Duty.

This column gives the various applications and level of duty. If the machine or application is not in this list, try to identify a similar machine or application. If in doubt pleas contact your supplier.

- Problem.

This column describes possible problems that are familiar for this kind of application.

- Solution MSF.

Gives the possible solution for the problem using one the MSF function.

- Menus.

Gives the menu numbers and selection for the MSF function.
"25;=1", means: program selection 1 in menu 25. " $36 ;=1 / 34,35$ ", means: program selection 1 in menu 36 , menus 34 and 35 are related to this function.

Table 2 Application Function List

| Application/ Duty | Problem | Solution MSF | Menus |
| :---: | :---: | :---: | :---: |
| PUMP Normal | Too fast start and stops | MSF Pump application with following start/stop features: | 22 |
|  | Non linear ramps | Linear ramps without tacho. |  |
|  | Water hammer | Torque ramps for quadratic load |  |
|  | High current and peaks during starts. |  |  |
|  | Pump is going in wrong direction | Phase reversal alarm | 88 |
|  | Dry running | Shaft power underload | 96-99 |
|  | High load due to dirt in pump | Shaft power overload | 92-95 |
| COMPRESSOR Normal | Mechanical shock for compressor, motor and transmissions | Linear Torque ramp or current limit start. | $\left\lvert\, \begin{aligned} & 25:=1 \text { or } \\ & 20,21 \end{aligned}\right.$ |
|  | Small fuses and low current available. |  |  |
|  | Screw compressor going in wrong direction | Phase sequence alarm | 88 |
|  | Damaged compressor if liquid ammonia enters the compressor screw. | Shaft power overload | 92-95 |
|  | Energy consumption due to compressor is running unloaded | Shaft power underload | 96-99 |
| CONVEYOR Normal/Heavy | Mechanical shocks for transmissions and transported goods. | Linear Torque ramp | 25; $=1$ |
|  | Filling or unloading conveyors | Slow speed and accurate position control. | 37-40,57,58 |
|  | Conveyor jammed | Shaft power overload | 92-95 |
|  | Conveyor belt or chain is off but the motor is still running | Shaft power underload | 96-99 |
|  | Starting after screw conveyor have stopped due to overload. | Jogging in reverse direction and then starting in forward. |  |
|  | Conveyor blocked when starting | Locked rotor function | 75 |
| FAN Normal | High starting current in end of ramps | Torque ramp for quadratic need | $25:=2$ |
|  | Slivering belts. |  |  |
|  | Fan is going in wrong direction when starting. | Catches the motor and going easy to zero speed and then starting in right direction. |  |
|  | Belt or coupling broken | Shaft power underioad | 96-99 |
|  | Blocked filter or closed damper. |  |  |
| PLANER Heavy | High inertia load with high demands on torque and current control. | Linear Torque ramp gives linear acceleration and lowest possible starting current. | $25 ;=1$ |
|  | Need to stop quick both by emergency and production efficiency reasons. | Dynamic DC brake without Contactor for medium loads and controlled sensor less soft brake with reversing contactor for heavy loads. | $\begin{aligned} & 36 ;=1,34,35 \\ & 36 ;=2,34,35 \end{aligned}$ |
|  | High speed lines | Conveyor speed set from planer shaft power analog output. | 54.56 |
|  | Worn out tool | Shaft power overload | 92-95 |
|  | Broken coupling | Shaft power underload | 96-99 |
| ROCK CRUSHER Heavy | High enertia | Linear Torque ramp gives linear acceleration and lowest possible starting current. | $25:=1$ |
|  | Heavy load when starting with material | Torque boost | 30,31 |
|  | Low power if a diesel powered generator is used. |  |  |
|  | Wrong material in crusher | Shaft power overload | 92-95 |
|  | Vibrations during stop | Dynamic DC brake without Contactor | 36;=1,34,35 |
| BANDSAW Heavy | High inertia load with high demands on torque and current control. | Linear Torque ramp gives linear acceleration and lowest possible starting current. | $25 ;=1$ |
|  | Need to stop quick both by emergency and production efficiency reasons. | Dynamic DC brake without Contactor for medium loads and controlled sensor less soft brake with reversing contactor for heavy loads. | $\begin{aligned} & 36 ;=1,34,35 \\ & 36 ;=2,34,35 \end{aligned}$ |
|  | High speed lines | Conveyor speed set from band saw shaft power analog output. | 54-56 |
|  | Worn out saw blade | Shaft power overload |  |
|  | Broken coupling, saw blade or belt | Shaft power underload |  |
| CENTRIFUGE Heavy | High inertia load | Linear Torque ramp gives linear acceleration and lowest possible starting current. | 25; $=1$ |
|  | To high load or unbalanced centrifuge | Shaft power overload |  |
|  | Controlled stop | Dynamic DC brake without Contactor for medium loads and controlled sensor less soft brake with reversing contactor for heavy loads. | $\begin{aligned} & 36 ;=1,34,35 \\ & 36:=2,34,35 \end{aligned}$ |
|  | Need to open centrifuge in a certain position. | Braking down to slow speed and then positioning control. | 37-40,57,58 |

Table 2 Application Function List

| Application/ Duty | Problem | Solution MSF | Menus |
| :---: | :---: | :---: | :---: |
| MIXER Heavy | Different materials | Linear Torque ramp gives linear acceleration and lowest possible starting current. | $25:=1$ |
|  | Need to control material viscosity | Shaft power analog output | 54.56 |
|  | Broken or damaged blades | Shaft power overioad | 92-95 |
|  |  | Shaft power underload | 96-99 |
| HAMMER MILL Heavy | Heavy load with high breakaway torque | Linear Torque ramp gives linear acceleration and lowest possible starting current. | $25 ;=1$ |
|  |  | Torque boost in beginning of ramp. | 30,31 |
|  | Jamming | Shaft power overioad | 92-95 |
|  | Fast stop | Controlled sensor less soft brake with reversing contactor for heavy loads. | 36: $=2,34,35$ |
|  | Motor blocked | Locked rotor function | 75 |

## EXAMPLE:

Hammer Mill:

- This is an application for heavy duty,
- Main function Torque ramp start (menu 25) will give the best results.
- Torque boost to overcome high breakaway torque (menu 30 and 31)
- Overload alarm function for jamming protection (menu 92 and 95)
- Stop function Soft Brake (menu 36, selection 2) can be used. Menu 34 and 35 to set the brake time and strength.


### 4.6 Function and combination matrix

Table 3 gives an overview of all possible functions and combination of functions.

1. Select function in the horizontal "Main Function" column. Only one function can be selected in this column, at a time.
2. In the vertical column "Additional Functions" you will find all possible function that can be used together with your selected main function.

Table 3 Combination matrix

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voitage ramp start/stop (default) | X | X | X | X | X | X | X | X | X | X | X |  |
| Torque control start/stop (menu 025) |  |  | X | X | X | X | X | X | X | X | X |  |
| Voltage ramp with current limit (menu 020) |  | X | X | X | X | X | X | X | X | X | X | X |
| Current limit start (menu 021) |  | X | X | X | X | X | X | x | X | X | X | x |
| Pump control (menu 022) |  |  | X |  |  |  |  |  | X | X |  |  |
| Analog input (menu 023) |  |  |  |  |  |  |  |  | X | X |  |  |
| Direct on line start (menu 024) |  |  | X |  |  |  |  |  | X | X |  |  |

By using one parameter set, the following start/stop table is given.

NOTE! Voltage and torque ramp for starting only with softbrake.

Table 4 Start/stop combination.

| START FUNCTION | 2 <br> ㅇㅡㅡㄴ <br> 2 <br> 2 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 |  |  |  |  |  |  |  |  | 0 0 0 0 0 0 4 0 0 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Voltage ramp start |  | X |  |  |  |  | X |  | X | X |
| Torque control start |  |  | x |  |  |  | X |  |  | $x$ |
| Current limit start |  | X |  |  |  |  | x |  | X | $x$ |
| Voltage ramp with current limit |  | X |  |  |  |  | X |  | X | $x$ |
| Pump control |  |  |  | X |  |  | X |  |  |  |
| Analog input |  |  |  |  |  | x | X |  |  |  |
| Direct on line start |  |  |  |  |  |  | X |  |  |  |

By using different parameter sets for start and stop, it is possible to combine all start and stop functions.

### 4.7 Special condition

### 4.7.1 Small motor or low load

The minimum load current for the soft starter is $10 \%$ of the rated current of the soft starter. Except for the MSE-017 there the min. current is 2 A . Example MSE-210, rated current $=210 \mathrm{~A}$. Min. Current 21 A . Please note that this is "min. load current" and not min . rated motor current.

### 4.7.2 Ambient temperature below $0^{\circ} \mathrm{C}$

For ambient temperatures below $0^{\circ} \mathrm{C}$ e.g. an electrical heater must be installed in the cabinet. The soft starter can also be mounted in some other place, due to that the distance between the motor and the soft starter is not critical.

### 4.7.3 Phase compensation capacitor

If a phase compensation capacitor is to be used, it must be connected at the inlet of the soft starter, not between the motor and the soft starter.

### 4.7.4 Pole-changing contactor and two speed motor

The switching device must be connected between the output of the soft starter and the motor.

### 4.7.5 Shielded motor cable

It is not necessary to use shielded wires together with soft starters. This is due to the very low radiated emissions.

NOTE! The soft starter should be wired with shlelded control cable to fulfill EMC regulations acc. to $\$ 1.5$, page 6.

### 4.7.6 Slip ring motors

Slip ring motors can not be used together with the soft starter. Unless the motor is rewinded (as a squirrel cage motor). Or keep the resistors in, please contact your supplier.

### 4.7.7 Pump control with soft starter and frequency inverter together

It is possible e.g. in a pump station with two or more pumps to use one frequency inverter on one pump and soft starters on each of the other pumps. The flow of the pumps can then be controlled by one common control unit.

### 4.7.8 Starting with counter clockwise rotating loads

It is possible to start a motor clockwise, even if the load and motor is rotating counter clockwise e.g. fans. Depending on the speed and the load "in the wrong direction" the current can be very high.

### 4.7.9 Running motors in parallel

When starting and running motors in parallel the total amount of the motor current must be equal or lower than the connected soft starter. Please note that it is not possible to make individual settings for each motor. The start ramp can only be set for an average starting ramp for all the connected motors. This applies that the start time may differ from motor to motor. This is also even if the motors are mechanically linked, depending on the load etc.

### 4.7.10 How to calculate heat dissipation in cabinets

See chapter 12. page 74 "Technical Data", "Power loss at rated motor load $\left(\mathrm{I}_{\mathrm{N}}\right)$ ", "Power consumption control card" and "Power consumption fan". For further calculations please contact your local supplier of cabinets, e.g. Rittal.

### 4.7.11 Insulation test on motor

When testing the motor with high voltage e.g. insulation test the soft starter must be disconnected from the motor. This is due to the fact that the thyristors will be seriously damage by the high peak voltage.

### 4.7.12 Operation above 1000 m

All ratings are stated at 1000 m over sea level.
If a MSF is placed for example at 3000 m it must be derated unless that the ambient temperature is lower than 40 C and compensate for this higher pressure.

To get information about motors and drives at higher altitudes please contact your supplier to get technical information nr 151.

### 4.7.13 Reversing

Motor reversing is always possible. See Fig. 31 on page 34 for the advised connection of the reverse contactors.

At the moment that the mains voltage is switched on, the phase sequence is monitored by the control board. This information is used for the Phase Reverse Alarm (menu 88, see $\S 7.22$, page 56 ).

However if this alarm is not used (factory default), it is also possible to have the phase reversal contactors in the input of the soft starter.
5. OPERATION OF THE SOFT STARTER


Fig. 12 MSF soft starter models.

### 5.1 General description of user interface



WARNING! Never operate the soft starter with removed front cover.

To obtain the required operation, a number of parameters must be set in the soft starter.

Setting/configuration is done either from the builtin keyboard or by a computer/control system through the serial interface or bus (option). Controlling the motor i.e. start/stop, selection of parameter set, is done either from the keyboard, through the remote control inputs or through the serial interface (option).

## Setting



WARNING! Make sure that all safety measures have been taken before switching on the supply.

Switch on the supply (normally $1 \times 230 \mathrm{~V}$ ), all segments in the display will light up for a few seconds. Then the display will show menu 001. An illuminated display indicates there is supply voltage on the PCB.

Check that you have voltage on the mains contactor or on the thyristors. To be able to use all extended functions and optimize of the performance, program the motor data.

### 5.2 PPU unit



Fig. 13 PPU unit.
The programming and presentation unit (PPU) is a build-in operator panel with two light emitting diodes, three + four seven-segment LED-displays and a keyboard.

### 5.3 LED display

The two light emitting diodes indicates start/stop and running motor/machine. When a start command is given either from the PPU, through the serial interface (option) or through the remote control inputs, the start/stop-LED will be illuminated.

At a stop command the start/stop-LED will switch off. When the motor is running, the running-LED is flashing during ramp up and down and is illuminated continuously at full motor voltage.


Fig. 14 LED indication at different operation situation.

### 5.4 The Menu Structure

The menus are organised in a simple one level structure with the possibility to limit the number of menus that are reachable by setting the value in menu 007 to "oFF" (factory setting). With this setting only the basic menus $001,002,003,004,005,006$ and 007 can be reached.

This to simplify the setting when only voltage start/ stop ramps are used.

If menu 007 is in "on" and menu 008 "oFF" it is possible to reach all viewing menus and alarm lists as well.


03-F30

Fig. 15 Menu structure.

### 5.5 The keys

The function of the keyboard are based on a few simple rules. At power up menu 001 is shown automatically. Use the "NEXT $\rightarrow$ " and "PREV $\leftarrow$ "keys to move between menus. To scroll through menu numbers, press and hold either the "NEXT $\rightarrow$ " or the "PREV $\leftarrow$ " key. The " + " and "-" keys are used to increase respectively decrease the value of setting. The value is flashing during setting. The "ENTER $\leftarrow$ " key confirms the setting just made, and the value will go from flashing to stable. The "START/STOP" key is only used to start and stop the motor/machine.
The $\Theta$ and $\Theta$ keys are only used for JOG from the keyboard. Please note one has to select enable in menu 103 or 104 , see $\$ 7.25$, page 61 .

Table 5 The keys

| Start/stop motor operation. | START |
| :--- | :--- |
| Sisplay previous menu. | PREV |
| Display next menu. |  |
| Decrease value of setting. |  |
| Increase value of setting. |  |
| Confirm setting just made. |  |
| Alarm reset. |  |
| JOG Reverse |  |
| JOG Forward |  |

Table 6 Control modes

| Control mode $\begin{gathered}\text { Operation/ } \\ \text { Set-up }\end{gathered}$ |  | Start/Stop | JOG fwd/rev | Alarm reset | Setting of parameters |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Parameter set with external selection Menu 061=0 |  |  | Parameter set with internal selection Menu 061=1-4 |
| Keyboard Menu 006=1 | Unlocked keyboard |  | Keyboard | Keyboard | Keyboard | - | Keyboard |
|  | Locked keyboard | $\square$ | $\bigcirc$ | - | -_-_ | - |
| Remote Menu 006=2 | Unlocked keyboard | Remote | Remote | Remote and keyboard | Remote | Keyboard |
|  | Locked keyboard | Remote | Remote | Remote | Remote | $\square$ |
| Serial comm. Menu 006=3 | Unlocked keyboard | Serial comm | Serial comm | Serial comm. and keyboard | -——— | Serial comm |
|  | Locked keyboard | Serial comm | Serial comm | Serial comm | - | Serial comm |

## 6. INSTALLATION AND CONNECTION

Mounting, wiring and setting the device into operation must be carried out by trained personnel (electricians specialised in heavy current technology):

- In accordance with the local safety regulations of the electricity supply company.
- In accordance with DIN VDE 0100 for setting up heavy current plants.
Care must be taken to ensure that personnel do not come into contact with live circuit components.


WARNING! Never operate the soft starter with removed front cover.

### 6.1 Installation of the soft starter in a cabinet

When installing the soft starter:

- Ensure that the cabinet will be sufficiently ventilated, after the installation.
- Keep the minimum free space, see the tables on page 25 .
- Ensure that air can flow freely from the bottom to the top.

NOTE! When Installing the soft starter, make sure it does not come into contact with live components. The heat generated must be dispersed via the cooling fins to prevent damage to the thyilstors (free circulation of air).

MSF-017 to MSF-835 soft starters are all delivered as enclosed versions with front opening. The units have bottom entry for cables etc. see Fig. 25 on page 29 and Fig. 27 on page 31 . MSF-1000 and MSF-1400 are delivered as open chassis.

NOTE! The soft starter should be wired with shlelded control cable to fulfill EMC regulations acc. to $\S 1.5$, page 6.

NOTE! For UL-approval use $75^{\circ} \mathrm{C}$ Copper wire only.
MSF-017 to MSF-250


Fig. 16 MSF-017 to MSF-250 dimensions.


Fig. 17 Hole pattern for MSF-017 to MSF-250 (backside view).


Fig. 18 Hole pattern for MSF-170 to MSF-250 with upper mounting bracket instead of DIN-rail.

MSF-017 to MSF-250

Table 7 MSF-017 to MSF-250.

| MSF <br> model | Class | Connection | Conv./ <br> Fan | Dimension <br> HxWxD $(\mathbf{m m})$ | Hole dist. <br> $\mathbf{w 1}(\mathbf{m m})$ | Hole dist. <br> $\mathbf{h 1}(\mathbf{m m})$ | Diam./ <br> screw | Weight <br> $\mathbf{( k g )}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $-017,-030$ | IP 20 | Busbars | Convection | $320 \times 126 \times 260$ | 78.5 | 265 | $5.5 / \mathrm{M} 5$ | 6.7 |
| $-045,-060$, | IP 20 | Busbars | Fan | $320 \times 126 \times 260$ | 78.5 | 265 | $5.5 / \mathrm{M} 5$ | 6.9 |
| $-075,-085$ |  |  | $400 \times 176 \times 260$ | 128.5 | 345 | $5.5 / \mathrm{M} 5$ | 12.0 |  |
| $-110,-145$ | IP 20 | Busbars | Fan | $40 \times 260 \times 260$ | 208.5 | 445 | $5.5 / \mathrm{M} 5$ | 20 |
| $-170,-210,-250$ | IP 20 | Busbars | Fan | $500 \times 26 \times 20$ |  |  |  |  |

Table 8 MSF-017 to MSF-250

| MSF <br> model | Minimum free space (mm): |  |  | Dimension Connection busbars Cu | Tightening torque for bolt (Nm) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | above 1) | betow | at side |  | Cable | PE-cable | Supply and PE |
| -017, -030, -045 | 100 | 100 | 0 | $15 \times 4$ (M6), PE (M6) | 8 | 8 | 0.6 |
| -060, -075, -085 | 100 | 100 | 0 | $15 \times 4$ (M8), PE (M6) | 12 | 8 | 0.6 |
| -110,-145 | 100 | 100 | 0 | $20 \times 4$ (M10), PE (M8) | 20 | 12 | 0.6 |
| -170, -210, -250 | 100 | 100 | 0 | 30x4 (M10), PE (M8) | 20 | 12 | 0.6 |
| 1) Above: wall-soft starter or soft starter-soft starter |  |  |  |  |  |  |  |

## MSF-310 to MSF-1400

Table 9 MSF-310 to MSF-1400 see Fig. 20 on page 26.

| MSF model | Class | Connection | Conv./ Fan | Dimension HxWxD (mm) | Hole dist. w1 (mm) | Hole dist. h1 (mm) | Diam./ screw | Weight (kg) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -310 | IP 20 | Busbars | Fan | $532 \times 547 \times 278$ | 460 | 450 | 8.5/M8 | 42 |
| -370, -450 | IP 20 | Busbars | Fan | $532 \times 547 \times 278$ | 460 | 450 | 8.5/M8 | 46 |
| -570 | IP 20 | Busbars | Fan | $687 \times 640 \times 302$ | 550 | 600 | 8.5/M8 | 64 |
| -710 | IP 20 | Busbars | Fan | $687 \times 640 \times 302$ | 550 | 600 | 8.5/M8 | 78 |
| -835 | IP 20 | Busbars | Fan | $687 \times 640 \times 302$ | 550 | 600 | 8.5/M8 | 80 |
| -1000, -1400 | IPOO | Busbar | Fan | $900 \times 875 \times 336$ | Fig. 23 |  | 8.5/M8 | 175 |

Table 10 MSF- 310 to MSF-1400.

| MSF model | Minimum free space (mm): |  |  | Dimension Connection, busbars AI | Tightening torque for bolt ( Nm ) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | above 1) | below | at side |  | Cable | PE-cable | Supply and PE |
| -310, -370, -450 | 100 | 100 | 0 | 40x8 (M12) | 50 | 12 | 0.6 |
| -570, -710, -835 | 100 | 100 | 0 | $40 \times 10$ (M12) | 50 | 12 | 0.6 |
| -1000, -1400 | 100 | 100 | 100 | $75 \times 10$ (M12) | 50 | 12 | 0.6 |



Fig. 19 MSF - 310 to MSF - 835.


Fig. 21 Busbar distances MSF-310 to MSF - 835 .

Table 11 Bisbar distances

| MSF model | Dist. h1 <br> (mm) | Dist. w1 <br> $(\mathbf{m m})$ | Dist. w2 <br> $(\mathbf{m m})$ | Dist. w3 <br> $(\mathbf{m m})$ |
| :--- | :--- | :--- | :--- | :--- |
| -310 to -450 | 104 | 33 | 206 | 379 |
| -570 to -835 | 129 | 35 | 239.5 | 444 |
| $-1000-1400$ |  | 55 | 322.5 | 590.5 |

Fig. 20 Hole pattern for screw attachment, MSF-310 to MSF-835. Hole distance (mm).


Fig. 22 MSF-1000 to -1400


Fig. 23 Hole pattern busbar MSF - 1000 to -1400.

### 6.2 Connections



Fig. 24 Connection of MSF-017 to MSF-085.

## Connection of MSF-017 to MSF-085

## Device connections

1. Protective earth, $\perp$ (PE), Mains supply, Motor (on the right and left inside of the cabinet)
2. Protective earth $\stackrel{\perp}{ \pm}(\mathrm{PE})$, Control voltage
3. Control voltage connection $\mathbf{0 1}, 02$
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (possible to mount outside for bypass see $\S 7.12$, page 43)
7. Mounting of EMC gland for control cables


Fig. 25 Connection of MSF-110 to MSF-145.

## Connection of MSF-110 to MSF-145

## Device connections

1. Protective earth, $\stackrel{\perp}{\bar{\circ}}$ (PE), Mains supply, Motor (on the left inside of the cabinet)
2. Protective earth $\perp$ (PE), Control voltage
3. Control voltage connection 01, 02
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (possible to mount outside for bypass see $\$ 7.12$, page 43 )
7. Mounting of EMC gland for control cables


Fig. 26 Connection of MSF-170 to MSF- 250

## Connection of MSF-170 to MSF-250

## Device connections

1. Protective earth, $\stackrel{\perp}{\underline{-}}$ (PE), Mains supply, Motor
(on the left inside of the cabinet)
2. Protective earth $\stackrel{\perp}{=}(\mathrm{PE})$, Control voltage
3. Control voltage connection 01, 02
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (possible to mount outside for bypass see $\$ 7.12$, page 43)
7. Mounting of EMC gland for control cables


Fig. 27 Connection of MSF-170 to MSF-1400.

## Connection of MSF-310 to MSF-1400

## Device connections

1. Protective earth, $\stackrel{\perp}{=}$ (PE), Mains supply and Motor
2. Protective earth, $\xlongequal{\perp}$ (PE), Control voltage
3. Control voltage connection 01,02
4. Mains supply L1, L2, L3
5. Motor power supply T1, T2, T3
6. Current transformers (possible to mount outside for bypass see $\S 7.12$, page 43)
7. Mounting of EMC gland for control cables
6.3 Connection and setting on the PCB control card


Fig. 28 Connections on the PCB, control card.
Table 12 PCB Terminals

| Terminal | Function | Eectrical characteristics |
| :---: | :---: | :---: |
| 01 | Supply voltage | $100-240$ VAC $\pm 10 \% / 380-500$ VAC $\pm 10 \%$ |
| 02 |  |  |
| PE | Gnd | $\stackrel{1}{2}$ |
| 11 | Digital inputs for start/stop and reset. | $0-3 \mathrm{~V}$-> $0 ; 8$-27 V-> 1. Max. 37 V for 10 sec. Impedance to $0 \mathrm{VDC}: 2.2 \mathrm{k} \Omega$. |
| 12 |  |  |
| 13 | Supply/control voltage to PCB terminal 11 and 12, $10 \mathrm{k} \Omega$ potentiometer, etc. | +12 VDC $\pm 5 \%$. Max. current from +12 VDC: 50 mA . Short circuit proof. |
| 14 | Remote analogue input control, 0-10 V, 2-10 V, 0-20 mA and 4-20 mA/digital input. | Impedance to terminal 15 ( 0 VDC ) voltage signal: $125 \mathrm{k} \Omega$, current signal: $100 \Omega$ |
| 15 | GND (common) | 0 VDC |
| 16 | Digital inputs for selection of parameter set. | $0-3 V \rightarrow 0 ; 8-27 \mathrm{~V} \rightarrow 1$. Max. 37 V for 10 sec. Impedance to $0 \mathrm{VDC}: 2.2 \mathrm{k} \Omega$. |
| 17 |  |  |
| 18 | Supply/control voltage to PCB terminal 16 and 17, $10 \mathrm{k} \Omega$ potentiometer, etc. | +12 VDC $\pm 5 \%$. Max. current from $+12 \mathrm{VDC}=50 \mathrm{~mA}$. Short circuit proof. |
| 19 | Remote analogue output control | Analogue Output contact: <br> $0-10 \mathrm{~V}, 2-10 \mathrm{~V}$; min load impedance $700 \Omega$ <br> $0-20 \mathrm{~mA}$ and $4-20 \mathrm{~mA}$; max load impedance $750 \Omega$ |
| 21 | Programmable relay K1. Factory setting is "Opera tion" indication by closing terminal 21-22. | 1-pole closing contact, 250 VAC 8 A or 24 VDC $8 A$ resistive, 250 VAC, 3 A inductive. |
| 22 |  |  |
| 23 | Programmable relay K2. Factory setting is "Full voltage" indication by closing terminal 23-24. | 1-pole closing contact, 250 VAC 8 A or 24 VDC 8 A resistive, $250 \mathrm{VAC}, 3 \mathrm{~A}$ inductive. |
| 24 |  |  |
| 31 | Alarm relay $\mathrm{K3}$, closed to 33 at alarm. | 1-pole change over contact, 250 VAC 8 A or 24 VDC 8 A resistive, 250 VAC, 3 A inductive. |
| 32 | Alarm relay K 3 , opened at alarm. |  |
| 33 | Alarm relay K3, common terminal. |  |
| 69-70 | PTC Thermistor input | Alarm level $2.4 \mathrm{k} \Omega$ Switch back level $2.2 \mathrm{k} \Omega$. |
| 71-72* | Clickson thermistor | Controlling soft starter cooling fine temperature MSF-310-MSF-1400 |
| 73-74* | NTC thermistor | Temperature measuring of soft starter cooling fine |
| 75 | Current transformer input, cable S1 (blue) | Connection of L1 or T1 phase current transformer |
| 76 | Current transformer input, cable S1 (blue) | Connection of L3, T3 phase (MSF 017-MSF 250) or L2, T2 phase (MSF 310 - MSF 1400) |
| 77 | Current transformer input, cable S2 (brown) | Common connection for terminal 75 and 76 |
| 78* | Fan connection | 24 VDC |
| 79* | Fan connection | O VDC |

*Internal connection, no customer use.

### 6.4 Minimum wiring



Fig. 29 Wiring circuit, "Minimum wiring".
The figure above shows the "minimum wiring". See
$\$ 6.1$, page 24, for tightening torque for bolts etc.

1. Connect Protective Earth (PE) to earth screw marked $\stackrel{\perp}{=}$ (PE).
2. Connect the soft starter between the 3-phase mains supply and the motor. On the soft starter the mains side is marked L1, L2 and L3 and the motor side with T1, T2 and T3.
3. Connect the control voltage ( $100-240 \mathrm{VAC}$ ) for the control card at terminal 01 and 02.
4. Connect relay K1 (terminals 21 and 22) to the control circuit.
5. Connect PCB terminal 12 and 13 (PCB terminal 11-12 must be linked) to, e.g. a 2 -position switch (on/oFF) or a PLC, etc., to obtain control of soft start/stop. (For start/stop command from keyboard menu 006 must be set to 01).
6. Ensure the installation complies with the appropriate local regulations.

NOTE! The soft starter should be wired with shlelded control cable to fulfill EMC regulations acc. to § 1.5, page 6.

NOTEI If local regulations say that a malns contactor should be used, the K1 then controls It. Always use standard commerclal, slow blow tuses, e.g. type gl, gG to protect the wiring and prevent short cliculting. To protect the thyristors against shortclrcult currents, superfast semiconductor fuses can be used if preferred. The normal guarantee is valld even If superfast semiconductor fuses are not used. All signal Inputs and outputs are galvanically Insulated from the malns supply.

### 6.5 Wiring examples

Fig. 30 gives an wiring example with the following
functions.

- Analogue input control, see $\$ 7.7$, page 40
- Parameter set selection, see $\$ 7.20$, page 54
- Analogue output, see $\S 7.18$, page 52
- PTC input, see $\S 7.21$, page 55

For more information see $\S 6.3$, page 32 .


Fig. 30 Analogue input control, parameter set, analogue output and $P T C$ input.


Fig. 31 Forward/reverse wiring circuit.

## 7. FUNCTIONAL DESCRIPTION SET-UP MENU

This chapter describes all the parameters and functions in numerical order as they appear in the MSF. Table 13 gives an overview of the menus, see also Chapter 13. page 79 (set-up menu list).

Table 13 Set-up Menu overview

|  | Menu number | Parameter group |  | Menu numbers | See § |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Basic functions | 001-008 | Basic | Ramp up/down parameters | 001-005 | 7.1 |
|  |  |  | Start/Stop/Reset command | 006 | 7.2 |
|  |  |  | Menu Expansion | 007-008 | 7.3 |
| Extended functions | 011-199 | Voltage control dual ramp |  | 011-014 | 7.4 |
|  |  | Torque control parameters |  | 016-018 | 7.5 |
|  |  | Main functions |  | 020-025 | 7.6-7.10 |
|  |  | Additional functions |  | 030-036 | 7.11-7.14 |
|  |  | Slow speed and Jog functions |  | $\begin{aligned} & 037-040,57-58, \\ & 103-104 \end{aligned}$ | $\begin{aligned} & 7.15,7.19 \\ & 7.25 \end{aligned}$ |
|  |  | Motor Data Setting |  | 041-046 | 7.16 |
|  |  | Outputs | Relays | 051.052 | 7.17 |
|  |  |  | Analogue output | 054-056 | 7.18 |
|  |  | Input | Digital input | 057-058 | 7.19 |
|  |  | Parameter set selection |  | 061 | 7.20 |
|  |  |  Motor protection <br>  Main |  | 071-075 | 7.21 |
|  |  |  | Main protection | 081-088 | 7.22 |
|  |  |  | Application protection | 089-099 | 7.23 |
|  |  |  | Resume alarms | 101, 102 | 7.24 |
|  |  | Auto return menu |  | 105 | 7.26 |
|  |  | Factory defaults |  | 199 | 7.28 |
| View functions | 201-915 | Main view |  | 201-208 | 7.29 |
|  |  | RMS current per phase |  | 211-213 | 7.29 |
|  |  | RMS voltage per phase |  | 214-216 | 7.29 |
|  |  | Keyboard lock status |  | 221 | 7.30 |
|  |  | Alarm list |  | 901-915 | 7.31 |

### 7.1 Ramp up/down parameters



Fig. 32 Menu numbers for start/stop ramps, initial voltage at start and step down voltage at stop.

Determine the starting time for the motor/machine. When setting the ramp times for starting and stopping, initial voltage at start and step down voltage at stop, proceed as follow:


Set the initial voltage. Normally the factory setting, $30 \%$ of $U_{n}$, is a suitable choice.

| 0 0 4 <br> 0   |
| :--- | :--- | :--- | :--- |
|  Setting of stop ramp 1   <br>  $O$ $F$ $F$ <br> Default: oFF   <br> Range: oFF, 2-120 sec   <br> oFF Stop ramp disabled   <br> $\mathbf{2 - 1 2 0}$ Set "Ramp down time" at stop   |

### 7.1.1 RMS current [005]

NOTE! Thls is the same read-out as functlon 201, see § 7.28, page 63.



### 7.2 Start/stop/reset command

Start/stop of the motor and reset of alarm is done either from the keyboard, through the remote control inputs or through the serial interface (option). The remote control inputs start/stop/reset (PCB terminals 11,12 and 13) can be connected for 2 -wire or 3 -wire control.

| 0060 |  |
| :---: | :---: |
|  | $2$ |
| Default: | 2 |
| Range: | 1,2,3 |
| 1 | START/STOP/RESET command via the keyboard. <br> - Press the "START/STOP" key on the keyboard to start and stop the soft starter. <br> - Press "ENTER/RESET" key to reset a trip condition. |
| 2 | Via Remote control. START/STOP/ RESET commands. The following control methods are possible: - 2-wire start/stop with automatic reset, see § 7.2.1, page 37. <br> - 2-wire start/stop with separate reset, see § 7.2.2, page 37. <br> - 3 -wire start/stop with automatic reset at start, see § 7.2.3, page 37. <br> WARNING! The motor will start if terminals 11, 12, 13 is in start posttion. |
| 3 | START/STOP/RESET commands via serial interface option. Read the operating instruction supplied with this option. |

NOTE! A reset vla the keyboard will not start or stop the motor.

## NOTE! Factory default setting is 2, remote control.

To start and stop from the keyboard, the "START/ STOP" key is used.

To reset from the keyboard, the "ENTER $\leftarrow$ / RESET" key is used. A reset can be given both when the motor is running and when the motor is stopped. A reset from the keyboard will not start or stop the motor.

### 7.2.1 2-wire start/stop with automatic reset at start



Closing PCB terminals 12 and 13 , and a jumper between terminal 11 and 12 , will give a start command. Opening the terminals will give a stop. If PCB terminals 12 and 13 is closed at power up a start command is given (automatic start at power up). When a start command is given there will automatically be a reset.

### 7.2.2 2-wire start/stop with separate reset



Closing PCB terminals 11,12 and 13 will give a start and opening the terminals 12 and 13 will give a stop. If PCB terminals 12 and 13 are closed at power up a start cormmand is given (automatic start at power up). When PCB terminals 11 and 13 are opened and closed again a reset is given. A reset can be given both when the motor is running and stopped and doesn't affect the start/stop.

### 7.2.3 3-wire start/stop with automatic reset at start.



PCB terminal 12 and 13 are normally closed and PCB terminal 11 and 13 are normally open. A start command is given by momentarily closing PCB terminal 11 and 13. To stop, $P C B$ terminal 12 and 13 are momentarily opened.

When a start command is given there will automatically be a reset. There will not be an automatic start at power up.

### 7.3 Menu expansion setting.

In order to use the viewing menus and/or the extended functions menu 007 must be set to "On", then one reach read out of the viewing menus 201915. To be able to set any extended functions in the menus 011-199 menu 008 must be set to "on" as well.


| 0 0 8 <br> 0   |  |
| :--- | :--- | :--- | :--- |
|  0 F |  |
| Default: | oFF |
| Range: | oFF, on |
| offecting of extended |  |
| functions |  |$\quad$| Only view function 201-915 are visi- |
| :--- |
| ble. |

NOTE! Menu 007 must be "on".

### 7.4 Voltage control dual ramp

To achieve even smoother ramps at start and or stop, a dual ramp can be used.


Fig. 33 Menu numbers for dual voltage ramp at start/stop, initial voltage at start and step down-voltage at stop.

The settings are carried out by beginning with the settings in menus 001-004 and 007-008 and proceed with the following steps:


Set the start voltage for start ramp 2. The initial volt age for start ramp 2 is timited to the initial voltage at start (menu 001), see § 7.1, page 36 .

| 0 1 2 0 <br>  Setting of start ramp 2   <br>  O F F |  |
| :--- | :--- | :--- | :--- |
| Default: | oFF |
| Range: | oFF, 1-60 sec |
| oFF | Start ramp 2 disabled |
| $\mathbf{1 - 6 0}$ | Set the start ramp 2 time. A dual <br> voltage ramp is active. |


| 01310 |  |  | Setting of step down voltage in stop ramp 2 |
| :---: | :---: | :---: | :---: |
|  | 4 | 0 |  |
| Default: |  | 40\% |  |
| Range: |  | 100-40\% U ${ }_{n}$ |  |
| Set the step down voltage for stop ramp 2. The step down voltage for stop ramp 2 is limited to the step down voltage at stop (menu 003). |  |  |  |


| 0 1 4 |  |  |  |
| :--- | :--- | :--- | :--- |
|  | Setting of stop ramp time 2 |  |  |
|  | O | F | F |

### 7.5 Torque control parameters

See also $\S 7.10$, page 42 and chapter 4. page 13 for more information on the Torque control setting.


Initial torque at start

| Default: | 10 |
| :--- | :--- |
| Range: | $0-250 \%$ of Tn |

Insert initial torque at start in percent of nominal shaft torque $(\mathrm{Tn})$, see chapter 13 . page 79 .

| 0 1 7 0 <br> 0    |
| :--- | :--- | :--- | :--- |
|  1 5 0 <br>     <br> Default: 150   <br> Range: $50-250 \%$ of Tn torque at start   <br> Insert end torque at start in percent of nominal <br> shaft torque.    |


| 0 1 8 |  |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  | 0 |

### 7.6 Current limit (Main Function)

The Current Limit function is used to limit the current drawn when starting ( $150-500 \%$ of In). This means that current limit is only achieved during set start-up time.

Two kinds of current limit starts are available.

- Voltage ramp with a limited current.

If current is below set current limit, this start will act exactly as a voltage ramp start.

- Current limit start.

The soft starter will control the current up to set current limit immediately at start, and keep it there until the start is completed or the set start-up time expires.
See Fig. 34 Current limit.
NOTE! Make sure that nominal motor current In menu 042 Is correctly inserted.

### 7.6.1 Voltage ramp with current limit

The settings are carried out in three steps:

1. Estimate starting-time for the motor/machine and select that time in menu 002 (see $\S 7.1$, page 36 ).
2. Estimate the initial voltage and select this voltage in menu 001 (see § 7.1, page 36).
3. Set the current limit to a suitable value e.g. $300 \%$ of In in menu 020.


NOTE! Only possible when Voltage Ramp mode is enabled. Menus 021-025 must be "oFF".


Fig. 34 Current limit

### 7.6.2 Current limit

The settings are carried out in two steps:

1. Estimate starting time for the motor/machine and select that time in menu 002 (see $\S 7.1$, page 36 ).
2. Set the current limit to a suitable value e.g. $300 \%$ of In in menu 021.


NOTE! Only possible when Voltage Ramp mode is enabled. Menus 020, 022-025 must be "oFF".

NOTE! Even though the current limit can be set as low as 150\% of the nominal motor current value, this minimum value cannot be used generally. Consideratlons must be glven to the starting torque and the motor before setting the approprlate current IImit. "Real start time" can be longer or shorter than the set values depending on the load conditions. This applles to both current limit methods.


Fig. 35 Current limit
If the starting time is exceeded and the soft starter is still operating at current level, an alarm will be activated. It is possible to let the soft starter to either stop operation or to continue. Note that the current will rise uncontrolled if the operation continues (see $\oint$ 7.24 .2 , page 61 ).

### 7.7 Pump control (Main Function)

By choosing pump control you will automatically get a stop ramp set to 15 sec . The optimising parameters for this main function are start and stop time; initial torque at start and end torque at start and stop. End torque at stop is used to let go of the pump when it's no longer producing pressure/flow, which can vary on different pumps. See Fig. 36.


Fig. 36 Pump control

## Pump application

The pump application is using Torque ramps for quadratic load. This gives lowest possible current and linear start and stop ramps. Related menus are 2,4 (see $\$ 7.1$, page 36 ), 16,17 and 18 (see $\S 7.5$, page 39 ).

| 0 2 2 0 |  |
| :--- | :--- | :--- | :--- |
|   | Setting of pump control |
| Default: | oFF |
| Range: | oFF, on |
| oFF | Pump control disabled. Voltage <br> Ramp enabled. |
| on | Pump control application is enabled. |

NOTE! Only possible when Voltage Ramp mode is enabled. Menu 020-021, 023-025 must be "oFF".

### 7.8 Analogue Input Control (Main Function)

Soft starting and soft stopping can also be controlled via the Analogue Input Control ( $0-10 \mathrm{~V}, 2-10 \mathrm{~V}, 0-20 \mathrm{~mA}$ and $4-20 \mathrm{~mA}$ ). This control makes it possible to connect optional ramp generators or regulators.

After the start command, the motor voltage is controlled through the remote analogue input.


WARNING! The remote analogue control may not be used for continuous speed regulation of standard motors. With this type of operation the increase in the temperature of the motor must be taken Into consideration.

To install the analogue input control, proceed by:

1. Connect the ramp generator or regulator to terminal $14(+)$ and $15(-)$.


Fig. 37 Wiring for analogue input.
2. Set Jumper J1 on the PCB control card to voltage (U) or current control (I) signal position, see Fig. 38 and Fig. 24 on page 28. Factory setting is voltage (U).


Fig. 38 Setting voltage or current for analogue input.

| 0 <br> 0 |  |  | Selection of Analogue input control |
| :---: | :---: | :---: | :---: |
| 0 | F | F |  |
| Default: |  | oFF |  |
| Range: |  | oFF, 1, 2 |  |
| oFF |  | Analogue input disabled. Voltage Ramp enabled. |  |
| 1 |  | Analogue input is set for 0-10V/ $0-20 \mathrm{~mA}$ control signal |  |
| 2 |  |  | ue input is set for 2-10V/ A control signal. |

NOTE! Only possible when Voltage Ramp mode is enabled. Menu 020-022, 024, 025 must be "oFF"

### 7.9 Full voltage start, D.O.L. (Main Function)

The motor can be accelerated as if it was connected directly to the mains. For this type of operation:

Check whether the motor can accelerate the required load (D.O.L.-start, Direct On Line start). This function can be used even with shorted thyristors.

| 0 2 4 <br> 0   |  |  |
| :--- | :--- | :--- |
|  | 0 | F |
|  | Fetting of D.O.L start |  |
| Default: | oFF |  |
| Range: | oFF, on |  |
| oFF | D.O.L. start disabled. <br> Voltage Ramp enabled. |  |
| on | D.O.L. start enabled |  |

NOTE! Only possible when Voltage Ramp mode is enabled. Menu 020-023, 025 must be "ofF".


Fig. 39 Full voltage start.

### 7.10 Torque control (Main function)

This main function can be used to make a start according to a pre-defined torque reference curve. Two different load characteristics, linear and square, are possible to select.

At start/stop the torque controller will follow the selected characteristic.

A torque start/stop behaviour can be seen in Fig. 40.

A perfect start and stop with torque ramps have a good linearity of current. To optimise this, use the setting of initial torque (menu 16) and end torque (menu $18)$. See also $\S 7.5$, page 39 .

## Example:

Default for initial torque is $10 \%$ so if starting a more heavy load this will result in a small current peak in beginning of ramp. By increasing this value to $30 /$ $70 \%$ the current peak will not appear.

| 0 2 5 |  |  |
| :--- | :--- | :--- | :--- |
|  | O | Torque control at start/stop |
|  | F | F |
| Default: | oFF |  |
| Range: | oFF, 1, 2 |  |
| oFF | Torque control is disabled Voltage <br> Ramp enabled. |  |
| $\mathbf{1}$ |  | Torque control with linear torque <br> characteristic |
| $\mathbf{2}$ |  | Torque control with square torque <br> characteristic |

NOTE! Torque control mode Is only possible when Voltage Ramp mode is enabled (menu 020-024 are "oFF").

The end torque is increased mainly if the application has a high inertial load, like planers, saws and centrifuges. A current peak will appear in the end of ramp because the load is pushing the speed more or less by itself. By increasing this level to 150-250\% the current will be linear and low.


Fig. 40 Torque control at start/stop.


Fig. 41 Current and speed in torque control.

### 7.11 Torque boost

The Torque Booster enables a high torque to be obtained by providing a high current during $0.1-2 \mathrm{sec}$ at start. This enables a soft start of the motor even if the break away torque is high at start. For example in crushing mills applications etc.

When the torque booster function has finished, starting continues according to the selected start mode.


Fig. 42 The principle of the Torque Booster when starting the motor in voltage ramp mode.

See $\int 4.6$, page 19 , which main function that can be used with the torque boost.



NOTE! Check whether the motor can accelerate the load with "Torque booster", without any harmful mechanical stress.

### 7.12 Bypass

In cases of high ambient temperatures or other reason it may sometimes be necessary to use a by-pass contactor to minimize the power loss at nominal speed (see Technical Data). By using the built-in Full Voltage Relay function an external contactor can be used to Bypass the soft starter when operating at nominal speed.

Bypass contactor can also be used if soft stop is required. Normally a Bypass contactor is not necessary as the device is designed for continues running conditions, see Fig. 29 on page 33 for wiring example.

NOTE! If one like to use the alarm functlons, the extended functlons or the vlewing functions the 2-pcs current transformers must be mounted outside the soft start as shown In Fig. 44 and Fig. 45 on page 45 . For this purpose an optional extension cable for the current transformers is avallable. Code No 01-2020-00.


CAUTION! If the current transformers are not mounted as In Fig. 43 on page 44 and $\S 6.2$, page 28, the alarm and vlewing functions will not work. Do not forget to set menu 032 to ON, otherwise there wIII be an F12 alarm and at the stop command will be a freewheelling stop.

For further information see chapter 6.2 page 28.


Fig. 43 Bypass wiring example MSF 310-1400.

SOFTSTARTER


MOTOR
Fig. 44 Current transformer position when Bypass MSF-017 to MSF-250.


Fig. 45 Current transformer pasition when Bypass MSF- 310 to MSF-1400.

### 7.13 Power Factor Control

During operation, the soft starter continuously monitors the load on the motor. Particularly when idling or when only partially loaded, it is sometimes desirable to improve the power factor. If Power factor control (PFC) is selected, the soft starter reduces the motor voltage when the load is lower. Power consumption is reduced and the degree of efficiency improved.


NOTE! If the PFC is used the EMC-directive is not fulfilled.

### 7.14 Brake functions

There are two built in braking methods for applications were the normal stop ramp is not enough.

## - Dynamic DC-brake

Increases the braking torque by decreasing speed.

- Soft brake

Gives a high torque at the start of the braking and then also increasing torque by decreasing speed.

In both methods the MSF detects when the motor is standing still, so rotating in wrong direction is avoided.

## Dynamic Vector Brake

- Possible to stop motors with high inertia loads from close to synchronous speed.
- At $70 \%$ of the nominal speed a DC-brake is activated until the motor is standing still or the selected Braking Time has expired (see menu 34, next page).
- No contactor needed.
- For extra safety, the soft starter has a digital input signal for monitoring standstill so that at real motor standstill will stop the output voltage immediately (see $₫ 7.19$, page 53 ).


## Soft brake

- Even very high inertia loads can be stopped
- The Soft brake is a controlled reversing of the motor as the MSF measures the speed during braking.
- Two contactors are needed which can be placed on the in- or output of the soft starter. On the input the first contactor is connected to relay K1 which is also used as a mains contactor.
- At $30 \%$ of the nominal speed a DC-brake is activated until the motor is standing still or the selected Braking Time has expired (menu 34, next page).
- For extra safety, the soft starter has a digital input signal for monitoring standstill. So that the output voltage is stopped immediately (see menu 57-58, 7.19 , page 53 ).

See Fig. 47 on page 47 for the following set-up sequence:

- Soft brake is activated if menu $36=2$ and menu 34 has a time selected (see next page).
- Menu 51 and 52 are automatically set to 5 and 4 to get the correct relay functions on K1 and K2 (see $\S$ 7.17, page 51).
- Relay K1 should be used to connect a contactor for supply L1, L2, L3 to MSE or motor.
- Relay K2 is used to connect phase shifting contactor to change L1, L2 and L3 to MSF or motor.
- At start K1 is activated and connects L1, L2, L3 then the motor starts. At stop K1 opens and disconnects L1, L2, and L3 and after 1s K2 connects with the other phase sequence and the braking of the motor is active.

NOTE! Soft brake uses both programmable relays. For other functlons, see also the function table in chapter 7. page 35.

NOTE! For several start/stops it is recommend to use the PTC Input.


WARNING! If the Soft Brake function has been selected once and after that the Bypass function Is selected, then the relay functions on K1 and K2 remaln In the Soft Brake functlonality. Therefore it Is necessary to change the relay functions in menu 51-52 manually to the Bypass functlons (see § 7.17, page 51) or reset to default In menu 199 (see $\S 7.28$, page 63) and select the Bypass function agaln.



Fig. 46 Braking time

| 0 3 0 |  |
| :--- | :--- | :--- | :--- |
|  1 0 |  |
| Default: | 100 |
| Range: | $100-500 \%$ |




Fig. 47 Soft brake wining example.

### 7.15 Slow speed and Jog functions

The soft starter is able to run the motor at a fixed slow speed for a limited period of time.

The slow speed will be about $14 \%$ of the full speed in the forward direction and $9 \%$ in the reverse direction.

The following functions are possible:

## - Slow speed controlled by an external signal.

The digital input is used to run at slow speed at a start or stop command for a selected number of pulses (edges) generated by an external sensor (photo cell, micro switch, etc.). See $\S 7.19$, page 53 for more instructions.

- Slow Speed during a selected time period.

The slow speed will be active after a stop command for a selected time period. See $\$ 7.19$, page 53 for more instructions.

- Slow Speed using the "JOG"-commands.

The slow Speed can be activated via the JOG keys on the keyboard or externally via the analogue input. See $\S 7.25$, page 61 for more instructions.

### 7.15.1 Slow speed controlled by an external signal.

With these setting it is possible to have an external pulse or edge signal controlling the time that the Slow Speed is active either after a Start command or a Stop command or at both commands. The following menu's are involved:

| Menu | Function | See page |
| :--- | :--- | :--- |
| 57 | Digital input selection | page 53 |
| 58 | Pulse selection | page 53 |
| 37 | Slow speed torque | page 49 |
| 38 | Slow speed time at start | page 49 |
| 39 | Slow speed time at stop | page 49 |
| 40 | DC-Brake at slow speed | page 49 |

Installation is as follows:

1. Set the analogue input selection for Slow Speed operation. Menu $57=2$. See $\S 7.19$, page 53 . See Fig. 37 on page 41 for a wiring example.
2. Select in menu 38 (see $\S 7.15 .2$, page 49 ) the Slow Speed at Start time. This time will now be the absolute maximum time for Slow Speed to be active after a start command, in case the external signal will not appear.
3. Select in menu 39 (see $\S 7.15 .2$, page 49) the Slow Speed at Stop time. This time will now be the absolute maximum time for Slow Speed to be active after a stop command, in case the external signal will not appear.
4. Select in menu 57 (see $\S 7.19$, page 53 ) the number of edges to be ignored by the Slow Speed input, before a start or stop is executed at slow speed. The edges are generated by an external sensor (photo cell, micro switch, etc.).

The Slow Speed torque (menu 37) and DC-Brake after Slow Speed (menu 40) can be selected if needed. (see § 7.15.4, page 49).

When the number of edges exceeds or the time expire, a start according to selected main function is made.

At stop, the motor will ramp down (if selected) and DC brake (if selected) before a slow speed forward at stop will begin. Slow speed will last as long as the number of edges on the external input is below parameter value in menu 036 and the max duration time doesn't expires. When the number of edges exceeds or the time expire, a stop is made.

In Fig. 48 on page 48 the selected number of edges are 4. It is recommended to select DC-brake (se $\S 7.14$, page 46) before a slow speed at stop if it is a high inertia load. See Fig. 29 on page 33 for wiring diagram. In case one use DC-brake, see $\S 7.15 .4$, page 49 .


Fig. 48 Slow speed controlled by an external signal.
This additional function can be used together with most of the main functions (see $\$ 4.6$, page 19).

| ${ }^{0} \mathbf{O}\|3\| 7{ }_{0}^{\circ}$ |  |  | Slow speed torque |
| :---: | :---: | :---: | :---: |
|  | $1$ | $0$ |  |
| Default: |  | 10 |  |
| Range: |  |  |  |
| Select the magnitude of the slow speed torque. |  |  |  |

### 7.15.2 Slow speed during a selected time

It is possible to have a slow speed in forward direction before a start and after a stop. The duration of the slow speed is selectable in menus 038 and 039.

It is recommended to select DC brake (sec $\S 7.14$, page 46) before a slow speed at stop if it is a high inertia load. This slow speed function is possible in all control modes, keyboard, remote and serial communication.


Fig. 49 Slow speed at start/stop during a selected time.
The Slow speed torque (menu 37) and the DC-Brake after Slow speed (menu $40, \S 7.15 .4$, page 49 ) can be selected if needed.

### 7.15.3 Jog Functions

The Jog commands can be used to let the motor run at a Slow speed (forward or reverse) as long as the Jog command is active.

The Jog commands can be activated in 2 different ways:

- Jog keys

The Jog-Forward and Jog-reverse keys on the control panel. The keys can be programmed separate for each function. See $\S 7.25$, page 61 for more instructions

- External Jog command

The external command is given via terminal 14 at the digital input. Only 1 function (forward or reverse) can be programmed to the digital input at the time. See $\S 7.19$, page 53 for more instructions.

### 7.15.4 DC-brake after slow speed at stop [040]

A DC-brake after a slow speed at stop is possible to have, i.e. for a high inertia load or for a precise stop.

The current is controlled and the reference value for the normal DC-brake function is used (see $\$ 7.15 .4$, page 49 ).
The duration for the DC-brake is possible to select.
This DC-brake function is not applied when the "JOG $\Omega$ " and "JOG $\Omega$ " keys are used.


### 7.16 Motor data setting

The first step in the settings is to set menu 007 and 008 to "on" to be able to reach the menus 041-046 and enter the motor data.

NOTE! The default factory settings are for a standard 4-pole motor acc. to the nominal current and power of the soft starter. The soft starter will run even if no specific motor data is selected, but the performance wIII not be optimal.


Make sure the soft starters maximum voltage rating is suitable for chosen motor voltage.




NOTE! Now go back to menu 007, 008 and set it to "oFF" and then to menu 001.


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## 7．17 Programmable relay K1 and K2

The soft starter has three built－in auxiliary relays，K3 （change over contacts），is always used as an alarm relay． The other two relays，K1 and K2（closing contacts），are programmable．

K1 and K2 can be set to either＂Operation＂，＂Full Voltage＂or＂Pre－alarm＂indication．If DC－brake is chosen the relay K2 will be dedicated to this function．


| $O$ 5 2 |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  | 2 |  |

WARNING！If the Soft Brake function has been selected once and after that the Bypass function Is selected，then the relay functions on K1 and K2 remain In the Soft Brake functionallty．Therefore it Is necessary to change the relay functlons In menu $51-52$ manually to the Bypass functlons（see $\S$ 7．12，page 43）or reset to default In menu 199 （see $\S 7.28$ ，page 63）and select the Bypass functlon agaln．

Fig． 50 Start／stop sequence and relay function＂Operation＂and ＂Full voltage＂．

| 0 5 1 <br> 0   |  |  |
| :--- | :--- | :--- |
|  |  |  |
|  | Setting of K1 indication |  |
| Default： | 1 |  |
| Range： | $1,2,3,4,5$ |  |
| $\mathbf{1}$ | K1 is set for＂Operation＂ |  |
| $\mathbf{2}$ |  | K1 is set for＂Full Voltage＂ |
| $\mathbf{3}$ | K1 is set for＂Power pre－alarm＂ |  |
| $\mathbf{4}$ | No function |  |
| $\mathbf{5}$ | K1 is set for＂Run＂ |  |

### 7.18 Analogue output

The soft starter can present current, voltage and power on an analogue output terminal, for connection to a recording instrument or a PLC. The output can be configured in 4 different ways, $0-10 \mathrm{~V}$,
$2-10 \mathrm{~V}, 0-20 \mathrm{~mA}$ or $4-20 \mathrm{~mA}$. To install the instrument proceed as follows:

1. Connect the instrument to terminal $19(+)$ and $15(-)$.


Fig. 51 Wiring for analogue output.
2. Set Jumper J2 on the PCB board to voltage ( U ) or current (I) signal position. Factory setting is voltage (U). See Fig. 52 on page 52 and Fig. 24 on page 28.

4. Choose a read-out value in menu 055


|  |  | 1 |
| :--- | :--- | :--- |
| Analogue output value |  |  |
| Default: | 1 |  |
| Range: | $1,2,3$ |  |
| $\mathbf{1}$ | RMS current, default range 0-5xIn |  |
| $\mathbf{2}$ | Line input RMS voltage, default <br> range 0-720V |  |
| $\mathbf{3}$ | Output shaft power, default range <br> $0-2 \times P n$ |  |

5. Set analogue output gain to adjust the range of chosen analogue output value in menu 056.


Example on settings:

| Set value | $\mathbf{I}_{\text {scale }}$ | $\mathbf{U}_{\text {scale }}$ | $\mathbf{P}_{\text {scale }}$ |
| :--- | :--- | :--- | :--- |
| $100 \%$ | $0-5 \times I_{n}$ | $0-720 \mathrm{~V}$ | $0-2 \times P_{\mathrm{n}}$ |
| $50 \%$ | $0-2.5 x \mathrm{I}_{\mathrm{n}}$ | $0-360 \mathrm{~V}$ | $0-P_{\mathrm{n}}$ |

Fig. 52 Setting of current or voltage output.
3. Set the parameter in menu 054.

| 0.5 4 |  |  |
| :--- | :--- | :--- |
|  | 0 | Analogue output |
|  |  | F |
| Default: | oFF |  |
| Range: | oFF, 1, 2 |  |
| oFF | Analogue ouput is disabled |  |
| $\mathbf{1}$ | Analogue output is set to <br> O-10V/0-20mA |  |
| $\mathbf{2}$ | Analogue output is set to <br> $0-10 \mathrm{~V} / 4-20 \mathrm{~mA}$ |  |

### 7.19 Digital input selection

The analogue input can be used as a digital input. This is programmed in Menu 57. There are 4 different functions:

- Rotation sensor input for braking functions. See $\$ 7.14$, page 46 .
- Slow speed external controlled. See $\S 7.15 .1$, page 48.
- Jog functions forward or reverse enabled. See $\oint$ 7.25 , page 61 .

Fig. 53 shows how to set the input for voltage or current control, with jumper J1 the control board. The default setting for J 1 is voltage control.


Fig. 53 Setting of J1 for current or voltage control.
Fig. 54 shows a wiring example for the analogue input as it is used for digital input.


Fig. 54 Wiring for slow speed external input.
NOTE! If the Main Function Analogue control Is programmed (see § 7.8, page 41) the analogue Input can not be used for digltal signal input. The menu 57 is then automatlcally set to OFF.

| 0 5 7 <br> 0   |  |  |  |
| :--- | :--- | :--- | :--- |
|  | 0 | Digital input selection |  |
|  | 0 | $F$ | F |
| Default: | oFF |  |  |
| Range: | oFF, 1-4 |  |  |
| oFF | No digital input control |  |  |
| $\mathbf{1}$ |  | Rotation sensor for brake functions |  |
| $\mathbf{2}$ | Slow speed function |  |  |
| $\mathbf{3}$ |  | Jog forward command |  |
| $\mathbf{4}$ |  | Jog reverse command |  |

NOTE! Jog forward, reverse has to be enabled, see $\$ \mathbf{7 . 2 5}$, page 61.

Depending on the selection made in menu 57, menu 58 is used to program the number of the edges. The edges can be generated by an external sensor (photo cell, micro switch etc.).

## $0588_{\circ}^{\circ}$

|  |  |  |
| :--- | :--- | :--- |

### 7.20 Parameter Set

Parameter Set, an important function which can be handy when using one soft starter to switch in and start different motors, or working under variable load conditions. For example; starting and stopping conveyor belts with different weight on the goods from time to time.

For sets of parameters can be controlled either from the keyboard, the external control inputs or the serial interface (option). Up to 51 different parameters can be set for each Parameter Set.


Fig. 55 Parameter overview
When 'Parameter set' in menu 061 is set to 0 (external selection), only parameters in menu 006 (Control mode) and 061 (Parameter set) can be changed. All other parameters are not allowed to change.

It is possible to change parameter set at stop and at full voltage running.

Parameter set

| Default: | 1 |
| :--- | :--- |
| Range: | $0,1,2,3,4$ |
| $\mathbf{0}$ | Parameter set are selected by the <br> external input 16 and 17 (see <br> below). |
| $\mathbf{1 , 2 , 3 , 4}$ | Selection of parameter set 1-4. |



Fig. 56 Connection of external control inputs.

| Parameter Set | PS1 (16-18) | PS2 (17-18) |
| :---: | :---: | :---: |
| 1 | Open | Open |
| 2 | Closed | Open |
| 3 | Open | Closed |
| 4 | Closed | Closed |

7.21 Motor protection, overload (F2 alarm)
In many cases it is convenient to have a complete starter. The soft starter have a possibility to use either an input PTC signal from the motor, an internal thermal model of the motor for thermal protection or both together at the same time. Slight overload for long time and several overloads of short duration will be detected with both methods.


NOTE! Open terminals will give an F2 alarm immedlately. Make sure the PTC is always connected or the terminals are shorted.

NOTE! The Internal motor thermal protection will stlll generate an alarm If it is not selected oFF.

| 0 | 7 | 2 | Internal motor thermal <br> protection |
| :--- | :--- | :--- | :--- |
| Default: | 10 |  |  |
| Range: | ofF, 2-40 sec |  |  |
| oFF | Internal motor protection is disabled. <br> $2-40$ <br> Selection of the thermal curve <br> according to Fig. 57 <br> - Check that menu 042 is set to the <br> proper motor current (see § 7.16, <br> page 50). <br> - If the current exceeds the 100\% <br> level an F2 alarm is activated. <br> - The motor model thermal capacity <br> must cool down to 95\% before reset <br> can be accepted. <br> - Used thermal capacity in menu 073 <br> in § 7.21, page 55. |  |  |

NOTE! If 'Bypass' Is used check that the current transformers are placed and connected correctly (see Fig. 43 on page 44).


CAUTION! Used thermal capacity is set to 0 if the control board loses its supply (terminal 01 and 02). This means that the Internal thermal model starts with a 'cold' motor, which perhaps in reallty Is not the case. Thls means that the motor can be overheated.


Fig. 57 The thermal curve

### 7.22 Mains protection



Read-out of the used thermal capacity. If menu 072 'Internal motor thermal protection' is selected oFF, the capacity is shown as if the default class 10 was selected.


Insert limit in \% of nominal motor voltage. Max voltage of the 3 input phases is compared with the selected value. This is a category 2 alarm.

| 0 8 4 0 <br> 0    |  |  |  |
| :--- | :--- | :--- | :--- |
|  | 0 | F | F |
| Response delay over voltage |  |  |  |
| alarm |  |  |  |$|$



Insert limit in \% of nominal motor voltage. Min voltage of the 3 input phases is compared with the selected value. This is a category 2 alarm.

| 086 |  |  | Response delay under voltage alarm |
| :---: | :---: | :---: | :---: |
| 0 | $F$ | F |  |
| Default: |  | oFF |  |
| Range: |  | oFF, 1-60 sec |  |
| OFF |  | Under voltage alarm is disabled |  |
| 1-60 |  | Set the response delay time for under voltage alarm F10 |  |


| 08 7 0  <br>     <br>   - - |  |
| :--- | :--- | :--- |
| Phase sequence |  |
| Default: | - |
| Range: | L123, L321 |
| L123 is the direct phase sequence. <br> L321 is the reverse phase sequence. |  |


| 08 8 0 |
| :--- | :--- | :--- | :--- |
|  0 $F$ Phase reversal alarm <br> Default: oFF   <br> Range: oFF, on   <br> oFF Phase reversal alarm is disabled   <br> on Sets the phase reversal Alarm. <br> - Switch on the power supply first. <br> The phase sequence is stored as <br> the correct sequence. <br> - Sets the menu 088 to "on". <br> - Any reversal of phase sequence will <br> cause alarm F16.   |

NOTE! The actual phase sequence can be vlewed in menu 87.

### 7.23 Application protection (load monitor)

### 7.23.1 Load monitor max and min/protection (F6 and F7 alarms)

MSF has a built in load monitor based on the output shaftpower. This is a unique and important function which enables protection of machines and processes driven by the motor connected to the soft starter. Both a Min and Max limit is possible to select.

In combination with the pre-alarm function, see $\oint 7.23 .2$, page 58 , this create a powerful protection. An auto set function is also included for an automatic setting of the alarm limits. A start-up delay time can be selected to avoid undesired alarms at start-up, see Fig. 58 on page 60.

NOTE! The load monitor alarms are all dlsabled during a stop ramp.

| 089 0  <br>   Auto set power limits <br>   $n$ |  |
| :--- | :--- | :--- |
| Default: | no |
| Range: | no, YES |
| no | Auto set is disabled |
| YES | Auto set is activated if ENTER is <br> pressed. |


| 0 9 0  <br>     <br>    0 |  |
| :--- | :--- | :--- | :--- |
| Default: | - |
| Range: | $0-200 \%$ |
| Measured output shaftpower in \% of nominal motor <br> power. |  |

NOTE! System must be in full voltage running before an auto set ls permitted.

The actual power is regarded as $1.00 \times \mathrm{xPact}$.
The set levels are:

| Power max alarm limit[092]: | $1.15 \times P$ actual |
| :--- | :--- |
| Power max pre-alarm limit[094]: | $1.10 \times P$ actual |
| Power min pre-alarm limit[096]: | $0.90 \times P$ actual |
| Power min alarm limit[098]: | $0.85 \times P$ actual |

A successful auto set shows a message 'Set' for 3 s and if something goes wrong a message 'no' will be showed.

### 7.23.2 Pre-alarm

It could be useful to know if the load is changing towards a load alarm limit. It is possible to insert both a Max and Min pre-alarm limit based on the motor output shaft power. If the load exceeds one of these limits, a pre-alarm condition occurs.

It should be noted that it is not normal alarms. They will not be inserted in the alarm list, not activating the alarm relay output, not displayed on the display and they will not stop operation. But it is possible to activate relay K 1 or K 2 if a pre-alarm condition occurs. To have pre-alarm status on any of these relays, select value 3 in menu 051 or 052 (see $\S 7.17$, page 51 ).

A start-up delay time can be selected in menu 091 to avoid undesired pre-alarms at start-up. Note that this time is also shared with power Max and Min alarms.

NOTE! The pre-alarm status is always avallable on the serlal communication.


Insert limit in \% of nominal motor power. The actual power in \% of nominal motor power, could be read out in menu 090. If output shaft power exceeds selected limit, a pre-alarm occurs after the response delay time. The 'Auto set' function in menu 089, affect selected limit even if the pre-alarm is set "oFF" in menu 095.

| 0 9 5 0 |  |
| :--- | :--- | :--- | :--- |
|  0 F F <br> Max pre-alarm response    <br> delay    |  |
| Default: | OFF |
| Range: | oFF, 0.1 - 25.0 sec |
| oFF | Max Pre-Alarm is disabled. |
| $\mathbf{0 . 1 - 2 5 . 0}$ | Sets the response delay of the Max <br> Pre-Alarm level. |


| 0 | 9 | 6 | 0 |
| :--- | :--- | :--- | :--- |


| 0 9 9 |  |  |  |
| :--- | :--- | :--- | :--- |
|  | O | F | Min alarm response delay |
| Default: | oFF |  |  |
| Range: | oFF, O.1-25.0 sec |  |  |
| oFF | Min Alarm is disabled |  |  |
| $\mathbf{0 . 1 - 2 5 . 0}$ | Sets the response delay of the Min <br> Alarm level. The Min alarm is disa- <br> bled during a stop ramp down. |  |  |





### 7.24 Resume alarms

### 7.24.1 Phase input failure F1

- Multiple phase failure.

Shorter failure than 100 ms is ignored. If failure duration time is between 100 ms and 2 s , operation is temporary stopped and a soft start is made if the failure disappears before 2 s . If failure duration time is longer than 2 s , an F1 alarm is given in cat. 2.

- Single phase failure.

During start up (acceleration) the behaviour is like multiple phase failure below. When full voltage running there is a possibility to select the behaviour.

| 1 $O$ 1 Run at single phase loss <br>   $n$ 0 <br> Default: no   <br> Range: no, YES   <br> no Soft starter trips if a single phase <br> loss is detected. Alarm F1 (category <br> 2) will appear after 2 sec.   <br> YES Soft starter continues to run after a <br> single phase loss. <br> - Alarm F1 appears after 2 sec. <br> - If the loose phase is reconnect the <br> alarm is reset automatically. <br> - If running on 2 phases, a stop com- <br> mand will give a Direct on line stop <br> (freewheel)   |
| :--- | :--- | :--- | :--- |

### 7.24.2 Run at current limit time-out F4

In modes 'Current limit at start' and 'Voltage ramp with current limit at start' an alarm is activated if still operating at current limit level when selected ramp time exceeds. If an alarm occurs there is a possibility to select the behaviour.

| $1\|0\| 20$ |  |  | Run at current limit time-out |
| :---: | :---: | :---: | :---: |
|  | n | 0 |  |
| Default: |  | no |  |
| Range: |  |  |  |
| no |  |  | tarter trips if the current limit ut is exceeded. Alarm F4 (cate 2) appears. |
| YES |  |  | tar ter continues to run after the timit time-out has exceeded: F4 appears current is no longer controlled he soft starters ramps up to full ge with a 6s ramp time. the alarm with either ENTER/ ET key or by giving a stop comd. |

### 7.25 Slow speed with JOG

Slow speed with "JOG" is possible from the "JOG" keys, but also from terminals, see menu 57 page 53 and serial comm. The "JOG" is ignored if the soft starter is running. The slow speed "JOG" function has to be enabled for both forward and reverse directions in menus 103 and 104 , see below.

NOTE! The enable functions is for all control modes.

| 1 | 0 | 3 | 0 |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  |  |  |
|  |  | 0 | JOG forward enable |
|  |  | $F$ | $F$ |
| Default: | oFF |  |  |
| Range: | oFF, on |  |  |
| oFF | JOG forward disabled |  |  |
| on | JOG forward enabled |  |  |



Fig. 59 The 2 Jog keys.

### 7.26 Automatic return menu

Often it is desirable to have a specific menu on the display during operation, i.e. RMS current or power consumption. The Automatic return menu function gives the possibility to select any menu in the menu system.

The menu selected will come up on the display after 60 sec . if no keyboard activity. The alarm messages (F1-F16) have a priority over menu 105 (as they have for all menus).


### 7.27 Communication option, related Parameters

The following parameters have to be set-up:

- Unit address.
- Baud rate.
- Parity
- Behaviour when contact broken.

Setting up the communication parameter must be made in local 'Keyboard control' mode. See $\S 7.2$, page 37.


| 1 1 3 0 <br>     <br>    Serial comm parity <br>    0 <br> Default: 0   <br> Range: 0.1   <br> This parameter will select the parity. <br> 0 <br> 1 No parity. <br> Even parity.   |
| :--- | :--- | :--- |

## Serial comm. broken alarm

If control mode is 'Serial comm. control' and no contact is established or contact is broken the Soft starter consider the contact to be broken after 15 sec , the soft starter can act in three different ways:

1 Continue without any action at all.
2 Stop and alarm after 15 sec .
3 Continue and alarm after 15 sec .
If an alarm occurs, it is automatically reset if the communication is re-established. It is also possible to reset the alarm from the soft starter keyboard.

| 1 1 4 0 <br> 0    |  |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
|  |  | Serial comm. contact <br> interrupted |  |
| Default: | 1 |  |  |
| Range: | oFF, 1, 2 |  |  |
| This parameter will control the behaviour in the soft <br> starter when the serial comm. is interrupted. <br> oFF No alarm and continue operation. <br> 1 | Alarm and stop operation. |  |  |
| 2 | Alarm and continue operation. |  |  |



### 7.28 Reset to factory setting [199]

When selecting reset to factory settings:

- All parameters in all parameter sets will have default factory settings.
- Menu 001 will appear on the display.
- Note that the alarm list, the power consumption and the operation time will not have default settings.

| $\|$19 0 <br> 0  |  |
| :--- | :--- | :--- |
|   Reset to factory settings <br>   n |  |
| Default: | no |
| Range: | no, YES |
| no | No reset |
| YES | Reset all functions to the factory <br> defaults incl. all 4 Parameter Sets. |

NOTE! Reset to factory settings is not allowed at run.

### 7.29 View operation

## General

The soft start includes as standard a numerous metering functions which eliminates the need of additional transducers and meters.

## Measured values

- Current RMS 3-phase current and per phase
- Voltage RMS 3-phase voltage and per phase
- Output shaft power/torque $\mathrm{kW} / \mathrm{Nm}$
- Power factor
- Power consumption in kWh
- Operation time in hours


## Viewing of the measured values

After setting motor data and extended functions one can set menu 008 in oFF and will then automatically move to menu 201, the first menu viewing the measured values and thus eliminate to scroll through menu 011 to menu 199.



NOTE! The power factor vlewing will not work at bypass even If the current transformers are mounted outside the soft start.


View the total power consumption.

NOTE! Thls Is the same read-out as menu 005 see $\mathbb{\S} \mathbf{7 . 1 . 1}$, page 36.


RMS current in phase L1

|  | - |
| :--- | :--- |
| Default: | - |
| Range: | $0.0-9999 A m p$ |
| View the current in phase L1. |  |



### 7.30 Keyboard lock

The keyboard can be locked to prohibit operation and parameter setting by an unauthorised. Lock keyboard by pressing both keys "NEXT $\rightarrow$ " and "ENTER $\boldsymbol{L}^{\prime \prime}$ for at least 2 sec . The message '- Loc' will display when locked. To unlock keyboard press the same 2 keys "NEXT $\rightarrow$ " and "ENTER $\downarrow$ " for at least 2 sec. The message 'unlo' will display when unlocked.

In locked mode it is possible to view all parameters and read-out, but it is forbidden to set parameters and to operate the soft starter from the keyboard.

The message '-Loc' will display if trying to set a parameter or operate the soft starter in locked mode.

The key lock status can be read out in menu 221.

| 2 2 1 <br> 0   |  |  | Locked keyboard info |
| :---: | :---: | :---: | :---: |
|  | n | 0 |  |
| Default: |  | no |  |
| Range: |  |  |  |
| no |  |  | ard is not locked |
| YES |  | Key | ard is locked |

### 7.31 Alarm list

The alarm list is generated automatically. It shows the latest 15 alarms (F1 - F16). The alarm list can be useful when tracing a failure in the soft starter or its control circuit. Press key "NEXT $\rightarrow$ " or "PREV $\leftarrow$ " to reach the alarm list in menus 901-915 (menu 007 has to be ON).

8. PROTECTION AND ALARM

The soft starter is equipped with a protection system for the motor, the machine and for the soft starter itself.
Three categories of alarm are available:

## Category 1

Alarm that stops the motor and need a separate reset before a new start can be accepted.

## Category 2

Alarm that stops the motor and accepts a new start command without any separate reset.

## Category 3

Alarm that continues to run the motor.
All alarm, except pre-alarm, will activate the alarm relay output K3, flash a red fault number on the display and it will also be placed in the alarm list. As long as the alarm is active, the display is locked in the alarm indication.

The relay output K3 can be used in the control circuit for actions needed when alarm occurs.

If more than one alarm is active, it is the last alarm that is presented on the display.

### 8.1 Alarm description

### 8.1.1 Alarm with stop and requiring a separate reset

Operation will stop for a category 1 alarm. A separate reset is needed before a new start command is accepted. It is possible to reset from keyboard (pushing "ENTER/RESET") regardless of selected control mode. It is also possible to reset the alarm from the actual control mode (i.e. if control mode is serial communication, a reset is possible to do from serial communication).

A reset is accepted first when the alarm source goes back to normal.

When a reset is made, the alarm relay output K 3 is deactivated, the alarm indication on the display disappear and the original menu shows.

After a reset is made the system is ready for a new start command.

### 8.1.2 Alarm with stop and requiring only a new start command

Operation will stop for a category 2 alarm. A restart can be done and at the same time the alarm relay output K3 is deactivated, the alarm indication on the display disappear and the original menu shows.

It is still possible to reset the alarm in the same way as for category 1 alarms (see 8.1.1), if a start is not required at the time.

### 8.1.3 Alarm with continue run

Operation will continue run for a category 3 alarm. Some different reset behaviour is possible (see remarks for the specific alarms in $\$ 8.2$, page 67 ).

- Automatic reset when the alarm source goes back to normal.
- Automatic reset when a stop command is given.
- Manual reset during run.

When the reset occurs, the alarm relay output K3 is deactivated, the alarm indication on the display disappear and the original mentu shows.
8.2 Alarm overview

| Display Indication | Protective function | Alarm category | Remark |
| :---: | :---: | :---: | :---: |
| F1 | Phase input failure. | Cat 3. Run with auto reset. | Single phase failure when full voltage running if menu 101 'Run at phase loss' = YES. If the fault phase comes back, an automatic reset is made. |
|  |  | Cat 2. Stop with reset in start. | Multiple phase failure or single phase failure when not full voltage running or if menu 101 ' Run at phase loss' = no. |
| F2 | Motor protection, overload. | Cat 1. Stop with manual reset. | If menu 071 'Motor PTC input' = YES, cool down the motor. <br> If menu 071 'Motor PTC input' = no, the internal model has to 'cool' down. |
| F3 | Soft start overheated | Cat 1. Stop with manual reset. | If not cooled down, a reset will not be accepted. |
| F4 | Full speed not reached at set current limit and start time. | If menu 102 'Run at current limit time-out' $=$ no. <br> Cat 2. Stop with reset in start. | The current limit start is not completed. |
|  |  | If menu 102 'Run at current limit time-out' = YES. <br> Cat 3. Run with manual reset. | When start time expired, a 6 sec ramp is used to reach full voltage, without control of the current. Reset the alarm with either a manual reset or a stop command. |
| F5 | Locked rotor. | Cat 1. Stop with manual reset. | Motor and/or machine protection. |
| F6 | Above max power limit. | Cat 1. Stop with manual reset. | Machine protection. |
| F7 | Below min power limit. | Cat 1. Stop with manual reset. | Machine protection. |
| F8 | Voltage unbalance. | Cat 2. Stop with reset in start. | Motor protection. |
| F9 | Over voltage. | Cat 2. Stop with reset in start. | Motor protection. |
| F10 | Under voltage. | Cat 2. Stop with reset in start. | Motor protection. |
| F11 | Starts / hour exceeded. | Cat 2. Stop with reset in start. | Motor and/or machine protection. |
| F12 | Shorted thyristor. | Cat 3. Run with manual reset. | When stop command comes, the stop will be a 'Direct On Line' stop, and the soft starter will be resetted. After this fault it is possible to start only in 'Direct On Line' mode. One or more thyristors probably damaged. |
| F13 | Open thyristor. | Cat 1. Stop with manual reset. | One or more thyristors probably damaged. |
| F14 | Motor terminal open. | Cat 1. Stop with manual reset. | Motor not correctly connected. |
| F15 | Serial communication broken. | If menu 114 Serial comm. contact broken $=1$. Cat 2 . Stop with reset in start. | Serial communication broken will stop operation. Run from keyboard if necessary. |
|  |  | If menu 114 Serial comm. contact broken $=2$. Cat 3 . Run with auto reset. | Serial communication broken will not stop operation. Stop from keyboard if necessary. |
| F16 | Phase reversal alarm. | Cat 1. Stop with manual reset. | Incorrect phase order on main voltage input. |

## 9. TROUBLESHOOTING

### 9.1 Fault, cause and solution

| Observation | Fault indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The display is not illuminated. | None | No control voltage. | Switch on the control voltage. |
| The motor does not run. | F1 <br> (Phase input failure) | Fuse defective. | Renew the fuse. |
|  |  | No mains supply. | Switch the main supply on. |
|  | F2 <br> (Motor protection, overload) | Perhaps PTC connection. Perhaps incorrect nominal motor current inserted (menu 042). | Check the PTC input if PTC protection is used. <br> If internal protection is used, perhaps an other class could be used (menu 072). <br> Cool down the motor and make a reset. |
|  | F3 <br> (Soft start overheated) | Ambient temperature to high. soft starter duty cycle exceeded. Perhaps fan failure. | Check ventilation of cabinet. Check the size of the cabinet. Clean the cooling fins. If the fan(s) is not working correct, contact your local MSF sales outlet. |
|  | F4 <br> (Full speed not reached at set current limit and start time) | Current limit parameters are perhaps not matched to the load and motor. | Increase the starting time and/or the current limit level. |
|  | F5 (Locked rotor) | Something stuck in the machine or perhaps motor bearing failure. | Check the machine and motor bearings. Perhaps the alarm delay time can be set longer (menu 075). |
|  | F6 <br> (Above max power limit) | Overload | Over load. Check the machine. Perhaps the alarm delay time can be set longer (menu 093). |
|  | F7 <br> (Below min power limit) | Underload | Under load. Check the machine. Perhaps the alarm delay time can be set longer (menu 099). |
|  | F8 <br> (Voltage unbalance) | Main supply voltage unbalance. | Check mains supply. |
|  | F9 (Over voltage) | Main supply over voltage. | Check mains supply. |
|  | F10 (Under voltage) | Main supply under voltage. | Check mains supply. |
|  | F11 <br> (Starts / hour exceeded) | Number of starts exceeded according to menu 074. | Wait and make a new start. Perhaps the number of starts / hour could be increased in menu 074. |
|  | F13 <br> (Open thyristor) | Perhaps a damaged thyristor. | Make a reset and a restart. If the same alarm appears immediately, contact your local MSF sales outlet. |
|  | F14 <br> (Motor terminal open) | Open motor contact, cable or motor winding. | If the fault is not found, reset the alarm and inspect the alarm list. If alarm F12 is found, a thyristor is probably shorted. <br> Make a restart. If alarm F14 appears immediately, contact your local MSF sales outlet. |

O
$\cdots$

| Observation | Fault indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The motor does not run. | F15 <br> (Serial communication broken) | Serial communication broken. | Make a reset and try to establish contact. Check contacts, cables and option board. <br> Verify <br> - System address (menu 111). <br> - Baudrate (menu 112). <br> - Parity (menu 113). <br> If the fault is not found, run the motor with keyboard control if urgent (set menu 006 to "1"). See also manual for serial communication. |
|  | F16 (Phase reversal) | Incorrect phase sequence on main supply. | Switch L2 and L3 input phases. |
|  | --. - | Start command comes perhaps from incorrect control source. (l.e. start from keyboard when remote control is selected). | Give start command from correct source (menu 006). |
|  | -Loc | System in keyboard lock. | Unlock keyboard by pressing the keys 'NEXT' and 'ENTER' for at least 3 sec . |
| The motor is running but an alarm is given. | F1 (Phase input failure) | Failure in one phase. Perhaps fuse defective. | Check fuses and mains supply. Deselect 'Run at single phase input failure' in menu 101, if stop is desired at single phase loss. |
|  | F4 <br> (Full speed not reached at set current limit and start time) | Current limit parameters are perhaps not matched to the load and motor. | Increase the starting time and/or the current limit level. Deselect 'Run at current limit time-out' in menu 102, if stop is desired at current limit time-out. |
|  | F12 <br> (Shorted thyristor) | Perhaps a damaged thyristor. | When stop command is given, a free wheel stop is made. Make a reset and a restart. If alarm F14 appears immediately, contact your local MSF sales outlet. <br> If it is urgent to start the motor, set soft starter in 'Direct On Line' (menu 024). It is possible to start in this mode. |
|  |  | By pass contactor is used but menu 032 'Bypass' is not set to "on". | Set menu 032 'Bypass' to "on". |
|  | F15 <br> (Serial communication broken) | Serial communication broken, | Make a reset and try to establish contact. Check contacts, cables and option board. <br> Verify <br> - System address (menu 111). <br> - Baudrate (menu 112). <br> - Parity (menu 113). <br> If the fault is not found, run the motor with keyboard control if urgent, see also manual for serial communication. |


| Observation | Fault indication | Cause | Solution |
| :---: | :---: | :---: | :---: |
| The motor jerks etc. | When starting, motor reaches full speed but it jerks or vibrates. | If 'Torque control' or 'Pump control' is selected, it is necessary to input motor data into the system. | Input nominal motor data in menus 041-046. Select the proper load characteristic in menu 025. Select a correct initial- and end torque at start in menus 016 and 017. If 'Bypass' is selected, check that the current transformers are correct connected. |
|  |  | Starting time too short. | Increase starting time. |
|  |  | Starting voltage incorrectly set. | Adjust starting voltage. |
|  |  | Motor too small in relation to rated current of soft starter. | Use a smaller model of the soft starter. |
|  |  | Motor too large in relation to load of soft starter. | Use larger model of soft starter. |
|  |  | Starting voltage not set correctly | Readjust the start ramp. |
|  |  |  | Select the current limit function. |
|  | Starting or stopping time too long, soft does not work. | Ramp times not set correctly. | Readjust the start and/or stop ramp time. |
|  |  | Motor too large or too small in relation to load. | Change to another motor size. |
| The monitor function does not work. | No alarm or pre-alarm | It is necessary to input nominal motor data for this function. Incorrect alarm levels. | Input nominal motor data in menus 041-046. Adjust alarm levels in menus 091-099. If 'Bypass' is selected, check that the current transformers are correct connected. |
| Unexplainable alarm. | F5, F6, F7, F8, F9, F10 | Alarm delay time is to short. | Adjust the response delay times for the alarms in menus 075, 082, 084, 086, 093 and 099. |
| The system seems locked in an alarm. | F2 <br> (Motor protection, overload) | PTC input terminal could be open. <br> Motor could still be to warm. If internal motor protection is used, the cooling in the internal model take some time. | PTC input terminal should be short circuit if not used. Wait until motor PTC gives an OK (not overheated) signal. Wait until the internal cooling is done. Try to reset the alarm after a while. |
|  | F3 (Soft start overheated) | Ambient temperature to high. Perhaps fan failure. | Check that cables from power part are connected in terminals 073, 074, 071 and 072. MSF-017 to MSF-145 should have a short circuit between 071 and 072 . Check also that the fan(s) is rotating. |
| Parameter will not be accepted. | $\cdots$ | If the menu number is one of 020-025, only one can bee selected. <br> In other words only one main mode is possible at a time. | Deselect the other main mode before selecting the new one. |
|  |  | If menu 061, 'Parameter set' is set to " 0 ", the system is in a remote parameter selection mode. It is now impossible to change most of the parameters. | Set the menu 061, 'Parameter set' to a value between " 1 " - " 4 " and then it is possible to change any parameter. |
|  |  | During acceleration, deceleration, slow speed, DC brake and Power factor control mode, it is impossible to change parameters. | Set parameters during stop or full voltage running. |
|  |  | If control source is serial comm., it is impossible to change parameters from keyboard and vice versa. | Change parameters from the actual control source. |
|  |  | Some menus include only read out values and not parameters. | Read-out values can not be altered. In table 13, page 35, read-out menus has '-...' in the factory setting column. |
|  | -Loc | Keyboard is locked. | Unlock keyboard by pressing the keys 'NEXT' and 'ENTER' for at least 3 sec. |

## 10. MAINTENANCE

In general the soft starter is maintenance free. There are however some things which should be checked regularly. Especially if the surroundings are dusty the unit should be cleaned regularly.

WARNING! Do not touch parts inside the enclosure of the unit when the control and motor voltage is switched on.

## Regular maintenance

- Check that nothing in the soft starter has been damaged by vibration (loose screws or connections).
- Check external wiring, connections and control signals. Tighten terminal screws and busbar bolts if necessary.
- Check that PCB boards, thyristors and cooling fin are free from dust. Clean with compressed air if necessary. Make sure the PCB boards and thyristors are undamaged.
- Check for signs of overheating (changes in colour on PCB boards, oxidation of solder points etc.). Check that the temperature is within permissible limits.
- Check that the cooling fan/s permit free air flow. Clean any external air filters if necessary.

In the event of fault or if a fault cannot be cured by using the fault-tracing table in chapter 9. page 68.

## 11. OPTIONS

The following option are available. Please contact your supplier for more detailed information.

### 11.1 Serial communication

For serial communication the MODBUS RTU (RS232/RS485) option card is available order number: 01-1733-00.


Fig. 60 Option RS232/485

### 11.2 Field bus systems

Various option cards are available for the following bus systems:

- PROFIBUS DP order number: 01-1734-01
- Device NET, order number: 01-1736-01
- LONWORKS: 01-1737-01
- FIP IO:

01-1738-01

- INTERBUS-S:

01-1735-01

Each system has his own card. The option is delivered with an instruction manual containing the all details for the set-up of the card and the protocol for programming.


Fig. 61 Option Profibus

### 11.3 External PPU.

The external PPU option is used to move the PPU (keyboard) from the soft starter to the front of a panel door or control cabinet.

The maximum distance between the soft starter and the external PPU is 3 m .
The option can be factory mounted (01-2138-01) or it can be built in later (01-2138-00). For both versions instruction / data sheet are available.


Fig. 62 Shows an example of the External PPU after it has been built in.

### 11.3.1 Cable kit for external current transformers

This kit is used for the bypass function, to connect the external current transformers more easy. order number: 01-2020-00.


Fig. 63 Cable kit

### 11.4 Terminal clamp

Data: Single cables, Cu or Al
Cables
MSF type Cu Cable
Bolt for connection to busbar
Dimensions in mm
Order No. single
Data: Parallel cables, Cu or Al
Cables
MSF type and Cu Cable
Bolt for connection to busbar
Dimensions in mm
Order No. parallel


Fig. 64 The terminal clamp.

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12. TECHNICAL DATA

| 3x200-525 V 50/60 Hz Model | MSF017 |  | MSF-030 |  | MSF-045 |  | MSF-060 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Soft starter rating according to AC35a, see chapter 4. page 13 | $\begin{gathered} 5.0-30: 50-10 \\ \text { heavy } \end{gathered}$ | $\begin{array}{\|l\|} \hline 3.0-30: 50-10 \\ \text { normal/IIght } \end{array}$ | $\begin{gathered} 5.0-30: 50-10 \\ \text { heavy } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { 3.0-30:50-10 } \\ \text { normal//light } \end{array}$ | $\begin{array}{\|c\|} \hline 5.0-30: 50-10 \\ \text { heavy } \end{array}$ | $\left.\begin{array}{\|c\|} \hline \text { 3.0-30:50-10 } \\ \text { normal/llght } \end{array} \right\rvert\,$ | $\begin{array}{\|c\|} \hline \text { 5.0-30:50-10 } \\ \text { heavy } \end{array}$ | $\left\|\begin{array}{l\|} \text { 3.0-30:50-10 } \\ \text { normal/llght } \end{array}\right\|$ |
| Rated current of soft starter (A) | 17 | 22 | 30 | 37 | 45 | 60 | 60 | 72 |
| Recommended motor size (kW) for 400 V | 7.5 | 11 | 15 | 18.5 | 22 | 30 | 30 | 37 |
| Recommended motor size (kW) for 525 V | 11 | 15 | 18.5 | 22 | 30 | 37 | 37 | 45 |
| Order number: supply voltage ( $100-240 \mathrm{~V}$ ) | 01.1301-01 |  | 01-1302-01 |  | 01-1303-01 |  | 01-1304-01 |  |
| Order number: supply voltage ( $380-500 \mathrm{~V}$ ) | 01-1301-02 |  | 01.1302-02 |  | 01-1303-02 |  | 01-1304-02 |  |
| 3x200690V 50/60Hz Model | MSF-017 |  | MSF-030 |  | MSF-045 |  | MSF060 |  |
| Rated current of soft starter (A) | 17 | 22 | 30 | 37 | 45 | 60 | 60 | 72 |
| Motor power for 690V | 15 | 18.5 | 22 | 30 | 37 | 55 | 55 | 75* |
| Order number: supply voltage ( $100-240 \mathrm{~V}$ ) | 01-1321-01 |  | 01-1322-01 |  | 01-1323-01 |  | 01-1324-01 |  |
| Order number: supply voltage ( $380-500 \mathrm{~V}$ ) | 01-1321-02 |  | 01-1322-02 |  | 01-1323-02 |  | 01-1324-02 |  |
| Electrical Data |  |  |  |  |  |  |  |  |
| Recommended wiring fuse (A) 1) | 25/50 | 32 | 35/80 | 50 | 50/125 | 80 | 63/160 | 100 |
| Semi-conductor fuses, if required | 80 A |  | 125 A |  | 160 A |  | 200 A |  |
| Power loss at rated motor load (W) | 50 | 70 | 90 | 120 | 140 | 180 | 180 | 215 |
| Power consumption control card | 20 VA |  | 20 VA |  | 25 VA |  | 25 VA |  |
| Mechanical Data |  |  |  |  |  |  |  |  |
| Dimensions in $\mathrm{mm} \mathrm{H} \mathrm{\times W} \mathrm{\times D}$ | 320x126×260 |  | $320 \times 126 \times 260$ |  | 320x 126x 260 |  | 320×126×260 |  |
| Mounting position (Vertical/Horizontal) | Vertical |  | Vertical |  | Vert. or Horiz. |  | Vert. or Horiz. |  |
| Weight (kg) | 6.7 |  | 6.7 |  | 6.9 |  | 6.9 |  |
| Connection busbars Cu, (bolt) | 15x4 (M6) |  | 15×4 (M6) |  | 15x4 (M6) |  | 15×4 (M8) |  |
| Cooling system | Convection |  | Convection |  | Fan |  | Fan |  |
| General Electrical Data |  |  |  |  |  |  |  |  |
| Number of fully controlled phases | 3 |  |  |  |  |  |  |  |
| Voltage tolerance control | Control +/-10\% |  |  |  |  |  |  |  |
| Voltage tolerance motor | Motor $200-525+/-10 \% / 200-690+5 \%,-10 \%$ |  |  |  |  |  |  |  |
| Recommended fuse for control card (A) | Max 10 A |  |  |  |  |  |  |  |
| Frequency | $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |
| Frequency tolerance | +/-10\% |  |  |  |  |  |  |  |
| Relay contacts | $3 \times 8 \mathrm{~A}, 250 \mathrm{~V}$ resistive load, 3A 250VAC inductive ( $\mathrm{PF}=0.4$ ) |  |  |  |  |  |  |  |
| Type of protection/Insulation |  |  |  |  |  |  |  |  |
| Type of casing protection | IP 20 |  |  |  |  |  |  |  |
| Other General Data |  |  |  |  |  |  |  |  |
| Ambient temperatures |  |  |  |  |  |  |  |  |
| In operation | $0.40{ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| Max.e.g. at $80 \%$ in | $50^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| In storage | $(-25)-(+70)^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| Relative air humidity | 95\%, non-condensing |  |  |  |  |  |  |  |
| Max. altitude without derating | (See separate: Technical information 151) 1000 m |  |  |  |  |  |  |  |
| Norms/Standards, Conform to: | IEC 947-4-2, EN 292, EN 60204-1, UL508 |  |  |  |  |  |  |  |
| EMC, Emission | EN 50081-2, (EN 50081-1 with bypass contactor) |  |  |  |  |  |  |  |
| EMC, Immunity | EN 50082-2 |  |  |  |  |  |  |  |
| 1) Recommended wiring fuses for: $\begin{aligned} & \text { Heavy (first column): ramp/direct start } \\ & \text { Normal/ Lght (second column): ramp start }\end{aligned}$ |  |  |  |  |  |  |  |  |
| NOTEI Short clrcult withstand MSF017-060 5000 rms A when used with K5 or RK5 fuses. |  |  |  |  |  |  |  |  |

* 2-pole motor

| 3x200-525 V 50/60 Hz Model | MSF075 |  | MSF-085 |  | MSF-110 |  | MSF-145 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Soft starter rating according to AC35a, see chapter 4. page 13 | 5.0-30:50-10 heavy | 3.0-30:50-10 normal/light | $\begin{gathered} 5.0-30: 50-10 \\ \text { heavy } \end{gathered}$ | 3.0-30:50-10 normal/light | $\begin{gathered} 5.0-30: 50-10 \\ \text { heavy } \end{gathered}$ | $3.0-30: 50-10$ normal/light | $\begin{gathered} 5.0-30: 50-10 \\ \text { heavy } \end{gathered}$ | $\begin{aligned} & \text { 3.0-30:50-10 } \\ & \text { normal/Ilght } \end{aligned}$ |
| Rated current of soft starter (A) | 75 | 85 | 85 | 96 | 110 | 134 | 145 | 156 |
| Recommended motor size (kW) for 400 V | 37 | 45 | 45 | 55* | 55 | 75 | 75 |  |
| Recommended motor size (kW) for 525 V | 45 | 55 | 55 | 75* | 75 | 90 | 90 | 110 |
| Order number for supply voltage (100-240 V) | 01-1305-01 |  | 01-1306-01 |  | 01-1307-01 |  | 01-1308-01 |  |
| Order number for supply voltage (380-550 V) | 01-1305-02 |  | 01-1306-02 |  | 01-1307-02 |  | 01-1308-02 |  |
| 3x200-690 V 50/60 Hz Model | MSF-075 |  | MSF-085 |  | MSF-110 |  | MSF-145 |  |
| Rated current of soft starter (A) | 75 | 85 | 85 | 90 | 110 | 134 | 145 | 156 |
| Motor power for 690V | 55 | 75 | 75 | 90 | 90 | 110 | 132 | 160* |
| Order number for supply voltage (100-240 V) | 01-1325-01 |  | 01-1326-01 |  | 01.1327.01 |  | 01-1328-01 |  |
| Order number for supply voltage (380-550 V) | 01-1325-02 |  | 01-1326-02 |  | 01-1327-02 |  | 01-1328-02 |  |
| Electrical Data |  |  |  |  |  |  |  |  |
| Recommended wiring fuse (A) 1) | 80/200 | 100 | 100/250 | 125 | 125/315 | 180 | 160/400 | 200 |
| Semi-conductor fuses, if required | 250 A |  | 315 A |  | 350 A |  | 450 A |  |
| Power loss at rated motor load (W) | 230 | 260 | 260 | 290 | 330 | 400 | 440 | 470 |
| Power consumption control card | $25 \mathrm{VA}$ |  | 25 VA |  | 25 VA |  | 25 VA |  |
| Mechanical Data |  |  |  |  |  |  |  |  |
| Dimensions in mm HxW×D | $320 \times 126 \times 260$ |  | $320 \times 126 \times 260$ |  | $400 \times 176 \times 260$ |  | $400 \times 176 \times 260$ |  |
| Mounting position (Vertical/Horizontal) | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  |
| Weight (kg) | 6.9 |  | 6.9 |  | 12 |  | 12 |  |
| Connection, busbars Cu , (bolt) | 15x4 (M8) |  | 15×4 (M8) |  | 20×4 (M10) |  | $20 \times 4$ (M10) |  |
| Cooling system | Fan |  | Fan |  | Fan |  | Fan |  |
| General Electrical Data |  |  |  |  |  |  |  |  |
| Number of fully controlled phases | 3 |  |  |  |  |  |  |  |
| Voltage tolerance control | Control +/-10\% |  |  |  |  |  |  |  |
| Voltage tolerance motor | Motor $200-525+/-10 \% / 200-690+5 \%,-10 \%$ |  |  |  |  |  |  |  |
| Recommended fuse for control card (A) | Max 10 A |  |  |  |  |  |  |  |
| Frequency | $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |
| Frequency tolerance | +/-10\% |  |  |  |  |  |  |  |
| Relay contacts | $8 \mathrm{~A}, 250 \mathrm{~V}$ resistive load, 3A, 250 V inductive load ( $\mathrm{PF}=0.4$ ) |  |  |  |  |  |  |  |
| Type of protection/Insulation |  |  |  |  |  |  |  |  |
| Type of casing protection | IP 20 |  |  |  |  |  |  |  |
| Other General Data |  |  |  |  |  |  |  |  |
| Ambient temperatures In operation | $0.40^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| Max. e.g. at $80 \% \mathrm{I}_{\mathrm{N}}$ | $50^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| In storage | $(-25)-(+70)^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |
| Relative air humidity | 95\%, non-condensing |  |  |  |  |  |  |  |
| Max. altitude without derating | (See separate: Technical information 151) 1000 m |  |  |  |  |  |  |  |
| Norms/Standards, Conform to: | IEC 947-4-2, EN 292, EN 60204-1, UL508 |  |  |  |  |  |  |  |
| EMC, Emission | EN 50081-2, (EN 50081-1 with bypass contactor) |  |  |  |  |  |  |  |
| EMC, Immunity | EN 50082-2 |  |  |  |  |  |  |  |
| 1) Recommended wiring fuses for: Heavy | (first column) <br> al/Ught (second | ramp/direct nd column): ra | start <br> mpstart |  |  |  |  |  |
| NOTE! Short clrcult withstand MSF075-145 $\mathbf{1 0 0 0 0 ~ r m s ~ A ~ w h e n ~ u s e d ~ w i t h ~ K 5 ~ o r ~ R K 5 ~ f u s e s . ~}$ |  |  |  |  |  |  |  |  |

* 2 -pole motor

| 3x200-525 V 50/60 Hz Model | MSF-170 |  | MSF-210 |  | MSF-250 |  | MSF-310 |  | MSF-370 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Soft starter rating according to AC35a, see chapter 4. page 13 | 5.0.30: 50-10 heavy | $\left\lvert\, \begin{gathered} 3.0-30: \\ 50-10 \\ \text { normal/IIght } \end{gathered}\right.$ | $\begin{aligned} & \text { 5.0.30: } \\ & 50-10 \\ & \text { heary } \end{aligned}$ | $\left\|\begin{array}{c} 3.030: \\ 50-10 \\ \text { normal/IIght } \end{array}\right\|$ | 5.0.30: 50.10 heavy | $\left\lvert\, \begin{gathered} \text { 3.0.30: } \\ 50-10 \\ \text { normal/light } \end{gathered}\right.$ | 5.0.30: 50-10 heavy | $\begin{gathered} 3.0-30: \\ 50-10 \\ \text { normal/IIght } \end{gathered}$ | $\begin{aligned} & \text { 5.0-30: } \\ & 50-10 \\ & \text { heary } \end{aligned}$ | $\begin{gathered} 3.0-30: \\ 50-10 \\ \text { normal/Ilght } \end{gathered}$ |
| Rated current of soft starter ( A ) | 170 | 210 | 210 | 250 | 250 | 262 | 310 | 370 | 370 | 450 |
| Recommended motor size (kW) for 400 V | 90 | 110 | 110 | 132 | 132 | 160* | 160 | 200 | 200 | 250 |
| Recommended motor size (kW) for 525 V | 110 | 132 | 132 | 160 | 160 | 200* | 200 | 250 | 250 | 315 |
| Order no. for supply voltage ( $100-240 \mathrm{~V}$ ) | 01-1309-11 |  | 01.1310-11 |  | 01-1311-11 |  | 01.1312.01 |  | 01.1313-01 |  |
| Order no. for supply voltage ( $380-550 \mathrm{~V}$ ) | 01-1309-12 |  | 01-1310-12 |  | 01-1311-12 |  | 01.1312.02 |  | 01-1313-02 |  |
| 3x200-690 V 50/60 Hz Model | MSF-170 |  | MSF-210 |  | MSF-250 |  | MSF-310 |  | MSF-370 |  |
| Rated current of soft starter (A) | 170 | 210 | 210 | 250 | 250 | 262 | 310 | 370 | 370 | 450 |
| Motor power for 690 V | 160 | 200 | 200 | 250 | 250 | 250 | 315 | 355 | 355 | 400 |
| Order no. for supply voltage ( $100-240 \mathrm{~V}$ ) | 01-132901 |  | 01-1330-01 |  | 01.1331.01 |  | 01-1332.01 |  | 01-1333-01 |  |
| Order no. for supply voltage ( $380-550 \mathrm{~V}$ ) | 01-1329-02 |  | 01.1330-02 |  | 01.1331.02 |  | 01.1332.02 |  | 01-1333-02 |  |
| Electrical Data |  |  |  |  |  |  |  |  |  |  |
| Recommended wiring fuse (A) 1) | 200/400 | 200 | 250/400 | 315 | 250/500 | 315 | 315/630 | 400 | 400/800 | 500 |
| Semi-conductor fuses, if required | 700 A |  | 700 A |  | 700 A |  | 800 A |  | 1000 A |  |
| Power loss at rated motor load (W) | 510 | 630 | 630 | 750 |  | 50 W | 930 | 1100 | 1100 | 1535 |
| Power consumption control card | 35 VA |  | 35 VA |  | 35 VA |  | 35 VA |  | 35 VA |  |
| Mechanical Data |  |  |  |  |  |  |  |  |  |  |
| Dimensions mm HxW×D incl. brackets | $500 \times 260 \times 260$ |  | $500 \times 260 \times 260$ |  | $500 \times 260 \times 260$ |  | $532 \times 547 \times 278$ |  | 532x547×278 |  |
| Mounting position (Verticel/Horizontal) | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  |
| Welght (kg) | 20 |  | 20 |  | 20 |  | 42 |  | 46 |  |
| Connection, Busbars Al/Cu (bolt) | 30x 4 (M10) |  | $30 \times 4$ (M10) |  | $30 \times 4$ (M10) |  | $40 \times 8$ (M12) |  | 40x8 (M12) |  |
| Cooling system | Fan |  | Fan |  | Fan |  | Fan |  | Fan |  |
| General Electrical Data |  |  |  |  |  |  |  |  |  |  |
| Number of fully controlled phases | 3 |  |  |  |  |  |  |  |  |  |
| Voltage toterance control | Control +/.10\% |  |  |  |  |  |  |  |  |  |
| Voltage tolerance motor | Motor 200-525 +/-10\%/200-690 + 5\%, -10\% |  |  |  |  |  |  |  |  |  |
| Recommended fuse for control card (A) | Max 10 A |  |  |  |  |  |  |  |  |  |
| Frequency | $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |  |  |
| Frequency tolerence | +/10\% |  |  |  |  |  |  |  |  |  |
| Relay contacts | 8A, 250 V resistive load, $3 \mathrm{~A}, 250 \mathrm{~V}$ inductive load ( $\mathrm{PF}=0.4$ ) |  |  |  |  |  |  |  |  |  |
| Type of protection/Insulation |  |  |  |  |  |  |  |  |  |  |
| Type of casing protection | IP 20 |  |  |  |  |  |  |  |  |  |
| Other General Data |  |  |  |  |  |  |  |  |  |  |
| Ambient temperatures $\ln$ operation | $0.40{ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| Max.e.g. at $80 \% \mathrm{I}_{\mathrm{N}}$ | $50^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| In storage | $(-25)-(+70)^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| Relative air humidity | 95\%, nor-condensing |  |  |  |  |  |  |  |  |  |
| Max. altitude without derating | (See separate: Technical information 151) 1000 m |  |  |  |  |  |  |  |  |  |
| Norms/Standards, Conform to: | IEC 947-4-2, EN 292, EN 60204-1, (UL508, only MSF-170 to MSF-250) |  |  |  |  |  |  |  |  |  |
| EMC, Emission | EN 50081-2, (EN 50081-1 with bypass contactor) |  |  |  |  |  |  |  |  |  |
| EMC, Immunity | EN 50082-2 |  |  |  |  |  |  |  |  |  |
| 1) Recommended wiring fuses for: Heary (first column): ramp/direct start <br> Normal/Light (second column): ramp start |  |  |  |  |  |  |  |  |  |  |
| NOTE! Short clrcult withstand MSF170-250 18000 mms A when used with K5 or RK5 fuses. |  |  |  |  |  |  |  |  |  |  |

* 2-pole motor

管

| $3 \times 200-525 \mathrm{~V} 50 / 60 \mathrm{~Hz}$ Model | MSF-450 |  | MSF-570 |  | MSF-710 |  | MSF-835 |  | MSF-1000 |  | MSF-1400 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Soft starter rating according to AC36a, see chapter 4. page 13 | $\begin{aligned} & \text { B.0-30: } \\ & \text { 80-10 } \\ & \text { heavy } \end{aligned}$ | $\begin{gathered} \text { 3.0.30: } \\ \text { 80.10 } \\ \text { normal/ } \\ \text { light } \end{gathered}$ | $\begin{aligned} & \text { B.0-30: } \\ & \text { B0.10: } \\ & \text { heavy } \end{aligned}$ | $\begin{aligned} & 3.0-30: \\ & \text { 80-10 } \\ & \text { normal/ } \\ & \text { light } \end{aligned}$ | $\begin{aligned} & \text { 5.0-30: } \\ & \text { 80.10 } \\ & \text { heavy } \end{aligned}$ | $\begin{gathered} 3.0-30: \\ \text { no-10 } \\ \text { nombly } \\ \lg \mathrm{ght} \end{gathered}$ | $\begin{aligned} & 5.0-30: \\ & 80-10 \\ & \text { heavy } \end{aligned}$ | $\begin{gathered} 3.0-30: \\ \text { B0-10 } \\ \text { nombi/ } \\ \text { fight } \end{gathered}$ | $\begin{aligned} & \text { s.0-30: } \\ & \text { 60-10 } \\ & \text { heavy } \end{aligned}$ | $\begin{gathered} \text { 3.0-30: } \\ \text { 50-10 } \\ \text { nomal/ } \\ \text { light } \end{gathered}$ | $\begin{aligned} & \text { 8.0-30: } \\ & \text { 80-10 } \\ & \text { heavy } \end{aligned}$ | $\begin{array}{\|c} \text { 3.0-30: } \\ \text { 80-10 } \\ \text { nonmal/ } \\ \text { light } \end{array}$ |
| Rated current of soft starter (A) | 450 | 549 | 570 | 710 | 710 | 835 | 835 | 960 | 1000 | 1125 | 1400 | 1650 |
| Recommended motor size \{ $k$ W\} for 400 V | 250 | 315 | 315 | 400 | 400 | 450 | 450 | 560 | 560 | 630 | 800 | 930 |
| Recommended motor size (kW) for 525 V | 315 | 400 | 400 | 500 | 500 | 560 | 600 | 630 | 660 | 710 | 1000 | 250 |
| Order no. for supply voltage (100-240V) | 01.134101 |  | 01.1315-01 |  | 01.1316-01 |  | 01-1317-01 |  | 01-1318-01 |  | 01-1319-01 |  |
| Order no. for supply voltage (380-550V) | 01-1314-02 |  | 01.1315-02 |  | 01-1316-02 |  | 01-1317-02 |  | 01.1318-02 |  | 01-1319.02 |  |
| 3x200-690V 50/60Hz Model | MSF-450 |  | MSF-570 |  | MSF-710 |  | MSF-835 |  | MSF-1000 |  | MSF-1400 |  |
| Rated current of soft starter (A) | 450 | 549 | 570 | 640 | 710 | 835 | 835 | 880 | 1000 | 1125 | 1400 | 1524 |
| Motor power for 690 V | 400 | 560 | 560 | 630 | 710 | 800 | 800 |  | 1000 | 1120 | 1400 | 1600 |
| Order no. for supply voltage ( $100-240 \mathrm{~V}$ ) | 01.1334.01 |  | $01.1335-01$ |  | 01-1336-01 |  | 01-1337-01 |  | 01-1338-01 |  | 01-1339-01 |  |
| Order no. for supply voltage (380-550V) | 01.1334-02 |  | 01-1335-02 |  | 01-1336-02 |  | 01-1337-02 |  | 01-1338-02 |  | 01-1339-02 |  |
| Electrical Data |  |  |  |  |  |  |  |  |  |  |  |  |
| Recommended wiring fuse (A 1) | 500/1 k | 630 | 630/1 k | 800 | 800/1 k | 1 k | $1 \mathrm{k} / 1.2 \mathrm{k}$ | 1 k | 1k/1.4 k | 1.2 k | 1.4 k/1.8 | 1.8 k |
| Semi-conductor fuses, if required | 1250 A |  | 1250 A |  | 1800 A |  | 2500 A |  | 3200 A |  | 4000 A |  |
| Power loss at rated motor load (W) | 1400 | 1730 | 1700 | 2100 . | 2100 | 2500 | 2500 | 2875 | 3000 | 3375 | 4200 | $\cdot 4950$ |
| Power consumption control card | 35 VA |  | 35 VA |  | 35 VA |  | 35 VA |  | 35 VA |  | 35 VA |  |
| Mechantcal Date |  |  |  |  |  |  |  |  |  |  |  |  |
| Dimensions mm HxWxD incl, brackets | $532 \times 547 \times 278$ |  | 687x640x302 |  | 687x640x302 |  | $687 \times 640 \times 302$ |  | $900 \times 875 \times 336$ |  | $900 \times 875 \times 336$ |  |
| Mounting position (Vertical/Horizontal) | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horl2. |  | Vert. or Horiz. |  | Vert. or Horiz. |  | Vert. or Horiz. |  |
| Weight (kg) | 46 |  | 64 |  | 78 |  | 80 |  | 175 |  | 175 |  |
| Connection, Busbars Al (bolt) | 40×8 (M12) |  | $40 \times 10$ (M12) |  | 40×10 (M12) |  | 40×10(M12) |  | $75 \times 10$ (M12) |  | $75 \times 10$ (M12) |  |
| Cooling system | Fan |  | Fan |  | Fan |  | Fan |  | Fan |  | Fan |  |
| General Electricas Data |  |  |  |  |  |  |  |  |  |  |  |  |
| Number of fully controlled phases | 3 |  |  |  |  |  |  |  |  |  |  |  |
| Vortage tolerance control | Control +/-10\% |  |  |  |  |  |  |  |  |  |  |  |
| Voltage tolerance motor | Motor $200-525+/-10 \% / 200-690+5 \%,-10 \%$ |  |  |  |  |  |  |  |  |  |  |  |
| Recommended fuse for control card (A) | Max 10 A |  |  |  |  |  |  |  |  |  |  |  |
| Frequency | $50 / 60 \mathrm{~Hz}$ |  |  |  |  |  |  |  |  |  |  |  |
| Frequency tolerance | +/-10\% |  |  |  |  |  |  |  |  |  |  |  |
| Relay contacts | $8 \mathrm{~A}, 250 \mathrm{~V}$ reststive load, 3A, 250 V inductive load ( $\rho \mathrm{F}=0.4$ ) |  |  |  |  |  |  |  |  |  |  |  |
| Type of protection/Insulation |  |  |  |  |  |  |  |  |  |  |  |  |
| Type of casing protection | IP 20 |  |  |  |  |  |  |  | 1900 |  |  |  |
| Other Qeneral Data |  |  |  |  |  |  |  |  |  |  |  |  |
| Ambient temperatures In operation | $0.40^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |
| Max. e.g. at $80 \% \mathrm{I}_{\mathrm{N}}$ | $50^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |
| In storage | $(-25) \cdot(+70)^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |
| Relative air humidity | 95\%, non-condensing |  |  |  |  |  |  |  |  |  |  |  |
| Max. altitude without derating | 〈See separate: Technical information 151) 1000 m |  |  |  |  |  |  |  |  |  |  |  |
| Norms/Standards, Corriom to: | IEC 947-4-2, EN 292, EN 60204-1 |  |  |  |  |  |  |  |  |  |  |  |
| EMC, Emission | EN 50081-2, (EN 50081-1 with bypass contactor) |  |  |  |  |  |  |  |  |  |  |  |
| EMC, Immunity | EN 50082-2 |  |  |  |  |  |  |  |  |  |  |  |
| 1) Recommended wiring fuses for: | Heavy (first column); ramp/direct start Normal/Ught (second column): ramp start |  |  |  |  |  |  |  |  |  |  |  |

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## Semi-conductor fuses

Always use standard commercial fuses to protect the wiring and prevent short circuiting. To protect the thyristors against short-circuit currents, superfast semiconductor fuses can be used if preferred (e.g. Bussmann type FWP or similar, see table below).

The normal guarantee is valid even if superfast semiconductor fuses are not used.

| Type | A | FWP Bussmann fuse |
| :---: | :---: | :---: |
| MSF-017 | 80 | $\mathbf{r}^{\mathbf{2} \mathbf{t} \text { (fuse) } \times \mathbf{1 0 0 0}}$ |
| MSF-030 | 125 | 2.4 |
| MSF-045 | 150 | 7.3 |
| MSF-060 | 200 | 11.7 |
| MSF-075 | 250 | 22 |
| MSF-085 | 300 | 42.5 |
| MSF-110 | 350 | 71.2 |
| MSF-145 | 450 | 95.6 |
| MSF-170B | 700 | 137 |
| MSF-210B | 700 | 300 |
| MSF-250B | 800 | 300 |
| MSF-310 | 800 | 450 |
| MSF-370 | 1000 | 450 |
| MSF-450 | 1200 | 600 |
| MSF-570 | 1400 | 2100 |
| MSF-710 | 1800 | 2700 |
| MSF-835 | 2000 | 5300 |
| MSF-1000 | 2500 |  |
| MSF-1400 | 3500 |  |

## 13. SET-UP MENU LIST

| Menu number | Function/Parameter | Range | Par.set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 001 | Initial voltage at start | 25-90\% of U | 1.4 | 30 |  | page 36 |
| 002 | Start time ramp 1 | 1-60 sec | 1.4 | 10 |  | page 36 |
| 003 | Step down voltage at stop | 100-40\% U | 1.4 | 100 |  | page 36 |
| 004 | Stop time ramp 1 | oFF, 2-120 sec | 1-4 | oFF |  | page 36 |
| 005 | Current | 0.0-9999 Amp | ----- | $\cdots$ |  | page 36 |
| 006 | Control mode | 1, 2, 3 | 1-4 | 2 |  | page 37 |
| 007 | Extended functions \& metering | oFF, on | - - | oFF |  | page 38 |
|  |  |  |  |  |  |  |
| 008 | Extended functions | OFF, on | - | oFF |  | page 38 |
|  |  |  |  |  |  |  |
| 011 | Initial voltage start ramp 2 | 30-90\% U | 1-4 | 90 |  | page 38 |
| 012 | Start time ramp 2 | oFF, 1-60 sec | 1-4 | oFF |  | page 38 |
| 013 | Step down voltage stop ramp 2 | 100-40\% U | 1-4 | 40 |  | page 38 |
| 014 | Stop time ramp 2 | oFF, 2-120 sec | 1-4 | oFF |  | page 38 |
|  |  |  |  |  |  |  |
| 016 | Initial torque at start | 0-250\% Tn | 1-4 | 10 |  | page 39 |
| 017 | End torque at start | 50-250\% Tn | 1.4 | 150 |  | page 39 |
| 018 | End torque at stop | 0-100\% Tn | 1-4 | 0 |  | page 39 |
| 020 | Voltage ramp with current limit at start | oFF, $150 \cdot 500 \% \mathrm{I}_{\mathrm{n}}$ | 1-4 | oFF |  | page 39 |
| 021 | Current limit at start | oFF, $150 \cdot 500 \% \mathrm{I}_{\mathrm{n}}$ | 1-4 | ofF |  | page 40 |
| 022 | Pump control | OFF, on | 1.4 | ofF |  | page 40 |
| 023 | Remote analogue control | oFF, 1, 2 | 1-4 | oFF |  | page 41 |
| 024 | Full voltage start D.O.L | OFF, on | 1-4 | oFF |  | page 41 |
| 025 | Torque control | ofF, 1, 2 | 1-4 | oFF |  | page 42 |
|  |  |  |  |  |  |  |
| 030 | Torque boost active time | oFF, 0.1-2.0 sec | 1-4 | oFF |  | page 43 |
| 031 | Torque boost current limit | 300-700\% $I_{n}$ | 1-4 | 300 |  | page 43 |
| 032 | Bypass | oFF, on | 1.4 | oFF |  | page 43 |
| 033 | Power Factor Control PFC | oFF, on | 1-4 | oFF |  | page 46 |
| 034 | Brake active time | oFF, 1.120 sec | 1-4 | oFF |  | page 47 |
| 035 | Braking strength | 100-500\% | 1-4 | 100 |  | page 47 |
|  |  |  |  |  |  |  |
| 036 | Braking methods | 1,2 | 1-4 | 1 |  | page 47 |
| 037 | Slow speed torque | 10-100 | 1-4 | 10 |  | page 49 |
| 038 | Slow speed time at start | oFF, 1-60 sec | 1-4 | oFF |  | page 49 |
| 039 | Slow speed time at stop | oFF, 1-60 sec | 1.4 | oFF |  | page 49 |
| 040 | DC-Brake at slow speed | oFF, 1-60 sec | 1-4 | oFF |  | page 49 |
|  |  |  |  |  |  |  |
| 041 | Nominal motor voltage | 200-700 V | $1 \cdot 4$ | 400 |  | page 50 |
| 042 | Nominal motor current | $25-150 \% I_{\text {nsoft }}$ in Amp | 1-4 | $I_{\text {nsoft }}$ in Amp |  | page 50 |
| 043 | Nominal motor power | $\begin{gathered} 25 \cdot 300 \% \text { of } P_{\text {kwoft }} \text { in } \end{gathered}$ | $1 \cdot 4$ | $P_{\text {nsoft }}$ in kW |  | page 50 |
| 044 | Nominal speed | $500 \cdot 3600 \mathrm{rpm}$ | 1-4 | $\mathrm{N}_{\text {nsoft }}$ in rpm |  | page 50 |
| 045 | Nominal power factor | 0.50-1.00 | 1-4 | 0.86 |  | page 50 |
| 046 | Nominal frequency | $50,60 \mathrm{~Hz}$ | $\cdots$ | 50 |  | page 50 |


| Menu number | Function/Parameter | Range | Par.set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 051 | Programmable relay K1 | 1, 2, 3, (4), 5 |  | 1 |  | page 51 |
| 052 | Programmable relay K2 | 1, 2, 3, 4, 5 | --- | 2 |  | page 51 |
| 054 | Analogue output | OFF, 1, 2 | 1-4 | oFF |  | page 52 |
| 055 | Analogue output value | 1, 2, 3 | 1-4 | 1 |  | page 52 |
| 056 | Scaling analogue output | 5-150\% | 1.4 | 100 |  | page 52 |
| 057 | Digital input selection | oFF, 1, 2, 3, 4 | 1-4 | oFF |  | page 53 |
| 058 | Digital input pulses | 1-100 | 1-4 | 1 |  | page 53 |
|  |  |  |  |  |  |  |
| 061 | Parameter set | 0, 1, 2, 3, 4 | $\cdots$ | 1 |  | page 54 |
|  |  |  |  |  |  |  |
| 071 | Motor PTC input | no, YES | - | no |  | page 55 |
| 072 | Internal motor thermal protection class | OFF, 2.40 sec | ------ | 10 |  | page 55 |
| 073 | Used thermal capacity | 0-150\% | - | - |  | page 55 |
| 074 | Starts per hour limitation | oFF, 1.99/hour | 1-4 | oFF |  | page 55 |
| 075 | Locked rotor alarm | OFF, 1.0-10.0 sec | 1-4 | OFF |  | page 55 |
|  |  |  |  |  |  |  |
| 081 | Voltage unbalance alarm | $2-25 \% U_{n}$ | 1-4 | 10 |  | page 56 |
| 082 | Response delay voltage unbalance alarm | ofF, 1-60 sec | 1.4 | OFF |  | page 56 |
| 083 | Over voltage alarm | 100-150\% U ${ }_{n}$ | 1-4 | 115 |  | page 56 |
| 084 | Response delay over voltage alarm | ofF, 1-60 sec | 1-4 | oFF |  | page 56 |
| 085 | Under voltage alarm | 75-100\% Un | 1-4 | 85 |  | page 57 |
| 086 | Response delay under voltage alarm | ofF, 1-60 sec | 1-4 | oFF |  | page 57 |
| 087 | Phase sequence | L123, L321 | - | - |  | page 57 |
| 088 | Phase reversal alarm | oFF, on | - | oFF |  | page 57 |
|  |  |  |  |  |  |  |
| 089 | Auto set power limits | no, YES | $\square$ | no |  | page 57 |
| 090 | Output shaft power | 0.0-200.0\% Pn | - | --- |  | page 57 |
| 091 | Start delay power limits | 1.250 sec | 1-4 | 10 |  | page 58 |
| 092 | Max power alarm limit | 5-200\% Pn | 1-4 | 115 |  | page 58 |
| 093 | Max alarm response delay | oFF, $0.1-25.0 \mathrm{sec}$ | 1-4 | ofF |  | page 58 |
| 094 | Max power pre-alarm limit | 5-200\% Pn | 1-4 | 110 |  | page 58 |
| 095 | Max pre-alarm response delay | oFF, $0.1-25.0 \mathrm{sec}$ | 1-4 | oFF |  | page 58 |
| 096 | Min pre-alarm power limit | 5-200\% Pn | 1.4 | 90 |  | page 58 |
| 097 | Min pre-alarm response delay | oFF, $0.1-25.0 \mathrm{sec}$ | 1.4 | oFF |  | page 59 |
| 098 | Min power alarm limit | 5-200\%Pn | 1-4 | 85 |  | page 59 |
| 099 | Min alarm response delay | oFF, 0.1-25.0 sec | 1-4 | oFF |  | page 59 |
|  |  |  |  |  |  |  |
| 101 | Run at single phase input failure | no, YES | 1.4 | no |  | page 61 |
| 102 | Run at current limit time-out | no, YES | 1-4 | no |  | page 61 |
|  |  |  |  |  |  |  |
| 103 | Jog forward enable | oFF, on | 1-4 | oFF |  | page 61 |
| 104 | Jog reverse enable | oFF, on | 1-4 | oFF |  | page 61 |
|  |  |  |  |  |  |  |
| 105 | Automatic return menu | oFF, 1-999 | - | oFF |  | page 62 |
|  |  |  |  |  |  |  |
| 111 | Serial comm. unit address | 1-247 | --- | 1 |  | page 62 |
| 112 | Serial comm. baudrate | 2.4 - 38.4 kBaud | $\square$ | 9.6 |  | page 62 |


| Menu number | Function/Parameter | Range | Par.set | Factory setting | Value | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 113 | Serial comm. parity | 0,1 | $\cdots$ | 0 |  | page 62 |
| 114 | Serial comm. contact broken | oFF, 1, 2 | - | 1 |  | page 62 |
| 199 | Reset to factory settings | no, YES | - | no |  | page 63 |
| 201 | Current | 0.0-9999 Amp | --7-1-- | $\cdots$ |  | page 63 |
| 202 | Line main voltage | 0.720 V | - | $\underline{\square}$ |  | page 63 |
| 203 | Output shaft power | -9999-9999 kW | - | --- |  | page 63 |
| 204 | Power factor | 0.00-1.00 | -—— | - - |  | page 63 |
| 205 | Power consumption | 0.000 - 2000 MWh | - | - |  | page 63 |
| 206 | Reset power consumption | no, YES | - - | no |  | page 64 |
| 207 | Shaft torque | -9999-9999 Nm | ------ | ------- |  | page 64 |
| 208 | Operation time | Hours | $\underline{\square}$ | - |  | page 64 |
|  |  |  |  |  |  |  |
| 211 | Current phase L1 | 0.0.9999 Amp | $\cdots$ | $\cdots$ |  | page 64 |
| 212 | Current phase L2 | 0.0 - 9999 Amp | -- | - - |  | page 64 |
| 213 | Current phase L3 | $0.0 \cdot 9999 \mathrm{Amp}$ | $\cdots$ | $\cdots$ |  | page 64 |
|  |  |  |  |  |  |  |
| 214 | Line main voltage L1 - L2 | 0.720 V | -—— | - |  | page 64 |
| 215 | Line main voltage L1-L3 | $0 \cdot 720 \mathrm{~V}$ | -- | ---- |  | page 64 |
| 216 | Line main voltage L2 - L3 | 0-720V | $\cdots$ | $\cdots$ |  | page 64 |
|  |  |  |  |  |  |  |
| 221 | Locked keyboard info | no, YES | ----- | no |  | page 65 |
|  |  |  |  |  |  |  |
| 901 | Alarm list, Latest error | F1-F16 | ----- | - |  | page 65 |
| 902-915 | Alarm list, Older error in chronological order | F1-F16 | $\square$ | - - - |  | page 65 |

Explanation of units:
$U \quad$ Input line voltage
Un Nominal motor voltage.
In Nominal motor current.
$\mathrm{Pn} \quad$ Nominal motor power.
$\mathrm{Nn} \quad$ Nominal motor speed.
Tn Nominal shaft torque.
Insoft Nominal current soft starter.
Pnsoft Nominal power soft starter.
Nnsoft Nominal speed soft starter.
Calculation shaft torque

$$
T_{n}=\frac{P_{n}}{\left(\frac{N_{n}}{60} \times 2 \pi\right)}
$$

NOTE! The slx main functlons for motor control, menus 020-025, can only be selected one at a time.

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# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144 Lavarack Av \#1 Eagle Farm

Equipment Type: Delivery Pressure Transmitter
Location: Common Control
Model Numbers: BR74XXGG1FHA2X
(SP119 50m Range \& SP175 100m Range)
Manufacturer: Vega
Supplier:
Vega
398 The Boulevard
Kirrawee ..... NSW2232


## Operating Instructions VEGABAR 74 <br> 4 ... $20 \mathrm{~mA} / \mathrm{HART}$



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## Supplementary documentation

- Information:

Depending on the ordered version, supplementary documentation belongs to the scope of delivery. You find this documentation in chapter "Product description".

## Instructions manuals for accessories and replacement parts

## 2 Tip:

 To ensure reliable setup and operation of your VEGABAR 74, we offer accessories and replacement parts. The associated documents are:- Supplementary instructions manual 32036 "Welded socket and seals"
- Operating instructions manual 32798 "Breather housing VEGABOX 02"
- Operating instructions manual 20591 "External indicating and adjustment unit VEGADIS 12"


## 1 About this document

## 1．1 Function

This operating instructions manual provides all the information you need for mounting，connection and setup as well as important instructions for maintenance and fault rectification． Please read this information before putting the instrument into operation and keep this manual accessible in the immediate vicinity of the device．

## 1．2 Target group

This operating instructions manual is directed to trained personnel．The contents of this manual should be made available to these personnel and put into practice by them．

## 1．3 Symbolism used



Information，tip，note
This symbol indicates helpful additional information．


Caution：If this warning is ignored，faults or malfunc－ tions can result．
Warning：If this warning is ignored，injury to persons and／or serious damage to the instrument can result．
Danger：If this warning is ignored，serious injury to persons and／or destruction of the instrument can result．

## Ex applications

This symbol indicates special instructions for Ex applications．
－List
The dot set in front indicates a list with no implied sequence．
$\rightarrow \quad$ Action
This arrow indicates a single action．

## Sequence

Numbers set in front indicate successive steps in a procedure．

## 2 For your safety

### 2.1 Authorised personnel

All operations described in this operating instructions manual must be carried out only by trained specialist personnel authorised by the operator.

During work on and with the device the required personal protection equipment must always be worn.

### 2.2 Appropriate use

VEGABAR 74 is a pressure transmitter for measurement of gauge pressure, absolute pressure and vacuum.

You can find detailed information on the application range in chapter "Product description".

Operational reliability is ensured only if the instrument is properly used according to the specifications in the operating instructions manual as well as possible supplementary instructions.

Due to safety and warranty reasons, any invasive work on the device beyond that described in the operating instructions manual may be carried out only by personnel authorised by the manufacturer. Arbitrary conversions or modifications are explicitly forbidden.

### 2.3 Warning about misuse

Inappropriate or incorrect use of the instrument can give rise to application-specific hazards, e.g. vessel overfill or damage to system components through incorrect mounting or adjustment.

### 2.4 General safety instructions

This is a high-tech instrument requiring the strict observance of standard regulations and guidelines. The user must take note of the safety instructions in this operating instructions manual, the country-specific installation standards as well as all prevailing safety regulations and accident prevention rules.

The instrument must only be operated in a technically flawless and reliable condition. The operator is responsible for troublefree operation of the instrument.

During the entire duration of use, the user is obliged to determine the compliance of the required occupational safety measures with the current valid rules and regulations and also take note of new regulations.

### 2.5 Safety approval markings and safety tips

The safety approval markings and safety tips on the device must be observed.

### 2.6 CE conformity

VEGABAR 74 is in CE conformity with EMC (89/336/EWG), fulfils NAMUR recommendation NE 21 and is in CE conformity with LVD (73/23/EWG).

Conformity has been judged according to the following standards:

- EMC:
- Emission EN 61326: 2004 (class B)
- Susceptibility EN 61326: 2004 including supplement A
- LVD: EN 61010-1: 2001

VEGABAR 74 is not subject to the pressure device guideline.1)

### 2.7 Fulfilling NAMUR recommendations

VEGABAR 74 fulfills the following NAMUR recommendations:

- NE 21 (interference resistane and emitted interference)
- NE 43 (signal level for failure information)
- NE 53 (compatibility sensor and indicating/adjustment components)
VEGA instruments are generally upward and downward compatible:
- Sensor software to DTM VEGABAR 74 HART
- DTM VEGABAR 74 for adjustment software PACTware ${ }^{\text {TM }}$

The parameter adjustment of the basic sensor functions is independent of the software version. The range of available functions depends on the respective software version of the individual components.

The software version of VEGABAR 74 HART can be read out via PACTware ${ }^{\text {TM }}$.

[^6]You can view all software histories on our website www.vega. com. Make use of this advantage and get registered for update information via e-mail.

### 2.8 Safety instructions for Ex areas

Please note the Ex-specific safety information for installation and operation in Ex areas. These safety instructions are part of the operating instructions manual and come with the Exapproved instruments.

### 2.9 Environmental instructions

Protection of the environment is one of our most important duties. That is why we have introduced an environment management system with the goal of continuously improving company environmental protection. The environment management system is certified according to DIN EN ISO 14001.

Please help us fulfil this obligation by observing the environmental instructions in this manual:

- Chapter "Packaging, transport and storage"
- Chapter "Disposal"

3 Product description

### 3.1 Configuration

## Scope of delivery

## Components

The scope of delivery encompasses:

- VEGABAR 74 pressure transmitter
- Documentation
- this operating instructions manual
- Test certificate for pressure transmitters
- Ex-specific "Safety instructions" (with Ex-versions)
- if necessary, further certificates

VEGABAR 74 consists of the following components:

- Process fitting with measuring cell
- Housing with electronics
- Connection cable (direct cable outlet)

The components are available in different versions.


Fig. 1: Example of a VEGABAR 74 with process fitting G112 A
1 Connection cable
2 Housing with electronics
3 Process fitting with measuring cell

## Area of application

## Functional principle

Supply

### 3.2 Principle of operation

VEGABAR 74 is a pressure transmitter for use in the paper, food processing and pharmaceutical industry. Thanks to the high protection class IP 68/IP 69K it is particularly suitable for use in humid environment. Depending on the version, it is used for level, gauge pressure, absolute pressure or vacuum measurements. Measured products are gases, vapours and liquids, also with abrasive contents.

The sensor element is the CERTEC ${ }^{(®)}$ measuring cell with flush, abrasion resistant ceramic diaphragm. The hydrostatic pressure of the medium or the process pressure causes a capacitance change in the measuring cell via the diaphragm. This change is converted into an appropriate output signal and outputted as measured value.
The CERTEC ${ }^{\circledR}$ measuring cell is also equipped with a temperature sensor. The temperature value can be processed via the signal output.

Two-wire electronics $4 \ldots 20 \mathrm{~mA} / \mathrm{HART}$ for power supply and measured value transmission over the same cable.

The supply voltage range can differ depending on the instrument version.

The data for power supply are stated in chapter "Technical data" in the "Supplement".

### 3.3 Operation

VEGABAR $744 \ldots 20 \mathrm{~mA} / \mathrm{HART}$ can be adjusted with different adjustment media:

- with external adjustment/indication VEGADIS 12
- an adjustment software according to FDT/DTM standard, e.g. PACTware ${ }^{\text {TM }}$ and PC
- with a HART handheld

The kind of adjustment and the adjustment options depend on the selected adjustment component. The entered parameters are generally saved in the respecitive sensor, when adjusting with PACTware ${ }^{\text {TM }}$ and PC optionally also in the PC.

## 3．4 Packaging，transport and storage

\(\left.$$
\begin{array}{ll}\text { Packaging } & \begin{array}{l}\text { Your instrument was protected by packaging during transport．} \\
\text { Its capacity to handle normal loads during transport is assured } \\
\text { by a test according to DIN EN } 24180 .\end{array}
$$ <br>
The packaging of standard instruments consists of environ－ <br>
ment－friendly，recyclable cardboard．For special versions，PE <br>
foam or PE foil is also used．Dispose of the packaging material <br>

via specialised recycling companies．\end{array}\right\}\)| Transport must be carried out under consideration of the notes |
| :--- |
| on the transport packaging．Nonobservance of these instruc－ |
| tions can cause damage to the device． |

Materials, wetted parts

Temperature limits

## Connection

## 4 Mounting

### 4.1 General instructions

Make sure that the wetted parts of VEGABAR 74, especially the seal and process fitting, are suitable for the existing process conditions such as pressure, temperature etc. as well as the chemical properties of the medium.

You can find the specifications in chapter "Technical data" in the "Supplement".

Higher process temperatures often mean also higher ambient temperatures. Make sure that the upper temperature limits stated in chapter "Technical data" for the environment of the electronics housing and connection cable are not exceeded.


Fig. 2: Temperature ranges
1 Process temperature
2 Ambient temperature

- The connection cable has a capillary for atmospheric pressure compensation
$\rightarrow$ Lead the cable end into a dry space or into a suitable terminal housing.


## Information:

VEGA recommends the breather housing VEGABOX 02 or the indication/adjustment VEGADIS 12. Both contain terminals and a ventilation filter for pressure compensation. For mounting outdoors, a suitable protective cover is available.

## 4．2 Mounting steps

Sealing／Screwing in threaded versions

## Sealing／Screwing in flange versions

Sealing／Screwing in hygienic fittings

Seal the thread with teflon，hemp or a similar resistant seal material on the process fitting thread $11 / 2$ NPT．
$\rightarrow$ Screw VEGABAR 74 into the welded socket．Tighten the hexagon on the process fitting with a suitable wrench． Wrench size，see chapter＂Dimensions＂．

Seal the flange connections according to DIN／ANSI with a suitable，resistant seal and mount VEGABAR 74 with suitable screws．

Use the seal suitable for the respective process fitting．You can find the components in the line of VEGA accessories in the supplementary instructions manual＂Welded socket and seals＂．

## 5 Connecting to power supply

### 5.1 Preparing the connection

## Note safety instructions

Always keep in mind the following safety instructions:

- Connect only in the complete absence of line voltage
- If overvoltage surges are expected, versions with integrated overvoltage arresters should be used or external overvoltage arresters should be installed

Tip:
We recommend the version of VEGABAR 74 with integrated overvoltage arrester or VEGA type ÜSB62-36G. $X$ as external overvoltage arreaster.

In hazardous areas you should take note of the appropriate regulations, conformity and type approval certificates of the sensors and power supply units.

Power supply and current signal are carried on the same twowire cable. The voltage supply range can differ depending on the instrument version.

The data for power supply are stated in chapter "Technical data" in the "Supplement".

Provide a reliable separation of the supply circuit from the mains circuits according to DIN VDE 0106 part 101.

VEGA power supply units VEGATRENN 149AEx, VEGASTAB 690, VEGADIS 371 as well as all VEGAMETs meet this requirement. When using one of these instruments, protection class III is ensured for VEGABAR 74.

Bear in mind the following factors regarding supply voltage:

- Output voltage of the power supply unit can be lower under nominal load (with a sensor current of 20.5 mA or 22 mA in case of fault message)
- Influence of additional instruments in the circuit (see load values in chapter "Technical data")

VEGABAR 74 is connected with standard two-wire cable without screen. An outer cable diameter of $5 \ldots 9 \mathrm{~mm}$ ensures the seal effect of the cable gland when connecting via VEGABOX 02 or VEGADIS 12. If electromagnetic interference is expected which is above the test values of EN 61326 for
industrial areas，screened cable should be used．For HART multidrop operation we recommend as standard practice the use of screened cable．


Fig．3：Connection of VEGABAR 74
1 Direct connection
2 Connection via VEGABOX 02 or VEGADIS 12

Cable screening and ground－ ing

Select connection cable for Ex applica－ tions

If screened cable is necessary，connect the cable screen on both ends to ground potential．In the VEGABOX 02 or VEGADIS 12，the screen must be connected directly to the internal ground terminal．The ground terminal on the outside of the housing must be connected to the potential equalisation （low impedance）．

If potential equalisation currents are expected，the connection on the processing side must be made via a ceramic capacitor （e．g． $1 \mathrm{nF}, 1500 \mathrm{~V}$ ）．The low frequency potential equalisation currents are thus suppressed，but the protective effect against high frequency interference signals remains．

Take note of the corresponding installation regulations for Ex applications．In particular，make sure that no potential equal－ isation currents flow over the cable screen．In case of grounding on both sides this can be achieved by the use of a capacitor or a separate potential equalisation．

### 5.2 Connection procedure

## Direct connection

Via VEGABOX 01 or VEGADIS 12

Proceed as follows:
1 Wire the connection cable up to the connection compartment. The bending radius must be at least $25 \mathrm{~mm} .{ }^{2)}$
2 Connect the wire ends to the screw terminals according to the wiring plan

Proceed as follows:
1 Snap connection housing onto the carrier rail or screw it to the mounting plate

2 Loosen the cover screws and remove the cover
3 Insert the cable through the cable entry into the connection housing housing
4 Loosen the screws with a screwdriver
5 Insert the wire ends into the open terminals according to the wiring plan
6 Tighten the screws with a screwdriver
7 Check the hold of the wires in the terminals by lightly pulling on them
8 Tighten the compression nut of the cable entry. The seal ring must completely encircle the cable
9 Connect the supply cable according to steps 3 to 8
10 Screw the housing cover back on
The electrical connection is finished.

## 5．3 Wiring plan

## Direct connection



Fig．4：Wire assignment，connection cable
1 brown（＋）：to power supply or to the processing system
2 blue（－）：to power supply or to the processing system
3 yellow：is only required with VEGADIS 12，otherwise connect to minus or with VEGABOX 01 to terminal $3^{3}$ ）
4 Screen
5 Breather capillaries with filter element

Fig．5：Terminal assignment VEGABAR 74
1 To power supply or the processing system
2 Screen ${ }^{4}$

| Wire number | Wire colour／Polarity | VEGABAR 74 terminal |
| :--- | :--- | :--- |
| 1 | brown $(+)$ | 1 |
| 2 | blue $(-)$ | 2 |
| 3 | Yellow | 2 |
|  | Screen | Ground |

3）For customer－specific versions already connected with blue $(-)$ when being shipped．
4）Connect screen to ground terminal．Connect ground terminal on the outside of the housing as prescribed．The two terminals are galvanically connected．


Fig. 6: Terminal assignment, VEGADIS 12
1 To power supply or the processing system
2 Control instrument (4 ... 20 mA measurement)
3 Screen ${ }^{5}$
4 Breather capillaries
5 Suspension cable

| Wire number | Wire colour/Polarity | Terminal VEGADIS <br> $\mathbf{1 2}$ |
| :--- | :--- | :--- |
| 1 | brown $(+)$ | 1 |
| 2 | blue $(-)$ | 2 |
| 3 | Yellow | 3 |

5) Connect screen to ground terminal. Connect ground terminal on the outside of the housing as prescribed. The two terminals are galvanically connected.

## 6 Set up

## 6．1 Setup steps without VEGADIS 12

After mounting and electrical connection，VEGABAR 74 is ready for operation．
$\rightarrow$ Switch on voltage
The electronics now carries out a self－check for approx． 2 seconds．Then VEGABAR 74 delivers a current of $4 \ldots 20 \mathrm{~mA}$ according to the actual level．

## 6．2 Setup steps with VEGADIS 12

Adjustment volume
－zero－measuring range begin
－span－measuring range end
－ti－Integration time

## Adjustment system



Fig．7：Adjustment elements of VEGADIS 12
1 Rotary switch：choose the requested function
$2[+]$ key，change value（rising）
3 ［－］key，change value（falling）
－With the rotary switch the requested function is selected
－With the［ $[+]$ and $[-]$ keys，the signal current or the integration time are adjusted
－Finally the rotary switch is set to position＂OPERATE＂
The set values are transmitted to the EEPROM memory and remain there even in case of voltage loss．

Adjustment steps，adjustment Proceed as follows for adjustment with VEGADIS 12：
1 Open housing cover
2 Connect hand multimeter to terminals 10 and 12
3 Meas．range begin：Set rotary switch to＂zero＂

Adjustment steps, integration time

Adjustment steps, scaling

4 Empty the vessel or reduce process pressure
5 Set a current of 4 mA with the [+] and [-] keys
6 Meas. range end: Set rotary switch to "span"
7 Fill the vessel or increase process pressure
8 Set a current of 20 mA with the [+] and [-] keys
9 Operation: Set rotary switch to "OPERATE"
10 Close housing cover
The adjustment data are effective, the output current $4 \ldots 20 \mathrm{~mA}$ corresponds to the actual level.

Proceed as follows for the adjustment of the integration time with VEGADIS 12:

1 Open housing cover
2 Set rotary switch to " $t i$ "
3 By pushing the [-] key 10 -times, make sure that the integration time is set to 0 sec .

4 For every 1 sec . requested integration time, push the [+] key once.
5 The integration time is the time required by the output current signal to reach $90 \%$ of the actual height after a sudden level change.
6 Set rotary switch to "OPERATE"
7 Close housing cover
The display outputs the current $4 \ldots 20 \mathrm{~mA}$ as bar graph and digital value.

With 4 mA no segment of the bar graph appears, with 20 mA all segments appear. This assignment is fix.

You can scale the digital value to any value between -9999 ... +9999 via the adjustment module.

Proceed as follows for scaling the indication of VEGADIS 12:
1 Open housing cover
2 Initial value: Set rotary switch to "zero"
3 Set the requested value, e.g. 0 with the [+] and [-] keys
4 Final value: Set the rotary switch to "span"
5 Set the requested value, e.g. 1000 with the [+] and [-] keys
6 Decimal point: Set the rotary switch to "point"
7 With the [+] and [-] keys you can adjust the requested value, e.g. 8888 (no decimal point)

8 Set rotary switch to "OPERATE"
9 Close housing cover
The adjustment data are effective, the output current $4 \ldots 20 \mathrm{~mA}$ corresponds to the actual level.

## 7 Setup with PACTware ${ }^{\text {TM }}$

### 7.1 Connect the PC with VEGACONNECT 3

Connecting the PC to the signal cable


Fig. 8: Connecting the PC to the signal cable
1 RS232 connection (with VEGACONNECT 3) or USB connection (with VEGACONNECT 4)
2 VEGABAR 74
3 HART adapter cable
4 HART resistance 250 Ohm (optional depending on the processing)

Necessary components:

- VEGABAR 74
- PC with PACTware ${ }^{\text {TM }}$ and suitable VEGA DTM
- VEGACONNECT 3 or 4 with HART adapter cable (art. no. 2.25397)
- HART resistance approx. 250 Ohm
- Power supply unit


## Note:

With power supply units with integrated HART resistance (internal resistance approx. 250 Ohm ), an additional external resistance is not necessary (e.g. VEGATRENN 149A, VEGADIS 371, VEGAMET 381/624/625, VEGASCAN 693). In such cases, VEGACONNECT 3 can be connected parallel to the $4 \ldots 20 \mathrm{~mA}$ cable.

## 7．2 Connect the PC with VEGACONNECT 4

## Connection via HART



Fig．9：Connecting the PC via HART to the signal cable
1 VEGABAR 74
2 HART resistance 250 Ohm（optional depending on the processing）
3 Connection cable with 2 mm pins and terminals
4 Processing system／PLCNoltage supply

Necessary components：
－VEGABAR 74
－PC with PACTware ${ }^{\text {TM }}$ ．and suitable VEGA DTM
－VEGACONNECT 4
－HART resistance 250 Ohm（optional depending on the processing）
－Power supply unit or processing system

## Note：

With power supply units with integrated HART resistance （internal resistance approx． 250 Ohm ），an additional external resistance is not necessary．This applies，e．g．to the VEGA instruments VEGATRENN 149A，VEGADIS 371，VEGAMET 381）．Also usual Ex separators are most of the time equipped with a sufficient current limitation resistor．In such cases， VEGACONNECT 4 can be connected parallel to the $4 \ldots 20 \mathrm{~mA}$ cable．

### 7.3 Parameter adjustment with PACTware ${ }^{\text {TM }}$

Further setup steps are described in the operating instructions manual "DTM Collection/PACTware ${ }^{\text {TM" }}$ attached to each CD and which can also be downloaded from our homepage. A detailed description is available in the online help of PACTware ${ }^{\text {M }}$ and the VEGA DTMs.

## Note:

Keep in mind that for setup of VEGABAR 74, DTM-Collection in the actual version must be used.

All currently available VEGA DTMs are provided in the DTM Collection on CD and can be obtained from the responsible VEGA agency for a token fee. This CD includes also the up-todate PACTware ${ }^{\text {TM }}$ version. The basic version of this DTM Collection incl. PACTware ${ }^{\text {TM }}$ is also available as a free-ofcharge download from the Internet.

Go via www.vega.com and "Downloads" to the item "Software".

### 7.4 Parameter adjustment with AMS $^{\text {TM }}$ and PDM

For VEGA sensors, instrument descriptions for the adjustment programs $\mathrm{AMS}^{\text {M }}$ and PDM are available as DD or EDD. The instrument descriptions are already implemented in the current versions of $A M S^{\top M}$ and PDM. For older versions of AMS $^{\text {TM }}$ and PDM, a free-of-charge download is available via Internet.

Go via www.vega.com and "Downloads" to the item "Software".

### 7.5 Saving the parameter adjustment data

It is recommended to document or save the parameter adjustment data. They are hence available for multiple use or service purposes.

The VEGA DTM Collection and PACTware ${ }^{\text {TM }}$ in the licensed, professional version provide suitable tools for systematic project documentation and storage.

## 8 Maintenance and fault rectification

## 8．1 Maintenance

When used as directed in normal operation，VEGABAR 74 is completely maintenance free．

## 8．2 Fault clearance

Reaction in case of failures

Causes of malfunction

Fault rectification

24 hour service hotline

Checking the 4 ．．． 20 mA sig－ nal

The operator of the system is responsible for taken suitable measures to remove interferences．

VEGABAR 74 offers maximum reliability．Nevertheless faults can occur during operation．These may be caused by the following，e．g．：
－Sensor
－Process
－Supply
－Signal processing
The first measures to be taken are to check the output signals as well as to evaluate the error messages via the indicating and adjustment module．The procedure is described below． Further comprehensive diagnostics can be carried out on a PC with the software PACTware ${ }^{\text {TM }}$ and the suitable DTM．In many cases，the causes can be determined in this way and faults can be rectified．

However，if these measures are not successful，call the VEGA service hotline in urgent cases under the phone no．＋491805 858550.

The hotline is available to you 7 days a week round－the－clock． Since we offer this service world－wide，the support is only available in the English language．The service is free of charge，only the standard telephone costs will be charged．

Connect a handheld multimeter in the suitable measuring range according to the wiring plan．
？ $4 \ldots 20 \mathrm{~mA}$ signal not stable
－Level fluctuations
$\rightarrow$ Adjust integration time via PACTware ${ }^{\text {TM }}$
－no atmospheric pressure compensation
$\rightarrow$ Check the capillaries and cut them clean
$\rightarrow$ Check the pressure compensation in the housing and clean the filter element, if necessary
? $4 \ldots 20 \mathrm{~mA}$ signal missing

- Wrong connection to power supply
$\rightarrow$ Check connection according to chapter "Connection steps" and if necessary, correct according to chapter "Wiring plan"
- No voltage supply
$\rightarrow$ Check cables for breaks; repair if necessary
- supply voltage too low or load resistance too high
$\rightarrow$ Check, adapt if necessary
? Current signal $3.6 \mathrm{~mA} ; 22 \mathrm{~mA}$
- electronics module or measuring cell defective
$\rightarrow$ Exchange instrument or return instrument for repair


## Reaction after fault rectification

In Ex applications, the regulations for the wiring of intrinsically safe circuits must be observed.

Depending on the failure reason and measures taken, the steps described in chapter "Set up" must be carried out again, if necessary.

### 8.3 Instrument repair

If a repair is necessary, please proceed as follows:
You can download a return form ( 23 KB ) from the Internet on our homepage www.vega.com under: "Downloads - Forms and certificates-Repair form".

By doing this you help us carry out the repair quickly and without having to call back for needed information.

- Print and fill out one form per instrument
- Clean the instrument and pack it damage-proof
- Attach the completed form and, if need be, also a safety data sheet outside on the packaging
- Please ask the agency serving you for the address of your return shipment. You can find the respective agency on our website www.vega.com under: "Company - VEGA worldwide"


## 9 Dismounting

## 9．1 Dismounting steps

## Warning：

Before dismounting，be aware of dangerous process con－ ditions such as e．g．pressure in the vessel，high temperatures， corrosive or toxic products etc．

Take note of chapters＂Mounting＂and＂Connecting to power supply＂and carry out the listed steps in reverse order．

## 9．2 Disposal

The instrument consists of materials which can be recycled by specialised recycling companies．We use recyclable materials and have designed the electronics to be easily separable．

## WEEE directive 2002／96／EG

This instrument is not subject to the WEEE directive 2002／96／ EG and the respective national laws（in Germany，e．g．
ElektroG）．Pass the instrument directly on to a specialised recycling company and do not use the municipal collecting points．These may be used only for privately used products according to the WEEE directive．

Correct disposal avoids negative effects to persons and environment and ensures recycling of useful raw materials．

Materials：see chapter＂Technical data＂
If you cannot dispose of the instrument properly，please contact us about disposal methods or return．

## 10 Supplement

### 10.1 Technical data

General data

Manufacturer
Type name
Parameter, pressure
Measuring principle
Communication interface

VEGA Grieshaber KG, D-77761 Schiltach
VEGABAR 74
Gauge pressure, absolute pressure, vacuum
Ceramic-capacitive, dry measuring cell
None

## Materials and weights

Material 316L corresponds to 1.4404 or 1.4435
Materials, wetted parts

- Process fitting
- Diaphragm
- Seal
- Seal process fitting thread $G 1 / 2 A$, G11⁄2 A

Materials, non-wetted parts

- Housing
- Ground terminal
- Connection cable
- type label support on cable

Weight

## Output variable

Output signal
Failure signal
Max. output current
Damping ( $63 \%$ of the input variable)
Step response or adjustment time
Fulfilled NAMUR recommendations

316L
sapphire ceramic ${ }^{\circledR}$ (99.9 \% oxide ceramic)
FKM (e.g. Viton), Kalrez 6375, EPDM, Chemraz 535
Klingersil C-4400

316L
316Ti/316L
PUR, FEP, PE
PE-HART
$0.8 \ldots 8 \mathrm{~kg}(1.8 \ldots 17.6 \mathrm{lbs})$, depending on process fitting

4 ... $20 \mathrm{~mA} / \mathrm{HART}$
$22 \mathrm{~mA}(3.6 \mathrm{~mA})$, adjustable
22.5 mA
$0 \ldots 10 \mathrm{~s}$, adjustable
70 ms (ti: $0 \mathrm{~s}, 0 \ldots 63 \%$ )
NE 43

## Additional output parameter - temperature

Processing is made via HART-Multidrop

Range
Resolution
Accuracy

- in the range of $0 \ldots+100^{\circ} \mathrm{C}$ ( $+32 \ldots+212{ }^{\circ} \mathrm{F}$ )
- in the range of $-50 \ldots 0^{\circ} \mathrm{C}$ $\left(-58 \ldots+32^{\circ} \mathrm{F}\right)$ and $+100 \ldots+150^{\circ} \mathrm{C}$ $\left(+212 \ldots+302{ }^{\circ} \mathrm{F}\right.$ )
$-50 \ldots+150^{\circ} \mathrm{C}\left(-58 \ldots+302^{\circ} \mathrm{F}\right)$
$1^{\circ} \mathrm{C}\left(1.8^{\circ} \mathrm{F}\right)$
$\pm 3 \mathrm{~K}$
typ. $\pm 4 \mathrm{~K}$


## Input variable

## Adjustment

Zero adjustable $-20 \ldots+95 \%$ of the nominal measuring range
Span adjustable
$3.3 \ldots+120 \%$ of the nominal measuring range
Recommended max. turn down
10:1

## Nominal measuring ranges and overload resistance

| Nominal range | Overload, max. pressure ${ }^{6}$ ) | Overload, min. pressure |
| :---: | :---: | :---: |
| Gauge pressure |  |  |
| $0 \ldots 0.1 \mathrm{bar} / 0 \ldots 10 \mathrm{kPa}$ | 15 bar/1500 kPa | -0.2 bar/-20 kPa |
| $0 \ldots 0.2 \mathrm{bar} / 0 . .20 \mathrm{kPa}$ | $20 \mathrm{bar} / 2000 \mathrm{kPa}$ | -0.4 bar/ 40 kPa |
| $0 \ldots 0.4 \mathrm{bar} / 0 . .440 \mathrm{kPa}$ | $30 \mathrm{bar} / 3000 \mathrm{kPa}$ | -0.8 bar/-80 kPa |
| 0... 1 bar/0 ... 100 kPa | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | -1 bar/-100 kPa |
| 0 ... 2.5 bar/0 ... 250 kPa | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| 0 ... 5 bar/0 .. 500 kPa | 65 bar/6500 kPa | -1 bar/-100 kPa |
| 0 ... $10 \mathrm{bar} / 0 \ldots 1000 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| 0 ... 25 bar/0 .. 2500 kPa | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| 0 ... $60 \mathrm{bar} / 0 \ldots 6000 \mathrm{kPa}$ | 200 bar/20000 kPa | -1 bar/-100 kPa |
| $-1 \ldots 0 \mathrm{bar} /-100 \ldots 0 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | -1 bar/-100 kPa |
| $-1 \ldots 1.5$ bar/-100 .. 150 kPa | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| $-1 \ldots 5 \mathrm{bar} /-100 \ldots 500 \mathrm{kPa}$ | $65 \mathrm{bar} / 6500 \mathrm{kPa}$ | -1 bar/-100 kPa |
| -1 ... $10 \mathrm{bar} /-100 \ldots 1000 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| -1 ... 25 barl-100 ... 2500 kPa | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| $-1 \ldots 60 \mathrm{bar} /-100 \ldots 6000 \mathrm{kPa}$ | $300 \mathrm{bar} / 30000 \mathrm{kPa}$ | -1 bar/-100 kPa |
| $-0.05 \ldots 0.05 \mathrm{bar} /-5 \ldots 5 \mathrm{kPa}$ | $15 \mathrm{bar} / 1500 \mathrm{kPa}$ | -0.2 bar/-20 kPa |
| -0.1 ... $0.1 \mathrm{bar} /-10 \ldots 10 \mathrm{kPa}$ | $20 \mathrm{bar} / 2000 \mathrm{kPa}$ | -0.4 bar/ 40 kPa |

8) Limited to 200 bar according to the pressure device directive.

| Nominal range | Overload，max．pres－ <br> sure6） | Overload，min．pressure |
| :--- | :--- | :--- |
| $-0.2 \ldots 0.2 \mathrm{bar} /-20 \ldots 20 \mathrm{kPa}$ | $30 \mathrm{bar} / 3000 \mathrm{kPa}$ | $-0.8 \mathrm{bar} /-80 \mathrm{kPa}$ |
| $-0.5 \ldots 0.5 \mathrm{bar} /-50 \ldots 50 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ | $-1 \mathrm{bar} /-100 \mathrm{kPa}$ |
| Absolute pressure | $15 \mathrm{bar} / 1500 \mathrm{kPa}$ |  |
| $0 \ldots 0.1 \mathrm{bar} / 0 \ldots 10 \mathrm{kPa}$ | $35 \mathrm{bar} / 3500 \mathrm{kPa}$ |  |
| $0 \ldots 1 \mathrm{bar} / 0 \ldots 100 \mathrm{kPa}$ | $50 \mathrm{bar} / 5000 \mathrm{kPa}$ |  |
| $0 \ldots 2.5 \mathrm{bar} / 0 \ldots 250 \mathrm{kPa}$ | $65 \mathrm{bar} / 6500 \mathrm{kPa}$ |  |
| $0 \ldots 5 \mathrm{bar} / 0 \ldots 500 \mathrm{kPa}$ | $90 \mathrm{bar} / 9000 \mathrm{kPa}$ |  |
| $0 \ldots 10 \mathrm{bar} / 0 \ldots 1000 \mathrm{kPa}$ | $130 \mathrm{bar} / 13000 \mathrm{kPa}$ |  |
| $0 \ldots 25 \mathrm{bar} / 0 \ldots 2500 \mathrm{kPa}$ | $200 \mathrm{bar} / 20000 \mathrm{kPa}$ |  |
| $0 \ldots 60 \mathrm{bar} / 0 \ldots 6000 \mathrm{kPa}$ |  |  |

## Reference conditions and influencing variables（similar to DIN EN 60770－1）

Reference conditions according to DIN EN 61298－1
－Temperature
－Relative humidity
－Air pressure

Determination of characteristics

Characteristics
Reference installation position
Influence of the installation position
$+15 \ldots+25^{\circ} \mathrm{C}\left(+59 \ldots+77^{\circ} \mathrm{F}\right)$
45 ．．． 75 \％
860 ．．． $1060 \mathrm{mbar} / 86 \ldots 106 \mathrm{kPa}$ （ 12.5 ．．． 15.4 psi ）

Limit point adjustment according to IEC 61298－2 linear upright，diaphragm points downward $<0.2 \mathrm{mbar} / 20 \mathrm{~Pa}(0.003 \mathrm{psi})$

## Deviation determined according to the limit point method according to IEC 607707）

Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$ ．
Specifications refer to the set span．Turn down（TD）＝nominal measuring range／set span．

## Deviation

－Turn down 1：1 up to 5：1
－Turn down up to 10：1
$<0.075 \%$
$<0.015 \% \times$ TD

Deviation with absolutely flush process fittings EV，FT
－Turn down 1：1 up to 5：1
$<0.05 \%$
－Turn down up to 10：1
$<0.01 \% \times$ TD

7）Incl．non－linearity，hysteresis and non－repeatability．

Deviation with absolute pressure measuring range 0.1 bar
－Turn down 1：1 up to 5：1 $<0.25 \% \times$ TD
－Turn down up to 10：1 $<0.05 \% \times$ TD

## Influence of the product or ambient temperature

Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$ ．
Specifications refer to the set span．Turn down（TD）＝nominal measuring range／set span．

## Average temperature coefficient of the zero signal

In the compensated temperature range of $0 \ldots+100^{\circ} \mathrm{C}\left(+212^{\circ} \mathrm{F}\right)$ ，reference temperature $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$ ：

Average temperature coefficient of the zero signal
－Turn down 1：1
$<0.05 \% / 10 \mathrm{~K}$
－Turn down 1：1 up to 5：1
－Turn down up to 10：1
$<0.15 \% / 10 \mathrm{~K}$
Outside the compensated temperature range：
Average temperature coefficient of the zero signal
－Turn down 1：1 typ．$<0.05 \% / 10 \mathrm{~K}$

## Thermal change of the current output

Applies also to the analogue $4 \ldots 20 \mathrm{~mA}$ current output and refers to the set span．
Thermal change，current output $<0.15 \%$ at $-40 \ldots+80^{\circ} \mathrm{C}\left(-40 \ldots+176{ }^{\circ} \mathrm{F}\right)$

## Long－term stability（similar to DIN 16086，DINV 19259－1 and IEC 60770－1）

Applies to digital HART interface as well as to analogue current output $4 \ldots 20 \mathrm{~mA}$ ．
Specifications refer to the set span．Turn down（TD）＝nominal measuring range／set span．
Long－term drift of the zero signal $<(0.1 \% \times$ TD $) / 1$ year

## Total deviation（similar to DIN 16086）

The total deviation（max．practical deviation）is the sum of basic accuracy and long－term stability：
$F_{\text {total }}=F_{\text {pert }}+F_{\text {stab }}$
$F_{\text {perf }}=\sqrt{ }\left(\left(F_{T}\right)^{2}+\left(F_{K I}\right)^{2}\right)$
With
－$F_{\text {total }}$ Total deviation
－$F_{\text {pert：}}$ Basic accuracy
－$F_{\text {stab }}$ ：Long－term drift

- $\mathrm{F}_{\mathrm{T}}$ : Temperature coefficient (influ-
ence of medium or ambient tem-
perature)
- $\mathrm{F}_{\mathrm{KI}}$ : Deviation


## Ambient conditions

Ambient, storage and transport temperature

- Connection cable PE
$-40 \ldots+60^{\circ} \mathrm{C}\left(-40 \ldots+140^{\circ} \mathrm{F}\right)$
- Connection cable PUR, FEP
$-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$


## Process conditions

The specifications of the pressure stage are used as an overview. The specifications on the ype plate are applicable.

Pressure stage, process fitting

- Thread 316L
- Thread Alu
- Hygienic fittings 316L
- Flange 316L, flange with extension 316L

PN 60
PN 25
PN 10, PN 16, PN 25, PN 40
PN 40 or $150 \mathrm{lbs}, 300 \mathrm{lbs}$

Product temperature depending on the measuring cell seal

- FKM (e.g. Viton)
- EPDM
- Kalrez 6375 (FFKM)
- Chemraz 535

Vibration resistance
Shock resistance
$-20 \ldots+100^{\circ} \mathrm{C}\left(-4 \ldots+212^{\circ} \mathrm{F}\right)$
$-40 \ldots+100^{\circ} \mathrm{C}\left(-40 \ldots+212^{\circ} \mathrm{F}\right), 1 \mathrm{~h}: 140^{\circ} \mathrm{C} /$
$284^{\circ} \mathrm{F}$ cleaning temperature
$-10 \ldots+100^{\circ} \mathrm{C}\left(+14 \ldots+212^{\circ} \mathrm{F}\right)$
$-30 \ldots+100^{\circ} \mathrm{C}\left(-22 \ldots+212^{\circ} \mathrm{F}\right)$
mechanical vibrations with 4 g and $5 \ldots 100 \mathrm{~Hz}^{8)}$
Acceleration $100 \mathrm{~g} / 6 \mathrm{~ms}^{9}$

## Electromechanical data

Connection cable

- Configuration
- Wire cross-section
- wire resistance
- Standard length
- max. length with VEGADIS 12
four wires, one suspension cable, one breather capillary, screen braiding, metal foil, mantle
$0.5 \mathrm{~mm}^{2}$ (AWG no. 20)
$<0.036 \mathrm{Ohm} / \mathrm{m}(0.011 \mathrm{Ohm} / \mathrm{tt})$
6 m (19.685 ft)
200 m ( 656.168 ft )

8) Tested according to the regulations of German Lloyd, GL directive 2.
${ }^{9}$ ) Tested according to EN 60068-2-27.
－Min．bending radius at $25^{\circ} \mathrm{C} / 77^{\circ} \mathrm{F}$
－Diameter
－Colour－standard PE
－Colour－standard PUR
－Colour－Ex－version

25 mm （ 0.985 in ）
approx． 8 mm （ 0.315 in ）
Black
Blue
Blue

## Voltage supply

Supply voltage
－Non－Ex instrument
$12 \ldots 36$ V DC
－EEx ia instrument
$12 . . .29 \mathrm{~V}$ DC
Permissible residual ripple
－$<100 \mathrm{~Hz}$
$\mathrm{U}_{\mathrm{ss}}<1 \mathrm{~V}$
－ 100 Hz ．． 10 kHz
$\mathrm{U}_{\mathrm{ss}}<10 \mathrm{mV}$
Load
see diagram


Fig．10：Voltage diagram VEGABAR 74
1 HART load
2 Voltage limit Ex instrument
3 Voltage limit non－Ex instrument
4 Voltage supply

Load in conjunction with VEGADIS 12 see diagram


Fig. 11: Voltage diagram VEGABAR 74 with VEGADIS 12
1 HARTload
2 Voltage limit Ex instrument
3 Voltage limit non-Ex instrument
4 Voltage supply

## Integrated overvoltage protection

Nominal leakage current ( $8 / 20 \mu \mathrm{~s}$ )
10 kA
Min. response time
$<25 \mathrm{~ns}$
Electrical protective measures
Protection
Overvoltage category
Protection class

## Approvals ${ }^{10)}$

ATEX ia

Ship approvals
Others

ATEX II 1G EEx ia IIC T6; ATEX II 2G EEx ia IIC T6
GL, LRS, ABS, CCS, RINA, DNV
WHG

IP 68 (25 bar)/IP 69K
III
III

## 10．2 Dimensions

VEGABAR 74 －threaded fitting


## VEGABAR 74 - hygienic fitting 1



Fig. 13: VEGABAR 74 hygienic fitting: $C C=$ Tri-Clamp 112", $C A=$ Tri-Clamp 2", $L A=$ hygienic fitting with compression nut F40, TA = Tuchenhagen Varivent DN 32, TB = Tuchenhagen Varivent DN 25, RA/RB = bolting DN 40/DN 50 according to DIN 11851

VEGABAR 74 －hygienic fitting 2


Fig．14：VEGABAR $74 K A K H=$ cone $D N 40, A A=D R D, S D / S E=$ Anderson $3^{\prime \prime}$ long／short fitting

## VEGABAR 74 - flange connection



EA, FB, FE, FQ, FH, FI


TV, TS

| (1) | DN | PN | $D$ | $b$ | $k$ | $d 2$ | $d 4$ | $f$ | $R L$ | $d 5$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EA | 40 | 40 | $529 / 32^{\prime \prime}$ | $45 / 64^{\prime \prime}$ | $421 / 64^{\prime \prime}$ | $4 \times 645 / 64^{\prime \prime}$ | $315 / 32^{\prime \prime}$ | $1 / 8^{\prime \prime}$ | - | - |
| FB | 50 | 40 | $61 / 2^{\prime \prime}$ | $25 / 32^{\prime \prime}$ | $459 / 64^{\prime \prime}$ | $4 \times 645 / 64^{\prime \prime}$ | $41 / 64^{\prime \prime}$ | $1 / 8^{\prime \prime}$ | - | - |
| FE | 80 | 40 | $77 / 8^{\prime \prime}$ | $15 / 16^{\prime \prime}$ | $619 / 64^{\prime \prime}$ | $8 \times 045 / 64^{\prime \prime}$ | $57 / 16^{\prime \prime}$ | $1 / 8^{\prime \prime}$ | - | - |


| (2) | " | Ibs | D | b | k | d2 | d4 | $f$ | RL | d5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FQ | $1^{1 / 2}{ }^{\prime \prime}$ | 150 | 5" | 11/16 ${ }^{11}$ | $314 / 16^{\prime \prime}$ | $4 \times 05 / 8{ }^{\prime \prime}$ | $27 / 8{ }^{\prime \prime}$ | $1 / 8{ }^{\prime \prime}$ | - | - |
| FH | 2" | 150 | $6{ }^{\prime \prime}$ | $3 / 4{ }^{11}$ | 43/4" | $4 x ø 5 / 8{ }^{\prime \prime}$ | $35 / 8^{\prime \prime}$ | $1 / 8{ }^{\prime \prime}$ | - | - |
| FI | 3" | 150 | $71 / 2^{\prime \prime}$ | $3 / 4{ }^{4}$ | 6 | $4 \mathrm{xo} \mathrm{5/8"}$ | 6 | $1 / 8{ }^{\prime \prime}$ | - | - |


| (3) | $D N$ | $P N$ | $D$ | $b$ | $k$ | $d 2$ | $d 4$ | $f$ | $R L$ | $d 5$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TV | 50 | 40 | $61 / 2^{\prime \prime}$ | $25 / 32^{\prime \prime}$ | $459 / 64^{\prime \prime}$ | $4 \times 945 / 64^{\prime \prime}$ | $41 / 64^{\prime \prime}$ | $1 / 8^{\prime \prime}$ | (4) | $11 / 2^{\prime \prime}$ |
| TS | 80 | 40 | $77 / 8^{\prime \prime}$ | $15 / 16^{\prime \prime}$ | $619 / 64^{\prime \prime}$ | $8 \times 045 / 64^{\prime \prime}$ | $57 / 16^{\prime \prime}$ | $1 / 8^{\prime \prime}$ |  | $11 / 2^{\prime \prime}$ |

Fig. 15: VEGABAR 74 - flange connection
1 Flange connection according to DIN 2501
2 Flange fitting according to ANSI B16.5
3 Flange with extension
4 Order-specific

## VEGABAR 74-threaded fitting for paper industry



Fig. 16: VEGABAR 74 - connection for paper industry: $B A / B B=M 44 \times 1.25$

VEGABAR 74 - extension fitting for paper industry


Fig. 17: VEGABAR 74 ~ extension fitting for paper industry: $E V / F T=$ absolutely flush for pulper ( $E V 2$ 2-times flattened), $E G=$ extension for ball valve fitting ( $L=$ order-specific)

## 10．3 Industrial property rights

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All statements concerning scope of delivery, application, practical use and operating conditions of the sensors and processing systems correspond to the information available at the time of printing.
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# TECHNICAL DATA SHEET 

For

## SEWERAGE PUMP STATION SP144

## Lavarack Av \#1 Eagle Farm

| Equipment Type: | Wet Well Level Transmitter |
| :--- | :--- |
| Location: | Common Control |
|  |  |
| Model Numbers: | FM167-A2BMD1A3 |
|  |  |
| Manufacturer: | Endress \& Hauser |
|  |  |
| Supplier: | Unit 8/277 Lane Cove Rd |
|  | North Ryde |
|  | NSW |
|  | 2113 |
|  | Tel: 0288777000 |
|  | Fax: 0288777099 |



## Technical Information

# Waterpilot FMX167 

## Hydrostatic Level Measurement Reliable and rugged level probe with ceramic measuring cell Compact device for level measurement in fresh water, wastewater and saltwater



## Applications

The Waterpilot FMX167 is a pressure sensor for hydrostatic level measurement. Three versions of FMX167 are available at Endress+Hauser:

- $\mathrm{FMX1} 167$ with an outer diameter $=22 \mathrm{~mm}$ ( 0.87 inch ): Version very suitable for drinking water applications and for use in probe tubes with small diameters
- FMX167 with an outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch ): Heavy version and very easy to clean thanks to the flush-mounted diaphragm. Very suitable for wastewater and sewage treatment plants
- $\mathrm{FMX1} 167$ with an outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch): Resistant version for use in saltwater and very suitable for applications on ships (e.g. ballast water tanks)


## Your benefits

- High mechanical resistance to overload and aggressive media
- High-precision and long-term stability ceramic measuring cell
- Resistant to climatic changes thanks to potted electronics and 2 -filter pressure compensation system
- $4 . . .20 \mathrm{~mA}$ oupput signal with integrated overvoltage protection
- Simultaneous level and temperature measurement by optional integrated temperature sensor Pt 100
- Drinking water approval: KTW, NSF, ACS
- Certified to ATEX, FM and CSA
- Marine approval: GL, ABS
- Complete measuring point solutions through comprehensive accessories


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Function and system design
Device selection

| Waterpilot FMX 167 |  |  |  |
| :---: | :---: | :---: | :---: |
| Field of application | Hydrostatic leve! measurement in deep wells e.g. drinking water | Hydrostatic level measurement in wastewater | Hydrostatic level measurement in saltwater |
| Process connection | - Suspension clamp <br> - Extension cable mounting screw with GI I/2 A or $11 / 2$ NPT thread |  |  |
| Outer diameter $\mathrm{d}_{0}$ | 22 mm (0.87 inch) | 42 mm (1.66 inch) | Max. 29 mm ( 1.15 inch) |
| Seals | - FKM Viton <br> - EPDM ${ }^{11}$ | - FKM Viton | - FKM Viton <br> - EPDM |
| Measuring ranges | - Nine fixed pressure measuring ranges in bar, $\mathrm{mH}_{2} \mathrm{O}$, psi and $\mathrm{ft} \mathrm{H}_{2} \mathrm{O}$, from $0 . .0 .1$ bar to $0 . . .20$ bar ( $0 . .1 \mathrm{mH}_{2} \mathrm{O}$ to $0 . . .200 \mathrm{mH}_{2} \mathrm{O}$ / $0 . . .1 .5 \mathrm{psi}$ to $0 . . .300 \mathrm{psi} / 0 . . .3 \mathrm{ft}_{2} \mathrm{O}$ to $0 \ldots 600 \mathrm{ftH}_{2} \mathrm{O}$ ) <br> - Customer-specific measuring ranges; factory-calibrated |  | - Seven fixed pressure measuring ranges in bar, $\mathrm{mH}_{2} \mathrm{O}$, psi and ft $\mathrm{H}_{2} \mathrm{O}$, from $0 . . .0 .1$ bar to $0 . . .4$ bar (0...1 $\mathrm{mH}_{2} \mathrm{O}$ to $0 \ldots 40 \mathrm{mH}_{2} \mathrm{O}$ / <br> $0 . .1 .5 \mathrm{psi}$ to $0 . . .60 \mathrm{psi} /$ $0 . .3 \mathrm{ftH}_{2} \mathrm{O}$ to $0 . . .150 \mathrm{ftH}_{2} \mathrm{O}$ ) <br> - Customer-specific measuring ranges; factory-calibrated |
| Overioad | Up to 40 bar ( 580 psi ) |  | Up to 25 bar (362 psi) |
| Process temperature | $-10 \ldots+70^{\circ} \mathrm{C}\left(-14 \ldots+158^{\circ} \mathrm{F}\right)$ |  | $0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$ |
| Ambient temperature range | $-10 \ldots+70^{\circ} \mathrm{C}\left(-14 \ldots+158^{\circ} \mathrm{F}\right)$ |  | $0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$ |
| Maximum measured error | $\pm 0.2 \%$ of upper range value (URV) |  |  |
| Supply voltage | 10... 30 V DC |  |  |
| Output | $4 . . .20 \mathrm{~mA}$ |  |  |
| Options | - Drinking water approval <br> - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT181 (4... 20 mA ) <br> - Marine approval | - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT181 (4... 20 mA ) <br> - Marine approval | - Integrated Pt 100 temperature sensor <br> - Integrated Pt 100 temperature sensor and temperature transmitter TMT181 (4... 20 mA$)$ <br> - Marine approval |
| Specialties | - Integrated overvoltage protection <br> - Large selection of approvals, including ATEX II 2 G, FM and CSA <br> - High-precision, long-term stable and rugged ceramic measuring cell |  |  |

1) Recommended for drinking water applications, not suitable for use in hazardous areas

## Measuring principle

The ceramic measuring cell is dry, i.e. pressure acts directly on the rugged ceramic diaphragm of Waterpilot FMX167 and causes it to move by max. 0.005 mm .
The effects of air pressure on the liquid surface are transferred via a pressure compensation tube through the extension cable to the rear of the ceramic diaphragm and compensated. Pressure-dependent changes in capacitance caused by diaphragm movement are measured at the electrodes of the ceramic carrier. The electronics convert the movement into a pressure-proportional signal which is linear to the medium level.


## FMXI 67 measuring principle

1 Ceramic measuring cell
2 Pressure compensation tube
$h$ Level height
p Total pressure $=$ hydrostatic pressure + atmospheric pressure
$\rho \quad$ Medium density
g Gravitational acceleration
$p_{\text {hrdr. }}$ Hydrostatic pressure
$p_{\text {atm }}$ Atmospheric pressure

## Temperature measurement with optional Pt 100

Endress+Hauser offers an optional 4-wire Pt 100 resistance thermometer for Waterpilot FMX167 to measure level and temperature simultaneously. The Pt 100 belongs to Accuracy Class B to DIN EN 60751.

Temperature measurement with optional Pt 100 and temperature transmitter TMT181
To convert the Pt 100 signal to a $4 \ldots 20 \mathrm{~mA}$ signal, Endress+Hauser also offers the TMT181 temperature transmitter.

The complete standard measuring system consists of Waterpilot FMX167 and a transmitter power supply unit with supply voltage of $10 \ldots 30 \mathrm{~V}$ DC.

Example for other measuring point solutions with transmitter and possible evaluation units from Endress+Hauser:


## Application examples with FMXI07

OP Overvoltage protection e.g. HAW from Endress+Hauser

1. Simple cost-effective measuring point solution: Power supply of Waterpilot in hazardous and nonhazardous areas using RN221N active barrier.
Power supply and additional control of two consumers, e.g. pumps, via limit switch RTA421 with onsite display.
2. Power supply, onsite display, two switch outputs and a signal adaptation (turn down) are integrated in evaluation devices RMA421 (for mounting on hat rails) and RIA250 (for panel mounting). The evaluation unit RMA421 also has a trend recognition function, e.g. optimizing pump control in stormwater overflow basins. This function detects and evaluates changes in a measurable value within a specific time period.
3. If several pumps are used, pump life can be prolonged by alternate switching. With alternating pump control, the pump which was out of service for the longest period of time is switched on. The evaluation units RIA452 (for panel mounting) and RMA422 (for mounting on hat rails) offer this function as well as several others.
4. State-of-the-art recording technology with monitor recorders from Endress+Hauser, e.g. Ecograph, Memograph or hardcopy recorders such as Alphalog for documenting, monitoring, visualizing and archiving.


Application examples with FMX167 with Pt 100
OP Overvoltage protection e.g. HAW from Endress + Hauser
5. If you want to measure, display and evaluate temperature as well as level, e.g. to monitor temperature in fresh water to detect temperature limits for germ formation, you have the following options:
The optional temperature transmitter can convert the Pt 100 signal into a $4 \ldots 20 \mathrm{~mA}$ signal and transfer it to any customary evaluation unit. Evaluation devices RMA421, RIA250 and RIA452 also offer a direct input for the Pt 100 signal.
6. If you want to detect and evaluate level and temperature with one device, choose the evaluation unit RMA422 with two inputs. It even includes the mathematical operation for linking the input signals.

## Input

| Measured variable | FMX167 + Pt 100 (optional) Temperature transmitter (optional) <br> - Hydrostatic pressure of a liquid - Temperature <br> - Pt 100: Temperature of a liquid  |
| :---: | :---: |
| Measuring range | - Nine fixed pressure measuring ranges in bar, $\mathrm{mH}_{2} \mathrm{O}$, psi and $\mathrm{ftH}_{2} \mathrm{O}$; $\rightarrow$ Page 18, "Ordering information" Section <br> - Customer-specific measuring ranges; factory-calibrated <br> - Temperature measurement from $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$ (optional with Pt 100 ) |
| Input signal | FMX167 + Pt 100 (optional) Temperature transmitter (optional) <br> - Change in capacitance a Pt 100 resistance signal, 4 -wire <br> - Pt 100: Change in resistance  |

## Output

| Output signal | FMX167 + Pt 100 (optional) <br> - FMX167: 4... 20 mA for hydrostatic pressure measured value, two-wire <br> - Pt 100: Temperature-dependent resistance of Pt 100 | Temperature transmitter (optional) <br> - $4 . . .20 \mathrm{~mA}$ for temperature measured value, twowire |
| :---: | :---: | :---: |
| Load | FMX167 + Pt 100 (optional) | Temperature transmitter (optional) |
|  | $R_{\mathrm{tot}} \leq \frac{\mathrm{U}_{\mathrm{b}}-10 \mathrm{~V}}{0.0225 \mathrm{~A}}-2 \cdot 0.09 \frac{\Omega}{\mathrm{~m}} \cdot 1-R_{\mathrm{add}}$ |  |
|  | $\begin{aligned} R_{\text {tot }}= & \text { Max. load resistance } / \Omega / \\ R_{\text {add }}= & \text { Additional resistances such as resistance of evaluating device and/or display instrument, } \\ & \text { line resistance } / \Omega] \end{aligned}$ |  |
|  | $U_{0}=\text { Supply voltage } N /$ |  |



Load chart FMXI67 for estimating load resistance. Subtract the additional resistances, e.g. resistance of extension cable, from the calculated value as shown in the equation.


Load chart temperature transmitter for estimating load resistance. Subtract the additional resistances from the calculated value as shown in the equation.

## Power supply

## Electrical connection

## Note!

- When using the measuring device in hazardous areas, national standards and regulations as well as the Safety Instructions (XAs) or Installation or Control Drawings (ZDs) have to be observed. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections.
- Reverse polarity protection is integrated in the Waterpilot FMX167 and in the temperature transmitter TMT181. Changing the polarities has no impact on operation.
- The cable must end in a dry room or in a proper terminal box. For installation outside, use the terminal box (IP 60/IP 67) with a GORE-TEX ${ }^{\oplus}$ filter from Endress+Hauser. The terminal box can be ordered using the order code of FMX167 ( $\rightarrow$ see Page 18, "Ordering information" Section) or an accessory (order number: 52000252).


## Waterpilot FMX167, standard



FMX107 electrical connection, versions "7" or "3" for
Feature 70 "Additional options" in the order code $\rightarrow$ see Page 18).

Waterpilot FMX167 with Pt 100


FMXI67 electrical connection with Pt 100 , versions " 1 " or "4" for Feature 70 "Additional options" in the order code $(\rightarrow$ see Page 18).

Waterpilot FMX167 with Pt 100 and TMT 181 temperature transmitter ( $4 \ldots 20 \mathrm{~mA}$ )


FMX167 with Pt 100 and TMT181 temperature transmitter ( $4 . .20 \mathrm{~mA}$ ), version " 5 " for Feature 70 in the order code $(\rightarrow$ see Page 18).
1 Not for FMXI 67 with outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch )
Wire colors: $\mathrm{RD}=$ red, $\mathrm{BK}=$ black, $\mathrm{WH}=$ white, $\mathrm{YE}=$ yellow, $\mathrm{BU}=$ biue, $\mathrm{BR}=$ brown

| Supply voltage |  |  |
| :---: | :---: | :---: |
| $\stackrel{\otimes}{s}$ | Note! <br> - When using the measuring device in bazar instructions (XAs) or Installation or Contro Instructions" and "Installation/Control Dr | s, national standards and regulations as well as the safety $s$ (ZDs) bave to he observed. $\rightarrow$ See also Page 20, "Safety ections. |
|  | FMX167 + Pt 100 (optional) <br> - FMX167: $10 \ldots 30$ VDC <br> - Pt 100: $10 \ldots . .30$ VDC | Temperature transmitter (optional) <br> - 8... 35 V DC |
| Cable specifications | FMX167 + Pt 100 (optional) <br> - Commercially available instrument cable <br> - Terminals, terminal housing FMX107: $0.08 \ldots . .2 .5 \mathrm{~mm}^{2}$ <br> - If the Pt 100 signal is directly connected to a display and/or evaluation unit, we recommend the use of a shielded cable. | Temperature transmitter (optional) <br> - Commercially available instrument cable <br> - Terminals, terminal housing FMXI67: $0.08 \ldots 2.5 \mathrm{~mm}^{2}$ <br> - Connection, cransmitter: Max. $1.75 \mathrm{~mm}^{2}$ |
| Power consumption | FMX167 + Pt 100 (optional) $\leq 0.675 \mathrm{~W}$ at 30 VDC | Temperature transmitter (optional) $\leq 0.875 \mathrm{~W} \text { at } 35 \mathrm{VDC}$ |
| Current consumption | FMX167 + Pt 100 (optional) <br> - Max. current consumption: $\leq 22.5 \mathrm{~mA}$ Min. current consumption: $\geq 3.5 \mathrm{~mA}$ <br> - Pt $100: \leq 0.6 \mathrm{~mA}$ | Temperature transmitter (optional) <br> - Max. current consumption: $\leq 25 \mathrm{~mA}$ <br> Min. current consumption; $\geq 3.5 \mathrm{~mA}$ <br> - Pt 100 via temperature transmitter: $\leq 0.0 \mathrm{~mA}$ |
| Residual ripple | FMX167 + Pt 100 (optional) <br> No effect for $4 \ldots 20 \mathrm{~mA}$ signal up to $\pm 5 \%$ residual ripple within permissible range | Temperature transmitter (optional) $\mathrm{U}_{\mathrm{ss}} \geq 5 \mathrm{~V} \text { at } \mathrm{U}_{\mathrm{B}} \geq 13 \mathrm{~V}, \mathrm{f}_{\text {max }}=1 \mathrm{kHz}$ |

## Performance characteristics



## Installation

## Installation instructions



Installation examples, here shown with $F M X 107$ with an outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$
1 Extension cable mounting screw can be ordered via order code or as an accessory, $\rightarrow$ see Page 14 and 19
2 Terminal housing can be ordered via order code or as an accessory, $\rightarrow$ see Page 15 and 19
3 Extension cable bending radius $>120 \mathrm{~mm}(4.72 \mathrm{inch})$
4 Suspension clamp can be ordered via order code or as an accessory, $\rightarrow$ see Page 14 and 19
5 Extension cable up to 300 m ( 384 ft ), for max. length $\rightarrow$ see Page 10 , "Extension cable" Section
$0 \quad$ Guide tube for FMXI 67 with outer diameter $=22 \mathrm{~mm}(0.87$ inch $)$ internal diameter $>23 \mathrm{~mm}(0.91$ inch)
7 Additional weight can be ordered as an accessory for FMXI 07 with outer diameter $=22 \mathrm{~mm}$ ( 0.87 inch) and 29 mm ( 1.15 inch), $\rightarrow$ see Page 19
8 Protection cap

## Note!

- A sideways movement of the level probe can lead to measuring errors. Therefore install the probe at a point free from flow and turbulence, or use a guide tube. The internal diameter of the guide tube should be at least 1 mm ( 0.04 inch ) bigger than the outer diameter of the selected FMX167.
- The cable must end in a dry room or in a proper terminal box. The terminal box from Endress+Hauser provides optimum humidity and climatic protection and is suitable for outdoor installation.
a Protective cap: to avoid mechanical damage to the measuring cell, the device is provided with a protective cap, which should not be removed during transport and installation.
- After shortening of the cable, the filter must be re-fitted on the pressure compensation hose.


## Environment

| Ambient temperature range | FMX167 + Pt 100 (optional) <br> - FMX167 with outer diameter $=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and 42 mm ( 1.66 inch ): $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$ <br> ( $=$ medium temperature) <br> - FMX167 with outer diameter $\begin{aligned} & =29 \mathrm{~mm}(1.15 \text { inch }): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right) \\ & (=\text { medium temperature }) \end{aligned}$ | Temperature transmitter (optional) $-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$ |
| :---: | :---: | :---: |
| Storage temperature | FMX167 + Pt 100 (optional) $-40 \ldots+80^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{F}\right)$ | Temperature transmitter (optional) $-40 \ldots+100^{\circ} \mathrm{C}\left(-40 \ldots+212^{\circ} \mathrm{F}\right)$ |
| gree of protection | FMX167 + Pt 100 (optional) <br> - IP 68 , permanently hermetically sealed <br> - Optional terminal box: IP 66/IP 67 | Temperature transmitter (optional) <br> - IP 00, moisture condensation permissible <br> - When mounted in the optional terminal boxes: <br> IP 66/IP67 |


| Electromagnetic | FMX167 + Pt 100 (optional) |
| :--- | :--- |
| compatibility (EMC) | - Interference emission to EN 61326 Class B |
|  | equipment, interference immunity to EN 61326 |
|  | Appendix A (Industrial) |
| - | Maximum deviation: $<0.5 \%$ of span |

## Overvoltage protection

FMX167 + Pt 100 (optional)
Integrated overvoltage protection to EN 61000-4-5 $\leq 1.2 \mathrm{kV}$
Install overvoltage protection $\geq 1.2 \mathrm{kV}$, external if necessary

## Temperature transmitter (optional)

- Interference emission to EN 61326 Class B equipment, interference immunity to EN 61326 Appendix A (Industrial)


## Temperature transmitter (optional)

Install overvoltage protection, external if necessary.

## Process

| Medium temperature range | FMX167 + Pt 100 (optional) |
| :---: | :---: |
| . | FMX167 with outer diameter $=22 \mathrm{~mm}$ ( 0.87 inch ) and 42 mm ( 1.66 inch): $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right)$ <br> - FMX167 with outer diameter $=29 \mathrm{~mm}(1.15 \mathrm{inch}): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$ |

Temperature transmitter (optional)
$-40 \ldots+85^{\circ} \mathrm{C}\left(-40 \ldots+185^{\circ} \mathrm{C}\right)(=$ ambient temperature $)$, install temperature transmitter outside medium.

FMX1 67 + Pt 100 (optional)

- FMX167 with outer diameter
$=22 \mathrm{~mm}$ ( 0.87 inch) and 42 mm ( 1.66 inch): $-20 \ldots+70^{\circ} \mathrm{C}\left(-4 \ldots+158^{\circ} \mathrm{F}\right)$
- FMX167 with outer diameter
$=29 \mathrm{~mm}(1.15 \mathrm{inch}): 0 \ldots+50^{\circ} \mathrm{C}\left(+32 \ldots+122^{\circ} \mathrm{F}\right)$
(You may operate the FMX167 in this temperature range. The specification can then be exceeded, e.g. measuring accuracy).


## Mechanical construction

Dimensions of level probe


## Versions of FMX107

1 FMX167, version " $A$ " or " $D$ " for Feature 30 "Probe tube" in the order code $(\rightarrow$ see Page 18)
2 FMX107, version " $B$ " for Feature 30 "Probe tube" in the order code $(\rightarrow$ see Page 18)
3 FMX107, version "C" for Feature 30 "Probe tube" in the order code $\rightarrow$ see Page 18)
Pressure compensation tube
Extension cable
Protection cap

## Dimensions of suspension clamp



Suspension clamp, version 2 for Feature 20 "Connection" in the order code $\rightarrow$ see Page 18)

Dimensions of extension cable mounting screws


Extension cable mounting screws
1 Extension cable mounting screw G $1 / 12$ A, version "3" for Feature 20 "Connection" in the order code $\rightarrow$ see Page 18)
2 Extension cable mounting screw I 1/2 NPT, version "4" for Feature 20 "Connection" in the order code $\rightarrow$ see Page 18)

## Dimensions of the terminal box IP 06/IP 67 with filter



Terminal box
Version "3", "4" or "5" for Feature 70 "Additional options" in the order code $(\rightarrow$ see Page 18)
1 Dummy plug M $20 \times 1.5$
2 CORE-TEX ${ }^{0}$ fiter
3 Terminals for $0.08 \ldots 2.5 \mathrm{~mm}^{2}$


Temperature transmitter TMT18) (4... 20 mA )
Version "5" for Feature 70 "Additional options" in the order code $\rightarrow \rightarrow$ see Page 18). The temperature transmitter can be used in non-hazardous areas and for $E E x \cap A$.

Weight

- Level probe, outer diameter $=22 \mathrm{~mm}(0.87 \mathrm{inch}): 290 \mathrm{~g}$
- Level probe, outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch): 1150 g
- Level probe, outer diameter $=29 \mathrm{~mm}$ ( t .15 inch ): 340 g
- Extension cable PE: $52 \mathrm{~g} / \mathrm{m}$
- Extension cable FEP: $108 \mathrm{~g} / \mathrm{m}$
- Suspension clamp: 170 g
- Extension cable mounting screw G $11 / 2$ A: 770 g
- Extension cable mounting screw 1 1/2 NPT: 724 g
- Terminal hox: 2358
- Temperature transmitter: 40 g
- Additional weight: 300 g

| Material | Level probe <br> - Level probe, outer diameter $=22 \mathrm{~mm}(0.87$ inch $): 1.4435$ (AISI 316L) <br> - Level probe, outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch ): 1.4435 (AISI 316L) <br> - Level probe, outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch): <br> - Level probe: 1.4435 (AISI 316L) <br> - Sensor sleeve: PPS (polyphenylene sulfide) <br> - Heat-shrink sleeve/cover: Polyolefin <br> Metal does not come into contact with the medium. <br> - Process ceramic: $\mathrm{Al}_{2} \mathrm{O}_{3}$ aluminium oxide ceramic <br> - Seal (internal): EPDM or Viton <br> - Protective cap: <br> - PE-HD (high-density polyethylene) for FMX167 with outer diameter $=22 \mathrm{~mm}$ and $29 \mathrm{~mm}(0.87 \mathrm{inch}$ and $1.15 \mathrm{inch})$. <br> - PFA (perlluoralkoxy) for FMX167 with outer diameter $=42 \mathrm{~mm}$ ( 1.66 inch). <br> - Extension cable insulation: Either PE-LD (low density polyethylene) or FEP (fluorinated ethylene propylene). For more information, see the next Section - "Extension cable" <br> - Suspension clamp: 1.4404 (AISI 316L) and glass fiber reinforced PA (polyamide) <br> - Extension cable mounting screw G 1 1/2 A: 1.4301 (AISI 304) <br> - Extension cable mounting screw 1 1/2 NPT: 1.4301 (AISI 304) <br> - Terminal box: PC (polycarbonate) <br> - Temperature transmitter: Housing PC (polycarbonate) |
| :---: | :---: |
| Extension cable | PE extension cable <br> - Slip-resistant extension cable with strain-relief members made of Dynemo; shielded using aluminium-coated film; insulated with polyethylene (PE), black; copper wires, twisted <br> - Pressure compensation tube with Teflon filter |
|  | FEP extension cable <br> - Slip-resistant extension cable; shielded using galvanized steel wire netting; insulated with fluorinated ethylene propylene (FEP), black; copper wires, twisted <br> - Pressure compensation tube with Teflon filter |
|  | Cross-section of PE and FEP extension cable <br> - Total outer diameter: $8.0 \mathrm{~mm} \pm 0.25 \mathrm{~mm}(0.315 \mathrm{inch} \pm 0.0098 \mathrm{inch})$ <br> - FMX167: $3 \times 0.227 \mathrm{~mm}^{2}+$ pressure compensation tube with Teflon filter <br> - FMX167 with Pt 100 (optional): $7 \times 0.227 \mathrm{~mm}^{2}+$ pressure compensation tube with Teflon filter <br> - Pressure compensation tube with Teflon filter: <br> Outer diameter $=2.5 \mathrm{~mm}(0.098$ inch $)$, internal diameter $=1.5 \mathrm{~mm}(0.059 \mathrm{inch})$ |
|  | Cable resistance of PE and FEP extension cable <br> - Cable resistance per wire: $\leq 0.09 \Omega / \mathrm{m}$ |
|  | Cable length of PE and FEP extension cable <br> - Please also refer to Page 7, "Load" Section. <br> - When using the measuring device in hazardous areas, national standards and regulations as well as the safety instructions (XAs) or Installation or Control Drawings (ZDs) have to be observed. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections. |
|  | Further technical data of PE and FEP extension cable <br> - Minimum bending radius: 120 mm ( 4.72 inch) <br> - Tensile strength: max. 950 N <br> - Cable extraction force: $\geq 450 \mathrm{~N}$ <br> (The extension cable could be extracted from the level probe at a tensile force of $\geq 450 \mathrm{~N}$.) <br> - Resistance to UV light <br> - PE: approved for use with drinking water |
| Terminals | - 3 standard terminals in terminal box <br> - 4-terminal strip can be ordered as accessory, Order No. 52008938 Wire cross-section $0.08 \ldots 2.5 \mathrm{~mm}^{2}$ |

## Certificates and approvals

| CE approval | By attaching the CE symbol, Endress+Hauser confirms that the instrument fulfills all the requirements of the relevant EC directives. |
| :---: | :---: |
| Ex approval, type of protection | - ATEX II 2 G EEx ia IIC T6 ${ }^{1}$ <br> - ATEXII 3 G EExnAII T6 <br> - FM: IS, Class I, Division 1, Groups A-D ${ }^{1}$ <br> - CSA: IS, Class I, Division 1, Groups A-D' |
|  | 1 Only for Waterpilot FMX167 without Pt 100 |
|  | Waterpilot FMX 167 with outer diameter $=22 \mathrm{~mm}(0.87 \mathrm{inch})$ is only suitable for use in hazardous areas with the FKM Viton seal. |
|  | All explosion protection data are contained in separate explosion protection documentation which you can also request. Explosion protection documents are supplied as standard for all devices approved for use in expiosion hazardous areas. $\rightarrow$ See also Page 20, "Safety Instructions" and "Installation/Control Drawings" Sections. |
| Drinking water approval (for FMXI 67 with $\left.\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}(0.87 \mathrm{inch})\right)$ | - KTW certificate <br> - NSF 61 approval <br> - ACS approval |
| Marine approval | - GL approval <br> - ABS approval |
| External standards and guidelines | DIN EN 60770 (IEC 60770): <br> Transmitters for use in industrial-control systems Part 1: Methods for performance evaluation |
|  | DIN 16086: <br> Electrical pressure measuring instruments, pressure sensors, pressure transmitters, pressure measuring instruments, concepts, specifications on data sheets |
|  | EN 01320 (IEC $01320-1$ ): <br> Electrical equipment for measurement, control and laboratory use - EMC requirements |
| Registered trademarks | CORE-TEX ${ }^{\text {® }}$ <br> Registered trademark of W.L. Gore \& Associates, Inc., USA |

## Ordering information

FMX167

| 10 | Approval |
| :---: | :---: |
|  | A Version for non-hazardous area <br> B ATEX II 2 G <br> CEx ia IIC To  <br> C ATEX II 3 G EEx nA II T6 <br> S FM <br> ES, Class I, Division I, Groups A - D  <br> E CSA IS, Class I, Division I, Groups A - D <br> F CSA <br>  General Puppose |
| 20 | Connection |
|  | Probe cable <br> Suspension clamp, AISI 316L <br> Cable mounting screw G $11 / 2$, AISI 304 <br> Cable mounting screw NPT 1 1/2, AISI 304 |


| 30 | Probe tube: |  |
| :---: | :---: | :---: |
|  | A | Outer diameter $\mathrm{d}=22 \mathrm{~mm}$ ( 0.87 inch), ASSI 316L <br> Outer diameter $\mathrm{d}=42 \mathrm{~mm}$ ( 1.66 inch), flush mount, AISI 316 L <br> Outer diameter $\mathrm{d}=29 \mathrm{~mm}$ ( 1.15 inch), AISI 316 L with heat-shrink sleeve PPS/polyolefin for saltwater applications <br> Outer diameter d $=22 \mathrm{~mm}(0.87$ inch $)$, ASSI 316L + drinking water approval KTW/NSF/ACS (can only be selected in conjunction with EPDM seal and PE probe cable) |




$\rightarrow$ Ordering information for FMX167 continued on next page.

| $\mid 70$ |
| :--- |
| 70 |

## Accessories

| Suspension clamp | - Endress + Hauser offers a suspension clamp for simple FMX167 mounting. $\rightarrow$ See also Page 14 . <br> - Material: 1.4404 (AISI 316L) and glass fiber reinforced PA (polyamide) <br> - Order number: 52006151 |
| :---: | :---: |
| Terminal box | - Terminal box IP $66 /$ IP 67 with GORE-TEX ${ }^{\otimes}$ filter incl. 3 mounted terminals. The terminal box is also suitable for installing a temperature transmitter (Order No. 52008794) or for four additional terminals (Order No. 52008938). $\rightarrow$ See also Page 15. <br> - Order number: 52006152 |
| Additional weight (for FMX167 with $\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}$ ( 0.87 inch$)$ and $\mathrm{d}_{\mathrm{O}}=29 \mathrm{~mm}$ ( 1.15 inch $)$ ) | - To prevent sideways movement leading to measuring errors or to ensure that the device lowers into a guide tube, Endress+Hauser provides additional weights. <br> You can screw several weights together. The weights are then attached directly to the FMX167. For FMX167 with outer diameter $=29 \mathrm{~mm}$ ( 1.15 inch), a maximum of 5 weights may be screwed on to FMXI67. <br> - Material: 1.4435 (AISI 316L) <br> - Weight: 300 g <br> - Order number: 52006153 |
| Temperature transmitter | - Temperature transmitter, 2 -wire, preset for measuring range from $-20 \ldots+80^{\circ} \mathrm{C}\left(-4 \ldots+176^{\circ} \mathrm{F}\right)$. This setting offers an easily displayable temperature range of 100 K . Note that the Pt 100 resistance thermometer is designed for a temperature range of $-10 \ldots+70^{\circ} \mathrm{C}\left(+14 \ldots+158^{\circ} \mathrm{F}\right) . \rightarrow$ See also Page 15 . <br> - Order number: 52008794 |
| Extension cable mounting screw | - Endress+Hauser offers extension cable mounting screws to simplify the installation of the FMX167 and to close the measuring open. $\rightarrow$ See also Page 14 . <br> - Material: 1.4301 (AISI 304) <br> - Order number for extension cable mounting screw with G I 1/2 A thread: 52008264 <br> - Order number for extension cable mounting screw with 1 1/2 NPT thread: 52009311 |
| Terminals | - Four terminals in strip for FMX167 terminal box, suitable for wire cross-section of $0.08 \ldots 2.5 \mathrm{~mm}^{2}$ <br> - Order number: 52008938 |

## Test adapter

## (for FMX167 with

$\mathrm{d}_{\mathrm{O}}=22 \mathrm{~mm}(0.87 \mathrm{inch})$ and
$\mathrm{d}_{\mathrm{O}}=29 \mathrm{~mm}(1.15$ inch $\left.)\right)$


Test adapter
A Connection suitable for level probe FMX107
B Connection compressed air hose, internal diameter, quick hose gland 4 mm (0.157 inch)

- Endress+Hauser offers a test adapter to simplify the function test of level probes.
- Note the maximum pressure for the compressed air hose and the maximum level probe overload. $\rightarrow$ See also Page 18.
- The maximum pressure for the supplied quick hose gland is 10 bar ( 145 psi ).
- Adapter material: 1.4301 (AISI 304)
- Quick hose gland material: Anodized aluminium
- Adapter weight: 39 g
- Order number: 52011868


## Documentation

| Field of Activities | - Pressure Measurement: FA004P/00/en <br> - Recording Technology: FA014R/09/de <br> - System Components: FAO16K/09/en |
| :--- | :--- |
| Technical Information | - Temperature Head Transmitter iTEMP PCP TMT181: T1070R/09/en |
| Operating Instructions | - Waterpilot FMX167: BA231P/00/en |
| Safety Instructions | - ATEX II 2 G |
|  | EEx ia IIC T6: XA131P/00/a3 |
| ATEX II 3 G EEx nA II T6: XA132P/00/a3 |  |

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[^0]:    Notes: ) Standard torque for the terminal screws M3.5 - 0.88~1.18 Nm (9-12 Kgf.cm).

[^1]:    Note: - Optional.
    Underlined values will be applied as standard ratings unless otherwise specified when ordering.

[^2]:    $r$ ".
    ' $\cdot$

[^3]:    !.

[^4]:    Note: PowerCad is a product of PowerCad Software Pty Ltd. Purchases of this software can be obtained from
    PowerCad. www.powercad.com.au

[^5]:    $1 \quad$ * SLIP $\circledR^{\text {TM }}$ KISS $®^{\text {TM }}$

[^6]:    1) Due to the flush diaphragm, no own pressure compartment is formed.
